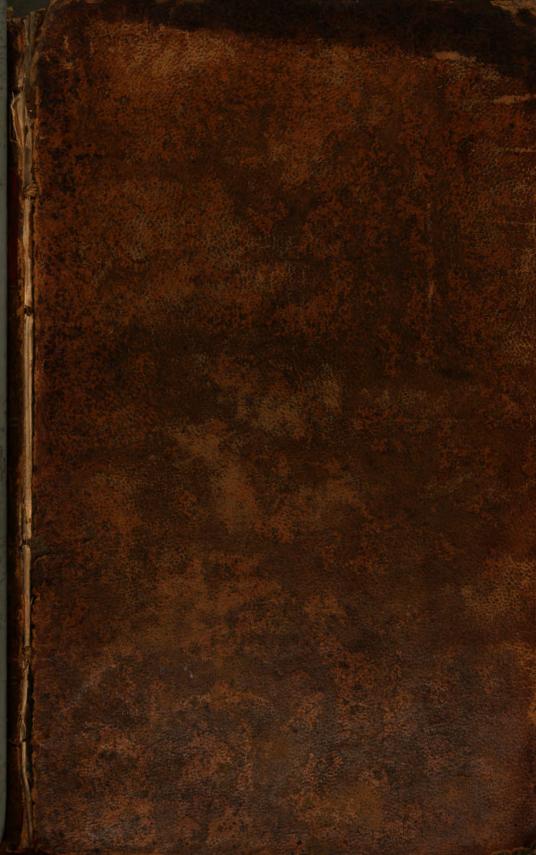
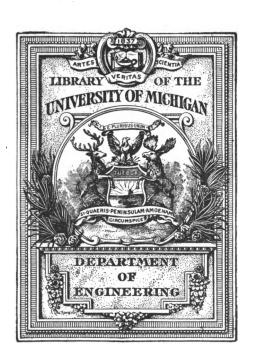
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W. SICENZOY

ELEMENTS

OF

SURVEYING.

WITH THE NECESSARY TABLES.

By CHARLES DAVIES,

PROFESSOR OF MATHEMATICS IN THE MILITARY ACADEMY AT WEST POINT.

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ELEMENTS OF SURVEYING.

INTRODUCTION.

CHAPTER I.

OF LOGARITHMS.

- 1. Logarriums of numbers are the indices that denote the different powers to which a given number must be raised to produce those numbers.
- 2. If a be the given number, whose indices and powers are to be considered, then $a^{\pm z}$ being put equal to n, a, the given number, or root, is called the *base* of the system of logarithms, n the number whose logarithm is considered, and $\pm x$, the logarithm of that number.
- 3. Any number, except 1, may be taken for the base of a system of logarithms. In the system in general use, the base is 10; and this system affords the greatest facilities in calculations, because 10 is the base of the common numeration, both in whole numbers and decimal fractions.
- 4. Taking $a^{\pm z} = n$, we have, $\pm x = \log n$; and putting $a^{\pm y} = m$, gives, $\pm y = \log m$. If the equations $a^z = n$, and $a^y = m$, be multiplied together, member by member, we have, $a^z \times a^y = n \times m$, or $a^{z+y} = n \times m$. In this expression, x+y is the logarithm of $n \times m$ (2); from which we conclude, that the sum of the logarithms of any two numbers, is equal to the logarithm of their product.

5. If the equations $a^x = n$, $a^y = m$, be divided, member by member, $\frac{a^x}{a^y} = \frac{n}{m}$; or $a^{x-y} = \frac{n}{m}$. In this expression, x-y is the logarithm of $\frac{n}{m}$ (2); from which we conclude, that, the difference of the logarithms of any two numbers, is equal to the logarithm of their quotient.

6. If in the equation $a^x = n$, both members be raised to the mth power, $a^{mx} = n^m$. Here, mx is the logarithm of n^m ; from which it appears, that the logarithm of the power of any number, is equal to the logarithm of that number, multiplied by the index of that power.

7. If the mth root of both members of the equation $a^x = n$, be taken, then, $a^{\frac{x}{m}} = n^{\frac{1}{m}}$; but $\frac{x}{m}$ is the logarithm of $n^{\frac{1}{m}}$; from which it appears, that the logarithm of the root of any number, is equal to the logarithm of that number divided by the index of the root.

- 8. It is evident, that the results obtained in the last four articles are equally true, whether the logarithms be positive or negative. These results show, that the addition of logarithms corresponds to the multiplication of their numbers; the subtraction of logarithms, to the division of numbers; their multiplication, to the raising of powers; and their division, to the extraction of roots.
- 9. Returning to the equation $a^{\pm x}=n$, in which $\pm x=\log n$, and applying it to the common system, in which the base is 10, we have,

Unity being the number which divides the whole numbers from the decimal fractions, we shall begin with it, and explain some properties of the logarithms of whole numbers. The logarithm of 1 is 0; and this is the case in all systems, for whatever be the base, its 0 power is 1: but the index of the base is the logarithm of the power; therefore, 0 is the logarithm of I. As the logarithms increase with the numbers

from unity upwards, the logarithms of all numbers, which are greater than 1, and less than 10, are greater than 0, and less than 1: their values are generally expressed by decimal fractions; thus, the log. 2=0.301030. The logarithms of numbers greater than 10, and less than 100, lie between 1 and 2, and are generally expressed by unity and a decimal fraction: thus, the log. 50=1.698970.

The logarithms of numbers greater than 100, but less than 1000, are greater than 2, and less than 3, and are expressed by uniting 2 with a decimal fraction: thus, the log. 126=2.100371. The whole number on the left of the decimal point is called the characteristic, or index of the logarithm. The number of units which it contains, is always one less than the number of places of figures in the number whose logarithm is taken. Thus, in the first case, for numbers between 1 and 10, there is but one place of figures, and the characteristic is 0. In the second case, for numbers between 10 and 100, there are two places, and the characteristic is 1. In the third case, for numbers between 100 and 1000, there are three places, and the characteristic is 2; and in like manner for any number of places whatsoever.

TABLE OF LOGARITHMS.

- 10. If the logarithms of all the numbers between 1 and any given number, be calculated and arranged in a tabular form, such table is called a table of logarithms. The table annexed shows the logarithms of all numbers between 1 and 10,000.
- 11. The first column, on the left of each page of the table of logarithms, is the column of numbers, and is designated by the letter N; the logarithms of these numbers are placed directly opposite them, and on the same horizontal line.
- 12. To find, from the table, the logarithm of any whole number. If the number be less than 100, look on the first page of the table of logarithms, along the column of numbers under N, until the number is found; the number directly opposite it, in the column designated Log., is the logarithm sought.
 - 13. When the number is greater than 100, and less than 10,000.

Find, in the column of numbers, the first three figures of the Then, pass across the page, along a horizontal given number. line, into the columns marked 0, 1, 2, 3, 4, &c., until you come to the column which is designated by the fourth figure of the given number: to the four figures so found, two figures taken from the column marked 0, are to be prefixed. If the first four figures found stand opposite to a row of six figures in the column marked 0, the two figures from this column, which are to be prefixed to the four before found, are the first two on the left hand: but, if the first four figures are opposite a line of only four figures, you are then to ascend the column, till you come to the line of six figures: the two figures at the left hand are to be prefixed, and then the decimal part of the logarithm is obtained; to which prefix the characteristic (9), and vou have the logarithm sought. In several of the columns designated 0, 1, 2, 3, 4, 5, &c., small dots are found. cases, a cipher must be written for each of those dots: and the two figures, from the first column, which are to be prefixed, are found in the horizontal line directly below. Thus, the log. 2188 is 3.340047, the two dots being changed into two ciphers, and the 34 from the column 0, prefixed. The two figures from the column 0, must also be taken from the line below, if any dots shall have been passed over, in passing along the horizontal line: thus, the logarithm of 3098 is 3.491081, the 49 from the column 0, being taken from the line 310.

14. If the number exceed 10,000, or consist of five or more places of figures, consider all the figures after the fourth from the left hand, as ciphers. Find from the table, the logarithm of this number, which will be the same as the logarithm of the first four places, excepting the characteristic. Take from the last column on the right of the page, marked D, the number on the same horizontal line with the logarithm, and multiply this number by the numbers that have been considered as ciphers: then, cut off from the right hand as many places for decimals as there are figures in the multiplier, and add the product, so obtained, to the first logarithm, for the logarithm sought.

Let it be required to find the logarithm of 672887. The

log. of 672800 is found, on the 11th page of the table, to be 5.827886, by prefixing the characteristic 5. The number corresponding in the column D is 65, which being multiplied by 87, the figures regarded as ciphers, gives 5655; then, pointing off two places for decimals, the number to be added is 56.55. This number being added to 5.827886, gives 5.827942 for the logarithm of 672887; the decimal part, .55, being omitted.

This method of finding the logarithms of numbers from the table, supposes that the logarithms are proportional to their respective numbers, which is not rigorously true. In the example, the logarithm of 672800 is 5.827886; of 672900, a number greater by 100, 5.827951: the difference of the logarithms is 65. Now, as 100, the difference of the numbers, is to 65, the difference of their logarithms, so is 87, the difference between the given number and the least of the numbers used, to the difference of their logarithms, which is 56.55: this difference being added to 5.827886, the logarithm of the less number, gives 5.827942 for the logarithm of 672887. The use of the column of differences is therefore manifest.

15. The logarithm of a fractional number is easily found, from what has already been said. If the fractional number exceed unity, as $\frac{1}{13}$, its logarithm is equal to the log. 136—log. 25 (5). If it be less than unity, as $\frac{1}{15}$, its logarithm may be written under two different forms. First, the log. $\frac{1}{15}$ = log. 15 - log. 125 = -(log. 125 - log. 15) = -(2.096910 - 1.176091) = -0.920819; the number 0.920819 being entirely negative. In the equation log.15—log.125 = -0.920819, if the log. 125 be transposed to the second member, the log. 15 = log. 125 - 0.920819. Let N' be the number whose logarithm is -0.920819, and N the number whose logarithm is +0.920819; then, the log. 15 - log. 125 = log. N'. Since the difference of logarithms of the two numbers is equal to the logarithm of their quotient (5), the log. 15 = log. $\frac{125}{N}$. But if the logarithms are equal, the numbers themselves are

equal; therefore, $15 = \frac{125}{N}$, or $\frac{15}{125} = \frac{1}{N} = N$, since $\frac{15}{125}$ is equal to the number whose logarithm is -0.920819. As the same reasoning holds true for any numbers whatever, we conclude, that the number answering to a negative logarithm, is the reciprocal of the number answering to this same logarithm regarded as positive.

16. To find the logarithm of a proper fraction under another form. Let the fraction be $N = \frac{1/2}{5\sqrt{5}}$. Let this fraction be multiplied by 10, 100, 1000, 10,000, or such higher power of 10, as to make it greater than unity. If it be multiplied by 10,000, we shall have, $10000 \text{ N} = \frac{10000 \times 125}{5627}$, and taking the logarithms, $4 + \log N = 4 + \log 125 - \log 5627 = 4 + 2.096910$ -3.750277 = 6.096910 -3.750277 = 2.346633: hence, the log. $N = 2.346633 - 4 = \overline{2.346633}$, the minus sign belonging to the characteristic only, and not to the decimal part of the loga-In such case, the minus sign is written above the number; thus, $\overline{2}$. If, then, it be required to express the logarithm of a fractional number, under such a form, that the characteristic only shall be negative, add such a whole number to the logarithm of the numerator, as will make it greater than the logarithm of the denominator; from this sum, subtract the logarithm of the denominator, and from the remainder, the whole number which was added to the logarithm of the numerator: the remainder is the logarithm sought.

17. To find the logarithm of a decimal number. If the number be composed of a whole number and a decimal, such as, 36.78, it may be put under the form $\frac{3}{100}$: the log. $\frac{36.78}{100}$ = log. 3678-2=3.565612-2=1.565612; from which we see, that the mixed number may be treated as a whole number, except in fixing the value of the characteristic, which is one less than the number of places on the left of the decimal point.

18. The logarithm of a decimal fraction is also readily found. The $\log 0.8 = \log ... = \log ... = -1 + \log ... = 8$. Now the $\log ... = 0.903090$, which is positive, and less than 1; hence $\log ... = 1.903090$, where the minus sign belongs to

the characteristic only (16): hence, it appears, that the logarithms of tenths, are the same as the logarithms of the corresponding whole numbers, excepting, that the characteristic instead of being 0, i - 1. If the fraction were of the form .06, it might be written $\frac{0.6}{10.0}$; taking the logarithms, $\log \frac{0.6}{10.0} = \log \frac{0.6}{0.0} = \log \frac{0.6}{0.0$ $-2 + \log$. 06. Now, the log 06 is but the log. 6; therefore, the $\log_{10}.06=2.778151$, the minus sign belonging only to the characteristic, the decimal part being positive (16). If the decimal were .006, its logarithm would be the same, excepting the characteristic, which would be -3. It is indeed, evident. that the negative characteristic will always be one greater, than the number of ciphers between the decimal point and the first significant place of figures; therefore, the logarithm of a decimal fraction is found, by considering it as a whole number, and then prefixing to its logarithm a negative characteristic. greater by unity than the number of ciphers between the decimal point and the first significant place of figures.

19. To find, in the tables, a number answering to a given logarithm.

Search, in the column of logarithms, for the decimal part of the given logarithm, and if it be exactly found, set down the corresponding number. Then, if the characteristic of the given logarithm be positive, point off, from the left of the number found, one more place of whole numbers than there are units in the characteristic of the given logarithm, and treat the other places as decimals: this will be the logarithm sought (9). If the characteristic of the given logarithm be 0, there will be one place of whole numbers; if it be -1, the number will be entirely decimal; if it be -2, there will be one cipher between the decimal point and the first significant figure; if it be -3, there will be two, &c. The number whose logarithm is 1.492481 is found in page 5, and is 31.08.

But if the decimal part of the logarithm cannot be exactly found in the table, take the number answering to the next less logarithm; take also from the table the corresponding difference in the column D: then, subtract this less logarithm from the given logarithm; divide the remainder by the difference taken from the column D, and annex the quotient to the number

answering to the less logarithm: this gives the required number, nearly. This rule, like the one for finding the logarithm of a number when the places exceed four, supposes the numbers to be proportional to their corresponding logarithms.

Ex. 1. To find the number answering to the logarithm 1.532708. Here,

Next less log. is 1.532627, its number 34.09, the diff. 128. The difference between the given log. 1.532708 and 1.532627 is 81; therefore,

128) 8100 (63

which being decimals of a unit, in respect of the 9 in the number 34.09 must be annexed, and being so annexed, gives 34.0963 for the number answering to the log. 1.532708.

Ex. 2. Required the number answering to the logarithm 3.233568.

The given logarithm = 3.233568

The next less tabular logarithm of 1712 = 3.233504

Diff. = 64

Tab. Diff. = 253) 64.00 (25

Hence the number sought is 1712.25, marking four places of integers for the characteristic 3.

MULTIPLICATION BY LOGARITHMS.

- 20. If it be required to multiply numbers by means of their logarithms, we take from the table the logarithms of the numbers to be multiplied; the sum of the logarithms is the logarithm of the product (4). The term sum is to be understood in its algebraical sense; therefore, if any of the logarithms have negative characteristics, the difference between the sum of such characteristics, and the sum of the positive characteristics, is to be taken, and the sign of the greater prefixed.
 - 1. To multiply 23.14 by 5.062.

Log. 23.14 = 1.364363

Log. 5.062 = 0.704322

Product 117.1347 = 2.068685

2. To multiply 3.902, 597.16, and .0314728 together.

Log. 3.902 = 0.591287Log. 597.16 = 2.776091 $<math>Log. .0314728 = \overline{2}.497935$

Product, 73.3353 = 1.865313

Here, the $\overline{2}$ cancels the +2, and the 1 carried from the decimal part, is set down.

3. To multiply 3.586, 2.1046, 0.8372, and 0.0294, together.

Log. 3.586 = 0.554610Log. 2.1046 = 0.323170Log. $0.8372 = \bar{1}.922829$ Log. $0.0294 = \bar{2}.468347$

Product, $0.1857618 = \bar{1}.268956$

Here, the 2 carried cancels $\overline{2}$, and there remains $\overline{1}$ to set down.

DIVISION BY LOGARITHMS.

- 21. If it be required to divide numbers by means of their logarithms, we have only to regard the dividend and divisor, as the numerator and denominator of a vulgar fraction; the logarithm of such fraction, found in the manner explained in articles 15 and 16, is the logarithm of the quotient. This additional caution may be added: that the difference of the logarithms, as there used, means the algebraical difference; so that, if the logarithm of the denominator have a negative characteristic, its sign must be changed to positive, after adding to it the unit, if any, carried in the subtraction from the decimal part of the logarithm. Or, if the characteristic of the logarithm of the numerator be negative, it must be treated as a negative number.
 - 1. To divide 24163 by 4567.

Log. 24163 = 4.383151 Log. 4567 = 3.659631

Quotient, 5.29078 = 0.723529

2. To divide .06314 by .007241.

 $Log..06314 = \overline{2}.800305$ $Log..007241 = \overline{3}.859799$

Quotient, 8.71979 = 0.940506

Here, 1 carried from the decimals to the $\bar{3}$, makes it become $\bar{2}$, which taken from $\bar{2}$, leaves 0 for the characteristic.

3. To divide 37.149 by 523.76.

Log. 37.149 = 1.569947Log. 523.76 = 2.719132

Quotient, $.0709275 = \bar{2}.850815$

4. To divide .7438 by 12.9476.

Log. $.7438 = \bar{1}.871456$ Log. 12.9476 = 1.112189

Quotient, $.057447 = \bar{2}.759267$ Here, the 1 taken from the $\bar{1}$ makes $\bar{2}$, as set down.

INVOLUTION BY LOGARITHMS.

22. If it be required to raise a number to any power by means of logarithms, take from the table the logarithm of the number, and multiply it by the index of the power; the product is the logarithm of the power: the number answering to this logarithm is the power required.

When the minus sign appears, it must be remembered, that it belongs to the characteristic only, and, therefore, the numbers which are carried for the tens, from the decimal part of the logarithm, are positive; hence, after the negative indices are multiplied by the index of the root, such numbers must be subtracted from the product, and the negative sign prefixed,

1. To square the number 2.5791.

Log. 2.5791 = 0.411468Index = 2

Power, 6.65175 = 0.822936

2. To raise .09163 to the 4th power.

$$Log. :09163 = \bar{2}.962038$$
 $Index = 4$

Power, $.000070494 = \bar{5.848152}$

3. To find the cube of 3.07146.

$$Log. 3.07146 = 0.487345$$
 $Index = 3$

Power, 28.9758 = 1.462035

4. To raise 1.0045 to the 45th power.

9750 7800

Power, 1.22391 = 0.087750

EVOLUTION BY LOGARITHMS.

23. When it is required to extract roots by means of logarithms, find, in the table, the logarithm of the number whose root is to be extracted; divide this logarithm by the index of the root: the quotient is the logarithm of the root sought.

If the logarithm of the number whose root is to be found, have a negative characteristic, and this be not divisible by the index of the root, it must be increased by so many negative units as will make it divisible by the index of the root, and carry the units borrowed, as so many tens to the decimal part of the logarithm. The reason of which is obvious. For, if the characteristic be not divisible by the index, the remainder, which is negative, cannot be carried to the decimal part of the logarithm, which is positive. But, by adding the negative units, and as many positive units, the value of the logarithm is not changed, and the difficulty is avoided.

- To find the square root of 365.
 Log. 365=2.562293,
 Divide by 2, the index of the root.
 Root 19.10496, its log. =1.281146½.
- 2. To find the 10th root of 2. Log. 2 = 0.301030

Divided by 10 = 0.030103Whose number, 1.0717, is the root.

3. To find the square root of 0.093. Log. $0.093 = \overline{2}.968483$

Divided by 2, gives $\overline{1}.484241\frac{1}{2}$ Whose number, 0.304959, is the root.

4. To find the cube root of 0.00048. Log. $0.00048 = \overline{4.681241}$

Divided by 3, gives $\overline{2}.893747$ Whose number, 0.0782973, is the root.

CHAPTER II.

PLANE TRIGONOMETRY.

- 24. Plane Trigonometry is that branch of Mathematics which treats of the methods of finding, by calculation, the unknown sides and angles of a plane triangle, from those sides and angles that are given.
- 25. For the purposes of trigonometrical calculations, the circumference of the circle is supposed to be divided into 360 equal parts, called degrees; each degree into 60 equal parts, called minutes; and each minute into 60 equal parts, called seconds.
- 26. As the circumference of a circle may be regarded as a proper measure of angles, having their vertices at the centre, the four right angles, which can be formed about the same point, are measured by 360 degrees; two right angles, by 180 degrees; one right angle, by 90 degrees; and an angle less than a right angle, by an arc less than 90 degrees.
- 27. Degrees, minutes, and seconds are usually designated by the respective characters, °' ". Thus, 16° 12′ 15" is read, 16 degrees, 12 minutes, and 15 seconds.
- 28. The complement of an angle is what remains after subtracting the angle from 90°. The sum of an angle and its complement, is equal to 90°.
- 29. The supplement of an angle is what remains after subtracting the angle from 180°. The sum of an angle and its supplement, is equal to 180°.
- 30. The sine of an angle is the perpendicular let fall from one extremity of the arc which measures it, on the diameter passing through the other extremity. Thus, BD (Pl. I. Fig. 1) is the sine of the angle AOC, or of the arc AB.

- 31. The cosine of an angle, or arc, is the part of the diameter intercepted between the foot of the sine and centre. OD is the cosine of AB.
- 32. The tangent of an arc is the line which touches it at one extremity, and is limited by a line drawn through the other extremity and the centre of the circle. AC is the tangent of the arc AB.
- 33. The secant of an arc is the line drawn from the centre of the circle through one extremity of the arc, and limited by the tangent passing through the other extremity. OC is the secant of the arc AB.
- 34. The three lines BD, AC, and OC, depend for their values on the arc AB and the radius OB, and are always determined by them. They are thus designated: BD=sin. AB, or sin. AOC, AC=tung. AB, or tang. AOC, OC=sec. AB, or sec. AOC.
- 35. If ABE be equal to a quadrant, or 90°, then EB is the complement of AB (28). Let the lines ST and FIB be drawn perpendicular to OE. Now, IB is the sine, ET the tangent, and OT the secant of the arc EB. Instead of writing sine, tangent, and secant, of this complemental arc EB, the lines are usually designated by means of the arc AB. Thus, BI=OD, is called the cosine of AB, or cosine of AOC, written cos. AB; ET is called the cotangent of AB, or cotangent of AOC, written cot. AB; and OT, the cosecant of AB, or cosecant of AOC, written cosec. AB. In general, if A be any arc or angle, we have the cos. A=sin. (90°—A), cot. A=tang. (90°—A), and cosec. A=sec. (90°—A).
- 36. The triangles OBD, and OCA, being similar, and also similar to the triangles OBI, OTE, the relations which exist between the lines that depend for their values on the arc AB, are readily ascertained.
- 37. The radius, sine, and cosine of any arc, forming a right-angled triangle, if we denote the radius by R, we have $R^2 = \sin^2 + \cos^2$. The radius, secant, and tangent, forming a right-angled triangle, the $\sec^2 = R^2 + \tan^2$; also, $\csc^2 = R^2 + \cot^2$. The similar triangles ODB, OAC, give, for any arc or angle, A:

Cos. A:
$$\sin A :: R : \tan A = R \frac{\sin A}{\cos A}$$

Cos. A: R:: R: sec.
$$A = \frac{R^2}{\cos A}$$
;

And the similar triangles, O1B, OET, give,

Sin. A: cos. A:: R: cot. A=R
$$\frac{\cos. A}{\sin. A}$$
,

Sin. A: R:: R: cosec.
$$A = \frac{R^2}{\sin A}$$
;

Also, OAC and OTE being similiar,

$$OA : AC :: ET : OE$$
, or, $R^2 = tang$. A cot. A.

We see, from these relations, that the cosine of an arc can be found, when radius and the sine are given; and if radius, the sine, and cosine be known, that the secant, cosecant, tangent, and cotangent are determined from them.

38. We see, in examining the figure, that if the point B coincides with the point A, or the arc AB=0, the sin. AB becomes =0, the tang. AB becomes =0, the sec. AB=R, the cos. AB=R; the cot. AB, and cosec. AB, become infinite, since OC and ET are then parallel. When the arc AB=45°, sin. A=cos. A, tang. A=cot. A, sec. A=cosec. A. When the arc AB becomes AE, or equal to 90°, then the sin. A, or sin. 90°=R; cos. A, or cos. 90=0; tang. A and sec. A become infinite, as the lines AC and OC do not intersect.

39. If the arc ABEF, greater than 90, be considered, FH is its sine (30); OH, its cosine (31); AQ, its tangent (32); and OQ, its secant (33). But FH is the sine of the arc GF, the supplement of ABF (29), and OH is its cosine (31); hence, the sine of an arc is equal to the sine of its supplement; and the cosine of an angle, to the cosine of its supplement.

Furthermore, AQ is the tangent of the arc AEF (32), and OQ is its secant (33); GL is the tangent, and OL the secant, of the supplemental arc GF. But, as AQ is equal to GL, and OQ to OL, it follows, that the tangent of an arc or angle is equal to its supplement; and the secant of an arc, to the secant of its supplement.*

^{*} These relations are between the values of the trigonometrical lines; the algebraic signs which they have in the different quadrants, are not considered.

- 40. If, in a circle of a given radius, the lengths of the sine, cosine, tangent, and cotangent be calculated for every minute or second of the quadrant, and arranged in a table, such table is called a table of sines and tangents. If the radius of the circle be I, the table is called a table of natural sines. A table of natural sines is, therefore, a table which shows the values of the sines, cosines, tangents, and cotangents, to seconds or minutes, of all the arcs of a quadrant. The corresponding values of the secants and cosecants are usually omitted, being readily found from those of the cosine and sine (37).
- 41. If the values of the sine, cosine, tangent, and secant be known for arcs or angles less than 90°, they are also known for arcs or angles which are greater. For, if an arc or angle is greater than 90°, its supplement is less than 90°, and the values of these lines are the same for an angle and its supplement (39).
- 42. We have not considered the sines, cosines, &c. of arcs greater that 180; for, as the sum of the three angles of a plane triangle is equal to 180°, it follows, that no larger arc can enter into the calculations of the sides and angles of plane triangles.

THEOREM.

43. The sides of a plane triangle are proportional to the sines of their opposite angles.

Let ABC (Pl. I. Fig. 2) be a triangle; then, CB: CA:: sin. A: sin. B.

For, with A as a centre, and AD, equal to the less side BC, as a radius, describe the arc DI; and with B as a centre, and BC as a radius, describe the arc CL. Now, ED is the sine of the angle A (30), and CF is the sine of the angle B, to the same radius AD or BC. But, by similar triangles,

AD: DE:: AC: CF; AD, being equal to BC, we have, BC: sin. A:: AC: sin. B, or

BC : AC :: sin. A : sin. B.

By comparing the sides AB, AC, in a similar manner, we should obtain,

AC : AB :: sin. B : sin. C.

THEOREM.

44. In any plane triangle, the sum of the two sides containing either angle, is to their difference, as the tangent of half the sum of the other two angles, to the tangent of half their difference.

Let ABC (Pl. I. Fig. 3) be a triangle; then,

 $AC+AB : AB-AC :: tang. \frac{1}{2}(C+B) : tang. \frac{1}{2}(C-B).$

With A as a centre, and a radius AC, the less of the two given sides, let the semicircle 1FCE be described, meeting AB in I, and AB produced, in E. Draw CI and AF. Since CAE is an outward angle of the triangle ACB, it is equal to the sum of the inward angles C and B (78)*.

But the angle CIE, being at the circumference, is half the angle CAE (126)*, that is, half the sum of the angles C and B, or, equal to $\frac{1}{4}$ (C+B).

The angle AFC=ACB, is equal to ABC+BAF; therefore, BAF=ACB-ABC. But ICF= $\frac{1}{2}$ BAF= $\frac{1}{2}$ (ACB-ABC), or $\frac{1}{2}$ (C-B).

With I and C as centres, and the common radius IC, let the arcs CD and IG be described, and let the lines CE and IH be drawn perpendicular to CI. EC passes through the extremity E of the diameter IE, since the right angle ICE is an angle in a semicircle (128)*. Now, CE is the tangent of CIE $=\frac{1}{2}$ (C+B); and IH the tangent of ICB= $\frac{1}{2}$ (C-B), to the common radius CI.

But since the lines CE and IH are parallel (57)*, the triangles BHI and BCE are similar, and give the proportion,

BE, or AB+AC : BI, or AB-AC :: CE : IH; That is, AB+AC : AB-AC :: tang. $\frac{1}{2}$ (C+B) : tang. $\frac{1}{2}$ (C-B),

THEOREM.

- 45. In any plane triangle, if a line be drawn from either angle perpendicular to the opposite side, dividing it into two segments, the whole side or sum of the segments, is to the sum of the other two sides, as the difference of those sides, to the difference of the segments.
- * The references marked thus, ()*, refer to the articles of the translations of Legendro's Geometry.

Let ABC (Pl. I. Fig. 4) be a triangle, and BD perpendicular to the base AC: then,

AC : AB + CB :: AB - CB : AD - DC;

For, AB² = AD² + BD², and BC² = CD² + BD² (186)*; by subtraction, AB² - BC² = AD² - CD²; but, the difference of the squares being equal to the rectangle under the sum and difference (184)*, we have,

 $\begin{array}{c} AB^2 - BC^2 = (AB + BC).(AB - BC),\\ \text{and } AD^2 - CD^2 = (AD + CD).(AD - CD) \ ;\\ \text{therefore, } (AB + BC).(AB - BC) = (AD + CD).(AD - CD) \ ;\\ \text{hence, } AD + CD \ : \ AB + BC \ :: \ AB - BC \ : \ AD - CD. \end{array}$

THEOREM.

46. In any right-angled plane triangle, radius is to either leg, as the tangent of the adjacent angle, to the opposite side.

Let ABC (Pl. I. Fig. 5) be a plane triangle, right-angled at B; then,

Radius: AB:: tang. A: BC.

For, with any radius, as AD, and the vertex of the angle A as a centre, let the arc DE be described, and the tangent DF drawn. Then, by similar triangles,

AD : AB :: DF : BC;

That is, calling the radius R, R: AB:: tang. A: BC. If the vertex of the angle C were used as a centre, and an arc described similar to DE, we should have,

R:CB::tang.C:AB.

47. The relations between the sides and angles of plane triangles, demonstrated in the last four articles, are sufficient to solve all the cases of Plane Trigonometry. In every plane triangle, there are six parts, three sides, and three angles. Of these six parts, at least three must be given, and one of these a side, to enable us to determine the others. If the three angles are given, it is plain, that an indefinite number of similar triangles may be constructed, whose angles shall be respectively equal to the angles that are given. In such case, [the sides being proportional to the sines of the opposite angles (43),] the ratio, or proportion of the sides, is known, although their magnitudes cannot be determined from these data.

Assuming, with this restriction, any three parts of a triangle as given, one of these three cases will always be presented.

- 1. When there are two angles and a side given.
- 2. When there are two sides and an angle given.
- 3. When the three sides are given.

In the first case, add the given angles together, and subtract their sum from 180°, the remainder is the third angle of the triangle (73)*. The remaining parts are then found by Art. 43.

In the second case, the given angle must either be included by the given sides, or opposite one of them; if the latter, the remaining parts are found by Art. 43; if the former, by Art. 44.

In the third case, a perpendicular is let fall on the greatest side, the segments found by Art. 45, and then the hypothenuse is to radius, as the base of either of the right-angled triangles, to the sine of the corresponding vertical angle.

A table of sines, cosines, tangents, &c. is necessary to afford the sines, cosines, or tangents of such angles as enter into the proportions. To find the fourth terms of these proportions, the second and third terms must be multiplied together, and their product divided by the first. This process is tedious. To avoid it, we have recourse to logarithms. As the addition of logarithms corresponds to the multiplication of their numbers (4), and their subtraction to the division of their numbers, it is requisite only to add the logarithms of the second and third terms together; this gives the logarithm of their product, and from this sum, to subtract the logarithm of the first term, and the remainder is the logarithm of the quotient, or fourth term of the proportion.

But we are unable to avail ourselves of the logarithmic computation, unless we are possessed of a table, showing the logarithms of the sines, cosines, tangents, &c. calculated for a given radius, of all the arcs of a quadrant. Such a table is annexed, and is called a table of logarithmic sines and tangents.

TABLE OF LOGARITHMIC SINES.

48. In this table are arranged the logarithms of the numerical values of the sines, cosines, tangents, and cotangents, of all

the arcs or angles of the quadrant, divided to minutes, and calculated for a radius of 1000000000. The logarithm of this radius is 10 (9). In the first and last horizontal line of each page, are written the degrees whose logarithmic sines, &c. are expressed on the page. The vertical columns on the left and right, are columns of minutes.

49. To find, in the table, the logarithmic sine, cosine, tangent, or cotangent of any given arc or angle.

- 1. If the angle be less than 45°, look in the first horizontal line of the different pages, until the number of degrees be found; then descend along the column of minutes, on the left of the page, till you reach the number representing the minutes; then pass along the horizontal line till you come into the column designated, sine, cosine, tangent, or cotangent, as the case may be: the number so indicated, is the logarithm sought. Thus, the sine, cosine, tangent, and cotangent of 19° 55′, are found on page 37, opposite 55, and are, respectively, 9.532312, 9.973215, 9.559097, 10.440903.
- 2. If the angle be greater than 45°, search along the bottom line of the different pages, till the number of degrees are found; then ascend along the column of minutes, on the right-hand side of the page, till you reach the number expressing the minutes; then pass along the horizontal line into the columns designated tang., cotang., sine, cosine, which correspond to the degrees indicated at the bottom of the page; the number so pointed out, is the logarithm required.

50. It will be seen, that the column designated sine at the top of the page, is designated cosine at the bottom; the one designated tang., by cotang; and the one designated cotang., by tang.

The angle found by taking the degrees at the top of the page, and the minutes from the first vertical column on the left, is the complement of the angle, found by taking the corresponding degrees at the bottom of the page, and the minutes traced up in the right-hand column to the same horizontal line. This being apparent, the reason is manifest, why the columns designated sine, cosine, tang., and cotang., when the degrees are pointed out at the top of the page, and the minutes counted downwards, ought to be changed, respectively, into cosine,

sine, cotang., and tang., when the degrees are shown at the bottom of the page, and the minutes counted upward (35).

- 51. If an angle be greater than 90°, we have only to subtract it from 180°, and take the sine, cosine, tangent, or cotangent of the remainder (39).
- 52. The secants and cosecants are omitted in the table, being easily found from the cosines and sines.

For, sec. =
$$\frac{R^2}{\cos}$$
 (37); or, taking the logarithms: log.sec. = 2 log.

R-log. cos.=20-log. cos; that is, the logarithmic secant is found by subtracting the logarithmic cosine from 20. And

cosec.
$$=\frac{R^2}{\text{sine}}$$
, or log. cosec. $=2$ log. R -log. sine $=20$ -log.

sine; that is, the logarithmic cosecant is found by subtracting the logarithmic sine from 20.

It has been shown (37), that $R^2 = \tan g$. × cotang.; therefore, 2 log. R.=log. tang.+log. cotang; or, $20 = \log$. tang.+log. cotang.

53. The column of the table, next to the column of sines, and on the right of it, is designated by the letter D. column is calculated in the following manner. Opening the table at any page, as 42, the sine of 24° is found to be 9.609313; of 24° 1′, 9.609597: their difference is 284; this being divided by 60, the number of seconds in a minute, gives 4.73, which is entered in the column D, omitting the decimal point. Now, supposing the increase of the logarithmic sign to be proportional to the increase of the arc, and it is nearly so for 60", it follows, that 473 (the last two places being regarded as decimals) is the increase of the sign for 1". Similarly, if the arc be 24° 20', the increase of the sine for 1" is 465, the last two places being decimals. The same remarks are equally applicable in respect of the column D, after the column cosine, and of the column D, between the tangents and cotangents. The column D, between the tangents and cotangents, is equally applicable to either of these columns; since of the same arc, the log. tang.+log. cotang.=20 (52). Therefore, having two arcs, a and b, log. tang. $b+\log$. cotang. $b=\log$. tang. $a+\log$. cotang. a; or log. tang. b—log. tang. a=log. cotang. b—log. cotang. a.

54. Now, if it were required to find the logarithmic sine of an arc expressed in degrees, minutes, and seconds, we have only to find the degrees and minutes as before; then multiply the corresponding tabular number by the seconds, cut off two places to the right-hand for decimals, and then add the product to the number first found, for the sine of the given arc. Thus, if we wish the sine of 40° 26′ 28″.

The sine 40° 26′ 9.811952

Tabular difference = 247 Number of seconds = 28

Product = 69.16, which being added = 69.16

Gives for the sine of $40^{\circ} 26' 28'' = 9.812021.16$

The tangent of an arc, in which there are seconds, is found in a manner entirely similar. In regard to the cosine and cotangent, it must be remembered, that they increase while the arcs decrease, and decrease while the arcs are increased; consequently, the proportional numbers found for the seconds must be subtracted, not added.

Ex. To find the cosine 3° 40′ 40′.
Cosine 3° 40′

Tabular difference = I3

Number of seconds = 40

Product = 5.20, which being subtracted = 5.80

9.999110

Gives for the cosine of $3^{\circ} 40' 40'' = 9.999104.20$

55. To find the degrees, minutes, and seconds answering to any given logarithmic sine, cosine, tangent, or cotangent.

Search in the table, and in the proper column, until the number be found; the degrees are shown either at the top or bottom of the page, and the minutes in the side columns, either at the left or right. But, if the number cannot be exactly found in the table, take the degrees and minutes answering to the nearest less logarithm, the logarithm itself, and also the corresponding tabular difference. Subtract the logarithm taken from the table from the given logarithm, annex two

ciphers, and then divide the remainder by the tabular difference: the quotient is seconds, and is to be connected with the degrees and minutes before found; to be added for the sine and tangent, and subtracted for the cosine and cotangent.

Ex. 1. To find the arc answering to the sine 9.880054 Sine 49° 20, next less in the table, 9.879963

Tab. Diff. 181) 9100 (50"

Hence, to the given sign 9.880054 corresponds the arc 49° 20' 50''.

Ex. 2. To find the arc corresponding to cotang. 10.008688. The given cotang. 10.008688

Cotang. 44° 26', next less in the table, 10.008591

Tab. Diff. 421) 9700 (23"

Hence, $44^{\circ} 26' - 23'' = 44^{\circ} 25' 37''$ is the arc corresponding to the given cotangent 10.008688.

56. All the principles applicable in the solution of the questions which arise in plane trigonometry, having been explained, we shall subjoin a few examples under each of the three cases.

CASE I.

57. Example I.—In a plane triangle ABC (Pl. I. Fig. 6), are given the angle $A=58^{\circ}$ 7′, the angle $B=22^{\circ}$ 37′, and the side AB=408 yards. Required the remaining angle and the other two sides.

To the angle $A = 58^{\circ}$ 7' Add the angle $B = 22^{\circ}$ 37'

Their sum = 80° 44' taken from 180°, leaves the angle C=99° 16'. This being greater than a quadrant, its sine is found by using its supplement 80° 44'.

To find the side BC. To find the side AC. As sine C, 99° 16′ As sine C, 99° 16' 9.994295 9.994295 To AB, 408 2.610660 To AB, 408 2.610660 So is sine A, 58° 7′ 9.928972 So is sine B, 22° 37' 9.584968 12.539632 To BC, 351.024 2.545337 To AC, 158.976 2.201333 BC is therefore 251.024, and AC, 158.976 yards.

58. In this example, instead of adding the second and third terms, and then writing the first under their sum and making the subtraction, the whole was performed in a single operation, by using what is called the arithmetical complement, which we shall now define, and whose use in the trigonometrical calculations is also to be explained. The arithmetical complement of any logarithm is the difference between this logarithm and any whole number greater than it; though we will limit the definition to the case when the logarithm is subtracted from 10.

It is now to be shown, that the difference between any two logarithms, is the same as the sum of the arithmetical complement of the logarithm to be subtracted and the other logarithm, diminished by the number 10.

In the first proportion, 12.539632 is the sum of the logarithms of the second and third terms: from this sum 9.994295 is to be subtracted; and 12.539632-9.994295 is equal to the difference. But 10-9.994295=A, the arithmetical complement; by transposing 10, and changing the signs of both numbers, 9.994295=10-A. Now, if the second number instead of the first be subtracted from 12.539632, the difference will be expressed by 12.539632 + A - 10 = 2.545337, and as a similar demonstration can be made for any other number, the proposition is manifest. The arithmetical complement is always found by subtracting the first figure on the right from ten, and each of the other figures from 9; so that these differences can be readily added with the lower and middle lines, and the ten rejected from the sum. Thus, in the first example, we say 2 and 0 are 2 and 5 are 7, set down 7; then 7 and 6 are 13 and 0 are 13, set down 3 and carry 1; then 1 and 9 are 10 and 6 are 16 and 7 are 23, set down 3 and carry 2; then 2 and 8 are 10 and 5 are 15, set down 5 and carry 1; 1 and 2 are 3 and 1 are 4 and 0 are 4: 9 and 6 are 15 and 0 are 15; 1 and 9 are 10 and 2 are 12 and 0 are 12: now, reject the 10 to be subtracted, and set down 2, and we have the logarithm of the fourth term. The arithmetical complement may also be written directly from the tables, or, if it be not used at all, the second and third terms may be added, and the first subtracted from their sum.

59. Example 2.—In a plane triangle ABC (Pl. I. Fig. 7),

are given, AC=216; CB=117, the angle A=22° 37′, to find the other parts.

Draw an indefinite right line ABB': from any point as A. draw AC making BAC=22.37; and make AC=216. With C as a centre, and a radius equal to 117, the other given side. describe the arc B'B; draw B'C, and BC; either of the triangles ABC, or ABC will answer all the conditions of the question.

To find the sides and angles by computation.

To find the angle B.

As BC, 117	2.068186
To sine A, 22° 37′	9.584968
So is AC, 216	2.334454

To sine B, Add to each 4.	45° 13′ 55″, or A, 22° 37′ 00	134° 46′ 9 22° 37	,	9) 9.85	1236
Take the sum From	67° 50° 55″ 180° 00° 00	157° 23′ 180° 00			
Remainder	112° 09′ 05″ or	· 22° 36′	55",	be ng	ACB'

and ACB.

To find AB or AB', reverse the terms of the former proportion, and sav

As sin. A, 22° 37′ To BC, or B'C, 117	9.584968 2.068186
So is sin. ACB', 112° 9' 5"	9.966701
To AB', 281.796	2.449919

The ambiguity in this, and similar examples, arises in consequence of the first proportion being true for both the triangles ACB and ACB'. As long as the two triangles remain, the ambiguity will continue. But, if the side CB, opposite the given angle, be greater than AC, the arc BB will cut the line ABB, on the same side of the point A, but in one point, and then there will be but one triangle answering the conditions.

If the side CB be equal to the perpendicular Cd, the arc BB' will be tangent to ABB', and in this case also there will be but one triangle. When CB is less than the perpendicular Cd, the arc BB' will not intersect the base ABB', and in that

40.000

case there will be no triangle, or the conditions are impossible.

To determine the value of Cd in terms of the given parts, we have the proportion $\sin .90^{\circ}$, or $R : AC :: \sin .A : Cd$, or $Cd = \frac{AC \sin .A}{R}$, or $\log .Cd = \log .AC + \log .\sin .A - 10$.

So that, when the logarithm of the opposide side CB is equal to log. AC+log. sin. A—10, there is one solution; when less, the problem is impossible; when greater, but less than the logarithm of AC, two solutions; and when greater than the logarithm of AC, but one.

Ex.~3.—Given two angles of a plane triangle 22° 37′ and 134° 46′, and the contained side 351: required the remaining parts.

Answer.—Angle 22° 37'; sides 351 and 648.

Example 4.—Given two sides of a plane triangle 50 and 40 respectively, and the angle opposite the latter equal to 32°; to determine the triangle.

Answer.—If the angle opposite to the side 50 be acute, it is $= 41^{\circ} 28'$, the third angle $= 106^{\circ} 32'$, and the remaining side = 72.36. If the angle opposite to side 50 be obtuse, it is $= 138^{\circ} 32'$, the other angle $= 9^{\circ} 28'$, and the side = 12.415.

CASE II.

60. When two sides and the included angle are given.

The solution is made by Art. 44. Take the given angle from 180°, the remainder is the sum of the other two angles, which being divided by 2, gives half their sum. Then find half their difference: their half difference being added to half their sum, gives the greater angle, and being subtracted from it, gives the less.* And as the greater angle is opposite the greater side, and the less angle opposite the less side, the three angles and two sides of the triangle become known: the third side may then be known by Case I.

62. Example 1.—Let there be given in any plane triangle ABC, AC=450, BC=540, and the included angle C=80°, to find the other angles and the remaining side.

^{*} Let a+b=s, and a-b=d: then by adding 2a=s+d, or $a=\frac{1}{2}s+\frac{1}{2}d$; and by subtracting 2b=s-d, or $b=\frac{1}{2}s-\frac{1}{2}d$.

To tang. \(\frac{1}{2}\) (A - B), 6° 11' \(\frac{9.034793}{}\)

Hence $50^{\circ}+6^{\circ}$ $11'=56^{\circ}$ 11'=A; and $50^{\circ}-6^{\circ}$ $11'=43^{\circ}$ 49'=B.

Then to find the third side AB.

As sin. B, 43° 49′ 9.840328 To AC, 450 2.653213 So is sin. C 80° 9.993351 To AB, 640.08 2.806236

Example 2.—Given two sides of a plane triangle, 1686 and 960, and their included angle 128° 4': to find the other parts.

Answer.—Angles 33° 34' 39", 18° 21' 21", side 2400.03.

CASE III.

62. When the three sides of a plane triangle are given, to find the angles. Let fall a perpendicular from the angle opposite the greater side, dividing the given triangle into two right-angled triangles; then find the difference of the segments by Art. 45. Half the difference being added to half the base, gives the greater segment; and, being subtracted from half the base, gives the less segment. Then since the greater segment belongs to the right-angled triangle having the greatest hypothenuse, we have the sides and right angle of two right-angled triangles, to find the acute angles.

Example 1.—The sides of a plane triangle (Pl. I. Fig. 4), are AC=40, AB=34, and BC=25. Required the angles.

As AC: AB+BC:: AB-BC: AD-CD,
That is 40: 59:: 9:
$$\frac{59 \times 9}{40}$$
=13.275;
Then $\frac{40+13.275}{2}$ =26.6375=AD;
And $\frac{40-13.275}{2}$ =13.3625=CD.

As AB, 34

1.531479 | As CB, 25

1.397940

34' 40") | 18' 35")

'Hence 90°—51° 34' 40"=38° 25' 20"=A; 90°—32° 18' 35"
=57° 41' 25"=C; and 51° 34' 40"+32° 18' 35"=83° 53' 15"
=ABC.

Example 2.—When the sides are 4, 5, and 6, what are the angles?

Answer.-41° 24′ 35″, 55° 46′ 16″, and 82° 49′ 9″.

SOLUTION OF RIGHT-ANGLED TRIANGLES.

63. The unknown parts of a right-angled triangle may be found by either of the three last cases: or, if two of the sides be given, by means of the property, that the square of the hypothenuse is equal to the sum of the squares of the other two sides; or the parts may be found by Art. 46.

Example 1.—In the right-angled triangle ABC, there are given the hypothenuse AC=25, and the base AB=24. Required the other parts.

As AC, 25	1.397940	As radius	10.000000
To sin. B, 90°	10.000000	To AB, 24	1.380211
So is AB, 24	1.380211	So is tang. A, 16	2) 0.464990
	·	So is tang. A, 16° 15′ 37″	3.404889
To sin. C,73°44′5	23" 9.982271		
90°-73° 44′ 23″ =	=16° 15′ 37″	To BC, 7.00004	40.845100
=A.		•	

Example 2.—In a right-angled triangle, there are given one leg equal to 384, and its opposite angle 53° 8', to find the other leg and the hypothenuse.

Answer.—Leg 280, hypothenuse 480.

Example 3.—In a right-angled triangle, are given the base 195, its adjacent angle 47° 55' to find the rest.

Answer. - Perp. 216, hyp. 291, vert. angle 42° 5′.

ELEMENTS OF SURVEYING.

CHAPTER I.

DEFINITIONS AND INTRODUCTORY REMARKS.

64. Surveying, in its most extensive signification, comprises all the operations necessary for determining the area, or content of any portion of the earth's surface, the lengths and direction of the bounding lines, and their accurate delineation on paper.

65. The earth being spherical, its surface is curved, and every line traced accurately on the surface, is also curved.

- 66. If large portions of the earth's surface are to be measured, such as states and territories, its curvature must be taken into account; and very material errors will arise if it be neglected. This method of measurement and computation is called *Geodesic Surveying*.
- 67. The radius of the earth, however, being large, the curvature of its surface is small, and when the measurement is limited to inconsiderable portions, the error is not sensible in supposing the surface a plane. This method of measurement and computation, is called *Plane Surveying*, which will be alone treated of in these Elements.
- 68. If at any point of the surface of the earth, a plane be drawn perpendicular to the radius passing through this point, such plane is tangent to the surface, and is called a horizontal plane. All planes parallel to such a plane, are also named horizontal planes.

- 69. A plane perpendicular to a horizontal plane, is called a vertical plane.
- 70. The lines of a horizontal plane, as well as all lines which are parallel to it, are named horizontal lines.
- 71. Lines which are perpendicular to a horizontal plane, are called *vertical lines*, and lines which are inclined to it, oblique lines.
- 72. The horizontal distance between two points, is the horizontal line intercepted between the two vertical lines passing through those points.
- 73. A horizontal angle is one whose sides are horizontal; its plane also is horizontal. A horizontal angle may also be defined, the angle included between two vertical planes passing through the angular point, and the two objects which subtend the angle.
 - 74. A vertical angle is one whose plane is vertical.
- 75. An angle of *elevation*, is a vertical angle having one of its sides horizontal, and the inclined side above the horizontal side.
- 76. An angle of *depression*, is a vertical angle having one of its sides horizontal, and the inclined side under the horizontal side.
- 77. An oblique angle, is one whose plane is oblique to the horizontal plane.
- 78. All lines, which can be the object of measurement, must belong to one of the three classes above named: that is, they are either horizontal, vertical, or oblique. The angles also are distributed into three classes; horizontal angles, vertical angles, and oblique angles: the class of vertical angles being subdivided into angles of elevation, and angles of depression.

CHAPTER II.

OF THE MEASUREMENT AND CALCULATION OF LINES AND ANGLES.

- 79. It has been shown (47), that at least one side and two of the other parts of a plane triangle, must be given or known, before the other parts can be found by computation. When, therefore, it is proposed to ascertain distances by trigonometrical calculations, the first steps necessary are, to measure certain lines on the ground, and also to measure as many angles as are required to render at least three parts of every triangle known; and then, by the aid of trigonometry, the other sides and angles may be calculated.
- 80. Our attention, then, is directed first, to the measurement of lines; secondly, to the measurement of angles; and thirdly, to the calculations for the unknown or required parts.
- 81. Any tape, rod, or chain, by means of which we can ascertain equal parts, may be used as a measure, and the unit of measure may be a foot, a yard, a rod, a mile, or any other ascertained distance. The measure in general use is a chain of 4 rods, or 66 feet, in length, called Gunter's chain, from the name of the inventor. This chain is made up of 100 links; every tenth, from either end, is marked by a small brass plate attached to it, and notched, to designate its number from the end. The division of the chain into one hundred equal parts, is a very convenient one, since the divisions, or links, are decimals of the whole chain, and in the calculations may be treated as such. The length of the chain being 4 poles, or 66 feet, is equal to 792 inches, which being divided by 100, gives 7.92 inches for the length of each link. A mile being equal to 320 rods, 80 chains=1 mile, 40 chains=1 a mile, and 20 chains=1 of a mile.

Besides the chain, there are wanted for measuring, 10 marking pins, and two staves about 6 feet in length, having a spike in the lower end, to aid in holding them firmly, and a horizontal strip of iron passing through them, to prevent the chain from slipping off; these staves are to be passed through the rings, at the ends of the chain.

TO MEASURE A HORIZONTAL LINE.

- 82. Being provided with a chain, the staves, and the marking pins, let two signal staves be planted, one where the measurement is to begin, and the other where it is to terminate; or, perhaps, some distant object, in the direction of the line to be measured, may serve as a sufficient guide, and render the second staff unnecessary. Let the ten marking pins, and one end of the chain be taken by the person that is to go forward. who is called the leader, and let him plant the staff as nearly as possible in the direction of the stations: then, taking the staff in his right hand, let him stand off at arm's length, so that the person at the other end of the chain can align it exactly; when the alignment is made, let the chain be stretched. and a marking pin placed: and so on till the whole line is measured. Great care must be taken to keep the chain horizontal; and if the acclivity or declivity of the ground be too great to admit of measuring a whole chain at a time, a part of a chain only must be measured: the sum of all the horizontal lines so measured, is evidently the horizontal distance between the stations.
- 83. We come now to the measurement of angles, and for this purpose several instruments are used. The one, however, which affords the most accurate results, and which indeed can alone be relied on for nice work or extensive operations, is called a theodolite. This instrument only will be described at present, others will be subsequently explained.

OF THE THEODOLITE.

84. The theodolite is an instrument used to measure horizontal and vertical angles. It is usually placed on a tripod ABC (Pl. II. Fig. 1), which enters by means of a screw the lower horizontal plate DE, and becomes firmly attached to the

body of the instrument. Through the horizontal plate DE, four small hollow cylinders are inserted with female screws in their interior, which receive four screws with milled heads, that work against a second horizontal plate, FG. The upper side of the plate DE terminates in a curved surface, which encompasses a ball, that is nearly a semisphere, with the plane of its base horizontal. This ball, which is hollow, is firmly connected with the smaller base of a hollow conic frustum, that passes through the curved part of the plate DE, and screws firmly into the curved part of the second horizontal plate FG.

A hollow conic spindle passes through the middle of the ball, and the hollow frustum with which it is connected. this spindle, a third horizontal and circular plate HI, called the limb of the instrument, is permanently attached. Within this spindle, and concentric with it, there is a second spindle, called the inner, or solid spindle. To this latter, is united a thin circular plate, called the vernier plate, which rests on the limb of the instrument, and supports the upper frame work. The two spindles terminate at the base of the spherical ball, where a small male screw enters the inner one, and presses a washer against the other, and the base of the ball. On the upper surface of the plate FG, rests a clamp which goes round the outer spindle, and being compressed by the clamp screw K, is made fast to it. This clamp is thus connected with the plate A small cylinder a, is fastened to the plate FG: through this cylinder a thumb screw L passes, and works into a small cylinder b, connected with the clamp. The cylinders b and aadmit of a motion round their axis, to relieve the screw L of the pressure which would otherwise be occasioned by working it.

Directly above the clamp, is the lower telescope MN. This telescope is connected with a hollow cylinder, which is worked freely round the outer spindle, by the thumb screw P, having a pinion acting with a concealed cog-wheel, that is permanently fastened to the limb of the instrument. By means of a clamp screw Q, the telescope is made fast to the limb, when it will have a common motion with the limb and outer spindle.

The circular edge of the limb is chamfered, and is generally

made of silver, and on this circle the graduation for horizontal angles is made. In the instrument described, the circle is cut into degrees and half degrees; the degrees are numbered from 0 to 360.

On the circular edge of the vernier plate, is a small space of silver called a *vernier*; this space is divided into 30 equal parts, and numbered from the line marked 0 to the left.

There are two levels attached to the vernier plate, at right angles to each other, by small adjusting screws; one of them is seen in the figure. The vernier plate, turning with the inner spindle, is moved round by the thumb screw T, which has a pinion working with a concealed cog-wheel, that is part of the limb of the instrument. The clamp screw S, fastens the vernier plate to the limb. In some theodolites, there is a tangent screw, similar to the screw L, by means of which, the smaller motions of the vernier plate are regulated.

There is a compass on the vernier plate that is concentric with it, the use of which is explained under the head, Compass.

The frame work which supports the horizontal axis of the vertical semicircle UV, and the upper telescope with its attached level, rosts on the upper plane of the vernier plate, to which it is made fast by three adjusting screws, placed at the angular points of an equilateral triangle. The vertical semicircle UV, is called the vertical limb; its motions are governed by the thumb screw Z, which has a pinion, that works with the teeth of the vertical plate. On the face of the vertical limb, opposite the thumb screw Z, the circle is divided into degrees and half degrees: the degrees are numbered both ways from the line marked 0. There is a small plate resting against the graduated face of the vertical limb, called the vernier; it is divided into 30 equal parts, and the middle line is designated by 0. On the other face of the vertical limb, are two ranges of divisions, commencing at the 0 point, and extending each way 45°. The one shows the vertical distance of any object to which the upper telescope is directed, above or below the place of the instrument in 100th parts of the horizontal distance: the other, the difference between the hypothenusal and base lines; the hypothenuse being supposed

to be divided into one hundred equal parts: therefore, by mere inspection we can ascertain the number of links, which must be subtracted from every chain of an oblique line, to reduce it to a true horizontal distance.

The supports of the upper telescope are called the wyes, and designated Y's. Two loops turning on hinges, pass over the telescope, and are made fast by the pins c and d; these loops confine the telescope in the Y's. By withdrawing the pins, and turning the loops on their hinges, the telescope may be removed for the purpose of being reversed in position; and in both situations, the telescope can be revolved in the Y's about its axis.

In the telescopes attached to the theodolite, are two principal lenses, one at each end. The one at the end where the eye is placed, is called the eye glass, the other, the object glass.

In order that the axis of the telescope may be directed to an object with precision, two spider's lines, or small hairs, are fixed at right angles to each other, in slides, and placed within the barrel of the telescope, and at the focus of the eye glass. The slide which holds the vertical hair, is moved by two small horizontal screws, one of which, f, is seen in the figure; and the slide which holds the horizontal hair, by two vertical screws, g and h, one screw being loosened, and the other tightened, in either case.

Before using the theodolite, it must be properly adjusted. The adjustment consists in bringing the different parts to their proper places.

The line of collimation, is the axis of the telescope. With this axis, the line drawn through the centre of the eye glass, and the intersection of the spider's lines, ought to coincide.

The first adjustment regards the line of collimation: it is, to fix the intersection of the spider's lines in the axis of the telescope.

Having screwed the tripod to the instrument, extend the legs, and place them firmly. Then loosen the clamp screw S of the vernier plate, and with the thumb screw T, direct the telescope to a small, well-defined, and distant object. By

means of a small pin *i*, on the under side of the telescope, slide the eye glass till the spider's lines are seen distinctly; then, with the thumb screw X, which forces out, and draws in, the object glass, adjust this glass to its proper focus, when the object, as well as the spider's lines, will be distinctly seen: after which, by the thumb screws T and L, bring the intersection of the spider's lines exactly upon a well-defined point of the object.

Having done this, revolve the telescope in Y's, half round, when the attached level mn, will come to the upper side. See. if in this position, the horizontal hair appears above or below the point, and in either case, loosen one, and tighten the other, of the two screws that work the horizontal slide, till the horizontal hair has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again the intersection of the spider's lines to the point, and repeat the operation till the horizontal hair neither ascends nor descends, while the telescope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted. This adjustment is made on the supposition, that the parts of the telescope which come in contact with the Y's, are truly cylindrical. To ascertain if they be so, reverse the telescope in the Y's, turn the vernier plate 180°, and if the intersection of the spider's lines is still directed to the same point, the adjustment may be relied on.

Second adjustment.—To make the axis of the attached level of the upper telescope, parallel to the line of collimation.—Turn the vernier plate, till the telescope comes directly over two of the levelling screws, between the plates DE and FG. Turn these screws contrary ways, keeping them firm against the plate FG, till the bubble of the level mn, stands at the middle of the tube. Then, open the loops, and reverse the telescope. If the bubble still stands in the middle of the tube, the axis of the tube is horizontal; but if not, it is inclined, the bubble being at the elevated end. In that case, by means of the small vertical screws m and n, at the ends of the level, raise the depressed end, or depress the elevated one, half the inclination; and then with the levelling screws, bring it into a

horizontal position. Reverse the telescope in the Y's, and make the same correction again, and so on, until the bubble stands in the middle of the tube, in both positions of the telescope: the axis of the level is then horizontal. Let the telescope be now revolved in the Y's. If the bubble continue in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recede from its centre, the axis of the level is inclined to the line of collimation, and must be made parallel to it by means of two small screws, (one of which is seen at p,) which work horizontally. By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation, and then, if the telescope be revolved in the Y's, the bubble will continue in the middle of the tube.

It is difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation; for if the level were truly horizontal in one position of the telescope, when the telescope is reversed, the bubble would not stand in the middle of the tube, except in one position of the level. This suggests the necessity of making the first part of the adjustment with tolerable accuracy; then, having made the second with care, let the first be again examined, and proceed thus till the adjustment is completed.

Third adjustment.—To make the limb of the instrument horizontal, or, to make the common axis of the limb and vernier plate truly vertical. This adjustment is effected, partly by the levelling screws, and partly by the thumb screw Z. Turn the vernier plate, until the upper telescope comes directly over two of the levelling screws, then turn them contrary ways, till the upper telescope is horizontal; after which, turn the vernier plate 180°, and if the bubble of the level remain in the middle of the tube, one line of the limb is horizontal. But if the bubble recede from the centre of the level, raise the lower, or depress the upper end, one-half by the levelling screws, the other by the thumb screw Z, till it is brought into a horizontal position. Bring the vernier plate back to its first position, and if the level be not horizontal, make it so, by dividing the error as before, and repeat the operation until the line of the limb is

truly horizontal. Then turn the vernier plate 90°, and level as before. The limb ought now to be truly horizontal; but lest the first horizontal line may have been changed, in obtaining the second, it is well to bring the telescope and level two or three times over the levelling screws, until an entire revolution can be made without displacing the bubble from the middle of the tube. As this can only be the case when the level revolves around a vertical line, it follows that the limb will then be horizontal, and the axis of the instrument vertical.

This adjustment being completed, the levels of the vernier plate are readily made parallel with it, by means of the small screws at their extremities. The three levels being then horizontal, and perpendicular in direction to the axis of the theodolite, the bubbles will retain the middle places in the tubes, during an entire revolution of the vernier plate, or of the limb and vernier plate together.

But the levels of the vernier plate may be made parallel with the limb, and the limb truly horizontal, without the aid of the upper level.

Let the upper telescope be placed directly over two of the levelling screws. One of the levels of the vernier plate will then be parallel to the line of these two screws, and the other level will be at right angles to this line, or parallel to the line of the other two levelling screws. In this situation, let the levels, by means of the levelling screws, be made horizontal. Then turn the vernier plate 180°, and, if they both continue horizontal, the limb is truly level. But if both, or either of them, be changed from a horizontal position, let the error be divided between the level and the limb, and repeat the operation until the levels will continue horizontal during an entire revolution: the limb is then horizontal, and the axis of the instrument truly vertical.

Fourth adjustment.—To make the axis of the vertical limb truly horizontal, or perpendicular to the axis of the instrument. Bring the intersection of the spider's lines of the upper telescope upon a plumb line, or any well-defined vertical object, and move the telescope with the thumb screw Z: if the intersection of the spider's lines continue on the vertical line, the

axis is horizontal. Or, the adjustment may be effected thus: Direct the intersection of the spider's lines to a well-defined point that is considerably elevated: then turn the vertical limb, until the axis of the telescope rests on some other well-defined point, upon or near the ground: reverse the telescope, and turn the vernier plate 180: now, if in elevating and depressing the telescope, the line of collimation passes through the two points before noted, the axis is horizontal. If it be found, by either of the above methods, that the axis is not horizontal, it must be made so by the screws which fasten the frame work to the vernier plate.

There are two important lines of the theodolite, the positions of which are determined with great care by the maker, and fixed permanently. First, the axis of the instrument is placed exactly at right angles with the limb and vernier plate; and unless it have this position, the vernier plate will not revolve at right angles to the axis, as explained in the third adjustment. Secondly, the line of collimation of the upper telescope, is fixed at right angles to the horizontal axis of the vertical limb. We can ascertain whether these lines are truly at right angles, by directing the intersection of the spider's lines to a well-defined point; then removing the caps which confine the horizontal axis in its supports, and reversing the axis: if the intersection of the spider's lines can be made to cover exactly the same point, without moving the vernier plate, the line of collimation is at right angles to the axis.

If the theodolite be so constructed that either of the Y's admit of being moved laterally, the position of the line of collimation, and the horizontal axis, can then be altered and easily arranged at right angles, if they have not been so placed by the maker.

The theodolite being properly adjusted, the particular uses of its several parts, and the manner of measuring angles, are now to be explained.

There are two verniers on the vernier plate, and the points of them marked 0, are at the opposite extremities of a diameter; which diameter is the intersection of a vertical plane passed through the line of collimation, with the vernier plate.

It is important to ascertain the exact arc intercepted on the limb, between its 0 point (this being the point from which the degrees are numbered,) and this diameter, for any position which it may assume. The limb being divided to half degrees, if we had only the line marked 0 on the vernier to guide us, the place of the diameter could only be ascertained with certainty to half degrees, there being no means of determining its exact position, when it falls between the lines of division of the limb. But the vernier affords results much more accurate. As most instruments for the measurement of angles have verniers, it will perhaps be best to explain their use generally.

First.—Count carefully the number of spaces into which the vernier is divided: this number is one less than the number of lines which limit them.

Secondly.—Turn the vernier till the line at one extremity coincides with a line of the graduated limb, when the line at the other extremity will also coincide with a line of the graduated limb; the sum of the spaces on the vernier being always exactly equal to a given number of spaces on the limb: then count the number of spaces on the limb which the vernier covers.

Thirdly.—Examine the limb of the instrument, and ascertain into what parts of a degree it is divided, or the value in minutes of the spaces shown thereon.

Let x represent the value of one of the equal spaces of the vernier, and n their number; then nx is equal to the space covered by the vernier. Let a represent the smallest equal space into which the limb is divided, and m the number of such spaces covered by the vernier; then ma is equal to the space on the limb covered by the vernier, which is also equal to nx.

The equation nx=ma is called the equation of the instrument. In this equation, $x=\frac{ma}{n}$; m, a, and n being known, x is known, as also the difference between a and x, which we shall show presently to be the smallest certain count of the instrument.

In the theodolite, m=29, n=30, and a=30, hence $x=\frac{29\times30}{30}=29$; and a-x=30-29=1, the excess of a space on the limb over a space on the vernier.

Let AB (Pl. 2. Fig. 2), be a portion of the limb of the instrument, and ECD the vernier in one of its positions, its 0 point coinciding with the line marked 10 on the limb. Now, since the spaces of the vernier are less by 1 than the spaces of the limb, the first line on the left of 0, will be 1' to the right of the first line on the left of the 10 on the limb, and if the vernier plate be moved 1' towards the left, the lines will coincide; when the second line from 0 will be 1' to the right of the second line from 10; and if the vernier be moved another minute, these lines will coincide. The vernier would then show 10° 2'.

If the vernier plate be turned still farther, till the third, fourth, fifth, &c. lines coincide, it is plain, that the 0 point of the vernier will have passed the line 10 on the limb, by as many minutes as there are lines of the vernier which shall have coincided with lines of the limb. When the last line of the vernier coincides with a line of the limb, the vernier will have been moved 30, or half a degree; the 0 point will coincide with a line of the limb at the same time, and show 10° 30′.

The general rule for reading the angle for any position of the vernier may now be stated.

When the 0 line of the vernier coincides with a line of the limb, the arc is easily read from the limb; but when it falls between two lines, note the degrees and half degrees up to the line on the right; then pass along the vernier till a line is found coinciding with a line of the limb: the number of this line from the 0 point, indicates the minutes which are to be added to the degrees and half degrees, for the entire angle.

On the vernier of the vertical limb, the 0 point is at the middle division line, and fifteen spaces lie on each side of it. The same relation, however, exists between the spaces of the vernier and those of the limb: the degrees and half degrees are read as before; and for the minutes, we have only to pass along the vernier, in the direction of the graduation of the

limb; and if we reach the extreme line, which is the fifteenth, without finding a coincidence, we must then pass to the other extremity of the vernier; and look along towards the 0 point, till two lines are found which coincide. The lines of this vernier are numbered both ways from the 0 point, and marked 5, 10, 15 to one extremity, and correspondingly from the other extremity 20, 25, 30 to the 0 point again.

The lower telescope being used merely as a guard, requires no adjustment, although it is better to make the axis, about which its vertical motions are performed, horizontal, or perpendicular to the axis of the instrument; and this is easily effected by means of the two small screws k and l, which work into the slide A', that is connected with the horizontal axis.

85. To measure a horizontal angle with the theodolite.

Place the axis of the instrument directly over the point at which the angle is to be measured. This is effected by means of a plumb, suspended from the plate which forms the upper and of the tripod.

Having made the limb truly level, place the 0 of the vernier at 0 or 360° of the limb, and fasten the clamp screw S of the vernier plate. Then, facing in the direction between the lines which subtend the angle to be measured, turn the limb with the outer spindle, until the telescope points to the object on the left, very nearly. Clamp the limb with the clamp screw K, and by means of the tangent screws L and Z, bring the intersection of the spider's lines to coincide exactly with the object.

Having loosened the clamp screw Q, of the lower telescope MN, direct it with the thumb screw P to the same object at which the upper telescope is directed; then tighten the clamp screw Q. . This being done, loosen the clamp screw S of the vernier plate, and with the thumb screws T and Z, direct the telescope to the other object: the arc passed over by the 0 point of the vernier, is the measure of the angle sought.

The lower telescope having been made fast to the limb, will indicate any change of its position, should any have taken place; and, as the accuracy of the measurements depends on the fixedness of the limb, the lower telescope ought to be often

examined, and if its position has been altered, the limb must be brought back to its place by the tangent screw L.

It is not necessary to place the 0 point of the vernier at the 0 point of the limb, previously to commencing the measurement of the angle, but convenient merely; for, whatever be the position of this point on the limb, it is evident that the arc which it passes over is the true measure of the horizontal angle. If, therefore, its place be carefully noted for the first direction, and also for the second, the difference of these two readings will be the true angle, unless the vernier shall have passed the 0 point of the limb, when the greater must be subtracted from 360°, and the remainder added to the less.

86. To measure a vertical angle.

The first thing to be done, is to ascertain the point of the vertical limb at which the 0 point of the vernier stands, when the line of collimation of the upper telescope, together with its attached level, is truly horizontal.

If the instrument be accurately constructed, and the parts shall not have been disarranged, this point is the 0 point of the limb. This, however, is easily ascertained by turning the limb till the 0's correspond, and then examining if the upper level. be truly horizontal. If not, direct the telescope to a distant and elevated object, and read the degrees on the vertical limb. Turn the vernier plate 180°, reverse the telescope, direct it a second time to the same point, and read the arc on the vertical limb. The half difference of these two readings, counted from the 0 point of the limb, in the direction of the greater arc read, gives the 0 point of the vertical limb; that is, the point at which the 0 of the vernier stands when the line of collimation is horizontal. This arc is called the correction, and is named minus, when estimated towards the eye-glass, and plus, when estimated in the contrary direction.

These preparatory steps being taken, let the axis of the telescope be directed to any point either above or below the plane of the limb, and read the arc indicated by the 0 of the vernier. If the angle be one of elevation, the correction, when plus, must be added to the arc read on the limb; but if the correction be minus, the difference of the arcs must be taken.

When the angle is one of depression, the correction when minus must be added, and when plus-the difference between it and the arc read, must be taken. These methods afford the true angles of elevation and depression, and are too obvious to require farther explanation.

87. The preliminary principles being explained, it remains to illustrate the application of trigonometry to the determination of heights and distances.

PROBLEM I.

88. To ascertain the horizontal distance from a point which is inaccessible by reason of an intervening river.

Let C (Pl. I. Fig. 8) be the given point. Measure a horizontal base line AB, such that its extremities, A and B, and the point C, shall not be in the same right line; and also, so that the point C can be seen from the two points A and B: then measure the horizontal angles, CAB and CBA.

Suppose AB=600 yards, CAB=57° 35′ and CBA=64° 51′. The angle $C=180^{\circ}-(A+B)=57^{\circ}$ 34′.

As sin. C, 57° 34′ To AB, 600 So is sin. A, 57° 35′	2.778151	As sin. C, 57° 34′ To AB, 600 So is sin. B, 64° 51′	9.926351 2.778151 9.956744
To BC, 600.11	2.778231	To AC, 643.49	2.808544

PROBLEM II.

89. To find the altitude of an inaccessible object, estimated from a horizontal plane passing through a given point.

FIRST METHOD.

Let D (Pl. I. Fig. 9) be the inaccessible object, on the top of a hill or tower, and B the point below, through which the horizontal plane is passed; it is required to find the perpendicular DC let fall on the horizontal plane passing through the point B.

Measure any horizontal line for a base, as BA; and the horizontal angles CAB and CBA, as also the angle of elevation DBC. Calculate the horizontal distance BC, then in

the right angled triangle CBD, there will be known CB and the angle CBD, from which the perpendicular CD may be found (46).

In measuring altitudes and depressions, the height of the limb of the instrument must not be neglected, provided we wish to estimate accurately from the surface of the ground.

Let AB = 780, $CAB = 56^{\circ} 28'$, $CBA = 61^{\circ} 24'$ and DBC =10° 43′. Angle ACB= 180° - $(56^{\circ}28+61^{\circ}24')=62^{\circ}08'$. As sin. ACB 62° 08′ 9.946471 | As radius 10.000000 To AB, 780 2.892095 To BC, 735.466 2.866563 So is tang. DBC So is sin. CAB 56° 28' 9.920939 10° 43' 9.277043 2.866563 To DC, 139.19 To CB, 735.466 2.143606

The angle of elevation may also be measured at the station A, and the altitude calculated, from the horizontal plane passing through that point: a comparison of these altitudes will show the elevation of one extremity of the base line above the other.

SECOND METHOD.

90. Let C (Pl. I. Figs. 10 and 11) be the point in which a perpendicular through the object D, meets the horizontal plane through B. At B measure the angle of elevation DBC. Then having placed a staff at B, and marked on it the exact height of the instrument, measure towards the object any convenient horizontal distance, to a point A, in the direction of the intersection of a vertical plane DBC with the ground. In measuring this line, great care must be taken to keep the chain horizontal; and then it is plain that the sum of the horizontal distances will be equal to the horizontal distance BE, in Fig. 10, or to AE in Fig. 11.

There are three cases:

- 1. When the point A is above the horizontal plane passing through B.
- 2. When the point A is below the horizontal plane passing through B; and,
 - 3. When it is a point of the plane.

CASE I.

91. In the first case, let BA (Fig. 10) represent the oblique line passing through A and the mark left on the staff at B; BE is equal to the horizontal distance measured (72). Place the theodolite at A, and measure the angle of elevation FAD, as also the angle of depression BAF; from these data, together with those before found, the vertical distances, DC and DF, can be determined.

Suppose the $\angle DBC = 38^{\circ}$, the horizontal distance BE=600 yards, the $\angle DAF = 46^{\circ}$ and the $\angle BAF = ABE = 27^{\circ} 30^{\circ} 25^{\circ}$.

In the triangle ABE,	to find	In the triangle A	BD to find
$AB. 90^{\circ}-EBA=EA$	$B=62^{\circ}$	AD.	
29′ 35″.		As sin. ∠ADB, 8°	9.143555
As sin. ∠EAB, 62°		To AB, 676.47	2.830250
29 ° 35 ° 9. 9	947901	So sin. ∠ABD, 10°	
To BE, 600 2.3	778151	29′ 35″	9.260349
So is radius 10.			0.0.170.44
		To AD, 885.20	2.947044
To BA, 676.47 2.8	30250		
To find AE.		In the triangle FA	D, to find
As sin. \angle EAB, 62°		DF.	
29′ 35″ 9.9	47901	As radius 1	0.000000
To BE, 600 2.7	78151	Is to AD, 885.20	2.947044
So is sin. EBA,		So is sin. A, 46°	9.856934
· 27° 30′ 25″ 9.6	64507		
T 4T 910 49		To DF, 636.76	2.803978
To AE, 312.43 2.4	94757		
$180^{\circ} - DAF = DAF' = 1$	34°.	To DF= 636.76	
DAF' + BAF' =		Add AE = 312.43	
$DAB = 161^{\circ}$	30′ 2 5″		
But DBC-ABE		Gives $CD = 949.19$	
$=DBA=10^{\circ}$	29′ 35″		
, DAD.			
Hence DAB+			
	00′ 00′′		
Therefore ADB=8°			

CASE II.

92. Let BA (Fig. 11) represent the oblique line passing through the mark left on the staff at B, and the second station A; and EA the horizontal distance between the points B and A, equal to 600 yards. Suppose the $\angle CBD = 38^{\circ} \angle FAD = 46^{\circ}$, and the angle of elevation $EAB = 27^{\circ} 30^{\circ} 25^{\circ}$.

From these data, the perpendicular CD is found to be equal 2869. 19 yards.

CASE III.

- 93. In the third case, the angle ADB is equal to the difference between the angles of elevation at the stations B and A, and the vertical line CD is found, as in the other cases.
- 94. If the ground between B and A inclines regularly, so that the oblique line can be measured with the chain, the calculation will be shortened by measuring this line, instead of the horizontal distance. But if the ground be broken and undulating, this cannot be done, and in such case the horizontal distance must be used.

PROBLEM III.

To find the perpendicular distance of an object below a given horizontal plane.

95. From any point of the plane measure a base line, and at its extremities, the horizontal angles included between it and the lines drawn to the given object; and also the angle of depression at that extremity of the base which is in the given plane. Then calculate the horizontal distance between this extremity and the given object; there will then be known the base and angle at the base of a right angled triangle, the perpendicular of which is the distance sought.

By measuring the angle of depression at the other extremity of the base, and calculating the perpendicular distance of the object below this point, we obtain, by a comparison of the distances, the elevation of one extremity of the base above the other. Let C (Pl. I. Fig. 12) be the given object, AB the base line, equal 672 yards, the horizontal angle ABC=39°20′, the horizontal angle BAC=72°29′, the angle of depression CAC′=27°49′, and the angle of depression CBC″=19 10′: CC′ is the vertical line drawn from the object C, and meeting the horizontal line AC′ at C′: CC″ is perpendicular to the horizontal line BC″.

The horizontal angle $ACB=180^{\circ}-(A+B)=180^{\circ}-111^{\circ}49^{\circ}=68^{\circ}-11'$.

To find AC'.		To find BC".	
As sin. C, 68° 11'	9.967725	As sin. C, 68° 11'	9.967725
To AB, 672	2.827369	To AB, 672	2.827369
So is sin. B, 39° 20	9.801973	So is sin. A, 72° 29'	9.979380
To AC', 458.792	2.661617	То ВС", 690.277	2.839024
To find CC'.		To find CC".	
As radius	10.000000	As radius	10.000000
Is to AC', 458.792	2.661617	ls to BC", 690.277	2.839024
So is tang. C'AC,		So is tang. C"BC,	
27° 49′	9.722315	19° 10′	9.541061
To CC', 242.065	2.383932	To CC", 239.93	2.380085
Hence, $\cdot CC' - C$	C'' = 242.06	5 - 239.93 = 2.135	yards—the
		${f A}$ and ${f B}$ above the ${f c}$	

We might also, as in the second method of the last problem, if the ground admitted of it, measure the base line directly towards or directly from the object, and then measure the angle of depression at each station: these data would be sufficient, from which to calculate the vertical distance.

96. In measuring a base line, if great accuracy be required, the theodolite should be placed at one extremity, and directed to the other; and the alignment of the staves made, by means of the vertical spider's line of the upper telescope. If the highest degree of accuracy be necessary, the base line should be measured with rods, which admit of being adjusted to a horizontal position by spirit levels.

EXAMPLES.

Example 1.—Wanting to know the distance between two inaccessible objects, which lie in a direct line from the bottom of a tower of 120 feet in height, the angles of depression are measured, and found to be, of the nearest, 57°; of the most remote, 25°30°. Required the distance between them. Ans. 173.656 feet.

Example 2.—In order to find the distance between two trees, A and B, which could not be directly measured because of a pool, which occupied the intermediate space, the distances of a third object C from each of them were measured, viz. CA=588, CB=672, and also, the contained angle ACB=55° 40. Required the distance AB. Ans. 593.8.

Example 3.—Being on a horizontal plane, and wanting to ascertain the height of a tower, standing on the top of an inaccessible hill, there were measured the angle of elevation of the top of the hill 40°, and of the top of the tower 51°; then measuring in a direct line 180 feet farther from the hill, the angle of elevation of the top of the tower was 33° 45′. Required the height of the tower. Ans. 83.9983 feet.

Example 4.—Wanting to know the horizontal distance between two inaccessible objects E and W, I measured a horizontal base line AB, of 536 yards, and at the extremities A and B, the horizontal angles BAW=40° 16′, WAE=57° 40′, ABE=42° 22′, EBW=71° 7′. Required the distance EW. Ans. 939.52 yards.

Example 5.—Wanting to know the horizontal distance between two inaccessible objects A and B, and not finding any station from which both of them could be seen, two points, C and D, were chosen, at a distance from each other equal to 200 yards, from the former of which A could be seen, and from the latter, B, and at each of the points C and D a staff was set up. From C a distance CF was measured, not in the direction of DC, equal to 200, and from D, a distance DE=200, and the following angles taken, viz.: AFC=83°, ACF=54° 31', ACD=53° 30', BDC=156° 25', BDE=54° 30', and BED=88° 30'. Required AB. Ans. 345.5.

Example 6.—From a station P there can be seen three ob-

jects, A, B, and C, whose distances from each other are known, viz. AB=800, AC=600, and BC=400 yards. Now there are measured the horizontal angles APC=33° 45′, BPC=22′ 30′. It is required, from these data, to determine the three distances PA, PC, and PB. Ans PA=709.33, PC=1042.66, PB=934 yards.

OF MEASUREMENTS WITH THE TAPE OR CHAIN ONLY.

97. As it may often happen, that instruments for the measurement of angles cannot easily be obtained, it seems not to be out of place to explain the best methods of determining distances by means of the chain, or tape only.

PROBLEM.

98. To trace, on the ground, the direction of a right line, that shall be perpendicular, at a given point, to a given right line.

Let AB (Pl. I. Fig. 13) be the direction of the given line, and D the given point.

FIRST METHOD.

Measure from D, on the line AB, two equal distances DA, DB, lying on different sides of the point D. Take a portion of the chain, or tape, greater than AB; mark the middle point of it, and fasten its extremities at A and B. Then, taking the chain by the middle point, stretch it tightly on either side of AB, and place a staff at C, or E. AB and EC are then at right angles to each other (55)*.

SECOND METHOD.

99. From the point D, measure the distance DB, equal to 8; with the point B as a centre, and a radius equal to 10, mark on the ground the arc PI: then with D as a centre, and a radius equal to 6, mark in like manner the arc cutting it; the line DC is at right angles to AB (186).

Remark. Any three lines, having the ratio of 6, 8, and 10, form a right angled triangle, of which the side 10 is the hypothenuse.

THIRD METHOD.

100. Take any distance, on the tape or chain, place one extremity at D, (Fig. 14) and fasten the other, on either side of AD, as at E. Plant a staff at E, take the extremity D of the chain, and carry it round, till it comes on the line DA at A. Place a staff at A, and carry the extremity D of the chain around, until it falls at F, on the line AE produced: then ADF is the right angle sought, being an angle in a semicircle (128)*.

PROBLEM.

101. To ascertain the horizontal distance from a given point to an inaccessible object.

FIRST METHOD.

Let A (Pl. I. Fig. 15) be an inaccessible object, and B the point from which the distance is to be estimated.

Measure directly from the object A, the horizontal line BE, of any convenient length; then lay off at E a right angle AED, and measure in the direction ED, any convenient distance to D. Place a staff at D; then, at the point B, lay off the right angle ABC, and measure along the line BC till a staff placed at C falls on the line DA. Now, DF being equal to DE—CB, is known: Hence, by similar triangles, DF: FC:: DE: EA: in which proportion all the terms are known except the fourth, which may, therefore, be regarded as found; hence BA is known.

SECOND METHOD.

102. At the point B, (Fig. 18) lay off BE perpendicular to the line BA, and measure along it any convenient distance BE. At E lay off the right angle BED, and measure any distance in the direction ED. Having placed a staff at the extremity D, place a second one at C, on the line BE, and also on the line DA, and measure either the distance BC or CE. The triangles CDE and CAB being similar, we have CE: ED:: CB: AB, in which all the terms are known except the fourth, which may therefore be regarded as found.

THIRD METHOD.

103. Measure any horizontal base line, as BC (Fig. 16). Then, having placed staves at B and C, measure any convenient distances BD and CE, such, that the points D, B, and A, shall be in the same right line, as also, the points E, C, and A; then measure the diagonal lines DC and EB.

Now, in the triangle BEC, the three sides are known, therefore, the angle ECB can be found (62). In the triangle CDB, the three sides are also known, and the angle CBD may be determined (62). These angles being respectively subtracted from 180°, the two angles ACB and ABC become known; and hence, in the triangle ABC, we have two angles and the included side, to find the side BA.

PROBLEM.

104. To find the altitude of an object, when the distance to the vertical line passing through the top of it is known.

Let CD (Fig. 17) be the altitude required, and AC the known distance. From A, measure on the line AC, any convenient distance AB, and place a staff vertically at B. Then placing the eye at A, sight to the object D, and let the point, at which the line AD cuts the staff BE, be marked. Measure the distance BE on the staff; then say, As AB: BE:: AC: CD, then, CD becomes known.

If the line AC cannot be measured, on account of intervening objects, it may be ascertained by calculation, as in the last problem, and then, having found the horizontal distance, the vertical line is readily determined as before.

CHAPTER III.

OF THE CONTENT OF GROUND.

105. It being one of the objects of surveying to ascertain the content or area of given pieces of land, it is important to have a distinct idea of the manner in which this area is to be estimated; and then, we can understand clearly the methods to be pursued, to find the data necessary for the computation.

The surface of the ground, being in general so broken and uneven, as to render it impossible, without great trouble and expense, to ascertain its true content, the method of referring it to a horizontal plane has been generally adopted; and now, in estimating the content, we consider the bounding lines as horizontal, and the whole surface reduced to a horizontal plane.

This manner of estimating land being established, the sum of the areas of all the parts, into which a tract of land may be divided, is equal to the area, estimating it as an entire piece; which would not be the case, if the areas of the parts had reference to the actual surface, and the area of the whole were calculated from its bounding lines.

106. In surveying, there are two kinds of measurement, linear, and superficial; and each of them has its appropriate unit of measure. The unit of measure of a quantity is an ascertained magnitude of the same kind with the quantity measured: thus, for a line, the unit of measure is a line of a given length, a foot, a yard, a rod, &c.: and the length of a line is known, when we know its unit of measure, and the number of times which the line contains it. For superficies, or areas, the unit of measure is an area of known dimensions, and for convenience, the square whose sides are the unit of

linear measure, is generally used. If, therefore, the linear dimensions of ground be estimated in feet, yards, rods, or chains, the superficial measure will be easiest found in square feet, square yards, square rods, or square chains, and when so determined, the number expressing the area will be nothing else, than the number of times which the unit of superficial measure is contained in the land measured.

307. It has already been observed (81) that Gunter's chain of four rods, or 66 feet in length, and which is divided into 100 links, is the chain in general use among surveyors. We shall, therefore, take the length of this chain for the unit of linear measure, and consequently, the square, of which it is the side, for the unit of superficial measure: this unit is generally called a square chain.

108. An acre is a surface equal in extent to ten square chains, or equal to a rectangle, of which one of the sides is 10 chains in length, and the other, one.

A rood is one quarter of an acre.

A chain being four rods in length, it follows that a square chain contains 16 square rods; and therefore, an acre, or 10 square chains, contains 160 square rods, and a rood, 40. The square rods are sometimes called perches.

Land is generally computed in acres, roods, and perches.

109. The dimensions of a survey being taken in chains and links, or in chains and decimals of a chain, (81) it becomes necessary to show, how the area is to be found in acres, roods, and perches, or square rods.

Now, I square chain = 10,000 square links; and consequently, 10 square chains, or one acre, = 100,000 square links. If, therefore, there be a rectangle, the sides of which are links, the area is found in acres and decimals of an acre, by multiplying together the sides, which gives the number of square links; and then, dividing the product by 100,000, or, what is the same thing, pointing off five decimal places from the right hand. If the decimal part be then multiplied by 4, and the same number of places pointed off in the product, the figures on the left of the decimal point, will show the roods; and, if the decimal places of the last product be multiplied by 40, and five places

of figures pointed off from the right hand in the product, the result will indicate the perches and decimals of a perch.

If one of the dimensions be in links and the other in chains, the chains may be regarded as links, by multiplying them by 100, or annexing two ciphers; or, if the multiplication be made without annexing the ciphers, the product is reduced to acres and decimals of an acre, by pointing off three places of decimals in the product.

If both the dimensions be in chains, the product is reduced to acres by dividing by 10, or pointing off one decimal place. From all which, we conclude,

- 1. That, if links be multiplied by links, the product is reduced to acres by pointing off five decimal places from the right hand.
- 2. That, if chains be multiplied by links, the product is reduced to acres by pointing off three decimal places from the right hand.
- 3. That, if chains be multiplied by chains, the product is reduced to acres by pointing off one decimal place from the right hand.
- 110. As there are 16.5 feet in a rod, a square rod is equal to $16.5 \times 16.5 = 272.25$ square feet. If this number be multiplied by 160, we shall have $272.25 \times 160 = 43560.00$, equal to the number of square feet in an acre. As there are 9 square feet in a square yard, if the number 43560.00 be divided by 9, the quotient, 4840, is the number of square yards in an acre.

PROBLEM.

111. To find the area of a square or rectangular piece of ground.

Multiply the two sides together; the product is the required area (173)*.

Remark. If the sides be estimated in rods, their product will express the area in square rods or perches: then, dividing the product by 160, and the remainder again by 40, will give the area in acres, roods, and perches. If the sides be estimated in chains and links, the manner of reducing their product to acres has already been explained. If the sides are estimated

in feet, or yards, the remainder should be divided by the number of square feet, or square yards in an acre, then, the remainder by the number of square feet or square yards in a rood, and the remainder again by the number of square feet or square yards in a perch.

As precisely the same remarks are applicable to all future examples, they need not be repeated.

PROBLEM.

- 112. To find the area of a triangular piece of ground.
- 1. If the base and perpendicular are known, multiply them together, and divide the product by 2, the quotient is the area of the triangle. (176)*.
- 2. If two sides and the included angle are known, add together the logarithms of the sides, and the logarithmic sine of the contained angle; from this sum subtract 10, which is the logarithm of the radius, and the remainder will be the logarithm of double the area of the triangle. Find, from the tables, the number answering to this logarithm, and divide it by 2, the quotient is the required area.*

Example 1.—Let AB=57.65 chains, AC=125.81 chains, and the angle CAB=57°25', and 2Q=twice the required area.

Then log.
$$2Q = \begin{cases} +\log. AB = \log. 57.65 & -1.760799 \\ +\log. AC = \log. 125.81 & -2.099715 \\ +\log. Sin. A = \log. Sin. 57^{\circ}25' 9.925626 \\ -\log. R & -10 \end{cases}$$

* Let ABC (Pl. I. Fig. 4) be the triangle, having the sides AB, AC, and the contained angle BAC given.

Let BD be drawn perpendicular to the base AC, and Q put equal to the area of the triangle.

Then R: AB:: Sin. A: BD (43); or BD=
$$\frac{AB \times Sin. A}{R}$$
.

But, $Q = \frac{AC \times BD}{2}$ (176)*.; hence by substituting for BD its value, $Q = \frac{AC \times AB \times Sin. A}{2R}$, or $2Q = \frac{AC \times AB \times Sin. A}{R}$.

Taking the logarithms, log. 2Q=log. AC+log. AB+log. Sin. A-log. R. which proves the rule given.

And 2Q=6111.4 square chains, or Q, the area of the triangle, equal to 3055.7 square chains, equal to 305 acres, 2 roods, and 11.2 perches.

Example 2.—What is the area of a triangle whose sides are 30 and 40, and their contained angle 28° 57'? Ans. 290.4276.

Example 3.—What is the number of square yards contained in a triangle, of which the sides are 25 and 21.25 feet, and the included angle 45°? Ans. 20.8694.

3. If the three sides are known, add them together and take half their sum; from this half sum subtract each of the sides severally; then multiply the half sum and the three remainders together; the product is the square of the area of the triangles: then extract the square root for the required area.*

Or, after having obtained the three remainders, add together the logarithm of the half sum and the logarithms of the respective remainders, and divide the sum by two: the quotient will be the logarithm of the area.

* Demonstration from Hutton's Mensuration.

Let ABC (pl. 1, fig. 19,) be the given triangle. Draw the parallels BD, AE meeting the two sides AC, and CB produced in the points D and E, and making CD=CB, and CE=CA. Also draw CFG bisecting DB and AE perpendicularly in F and G. Draw FHI parallel to AB, meeting CA in H, and AE produced, in I. Lastly, with the centre H, and radius HF, describe a circle, meeting AC produced in K: this circle will pass through I, because AI=FB=FD, hence HF=HI=½AB; and it will also pass through the point G, because CGA is a right angle.

Hence HA or HD is half the difference of the sides AC, CB; and HC=half their sum=\(\frac{1}{2}AC+\(\frac{1}{2}CB\); also KH=HI=\(\frac{1}{2}IF=\(\frac{1}{2}AB\); consequently, CK=\(\frac{1}{2}AC+\(\frac{1}{2}CB+\(\frac{1}{2}AB\)=half the sum of the sides of the triangle ABC, equal \(\frac{1}{2}S\), calling S the sum of those sides. Again HK=HI=\(\frac{1}{2}IF=\(\frac{1}{2}AB\), or KL=AB; therefore, CL=CK-KL=\(\frac{1}{2}S-AB\), and AK=CK-CA=\(\frac{1}{2}S-AC\), and AL=DK=CK-CB=\(\frac{1}{2}S-CB\).

Now $AG \times CG$ —the area of the triangle ACE, and $AG \times FG$ —ABE; therefore $AG \times CF$ —ACB. Also by the parallels AG : CG :: DF : CF, or AI : CF; therefore, $AG \times CF$ —triangle ABC— $CG \times AI$ — $CG \times DF$; consequently, $AG \times CF \times CG \times DF$ —the square of the area ABC.

But $CG \times CF = CK \times CL = \frac{1}{2}S \times (\frac{1}{2}S - AB)$; and $AG \times DF = AK \times AL = (\frac{1}{2}S - AC) \times (\frac{1}{2}S - BC)$, therefore, $AG \times CF \times CG \times DF = \frac{1}{2}S (\frac{1}{2}S - AB) \times (\frac{1}{2}S - AC) \times (\frac{1}{2}S - BC) = the square of the area of the triangle ABC.$

Example 1.—To find the area of a triangle whose three sides are 20, 30, and 40.

	,		
20	45	45	45 half sum.
30	20	30	40
40	-	-	
	25 1st rem.	15 2d rem.	5 3d rem.
2)90			

45 half sum.

Then $45 \times 25 \times 15 \times 5 = 84375$.

The square root of which is 290.4737, the required area.

Example 2.—How many acres are contained in the triangle whose sides are 2569, 4900, 5035 links? Ans. 61 acres, 2 roods, 8 perches.

PROBLEM.

113. To find the area of a piece of ground in the form of a trapezoid.

Multiply the half sum of the parallel sides by the perpendicular distance between them, the product is the required area. (178.*)

Example 1.—Required the area of the trapezoid, of which the parallel sides are, respectively, 30 and 49 rods, and their perpendicular distance 61.6.

Gives for the area in square rods 2433.20

Or 15 acres, 33.2 perches.

Example 2.—To find the area when the parallel sides are respectively 20 and 32 rods, and their perpendicular distance 26. Ans. 4 acres, 0 roods, and 36 perches.

PROBLEM.

114. To find the area of a quadrilateral.

Draw a diagonal dividing it into two triangles; find the areas of the triangles: the sum of these areas is the area required.

PROBLEM.

To measure long irregular figures having a right line for a base.

115. At the two extremities of the base, measure in perpendiculars to the base, the breadth of the figure. Then divide the base into any convenient number of equal parts, and measure the breadth of the figure at the points of division. Add together the intermediate perpendiculars and half the sum of the extreme ones, and multiply this sum by one of the equal parts of the base line; the product is the required area very nearly; or, multiply by the whole base, and divide the product by the number of equal parts.*

If it is not convenient to erect the perpendiculars at equal distances from each other, the areas of the trapezoids into which the whole figure will be divided, must be computed separately, and the sum taken.

Example 1.—The breadths of an irregular figure at five equidistant places, being 8.2, 7.4, 9.2, 10.2, 8.6, and the whole length 40, required the area.

* Let ABEeda (pl. 1, fig. 20.) be an irregular figure; AE its base, h, i, l, n, m, the perpendiculars drawn at equal distances from each other.

The area of the trapezoid ABba, is equal to
$$\frac{h+i}{2} \times AB$$

The area of the trapezoid BCcb= $\frac{i+1}{2} \times BC$

The area of CDdc= $\frac{1+n}{2} \times CD$

The area of DEed= $\frac{n+m}{2} \times DE$

The sum of these trapezoids, which is equal to the area of the figure, is equal to $\left(\frac{h+i}{2} + \frac{i+}{2} + \frac{l+n}{2} + \frac{n+m}{2}\right) \times AB$, since the divisions on AE are equal.

But this latter sum is evidently equal to $(\frac{h}{2} + \frac{m}{2} + i + l + n) \times AB$, hence the rule is manifest.

8.2	4)40(10 one equal part,
2) 16.8 sum of the extremes	35.2 sum 10
8.4 mean of the extremes 7.4 9.2	352 the area.
35.2 sum.	

Example 2.—The length of an irregular figure being 84, and the breadths, at six equidistant places, 17.4, 20.6, 14.2, 16.5, 20.1, 24.4 rods; required the area. Ans.—9 acres, 2 roods, 30.64 perches.

PROBLEM.

116. To find the area of a circle.

Square the radius and multiply the number so obtained by 3.1416, the product is the required area. (291.*)

PROBLEM.

117. To find the area of an ellipsis.

Multiply the axes together, and their product by .7854, the last product will be the area of the ellipsis.

Example. Required the area of an ellipsis, whose two axes are 70 and 50 poles. Ans.—17 acres, 28.9 perches.

118. With respect to the content of land, it may be remarked, that irregular pieces must, in general, be divided into triangles, rectangles, parallelograms, or trapezoids. The manner of making such divisions, depends on the lines and angles which are known. They should always, however, be so made as to simplify the calculations, and so that a sufficient number of known parts may fall into each figure, to determine its area.

CHAPTER IV.

OF THE INSTRUMENTS USED IN SURVEYING.

119. The measurements which are necessary on the field, and which furnish the data for the computation of the area of ground, are generally made with the theodolite and chain, the surveying cross, the plain table, and the compass. The uses of the theodolite and chain have already been explained, the remaining instruments are now to be described.

We shall also describe, in this chapter, the drawing instruments used for plotting a survey: they are, besides the dividers and common rule, the semicircular protractor, the circular protractor, the scale of chords, the diagonal scale of equal parts, the sectoral scale of equal parts, and Gunter's scale.

OF THE SURVEYING CROSS.

120. This instrument consists of two bars, AB and CD, (Pl. 4, Fig. 1,) permanently fixed at right angles to each other, and firmly attached at E to a pointed staff, which serves as a support. Four sights are screwed firmly to the bars by means of the screws a, b, c, and d. As the only use of this instrument is to lay off right angles, it is of the first importance that the lines of sight be truly at right angles. This can easily be ascertained: for, let the bar AB be turned until its sights mark some distinct object; then look through the other sights and place a staff on the line which they indicate: let the cross then be turned until the sights of the bar AB come to the same line: if the other sights are directed to the first object, the lines of sight are exactly at right angles.

The sights being at right angles, one of them being turned in the direction of a given line, the other will mark the direc-

. tion of a line perpendicular to it, at the point where the instrument is placed.

OF THE PLAIN TABLE.

121. This instrument consists of two parts, a rectangular board CDBA, (Pl. 3, Fig. 1,) and a tripod EHG, to which it is firmly screwed.

Directly under the rectangular board are four milled screws that pass through sockets inserted in a horizontal brass plate, and which are worked against a second horizontal plate, for the purpose of levelling the table: the table having a ball and socket motion, similar to the limb of the theodolite.

For the purpose of levelling the table, a small detached spirit level is used. This level being placed over the centre, and also over two of the levelling screws, the screws are turned contrariwise until the level is horizontal; after which, it is placed over the other two screws, and made horizontal in the same manner.

Between the upper horizontal plate and the table there is a clamp screw, similar to the clamp screw of the theodolite, which being loosened, the table can be revolved freely about its axis. There is, also, a small tangent screw, by which the smaller motions of the table are regulated after the clamp screw is made fast. Neither of these screws can be seen in the figure.

The upper side of the table is bordered by four brass plates, about one inch in width, and the centre of the table is marked by a small pin, F. If around this centre a circumscribing circle be described, its circumference, divided into degrees and parts of a degree, and radii drawn through the points of division, the points where such radii would intersect the outer edge of the brass border are marked by lines on the brass plates, and the degrees are numbered in the direction from left to right, from the point L to the point I, 180°, and from the point I to the point L, 180°. In some Plain Tables, however, they are numbered from 0 to 360°.

There are, generally, diagonal scales of equal parts cut on the plates DLC and AIB, the manner of using which will be explained hereafter. Near the other two edges of the table. two small grooves are made, into which the plates of brass DB and CA are fitted, and these plates are drawn to their places by means of milled screws which pass through the table from the under side, and screw firmly into the plates. The heads of two of the screws, Q and S, are seen in the figure, as also, one of the plates and its two screws in Fig. 3. object of these plates is to confine a sheet of paper on the By loosening the screws, and pressing them upwards. the plates are raised above the surface of the table; the edges of the paper can then be placed under them: then, by turning the screws back again the plates are drawn down and the paper held tightly. Fig. I represents the table with the paper partly put upon it: one edge of the paper has been placed under the plate DB, and the screws, S and Q, tighten-The paper, before being put on, should be moistened, in order to expand it, and, after it has been dried, it will fit closely to the table.

A ruler, AB, (Fig. 2) with open vertical sights, is used with the plain table. This ruler has a fiducial edge, which is in the same vertical plane with the hairs of the sights. A ruler with a telescope, and a vertical limb, similar to the vertical limb of the theodolite, is also sometimes used with the plain table.

A magnetic needle and compass are sometimes attached to the plain table, either by screws, or by fixing it directly under its centre, to show the direction of the lines.

The plain table is used for two distinct objects.

1st. For the measurement of horizontal angles.

2dly. For the determination of the shorter lines of a survey, both in extent and position.

122. To measure horizontal angles.—Place, by means of a plumb, the centre of the table directly over the angular point: then level the table; after which, place the fiducial edge of the ruler against the small pin at the centre, direct it to one of the objects and note the degrees on the brass plate; then turn the ruler and sights to the other object and note the degrees as before. If the ruler has not passed over the 0 point, the difference of the readings is the angle sought; but,

if it has, the larger taken from 180°, and the remainder added to the smaller gives the required angle.

123. Of the determination of lines in extent and position.— Having placed a paper on the table, examine the objects and lines, whose positions and lengths are to be determined, and measure a base line in such a direction, if possible, that all the objects can be seen from its extremities. Then place the plain table with its centre, nearly, though not accurately, over one extremity of the base; make it truly horizontal, and turn it until the larger part of the paper lies on the same side of the base with the objects.

Then, tighten the clamp screw, and mark with a pin the point of the paper directly over the station, which point is determined most accurately by suspending a plumb from the lower side of the table. Place the fiducial edge of the ruler AB, against the pin, it being held firmly, sight to the other extremity of the base line, and mark with the pin or pencil the direction of the ruler on the paper. Sight in like manner to every other object, and draw on the paper the corresponding lines, numbering them from the base line, 1, 2, 3, 4, &c.

Then, with a pair of dividers, take from the scale, a certain number of equal parts to represent the base, and lay off the distance on the base line from the place of the pin. Take up the table, carry it to the other extremity of the base, and place the point of the paper corresponding to that extremity. directly over it. Place the fiducial edge of the ruler on the base line, and turn the table, by means of the tangent screw, until the sights are directed to the first station. If, however, in bringing the table to this position, the corresponding point of the paper has been moved from over the extremity of the base line, move the legs of the tripod until it is brought back to its place. Let the table then be levelled, after which, place the ruler again on the base line, and bring the table to its proper position by the tangent screw, and so continue the adjustment until the extremity of the base line on the paper is directly over the station, and in the same vertical plane with the base line on the ground, and the table truly horizontal. Then direct the sights to all the objects sighted to

trom the other station, and mark the lines 1, 2, 3, 4, &c. from the base line as before. The intersections of the corresponding lines 1,1, 2,2, 3,3, 4,4, &c. determine on the paper the positions of the several objects; and a reference of these lines to the scale of equal parts, determine the actual distances.

124. Of changing the paper.—When one paper is filled, and there is yet more work to be done, let the paper be removed and a second paper put on the table; after which, the table may be used as before.

Now, in order that the two papers may be put together and form one entire plan, it is necessary that, two points, determined on the first paper, be also determined on the second; and then, by placing the lines joining these points upon each other, all the lines on the two papers will have the same relative position as the corresponding lines on the ground; and the same for as many papers as it may be necessary to use. If different scales are used, the corresponding points will not join, and then the work must be reduced to the same scale, before the papers can be put together.

OF THE CIRCUMFERENTER, OR SURVEYING COMPASS.

125. This instrument consists of a compass box DCE, (Pl. 4, Fig. 2,) a magnetic needle, a brass plate, AB, from twelve to fourteen inches long, two plain sights, AF, BG, and a stand, which is sometimes a tripod, and sometimes a single staff pointed with iron at the lower end, so that it may be planted firmly in the ground.

The open sights, AF, BG, are placed at right angles to the plate AB, and fastened to it by the screws a and b. In each sight, there is a large and small aperture, or slit; the larger aperture being above the smaller in one of the sights, and below it in the other. A hair, or thread of silk, is fastened vertically in the middle line of the large apertures. Fig. 3, on a larger scale, shows one of these sights.

The compass box, DCE, is circular, and generally about six inches in diameter. At the centre is a small pin, on which the magnetic needle is poised, This needle, if allowed to turn freely around the point of suspension, will settle to a state

of rest: the direction which it assumes, is called the magnetic meridian.

In the interior of the compass box, there is a graduated circle divided to degrees, and sometimes to half degrees; the degrees are usually numbered from the two extremities of the diameter NS, which is in the same plane with the hairs of the vertical sights, both ways, to 90°.

The length of the magnetic needle is a little less than the diameter of the graduated circle, so that the needle can move freely around its centre, within the circle, and its positions be noted on the graduated arc.

In using the compass, it is important to ascertain the exact angle, included between the magnetic meridian and the direction which may be given to the sights AF and BG, by turning the compass around on the stand.

For this end, a small arc, HI, is described on the bar AB, having its centre at the centre of the compass box. This arc is divided to degrees, and sometimes even to the parts of a degree, and a vernier is permanently attached to the compass box. When the 0 point of the vernier coincides with the 0 point of the graduated arc HI, the line of the compass box, marked NS, or the diameter from whose vertices the degrees of the graduated circle are numbered, is in the same vertical plane with the hairs of the sights.

The compass box is turned about its centre, without moving the plate AB, by the milled screw L; it is fastened to the plate AB, by the screw P.

Now, the 0 of the vernier coinciding with the 0 of the arc HI, if the needle does not stand at one of the lines of division of the graduated circle, let the whole degrees be read; then turn the compass box, by means of the screw L, until the needle points exactly to the line which marked the whole degrees, the space passed over by the 0 of the vernier indicates the minutes that are to be added.

Compasses are often constructed, not only for the purpose of ascertaining the angles which lines form with the magnetic meridian, but also, for the accurate measurement of horizontal angles. In such instruments, the horizontal plate AB is

made shorter, a vernier is attached to it, and it is mounted on a graduated circle, similar to the horizontal limb of the theodolite. This limb must always be made horizontal before measuring horizontal angles.

OF INSTRUMENTS FOR PLOTTING.

126. A plot or plan of a piece of ground is the accurate delineation, on paper, of its bounding or other principal lines—or such a representation of it, that all the lines and angles drawn on the paper have the same mutual relation as their corresponding lines and angles on the ground. In making such representations certain drawing instruments are used, some of which are now to be described.

The use of the common compasses, or dividers, as well as that of the plain rule, is too obvious to need particular explanation.

OF THE SEMICIRCULAR PROTRACTOR.

127. This instrument is used to lay down, or protract angles, and also to measure the angles included, by lines given in position, upon paper.

It is a brass semicircle ACB, (Pl. 5, Fig. 1,) divided to half degrees; the degrees are numbered to 180, both ways, from A and B. There is a small notch at the middle of the diameter AB, to show the centre of the protractor.

128. To lay off, with the protractor, any angle, at a given point of a right line.—Place the diameter AB on the line, so that the centre shall fall on the given point, then count the degrees contained in the given angle, from A towards B, or from B towards A, and mark the extremity of the arc with a pin; remove the protractor, and draw a line through the point so marked, and the given point: this line makes with the given line the required angle.

OF THE CIRCULAR PROTRACTOR.

129. This instrument consists of a brass circular limb, (Pl. 5, Fig. 2,) of about six inches diameter, with a moveable index AB, having a vernier at the extremity A, and a milled

screw at the other extremity B, with a concealed cog-wheel that works with the cogs of the limb, and thus moves the index AB, about the centre of the protractor. At the centre of the protractor, is a small circular glass plate, on which two lines are cut; the point of their intersection, is the exact centre of the instrument. The limb is generally divided to half degrees; the degrees are numbered from 0 to 360.

At the 0 point, and at the opposite extremity of the diameter passing through that point, are small lines on the inner edge of the limb; the two extremities of the diameter, perpendicular to this latter, are also designated in the same way.

Two angular pieces of brass, each having a small and sharp steel pin at its extremity, are fastened to the index, and revolve freely around the lines ab and cd. The small screws a, b, c, and d, move them in the directions of the lines ab, cd, for the purpose of bringing the steel pins exactly into the line which passes through the 0 of the index, and the centre of the protractor.

The vernier is generally divided into 30 parts, by means of which accurate readings can be made to 1'.

130. To lay off an angle with this protractor.—Let its centre be placed over the angular point, and the diameter passing through 0 and 180° on the given line: turn the screw that works the index until the 0 of the vernier coincides with the division corresponding to the given angle; then let the angular brass pieces be turned down; the points dotted by the steel pins will show the direction of the line making the required angle with the given line.

If this line does not pass through the angular point, the pins are out of place, as they ought to be in the line passing through the centre and the 0 of the vernier, in which case they must be adjusted by the screws a, b, c, and d.

OF THE SCALE OF CHORDS.

131. If a circle be described with any radius, and a diameter be drawn, and from either of its extremities arcs of 1, 2, 3, 4, 5, &c. to 90° be laid off, and the corresponding chords drawn; then, if the lengths of these chords be laid

down accurately on a scale, such scale is called a Scale of Chords.

The scale of chords being once constructed, the radius of the circle, from which the chords were obtained, is known, for the chord marked 60 is always equal to the radius of the circle. A scale of chords is generally laid down on the sectors which belong to cases of mathematical instruments, and marked Cho.

132. To lay off an angle with the scale of chords.—Take a radius equal to the chord marked 60, and with the angular point for a centre describe an arc of a circle; then, take from the scale, the chord of the given arc, and apply it from the point where the arc before described intersects the given line; the line drawn through the extremity of the chord and the angular point, makes, with the given line, the required angle.

OF SCALES OF EQUAL PARTS.

133. A scale of equal parts is one which shows any number of equal distances, or spaces. If a line of a given length, one inch for example, be divided into any number of equal parts, say thirty, such a scale is called a scale of thirty parts to an inch, and the same, whatever be the length of the line divided.

If a line, on the ground, of a given length, estimated in feet, yards, or rods, is to be laid down on paper, let a number of parts, equal to the number of feet, yards, or rods, in the given line, be taken from the scale, with a pair of dividers, and extended upon the paper.

If a number of lines be laid down after the same manner, their lengths on the paper will obviously have the same proportion as the lines on the ground, and if they be plotted with the further condition of making with each other the same angles as they formed on the ground, the plan on the paper will be, in every respect, similar to the figure which it represents.

If a line upon the paper, of one inch in length, represents any number of equal parts, say 20 feet, of a line on the ground,

the plan or plot is said to be made upon a scale of twenty feet to the inch: and similarly, whatever be the relation of the numbers that represent corresponding parts.

OF THE DIAGONAL SCALE.

This scale is thus constructed. Take a line, AD, (Pl. 5, Fig. 3,) equal in length to $\frac{1}{4}$, $\frac{1}{2}$, $\frac{3}{4}$, or 1 inch, or of any other convenient dimension, and describe on it the square ADCB. Divide the sides AD, AB, each into ten equal parts, join A and a, and draw the other nine parallels as in the figure. Produce DA, and lay off the distance AD any convenient number of times, from A to F, from F to G, from G to E, &c., and number the points of division 1, 2, 3, &c. Then divide the line DC into ten equal parts, and through the points of division draw parallels to ED, as in the figure. Now, the small divisions on the line AD are each one tenth (.1) of that line, and therefore .1 of AF, or FG. It follows from the proportion of similar triangles, that the part of the line .01, intercepted between the lines AB and Aa, is equal to .1 of Ba; the like intercepted part of the line .02, equal to .2 of Ba, the like intercepted part of .03, equal to .3 of Ba, and similarly for the other parallels.

These latter spaces, being tenths of the divisions A1, 12, &c. which are themselves tenths of AD, are hundredths of the line AB or AD.

Naming the line AD the unit of the scale, if it were required to take in the dividers the value of the unit and any number of tenths, let the dividers be placed at F, and extend to the figure between A and D, which designates the tenths. If two or more units were required, the dividers must be placed at that point on the line AE, which is designated by a number equal to the number of units. If units, tenths, and hundredths, are wanted, place the dividers at the intersection of the proper line of units with the line designating the hundredths, and then extend them to the intersection of the line designating the tenths with this line of hundredths: thus, for the number 2.44 the dividers are placed at b, and extended to d; for 3.58, they are placed at e, and extended to f.

If the line AD, instead of being regarded as a unit, be taken to represent ten, then, each of the divisions A1, 12, &c. will represent one, and the parts which were hundredths before, will now be tenths. If the line AD be taken to represent one hundred, the spaces A1, 12, 23, &c. will represent tens, and the tenths in the last case, units.

Diagonal scales are generally cut on two of the brass plates which border the plain table.

OF THE SECTORAL SCALE OF EQUAL PARTS.

134. The sector is an instrument generally made of ivory or brass. It consists of two arms, or sides, which open by turning round a joint at their common extremity. There are several scales laid down on the sector; those, however, which are chiefly used in plotting, are the scale of chords already described, and the scale of equal parts now to be explained.

On each arm of the sector, there is a diagonal line that passes through the point about which the arms turn; these lines are divided into equal parts. On the sectors which belong to the cases of English instruments, the lines are designated by the letter L, and numbered, from the centre of the sector, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, to the other extremity. On the sectors which belong to cases of French instruments, they are designated, "Les parties egales," and numbered, 10, 20, 30, &c. to 200. In the English sectors there are 20 divisions between the lines numbered 1, 2, 3, &c., so that there are 200 on the scale.

The advantage of the sectoral scale of equal parts, is this. When it is proposed to make a plan, of any given number of parts to the inch, or to the part of an inch, take the inch or part of the inch from the scale of inches on the sector; then open the sector, and place one foot of the dividers at the point designated by the number, and extend the sector till the other foot reaches to the corresponding number on the other arm; then lay the sector on the table without varying the angle. Now, regarding the lines on the sector as the sides of a triangle, of which the line measured across is the base, it is plain that, if any other line be similarly measured across the

sector, the angle of the sector remaining the same, the bases of the triangles so formed will be proportional to their sides: hence, the distances which are to represent lines on the plan, are to be measured across the sector, and from the numbers which represent the true lengths of the lines.

If a line be so long that the whole of it cannot be taken from the scale, it may be divided, and a part of it taken at a time. If a line be given on the paper, and it is required to ascertain the length of the line on the ground, to which it corresponds, we have only to take the line in the dividers, apply it to the scale, and see to how many parts it is equal. On the edges of the French sectors are scales of inches in English and French measure.

Example.—If a line of sixty-seven feet were to be plotted to a scale of twenty feet to the inch, take one inch from the scale of inches; then place one foot of the dividers at the twentieth division, and open the sector until the dividers will just reach the twentieth division on the other arm; the sector is then set to the proper angle: the required distance to be laid down on the paper, is found, by extending the dividers from the sixty-seventh division on one arm, to the sixty-seventh division on the other.

OF GUNTER'S SCALE.

135. This is a scale of two feet in length, on the faces of which a variety of scales are marked. The face on which the divisions of inches are made, contains, however, all the scales necessary for plotting. They are, the diagonal scale of equal parts, and the scale of chords, already explained.

CHAPTER V.

OF SURVEYING WITH THE COMPASS.

- 136. THE line about which the earth revolves, is called its axis.
- 137. Every plane passing through the axis, intersects the surface of the earth in a line, which is called a *meridian*.
- 138. Every point of the surface has a meridian line passing through it; since, through such point and the axis a plane may always be passed.
- 139. All these meridian lines intersect each other at the two points where the axis pierces the surface; but, as the part of the surface surveyed is so inconsiderable that the curvature of the earth is neglected, we may, without any sensible error, regard the meridians as right lines, and parallel to each other.
- 140. When the compass is placed on its stand, and the needle allowed to settle to a state of rest, the direction it assumes has been named the magnetic meridian (125). Although this line is different from the true meridian, as will be shown hereafter, yet, in the surveys made with the compass, we shall use the term, meridian, as synonymous with magnetic meridian, that is, to designate the direction of the magnetic needle.
- 141. If the right hand be turned towards the point where the sun rises, the direction pointed by the farthest end of the needle, is called *North*; the direction shown by the nearest end is called *South*; and the line thus indicated, is called a north and south line, as well as a meridian.
 - 142. The line perpendicular to the meridian, is called an

East and West line; the East point being on the right hand, and the West on the left.

- 143. In departing from any point, if the direction taken lies between the north and east lines, it is called north as many degrees east, as is equal to the angle which the line run, makes with the meridian of the point: thus, if it makes an angle of 30°, it is called north, 30° east, and written, N. 30° E. This angle is called the bearing or course, and the line run, the distance. If the course lies between the north and west lines, the bearing is called north west; if between the south and west, south west; if between the south and east, south east; the bearing, as before, being written between the letters which designate the direction of the lines.
- 144. If, after having passed over a line, the bearing be taken to the back station, this bearing is called the back sight, or, reverse bearing.
- 145. The perpendicular distance between the east and west lines passing through the extremities of a line, is called the *northing*, or *southing*, of that line, according as it was run, north or south: the term difference of latitude designates this perpendicular distance in either case.
- 146. The perpendicular distance between the meridians, passing through the extremities of a line, is called the *departure* of that line, and is east or west, according as the line lies on the east or west side of the meridian passing through the point of beginning.
- 147. The meridian distance of a point, is its distance from any assumed meridian. The meridian distance of a line, will be designated by the meridian distance of the middle point of that line.

OF THE TRAVERSE TABLE.

148. A table, called a *Traverse Table*, is used in computing the area of a survey made with the compass. Its use will be here explained.

This table shows the difference of latitude and departure, corresponding to any bearing; and for any distance less than

100, the one hundred being regarded as links, chains, rods, or any other dimension.

If (Pl. 6, Fig. 4) FG were a line measured, NFS the meridian, and SFG the bearing, or course; then FG' would be the southing, or difference of latitude, and GG' the departure east.

It is evident that the distance run, the difference of latitude, and the departure, are, respectively, the hypothenuse, the base, and the perpendicular, of a right angled triangle, of which, the course or bearing is the angle at the base.

If there be two bearings, which are complements of each other, or, of which the sum is 90°, the departure corresponding to the one, will be the latitude corresponding to the other.

For, if G'G were a meridian, and G'GF the bearing, instead of G'FG, then, GG' would be the difference of latitude, and FG' the departure.

In the table headed 'Traverse Table,' the figures at the top and bottom show the bearings, to degrees and parts of a degree; and the columns on the left and right of each page, the distances to which the latitudes and departures correspond.

If the bearing be less than 45°, the angle will be found at the top of the page, if greater at the bottom; then, if the distance be less than 50, it will be found in the columns ("distances") of the left hand page; if greater than 50, in the columns of the right hand page. The table is calculated only to quarter degrees, for the bearings cannot be accurately ascertained to smaller fractions of a degree.

149. For the same bearing, and lines of different lengths, it is evident, that the latitudes and departures will be proportional to the distances.

Therefore, when the distance is greater than 100, it may be divided by any number which will give a quotient less than 100; then, the latitude and departure of the quotient being multiplied by the divisor, the products are the latitude and departure of the whole course. It is also plain, that, for the same bearing, the latitude and departure of the sum of two

or more distances, is equal to the sum of the latitudes and departures of those distances respectively.

Hence, if we have any number greater than 100, as 614, we have only to regard the last figure as a cipher, and recollect, that, 610+4=614, and that the latitude and departure of 610 are ten times as great, respectively, as the latitude and departure of 61, that is, equal to the latitude and departure of 61, multiplied by 10, or, with the decimal point removed one place to the right.

Example 1.—To find the latitude and departure, the bearing being $29\frac{1}{4}$ °, and the distance 582.

Latitude for 580 Latitude for 5		Departure for 580 Departure for 5	283.40 2.44
Latitude for 585	510.36	Departure for 585	285.84

In this example, the latitude and departure answering to the course $29\frac{1}{4}$, and to the distance 58, were first taken from the table, and the decimal point moved one place to the right; then the latitude and departure answering to the same course, and the distance 5, were taken from the table and added.

Example 2.—To find the latitude and departure, the bearing being $62\frac{1}{2}$, and the distance 7855 chains.

Latitude 7800	3602.00	Departure 7800	6919.00
Latitude 55	25.40	Departure 55	48.79
Latitude 7855	3627.40	Departure 7855	6967.79

If the distances were expressed in whole numbers and decimals, the manner of finding the latitudes and departures would still be the same, except in pointing off the decimal places; which, however, is not difficult, when it is remembered that, the column of distances in the tables may be regarded as decimals by removing the decimal point to the left in the other columns.

159. The manner of surveying with the compass, is to go entirely around the land, measuring the bounding lines with the chain, and taking all their bearings with the compass.

In going round a piece of land, it is immaterial whether it be kept on the right hand or on the left; and all the rules deduced for one of the cases, are equally applicable to the other. To preserve, however, a uniformity in the language of the rules, we shall suppose it kept constantly on the left hand of the surveyor.

Let ABCD (Pl. 6, Fig. 1) be the plan of a piece of land to be surveyed, NS the north and south line; the lines parallel to it, are meridians, and those at right angles, east and west lines. Let the work be commenced at the station A. On a sheet of paper, rule three columns, as below, and head them, stations, bearings, and distances. At station A, designated by 1, in the column stations, take the bearing to station B, which is the angle BAb, N 23° E, and enter it in the column bearings, opposite 1; then measure the distance AB=5 ch. 40 l., which insert in the column distances. The station at B, is station 2, in the field notes, opposite which, are written the bearing FBC, N 84° W, and the distance BC equal to 6 ch. and 60 l.; and similarly for the other bearings and distances.

Stations.	Bearings.	Distances.
1	N 23° E	5.40
2	N 84° W	6.60
3	S 10° E	4.55
4	S 69½° E	3.74

160. In passing over the distance AB, the northing is Ab, and the departure, east, bB. For the distance BC, the northing is BF, and the departure, west, FC: Af, therefore, is equal to the sum of the northings. In passing over the

line CD, Cd is the southing, and Dd the departure east: for the line DA, Dh is the southing, and hA the departure, east: hence we conclude that, CG is equal to the sum of the southings, and equal also to Af, the sum of the northings.

If we consider also the departures, we see that bB, dD, and hA, are the departures east, and that their sum is equal to FC, the departure west; and as the same may be shown for any other figure, we conclude that, when any survey is correctly made, the sum of the northings is equal to the sum of the southings, and the sum of the eastings to the sum of the westings.

- 161. It would appear plain, even without demonstration, that, after having gone entirely round a piece of land, the distance passed over, in the direction due north, must be equal to the distance in the direction due south; and the distance in the direction due east, equal to the distance in the direction due west.
- 162. In computing the area of a survey, it becomes necessary to know double the meridian distance of the middle of each line, from a given meridian. This meridian may be taken at pleasure, though it is generally most convenient to use the one that passes through the most easterly or westerly station. The manner of calculating these double distances, which are called, the double meridian distances of the lines, is now to be explained.

Let all the departures in one direction, say west, be called *plus*; and the departures east, *minus*: then, through whatever station of the survey the assumed meridian be taken, we shall have this general method.

- 1. The double meridian distance of the first line is equal to its departure.
- 2. The double meridian distance of the second line is equal to the double meridian distance of the first line, plus its departure, plus the departure of the second line.
- 3. The double meridian distance of the third line, is equal to the double meridian distance of the second line, plus its departure, plus the departure of the third line.

4. And, the double meridian distance of any line, is equal to the double meridian distance of the preceding line, plus its departure, plus the departure of the line itself.

It ought, perhaps, to be remarked, that *plus* is here used in its algebraic sense; and that when the departures and double meridian distances are of *different names*, that is, one east and the other west, they have different algebraic signs, and are therefore to be subtracted.

Demonstration. Let FL (Fig. 1) be the assumed meridian. Let n be the middle point of the distance BC; np is the meridian distance of BC, and 2 np is double the meridian distance of BC, and is plus. But BC is bisected at n, hence, np, equal to qF, is half of FC; hence the departure of the first line, is equal to the double of its meridian distance.

Now, to 2np add 2Cq, equal to the departure FC; the sum is 2FC, and plus; to this sum add 2om, equal to the departure dD; this, being east, is minus, and the sum is 2ma, and plus.

To 2ma, add 2mi, or dD, which being minus, the sum is 2Dv, to which add hA, or 2ts, the sum is 2sc.

To 2sc add hA or 2rA; the sum is 2Aw; to this add Aw or 2IP, the sum is 2PL. As the same may be shown for any meridian, and every figure, we may regard the demonstration as general.

163. Those lines, the middle points of which, lie on the east side of the assumed meridian, are said to have eastern meridian distances, and those, whose middle points lie on the west of it, to have western meridian distances.

THEOREM.

164. Double the area of a piece of land, is equal to the difference between the sum of the products that arise from multiplying the double of each western meridian distance by its corresponding northing, and the double of each eastern meridian distance by its corresponding southing; and the sum of the products that arise from multiplying the double of each eastern meridian distance into its corresponding northing, and the double of each western meridian distance by its corresponding southing.

CASE I.

When the assumed meridian passes entirely without the land.

Let ABCD (Pl. 6, Fig. 2) represent a quadrangular piece of ground, NS the assumed meridian, from which the double distances are estimated; EF, IH, N'L, and PQ, the meridian distances of the lines AB, BC, CD, and DA respectively. These meridian distances are all east. Let $N \times W + S \times E$, designate the first set of products, that is, the products which arise from multiplying the northings by double the western meridian distances, and the southings by double the second set of products, or those which arise from multiplying the northings by double the eastern meridian distances, and the southings by double the western meridian distances, and the southings by double the western meridian distances.

 $N \times W + S \times E$

 $N \times E + S \times W$

2EF × AG=2 area AGB 2QP × AN=2 area ADN Sum=2AGB+2ADN 2HI × KG=2 area GBCK 2LN' × KN=2 area KCDN Sum=2 area GBCDN

The difference of these sums is twice the area of the figure ABCD.

The line AB runs south, and its meridian distance is east; therefore the product 2FE × AG belongs in the first column.

In a similar manner it might be shown that the other products are correctly placed. The product $2FE \times AG$ is double the area of the triangle AGB, since 2EF=GB; and the product $2IH \times GK$ is double the area of the trapezoid GBCK. (178.*)

CASE II.

When the meridian passes through the land.

165. Let ABC (Pl. 6, Fig. 3) represent a piece of ground, NS the assumed meridian, FE, PO, and ST, the meridian distances of the lines, AB, BC, and CA, respectively.

$N \times E + S \times W$.

Now, 2FE×GH or AD=2 area ZGHN=2ZGEa+2EHNa, And

20P×LN or BX=2MLNQ=2CLNB, since COM=OQB.

But, 2CLNB=2CRaB+2CLR+2aNB. Hence,

 $2OP \times LN = 2CRaB + 2CLR + 2aNB$. But,

 $2FE \times GH =$

2ZGEa + 2EHNAa.

Their sum =2CRaB+2CLR+2ZGEa+2EHB, or 2EAG.

=2CRaB+2CLR+2ZAa. But,

 $2\T \times LZ = 2RTVZ + 2LWTR...$ Hence, the sum of the three products = 2CRaB + 2RTVZ + 2CWT + 2ZAa.

=2CRaB+2RTVZ+2TAV+2ZAa.

=2CRaB+2RAZ+2ZAa.

=2 area of the triangle ABC.

In this figure there is no northing which has a western meridian distance, nor southing having an eastern meridan distance, and therefore there is but one set of products.

The demonstration would, however, be similar for every position of the assumed meridian, and the general theorem would be equally true.

166. It remains to illustrate these principles by an example.

<u> </u>	Bearings	Diet	Dif.	Dif. Lat.	Departures	tures		Balanced	peou		D.M.D.	$ D.M.D. \stackrel{N\times W+}{\sim} 1$	N×E+
o la			ż	zi.	편	*	Ŋ.	Ø	떠	W.		Z X X	×
-	N34°E	3.95	3.27		2.20		3.26		2.21		19.05E.		62.1030
જ	Z	4.60	4.60				4.59				• • •		97.5834
က	N36 f °W	8.14	6.54			4.84	6.53		•	4.82			107.3532
4	S59½°W	3.72		1.88		3.20		1.89		3.19		15.9327	
5	S25 W	6.24		5.65		2.63		5.66		2.65		14.8292	
9	S16E	3.50		3.36	8.			3.37	.97			3.2689	
<u>i-</u>	S65°E	8.20		3.46	7.43			3.46	7.45		9.39E.	32.4894	
						•							
	Sams		14.41	4.41 14.35 10.59 10.67	10.59	10.67	14.38	4.38 14.38 10.63 10.63	10.63	10.63		66.5202	267.0396
						=	_	_		_		_	

Hence 267.0396-66.5202=200.5194=2 area; or, area equal to 100.2597 square chains. But 10 square 10)100,2597(10,02597 acres chains make an acre; therefore,

.10388 roods 40

4.15520 perches

The area, therefore, is 10 acres, 0 roods, 4.15520 perches. In this example, the work on the field is begun at station 1. (Pl. 6, Fig. 4). The bearings are taken at all the stations, 1, 2, 3, 4, 5, 6, and 7; the distances are measured, and the entries made in the first three columns of the table. The distances are estimated in chains and links. The latitudes and departures are then found in the traverse table, and entered in their proper columns. These columns are then added up, and it is found that the northings exceed the southings by 6 links, and the westings the eastings by 8 links; but these sums should be equal. (160.)

The inequality arises from the inaccuracy of the measurement of the lines and bearings; but if the differences do not exceed four links for each station, it is deemed unnecessary to make a remeasurement. The corresponding columns are thus rendered equal. Divide the difference between the northings and southings by 2. Now, if this half difference be added in the smaller column, and subtracted in the larger, the amounts in the two columns become equal. But, to be strictly accurate, the half difference should be apportioned among the lines in proportion to their lengths. That is, we should make the proportions, as the sum of the northings, is to the half difference to be distributed, so is each northing to its portion of such half difference: and as the sum of the southings, is to half the difference, so is each southing to its portion of the half difference; the half difference being thus distributed among the northings and among the southings, their sums will be equal. The sums of the eastings and westings are made equal in the same way. This is called balancing the work, and the columns under balanced are the balanced latitudes and depar-It is, in general, hardly necessary to make the proportions; and, if the differences are not very unequal, the half difference may be distributed equally.

It is evident, from an inspection of the columns of departures, that 6 is the most westerly station; through this point let the assumed meridian be drawn.

The column D. M. D. is the column of double meridian distances, which are all east. They are calculated from the

columns of balanced departures; the mode of calculation has been too fully explained to need further illustration.

The columns $N \times W + S \times E$, $N \times E + S \times W$, contain the several products named in the general theorem.

167. It is now required to make a plot of the ground, whose dimensions and area are expressed in the table.

Draw any line on the paper, as NS, (Pl. 6, Fig. 4,) to represent the assumed meridian, which passes through station 6. The line which is run from station 6 lies on the east of the meridian, and makes with it an angle of 16°; its latitude in the balanced column is 3.37, and its departure .97. There are two ways of plotting this line. First, with a protractor, or scale of chords, make the angle SFG equal to 16°, and lay off, from a convenient scale of equal parts, the line FG', equal to 3.50, its length, taken from the column of distances. Or, secondly, from the scale of equal parts, lay off FG, equal to 3.37, the latitude: draw the perpendicular GG', and make it equal to .97, the departure, and join the points F and G. The latter method of plotting is preferred.

Through the station 7, draw a meridian, A'G, and lay down the line GA. Then draw the meridian AB, and lay down the line AB, and thus until all the lines are drawn: FGABCDE is the plot required.

Example 2.—To find the area of a piece of land, of which the following are the notes. Station 1, S. 40° W., dist. 70 rods; Station 2, N. 45° W., dist. 89 rods; 3, N. 36° E., 125; 4, North 54; 5, S. 81° E., 186; 6, S. 8° W., 137; 7, W., 130.

Answer.—207 acres, 3 roods, 22.69 perches.

Example 3.—Given the bearings and distances as follows: Station 1, S. $40\frac{1}{3}$ ° E., dist. 31.80 ch.; 2d, N. 54° E., 2.08 ch.; 3d, N. $29\frac{1}{4}$ ° E., 2.21 ch.; 4th, N. $28\frac{3}{4}$ ° E., 35.35 ch.; 5th, N. 57° W., 21.10 ch.; and 6th, S. 47° W., 31.30. Required the area.

Answer.—92 acres, 3 roods, 30 perches.

168. It was remarked, in article 159, that the field notes would be used, under the supposition of the land being kept on the left hand, in going round it. If, in taking the field notes

in example 1, we had gone round the land the other way, the bearing from A to G would have been B'AG, or N. the angle B'AG, W. But B'AG=AGA', which was the bearing from G to A, and was S. 65' E. Now, both the meridional and longitudinal letters are different, according as the line is run one way or the other, but the bearing and the distance remain the same. We may therefore conclude, that, a back sight, or reverse bearing, is equal to the corresponding forward sight; and that if the land be kept on the right hand, the notes will be the same as though it were kept on the left, excepting that the meridional and longitudinal letters, for the same course, will be different.

169. As the needle is sensibly affected by the presence of ferruginous substances, it is best to take both the forward and back sights. If they agree they may be relied upon, if not, the needle is influenced by local attraction. It then becomes necessary to ascertain at which of the stations at the extremities of the line, the local attraction exists. This is done by comparing the bearings of the line with the bearings of other lines of the survey.

170. In the operations of surveying it is sometimes necessary to know the angles which the lines make with each other. These are readily found from the field notes. At station A, (Pl. 6, Fig. 4,) for example, the bearing AB is BAB, N. 34° E,; the bearing of GA, from 7 to 1, is A'GA, S, 65° E.

But A'GA=GAB; hence GAB=GAB'+BAB=65°+34 =99°; and, in a similar manner, the angle of any two of the lines may be computed.

171. It is often necessary to ascertain the distance and bearing of two points, one of which cannot be seen from the other.

From either point measure a line lying as nearly as convenient in the direction of the second point, and take its bearing. From the extremity of this line, as a second station, take the bearing and measure the distance of a second line leading in the direction of the point, and so on, until the point is reached. Then arrange the notes in a tabular form, and find the latitudes and departures from the table: the difference

between the northings and southings, is the difference of latitude of the two points, and the difference between the eastings and westings, the departure of the line joining them. Suppose them joined. There is then formed a right-angled triangle, in which the base and perpendicular are known—the hypothenuse is the required distance, and the angle at the base the bearing.

Let A and B (Pl. 6, Fig. 5,) be the points, and 12, 23, &c. the lines measured; it is required to find AB, and the angle BAB', which it makes with the meridian AB'.

Sta.	Bearings	Dist.	N	s	E	W
1	S62°W	392		184.04	.:	346.07
2	N56½°.W	320	176.60			200.50
3	817 <u>‡</u> °E	375		357.67	112.80	**
4	S40°W	175		134.03		112.51
5	810°E	140		137.90	24 30	
6	8441°E	320		228.20	224.30	

176.60 1041.84 361.40 725.38 176.60 361.40 865.24 363.98

The difference of the northings and southings, 865.24, is equal to AB'; and the difference of the eastings and westings, 363.98 to BB'.

In the right-angled triangle ABB',

As AB', 865.24	2.937137	As sin. A22° 48′ 52″ Is to BB′ 363.98 So is radius	9.588539
Is to radius	lO.	Is to BB' 363.98	2,561077
So is BB' 363.98	2.561077	So is radius	10.
To tang. $\angle A$	• • • • • • • • • • • • • • • • • • • •	To AB 938.721	3.972538
To tang. ∠A) 22° 48′ 52′ {	9.623940	20112 000.721	Q.D. NOOQ

OF THE DIVISION AND LAYING OUT OF LAND.

171. The surveyor is often called upon to lay off a given quantity of land, in such a way, that its bounding lines shall form a particular figure, viz: a square, a rectangle, a triangle, &c.: and, also, to divide given pieces of land into parts containing given areas, or having certain relations with each other.

The manner of making such divisions, must always depend on a judicious application of the principles of geometry to the particular case.

If, for example, it were required to lay out an acre in a square form, it would first be necessary to find, by calculation, the side of such a square, and then, to trace on the ground four equal lines, respectively at right angles to each other.

PROBLEM.

172. To lay out a given quantity of land in a square form.

Reduce the given area to chains or rods; then extract the square root: such root is the side of the required square. This square being marked out on the ground is the figure required.

Example 1.—To find the side of a square which shall contain 15 acres, 0 roods, 12 perches.

15A=60R, and 60R=2400P, therefore, 15A 3R 12P=2412P. Hence, $\sqrt{2412}$ =49.111 rods, the side of the required square.

Example 2.—Required the side of a square, which shall contain 176 acres, 1 rood, 24 perches.

Answer 42 chains.

In this example, the area is reduced to square chains.

176A=1760. square chains.

$$1R = 2.5$$
 , $24P = 1.5$,

176A, 1R, 24P=1764 square chains, the square root of which is 42 chains.

PROBLEM.

173. To lay out a given quantity of land in a rectangular form, having one of the sides given.

Divide the given area, reduced to square chains or square rods, by the given side of the required rectangle; the quotient is the other side.

Example 1.—To lay off 240 acres in a rectangular form, one of the sides being given, equal to 80 rods.

240A=2400 square chains=38400 square rods.

8.0)3840.0(480 rods:—the required side of the rectangle.

174. A great number of similar problems might be proposed. The solution of them does not properly belong to surveying, but combines the application of geometrical and algebraical principles; it is tracing the lines only that belongs to surveying. The manner of tracing lines, having been already explained, it seems unnecessary to add the numerous examples usually given under this head of the subject.

OF THE VARIATION OF THE COMPASS.

175. The line, indicated by the magnetic needle when it is allowed to move freely about the point of support, has been named the magnetic meridian (140); and is, in general, a different line from the true meridian, which is determined by a plane passing through the place and the axis of the earth.

176. The angle which the magnetic meridian makes with the true meridian at any place on the surface of the earth, is called the *variation of the needle* at that place, and is east or west, according as the north end of the needle lies on the east or west side of the true meridian.

177. The variation is different at different places, and even at the same place it does not remain constant for any length of time. The variation is ascertained by comparing the magnetic, with the true meridian.

178. The best practical method of determining the true meridian of a place is by observing the north star. If this star were precisely at the point in which the axis of the earth, being produced, pierces the heavens, then, the intersection of

the vertical plane passed through it and the place, with the surface of the earth, would be the true meridian. But, the star being at a distance from the pole, equal to 1° 35′ 41″, it performs a revolution about the pole in a circle, the polar distance of which is 1° 35′ 41″: the time of revolution being 23 h, and 56 min.

To the eye of an observer, this star is continually in motion, and is due north but twice in 23 h. 56 min., and is then said to be on the meridian. Now, when it departs from the meridian, it apparently moves east or west, for 5 h. and 59 min., and then returns to the meridian again. When at its greatest distance from the meridian, east or west, it is said to be at its greatest eastern or western elongation.

The following tables show the times of its greatest eastern and western elongations.

Days	Ap	ril	M	ay	Ju	ne	Ju	ıly	Aug	gust	Se	pt.
	н.	M.	н.	M.	н.	M.	н.	M.	н.	M.	н.	M.
1	18	18	16	26	14	24	12	20	10	16	8	20
7	17	56	16	03	14	00	11	55	9	53	7	58
13	17	34	15	40	13	35	11	31	9	30	7	36
19	17	12	15	17	13	10	11	07	9	08	7	15
25	16	49	14	53	12	45	10	43	8	45	6	53

EASTERN ELONGATIONS.

WESTERN ELONGATIONS.

Days	0	ct.	Ne	ov.	De	ec.	Ja	n.	Fe	b.	Ma	rch
	н.	м.	н.	м.	н.	M.	Ħ.	M.	н.	M.	н.	M.
1	18	18	16	22	14	19	12	02	9	50	8	01
7	17	56	15	59	13	53	11	36	9	26	7	3 8
13	17	34	15	35	13	27	11	10	9	02	7	16
19	17	12	15	10	13	00	10	44	8	39	6	54
25	16	49	14	45	12	34	10	18	8	16	6	33

The eastern elongations are put down from the first of April to the first of October; and the western from the first of October to the first of April; the time is computed from 12 at noon. The western elongations in the first case, and the eastern in the second, occurring in the day time, cannot be used. Some of those put down, are also invisible, occurring before daylight is gone in the evening, or after daylight in the morning. In such case, if it be necessary to determine the meridian at that particular season of the year, let 5 h. and 59 min. be added to, or subtracted from, the time of greatest eastern or western elongation, and the observation be made at night, when the star is on the meridian.

The following table exhibits the angle which the meridian plane makes with the vertical plane drawn to the pole-star, when at its greatest eastern or western elongation: such angle is called the azimuth. The mean angle only is put down, being calculated for the first of July of each year.

Veare	Lat. 32°	Lat. 34°	Lat. 36°	Lat. 38°	Lat. 40°	Lat. 42°	Lat. 44°
	Azimuth	Azimuth	Azimuth	Azimuth	Azimuth	Azimuth	Azimuth
1830	1 53′	$1^{\circ} 55\frac{1}{2}'$	l° 59	% %	2, 51,	3° 01′	2° 13½′
1831	I. 52½	1° 55′	l° 58½′	2° 1½'	%	් රු රී	2° 13'
1832	l° 52′	l° 54½′	l° 58′	ř Š	2° 4½'		2° 12½,
1833	l° 51½′	l° 54′	l. 571,	$2^{\circ} 0^{\frac{1}{2}}$	2° 4′	Š	2° 12½
1834	1° 51′	l° 53½′	1. 57'	$1^{\circ} 59\frac{1}{2}'$	2° 4′		2, 12,
1835	$1^{\circ} 50^{\frac{1}{2}}$	l. 53	I° 56½′	l° 59	က် အိ	2° 61'	2, 11,
1836	1. 50	$1^{\circ} 52^{\frac{1}{2}'}$	1. 56.	1° $58\frac{1}{2}'$	2°		$2^{\circ} 10^{\frac{1}{2}}$
1837	$1^{\circ} 50^{\frac{1}{2}}$	l° 52½′	l° 55½'	$1^{\circ} 58\frac{1}{2}$	či či	$2^{\circ} 5^{\frac{1}{2}}$	2° 10'
1838	1. 50	$1^{\circ} 52^{\frac{1}{2}}$	l° 55′	1° 58′	2° 11/2	2í 3°	2° 91'
1839	$1^{\circ} 49^{\frac{1}{2}}$	1. 52.	l° 54½′	$1^{\circ} 57\frac{1}{2}'$		2° 4½'	ô %
1840	1. 49.	l° 511,	l° 54′	$1^{\circ} 57^{\frac{1}{2}}$	$2^{\circ} 0^{\frac{1}{2}}$	2° 4′	$\frac{2}{2}$ $8\frac{1}{2}$

The use of these tables, in finding the true meridian, will soon appear.

179. To find the true meridian with the theodolite.

Take a board, of about one foot square, paste white paper upon it, and perforate it through the centre; the diameter of the hole being somewhat larger than the diameter of the

telescope of the theodolite. Let this board be so fixed to a vertical staff, as to slide up and down freely: and let a small piece of board, about three inches square, be nailed to the lower edge of it.

About twenty-five minutes before the time of the greatest eastern or western elongation of the pole-star, as shown by the tables of elongations, let the theodolite be placed at a convenient point and levelled. Let the board be placed about one foot in front of the theodolite, a lamp or candle placed on the shelf at its lower edge; and let the board be slipped up or down until the pole-star can be seen through the hole. The light reflected from the paper will show the cross hairs in the telescope of the theodolite.

Then, let the vertical spider's line be brought exactly upon the pole-star, and, if it is an eastern elongation that is to be observed, and the star has not yet reached it, it will move from the line towards the east, and the reverse when the elongation is west.

At the time the star attains its greatest elongation, it will appear to coincide with the vertical spider's line for some time, and then leave it, in the direction contrary to its former motion.

As the star moves towards the point of greatest elongation, the telescope must be continually directed, by means of the tangent screw of the vernier plate; and when the star has attained its greatest elongation, great care should be taken that the instrument be not afterward moved.

Now, if it be not convenient to leave the instrument in its place until daylight, let a staff, with a candle or small lamp upon its upper extremity, be arranged at thirty or forty rods from the theodolite, and in the same vertical plane with the axis of the telescope. This is easily effected, by revolving the vertical limb about its horizontal axis without moving the vernier plate, and aligning the staff to coincide with the vertical hair. Then mark the point directly under the theodolite; the line passing through this point and the staff makes an angle with the true meridian equal to the azimuth of the polestar.

From the table of azimuths, take the azimuth corresponding to the year and nearest latitude. If the observed elongation were east, the true meridian lies on the west of the line which has been found, and makes with it an angle equal to the azimuth. If the elongation were west, the true meridian lies on the east of the line: and, in either case, laying off the azimuth angle with the theodolite, gives the true meridian.

180. To find the true meridian with the compass.

- 1. Drive two posts firmly into the ground, in a line nearly east and west; the uppermost ends, when driven firmly, being about three feet above the surface, and the posts about four feet apart: then lay a plank, or piece of timber three or four inches in width, and smooth on the upper side, upon the posts, and let it be pinned or nailed, to hold it firmly.
- 2. Prepare a piece of board four or five inches square, and smooth on the under side. Let one of the compass-sights be placed at right-angles to the upper surface of the board, and let a nail be driven through the board, so that it can be tacked to the timber resting on the posts.
- 8. At about twelve feet from the stakes, and in the direction of the pole-star, let a plumb be suspended from the top of an inclined stake or pole. The top of the pole should be of such a height that the pole-star will appear about six inches below it; and the plumb should be swung in a vessel of water to prevent it from vibrating.

This being done, about twenty minutes before the time of elongation, place the compass-sight, which is fixed in the piece of wood, on the horizontal timber, and slide it east or west, until the aperture of the compass-sight, the plumb line, and the star are brought into the same range. Then if the star depart from the plumb line, move the compass-sight, east or west, along the timber, as the case may be, until the star shall attain its greatest elongation, when it will continue behind the plumb-line for several minutes; and will then recede from it in the direction contrary to its motion before it became stationary. Let the compass-sight be now fastened to the timber. During this observation it will be necessary to have

the plumb line illuminated: this may be done by an assistant holding a small candle near it.

Let now a staff, with a candle or lamp upon it, be placed at a distance of thirty or forty rods from the plumb line, and in the same direction with it and the compass-sight. The line so determined, makes, with the true meridian, an angle equal to the azimuth of the pole star; and, from this line, the variation of the needle is readily determined, even without tracing the true meridian on the ground.

Place the compass upon this line, turn the sights in the direction of it, and note the angle shown by the needle. Now, if the elongation, at the time of observation, were west, and the north end of the needle lies on the west side of the line, the azimuth, plus the angle shown by the needle, is the true variation. But should the north end of the needle be found on the east side of the line, the elongation being west, the difference between the azimuth and the angle would show the variation: and reciprocally when the elongation is east.

Example 1.—Elongation west, azimuth	2° 04′
North end of the needle on the west, angle	4° 06′
	•
Variation	6° 10'west.
Example 2.—Elongation west, azimuth	1° 59'
North end of the needle on the east, angle	4° 50′
Variation	2° 51' east.
Example 3.—Elongation east, azimuth	2° 05′
North end of the needle on the west, angle	8° 30′
Variation	Co. 051
v ariation	6° 25' west.
Example 4.—Elongation east, azimuth	1° 57′
North end of the needle on the east, angle	8° 40′
Variation	10° 37′ east.

CHAPTER VI.

OF SURVEYING IN GENERAL.

181. We propose to explain in this chapter the manner of surveying a piece of land, for the determination both of its area and bounding lines. We shall use for this purpose the theodolite, the compass, the plain table, and the cross; and the instruments for plotting will also be used in delineating the survey on paper.

182. Plate 7 is the map of a piece of land to be surveyed. Looking upon it, the part on the right is bounded by a river, the upper side by a wood and cultivated land, the left-hand side by a fence and creek, and the lower part by a row of buildings.

183. The theodolite, being far the best of the surveying instruments, is to be used for determining the positions of the prominent points, or objects, and the more extended lines; after these are fixed, the shorter lines are to be traced with the compass, and auxiliary perpendiculars erected with the cross; then, the plain table is to be taken in hand, and the places of objects that are near each other, are to be determined by it.

184. Walk once or twice over the land, observe its general contour, the most prominent points for stations, and the best line that can be selected for a base. The base line should, in general, be as long as possible, though it would be useless to measure one of greater length than the average of the lines to be computed; it should, if convenient, be measured on the most level part of the land, and should always be so chosen, that the important points can be seen from its extremities.

185. Measure the base line agreeably to the directions in

Art. 82, and erect station staves, with flags on them, at the points to be determined. Suppose, in the present example, that we have measured the base line AB, and found it equal to 97 rods, and erected station staves at the points A, B, E, C, and D, which, for the sake of presenting a full example, we will name, Frog's point, Williams's corner, Day's house, Wood's barn, and Four corners, respectively.

We are now on the field with the theodolite. We remove the staff at A, place, by means of a plumb, the axis of the theodolite, over the station, and bring the 0 of the vernier. which is under the eye-glass of the telescope, to coincide with the 0 of the limb. Loosen the clamp screw and turn the body of the instrument until the telescope comes nearly on the base line: then tighten the clamp screw, and, by means of the tangent screw, bring the intersection of the hairs of the telescope to coincide with the bottom of the station staff at Then direct the lower telescope to the same point: sight from A to the stations C and E, (the only remaining ones that can be seen from A,) by turning the vernier plate, and without moving the limb, and read both the verniers. Enter in the notebook the degrees and minutes read at the vernier under the eye-glass, and in a separate column, the minutes shown by the other vernier: in a third column is to be entered the degrees read, and a mean between the minutes for the direction.

Take up the theodolite, replace the station staff, go to the other extremity B, of the base line, and place the instrument so that the line marked 0 and 180 shall coincide with the base BA, the 0 point being towards A; clamp the limb and sight to the stations E, C, and D, and read the angles as before.

Let the instrument be now removed to C. Place the 0 of the vernier under the eye-glass, to the angle that differs by 180° from the one which shows the direction from A to C, or from B to C, which latter arc is found in the column D. Then, without moving the vernier plate on the limb, direct the telescope to that extremity of the base from which the direction used was taken, when the line of the limb, marked 0 and 180°, will be parallel to the base line; since the line of direction so

intersects them, as to make the angles on the same side equal. Then sight to all the other stations which can be seen, and note the directions as before.

Let the instrument be now placed, after the same manner, at E, and the directions taken to B and A.

The following is the manner of entering the field notes.

FIELD NOTES.

	Field	Notes.	
A.	3 33 O K		* 8 2 8 g
⋖	00 78 116	\	48888
	3,00 K	D.	* 9 4 5 8 8 8 8
D.	D. 00 281 38		D. 180 206 116 146
E.G. V. O.V.	38 38 15	Station B. E. G. V. O.V.	* 8 & 6 &
>	36 11	m B.	* 8 4 5 8
편 명	381 381 381	Static E. G	D. 180 206 116 146
	To Williams's Corner, AB To Day's House, AE, LBAE To Wood's Barn, AC, LEAC	Williams's Corner, Station B.	To Frog's Point, BA, (back) To Day's House, BE, ∠ABE To Wood's Barn, BC, ∠EBC To Four Corners, BD, ∠CBD

Frog's Point, Station A.

Wood's Barn, Station U.

			ы S	<u>></u>	E. G. V. O.V.	Н	·	-	_i
			Ğ	×		Đ.	×	Ġ.	×
To Williams's Corner, CB, (back) -	ck)		296 16	16		536	91	1	
To Fros's Point, CA. LBCA		ا د	218 12	12	14	218	2	20	
To Four Corners, CD. LACD			172	37	37	172	37	45	36
- CBCD -								123	

	E. G. V. O.V.	>	0.V.	D.	•	7	i
	Ģ	Ä	Ä	Ď.	×	Ď.	K
To Frog's Point, EA, (back)	101	37	37	101 37 37 101	37		
Williams's Corner, EB, (back) ZAEB	98	413	421	26 41½ 42½ 26 42 74 55	42	74	22

In the first column of these tables, headed E. G. V., is written the arc read from the vernier under the eye-glass; in the second, marked O. V. the *minutes* read from the opposite vernier; in the third, marked D, the degrees before read, and a mean of the minutes; this column shows the true direction; and in the fourth, marked A, the angles which

the lines make with each other respectively; the letters designating the angles being on the same horizontal line on the left of the columns.

From an examination of the different positions of the instrument, it appears that a back sight to any station, as from C to B, or from C to A, differs from the forward sight by 180°. So that any errors in placing the theodolite, levelling it, or taking down the angles, will be detected at once on the field. The first and second columns only need be filled up on the ground; the others being calculated from them.

186. The necessary angles being measured with the theodolite, the compass is next to be used.

When the compass is used in conjunction with the theodolite, to fix the shorter lines and determine the smaller parts of the survey, the following is the manner of keeping the field notes.

Plate 8 is divided into two equal parts by the two parallel lines that are near each other, and each division is considered a separate leaf. Each leaf is divided into three spaces, the middle one being considerably smaller than the other two, which are equal. The notes begin at the bottom of the first leaf, run up the page to the top; then commencing again at the bottom of the next leaf, they are continued to the top, thence to the bottom of the third leaf, and thus, for as many leaves as the work may require.

The bearings are written in the middle space, and at the 0 points, where the lines run with the compass begin. At different points of these lines, perpendiculars are erected, called offsets. The numbers inserted in the middle columns show the distances of the offsets from the beginning of the lines respectively, and the numbers in the side columns, the distances, measured on the offsets, to objects that lie on the right and left.

The stations, at which the compass is placed, are numbered 1, 2, 3, 4, 5, 6, and 7. The characters in the left-hand columns are the conventional signs adopted by the Engineer Department to represent in topographical plans the objects for which they severally stand; they are used here for the double pur-

pose of showing the manner of determining points, and explaining the methods of delineation.

As it is rather inconvenient in practice to erect a perpendicular to a line that shall pass through a given point without the line, it is in general better to determine particular points lying without the compass lines, by oblique, than by perpendicular offsets. When this is done, the bearings and distances are inserted in the side columns. The manner in which the points C and D are determined, is an application of this method.

The work, with the compass, is begun at station A (Pl. 7), one extremity of the base line. From this point, the bearing of station D is taken, also the bearing of station 1, and both entered at the bottom and on the left of the page (Pl. 8), where the notes begin. The bearing of station D is due north, that of station 1, N. 27° E.

At station A, the distance AT to the river, measured on a perpendicular to A1, is 280 feet; this distance is also inserted in the notes. Passing along the line A1 to a, 100 feet, a like distance ab is 220 feet: the 100 feet is entered in the middle column (Pl. 8), and the perpendicular distance in the space on the right. At 100 feet from a, on the left of the line Al, and in the perpendicular ba produced, are several pieces of artillery: at c, 280 feet from A, the park of artillery is but 60 feet from A1; these distances are also entered in the notes. At d, 380 feet from A, the distance dd', to the river, is 150 feet, to the cannon battery, 130 feet; and at 1, 460 feet from A, the distance to the river is 110 feet, and to the mortar battery 60 feet. At this point a new course begins. Its bearing is N. 111. E. Its commencement, is indicated in the notes, by 0, which is placed at the beginning of each course, and by a figure which shows the number of the station. The line 12 is passed over in a manner entirely similar to that already explained for Al, and the distances to objects on the right and left entered in the notes in the same way. And similarly for the lines 23, 34, 45, 56, 67, and 7B.

The perpendiculars AT, ab, cc', dd', le, &c., are laid off with the surveying cross; they may, however, be laid off with the compass:

At station 3 the bearing is taken of station D; it is S. 33°W.; the distance is 110 feet, both are entered in the notes. At station 5, the bearing of station C is S. 54° E., the distance 90 feet.

If particular points are to be determined in position, and plotted on the map, it is best to use these oblique offsets; for, by taking the bearing and measuring the distance, the position of the object becomes known. The work with the compass finishes at station B.

187. We now take the plain table, put the paper upon it. place it at F, the extremity of the offset at B, and distant from it 265 feet (see notes); level it, mark the point that is directly over the station, lay the fiducial edge of the ruler on that point. and sight to station B; then fasten the table with the clamp Draw on the paper, with a pencil or leg of the dividers, a line corresponding to FB; then sight to the points G and H. and draw the lines FG and FH. Take the distance FB, equal to 265 feet, from a scale of equal parts, and apply it to the corresponding line on the paper; this determines the point B on the paper. Remove the table to B, and place it in such a manner that the point B and the line BF on the paper shall be directly over B and the line BF on the ground; the instrument being levelled, let it be clamped. Then sight to the points G and H successively, and draw the lines BG, BH; these lines, by their intersection with the corresponding lines from F, determine the points G and H.

Let now a new paper be placed on the table. Measure on BE, which is a known line, any distance BL, equal to 600 feet; and on the paper lay off this distance from a scale of equal parts. From B, sight to H, I, K, and the corners of the other building: then remove the table to L, and sight to H, and the other points.

The line BH is determined on both papers, and if this line on one of them, be laid on the same line of the other, all the points and lines of the former will be given in position with respect to the points and lines of the latter. The width of the buildings can now be laid off, and the buildings drawn. Let a fence be supposed to run from F to M, from M to E, and from E to O. A distance ER is now measured with the chain equal to 500 feet; the plain table is then placed at E and R, and the points O, P, and S determined.

188. All the data necessary for the calculations are now known. We shall begin by finding the lines determined with the theodolite.

CALCULATION.

In the triangle AEB $42'$, $\angle A = 78^{\circ} 23'$ (see not	are known A	B=97 roods	s, <b=26< th=""></b=26<>
As sin. \angle E 74° 55′ 9.98	4774 Assin	∠F 7/1° 55′	0 081771
Is to AB 97 - 1.98		B 97	
So is sin. ∠A 78° 23′ 9.99			
——————————————————————————————————————		III. 22 D 20 42	
To EB 98.403 - 1.99	3010 To AE	45.139 -	1.654553
In the triangle ABC are	e known AB=	=97 rods.∠1	B=EBC-
$EBA = 90^{\circ} 26 - 26^{\circ} 42' =$	=63°44′.∠C=	=78° 03'. ∠A	=EAC-
$EAB = 116^{\circ}36' - 78^{\circ}23 =$			
As sin. ∠C 78° 03′ 9.99	0485 As sin.	∠C 78°03′	9.990485
Is to AB 97 - I.98	6772 Is to A	В 97	1.986772
So is sin. ∠B 63° 44′ 9.95			
-			
To AC 88.911 - 1.94	8956 To BC	61.337	1.787723
In the triangle BCD, th	nere are knov	wn BC=61.	337, ∠B=
$30^{\circ} 23^{\circ}$, $C = 123 29^{\circ}$, and			
As sin \(\sigma \) 25° 58′ 9.641			
Is to BC 61.337 1.78"	7723 Is to B	C 61.337	1 787723
So is sin. C 123° 39° 9.920	0352 So is si	in. B 30° 23'	9.703964
-			
To BD 116.614 2.066	6751 To CD	70.854 -	1.850363
	·		
In the triangle ACD, the	here are knov	vn AC=88.9	911, CD=
70.854, and the angle C=	=45 ′ 36 ′.		
As AC+CD Is to AC-CD	- 159.765	2.20	03482
Is to $AC-CD$	- 18.057	1.25	56646
So is tang. $\frac{1}{2}$ (D+A)	670 10	10.37	6377
	- 07 12	10.0.	0011
To tang. $\frac{1}{2}$ (D-A)			

189. Having calculated the principal lines of the survey, it is, in general, best to plot the work before computing the area, because the division of it into triangles, rectangles, trapezoids, &c., can be made to greater advantage when the whole is at once presented to the eye.

We shall first plot the part surveyed with the theodolite.

Place the centre of the circular protractor at V, near the centre of the paper, and draw the line A'B, passing through the points 0 and 180°. Then lay off from the 0 point, an arc of 38° 13′ the direction from A to C (see notes), and draw A'C'. Lay off also the arc of 281° 37′, the direction from A to E, and draw A'E'. Proceed in the same manner to lay off the directions from B, viz.: BA=180′, which gives B A'; BE=206 42′, which gives B E; BC=116° 16′, which gives B'C'; and BD=146° 39′, which gives B'D'. The directions from C being laid down, give C'B', and C'A, before determined, as also C'D', the direction from C to D, being 172 37′. Laying off in like manner the directions from E, gives the lines E B', E'A.

This being done, let any line, as AB, be drawn on the paper parallel to AB, to represent the base line. Now, as the line 0 and 180°, on the limb of the theodolite, was parallel at all the stations to the base line AB, the 0 point being in the direction towards A, it follows that it was constantly parallel to the line A'B' of the protractor: and hence the lines A'C', A'E', &c. are respectively parallel to their corresponding lines on the ground; and thus the direction of every line is fixed without removing the protractor.

It is proposed to make the plot on a scale of 19 rods to the inch. Take a distance of one inch in the dividers, and extend the arms of the sector until the dividers will just reach across the angle, one foot standing at division 19 on one arm, and the other foot at division 19 on the other: the sector is then said to be set. Lay the sector carefully on the table; then take the distance, from 97 on one arm to 97 on the other, and apply it on the paper from the point A, marked as one extremity of the base line, to B, which will be the other, and AB will represent the base line.

Through B draw BC parallel to B'C'; take the distance BC from the scale, and apply it on the paper; this determines the place of station C. Through C draw CD parallel to C'D', and lay off CD; then join A and D, and B and D. Lastly, draw AE parallel to A'E', and lay off AE; this fixes the point E; then let the lines AE and BE be drawn. If the semicircular protractor were used, it would perhaps be best to lay off the angles at the several station points.

190. To plot the work done with the compass. Form the following table from the compass notes, and write the differences of latitude and departure in their proper columns.

Sta.	Bear.	Dist.	Dif.	Lat.	Dif.	Dep.
~) Down	2.50	N.	S.	E.	W.
A	N. 27° E.	460	409 9		208.8	
1	N. 111 E.	270 .	264.6		53.8	
2	N. 22 ⁵ W.	550	510			206
3	S.894°W.	760	i	6.6		760
4	S.71 W.	570		180.9		540.5
5	N. 84° W.	332	34.71			330.19
6	S. 22 W.	760		704.7		284.7
7	S 37 E.	385		307.49	231.71	

The scale used in the plot is one of 19 rods, or 314.5 feet to the inch. If one inch be taken in the dividers, and the arms of the sector extended until the dividers will just reach from 31.45 on one arm, to 31.45 on the other, then each division of the sector, the distances being measured across the angle, will

correspond to 10 feet. The sector having been thus opened to the proper angle, take from it the difference of latitude of the line A1; this is found, very nearly, by extending the dividers across from 41 to 41; and since AD is a meridian, lay off this distance from A to q. At q erect the perpendicular q1, and lay off on it a distance equal to the departure; join A and 1; A1 is the first line traced with the compass. At A erect the perpendicular AT, and make it equal to 280 feet (see notes); this gives the point T at the shore of the river. Lay off 100 feet from A to a, erect the perpendicular ab, and lay off 220 feet to the river on one side, and 100 feet to the artillery on the other; and the same for the offsets at c, d, and 1. At 1, draw a parallel to AD, to represent a meridian line, and lay down the line 1 2, and its offsets in the same manner, and similarly for all the other lines.

When there are oblique offsets, as at 3 and 5, they are readily plotted, as their lengths and the angles which they make with the meridian are known. In the present example, they serve to verify the work.

191. To join the work done with the plain table.

If the same scale was used with the plain table as that already used in the plot, we have only to transfer the work from one paper to the other. But if the scales are different, measure the angle contained by the lines BF, BG, on the paper of the table, either with a protractor or a scale of chords; and then extend the dividers from B to G, on the paper of the table, and refer the distance to the scale used with the table; this will show the true length of the line BG. Then, on the plot, make the angle FBG equal to the measured angle, and the distance BG equal to the measured distance; the point G will then be determined. In the same manner, the other lines may be laid down. Or the work may be transferred by letting fall perpendiculars on the paper of the table, from all the angular points G, H, I, K, &c. on the line BE, and then laying off on BE the distances from B to the foot of each perpendicular. as also the lengths of the respective perpendiculars.

It is best to plot the whole in pencil before making any of the lines in ink, as the plot will generally not unite exactly at the point where the work ends; in which case, if the error be small, it may be divided among the nearer lines; if it be large, it shows a mistake somewhere, which must be rectified.

192. We are now to compute the area, and will begin with that portion of the survey that was made with the theodolite.

We know (112) that,
$$log. BD 116.614 - 2.066751 + log. BA 97 - 1.986772 + log. sin. B 33° 21′ - 9.740167 - log. radius - -10.$$

$$2 BDA = 6218.56 - - 3.793690$$
And BDA = 3109.28 square rods.
$$log. BD 116.615 - 2.066751 + log. BC 61.337 - 1.787723 + log. sin. B 30° 23′ - 9.703964 - log. radius - -10.$$

$$2 BCD = 3617.74 - - - 3.558438$$
And BCD = 1808.87 square rods.
$$log. BA 97 - - 1.986772 + log. BE 98.403 - 1.993010 + log. sin. B 26° 42′ - 9.652555 - log. radius - - -10.$$

$$2 BEA = 4288.81 - - - - 3.632337$$
And BEA = 2144.405 square rods.

Therefore, the area BDA = 3109.28 square rods area BCD = 1808.87 square rods square rods
" " area BCD = 1808.87 square rods

The area ADCBEA - =7062.555 square rods, which being divided by 160 (108), gives for the entire area 44 acres, 0 rods, 22 perches.

We are next to ascertain the area of that portion of the land surveyed with the compass. Of this area, a part lies without the lines traced with the compass, and a part within them. The latter portion will be first computed. There are two methods by which this area may be calculated; first, by dividing it into triangles, trapezoids, &c.; and secondly, by the general method of computing surveys made with the compass. If the latter be chosen, and it is considered preferable, the bearings of the lines BC, CD, and DA, must be found; for which there are already sufficient data.

The bearing from A to D is due north; the angle DAB is 90° 22′ 04″; therefore, the bearing from A to B is S. 89° 38′ W. nearly; or from B to A, N. 89° 38′ E. (168). But the angle ABC=63° 44′; therefore, the bearing of C from B is N. 25° 54′ E., and the distance BC=61.337 rods, or 1012 feet. The bearing of B from C is S. 25° 54′ W., and the angle BCD being equal to 123° 39′, the bearing of D from C is N. 82° 15′ E., and the distance CD=70.854 rods, equal to 1169 feet. The bearing from A to D being north, the bearing from D to A is south, the distance is 1057.8 feet.

The bearings and distances being known, we form the following table.

Į													
Ü	St Bearing 1	jst	Dif. Lat.	Lat.	Dif. Dep.	Dep.		Bala	Balanced.		G ₩	N.X.W.	N.X.E.
2	9		Ŋ.	zż	ਜ਼	W.	Z.	χ <u>ο</u>	E.	W.		3. × E.	.× ₩ .×
∢	~		409.90		208.80		406.90		210.80		3897.48		1585876.47
_	Z		264.60		53.80	-	262.60		54.52		4162.80		1093151.28
R						908	202			25	4013.32		2034753.24
ಣ	8894°W	760		09.9		260		6.91		756		21098.44	
4	S714 W			180.90		540.50		182.90		537.50	1759.82	321871.07	
3	N84°W		34.71		-	330.19	314			328.19	894.13		30767.01
9	S22.W			704.70		284.70		708.70		282.97		200540.83	
7	837°			307.49	231.71			310.49			233.71	72564.61	
B	N26°E	$\overline{}$	909.79		443.26		904.79		446.26		913.08		826688.52
ပ	N824°E	_	157.30		1158.37		156.30		1163.37		2523.31		394393.35
Ω_	'n		•	1058.00				1063			3686.68	3686.68 3894039.84	
	Sum	١.	2286.30	2257.69	2095.94	2121.39	2272.00	2272.00	2286.30 2257.69 2095.94 2121.39 2272.00 2272.00 2108.66 2108.66	2108.66		4521985.79	4521985.79 5965629.35

The manner of calculating the area in this example is entirely similar to that explained in Art. 87. The meridian, from which the meridian distances are calculated, passes through station 7; the double meridian distances are all east. The half difference of the sums 5965629.35 and 4521955.79, is 721821.78: the number of square feet contained by the lines, AI, 1 2, 23, 34, 45, 56, 67, 7B, BC, CD, and DA. We are next to compute the area which lies without the lines traced with the compass.

Beginning at station A, and regarding the lines which join the extremities of the offsets as right, which we may do without any sensible error, the area of the trapezoids

$$ATba = \frac{AT + ab}{2} \times Aa = \frac{280 + 220}{2} \times 100 = 25000$$

$$abc'c = \frac{ab + ac'}{2} \times ac = \frac{220 + 80}{2} \times 180 = 27000$$

$$cc'd'd = \frac{cc' + dd'}{2} \times cd = \frac{80 + 150}{2} \times 100 = 11500$$

$$dd'el = \frac{dd' + le}{2} \times dl = \frac{150 + 110}{2} \times 80 = 10400$$

To compute the erea of the quadrilateral legh.

Join 1 and g. Then, in the right-angled triangle 1gh, there are known 1h=140, and kg=40: the remaining parts can therefore be found; they are, the angle $g1h=15^{\circ}$ 56' 43", the hypothenuse 1g=145.62, and its area =2000.

But the bearing from A to 1 is N. 27° E., consequently, from 1 to A, S. 27° W. (169); and since Le is perpendicular to A1, its bearing is known, viz. S. 63° E. The bearing of the line 1 2 is N. 11½° E.; hence the angle Le is known, it being equal to 189° - (63°+11° 30′)=105° 30′; and therefore the angle gle is known, being equal to 105° 30′—15° 56′ 43″ = 89° 83′ 17″. Therefore, the area of the triangle gle can be found, two sides and the contained angle being known; it is equal to 8007.9 square feet.

The areas of the quadrilaterals 2ikl, at station 3, and 3nmp at station 3, are computed in a similar manner by dividing them into the triangles 2ik, 2kl, and 3nm, 3mp; and the same for the quadrilaterals at stations 4, 5, 6, and 7.

The areas of the trapezoids and quadrilaterals will be arranged with reference to the lines to which they correspond, and for the sake of convenient reference, will be numbered from the beginning of those lines respectively.

Line Al.	Line 4 5.		
1st Trapezoid=25000	Quadrilateral =21184.3		
2d Do. $=27000$	1st Trapezoid=22500		
3d Do. $=10500$	2d Do. =44850		
4th Do. $=10400$	Line 5 6.		
Line 1 2.	Quadrilateral $=21879.7$		
Quadrilateral = 10807.9	1st Trapezoid=34400		
1st Trapezoid= 6500	Line 6 7.		
Line 2 3.	Quadrilateral $=46565.1$		
Quadrilateral = 5831.86	1st Trapezoid=30750		
1st Trapezoid=10800	2d Do. = 13800		
$2d$ D_0 . = 16100	3d Do. = 13020		
3d Do. =21450	4th Do. $= 7700$		
Line 3 4.	5th Do. = 5500		
Quadrilateral = 18766.85	Line 7B.		
1st Trapezoid=18700	Quadrilateral = 7793.28		
2d Do. =16200	1st Trapezoid=17100		
3d Do. =14400	2d Do. =33712.50		

193. We are yet to find the area of the ground surveyed with the plain table. This is done by dividing it into triangles, and measuring their bases and perpendiculars by means of the scale of equal parts. Thus, in the triangle BFM (the line BGM being nearly right), by applying the base BM to the scale of equal parts, it is found to be equal to 720 feet, and by applying the perpendicular Ff, it is found equal to 220 feet; and similarly, MQ=860, QW=250, BE, before found, =1623.65, EO=385, RN=470, OS=418, RS=310, TR=320, SS'=130, and AA"=210.

The area of the triangle BMF= 79200 square feet.

BMQ=309600 BQE =202956.25 ERO = 90475 ROS = 64790 RST = 10800 RTA = 33600

Collecting these several areas, we find,

The area within the compass lines=721821.78 square feet.

The area without the compass lines=534211.49

The area found with the plain table=791421.25

""

Sum, 2047454.52.

This sum being divided by 43560, the number of square feet in an acre, gives for the area, (110) 4 A., 2 R., 32 P.

Let this area, - - - 4 A., 2 R., 32 P., be added to the area ADCBEA - - =44 A., 0 R., 22 P., and we have

the total area - - - = 48 A., 3 R., 14 P.

GENERAL REMARKS.

194. Surveying being merely the application of the principles of geometry and trigonometry to the determination of the area of land, and the lengths and directions of lines, and such application varying with the kind of survey to be made, the form of the ground, and many other accidental circumstances, it is unnecessary, even were it possible, to follow the surveyor to every case that may arise, and give him a rule precisely applicable to it. In operations which run out into such a variety of detail, general principles only can be dwelt upon; hypothetical cases would be uninteresting, and might be useless.

The experienced surveyor will regard his theodolite with peculiar interest. It is the great instrument. It alone can be relied on for nice and accurate operations.

A large section of country may be accurately surveyed, by determining a system of consecutive triangles. In such a survey, stations should be chosen on the tops of hills or mountains, and at other prominent and important points; and this general rule ought never to be neglected—measure the three angles of every triangle, whenever it is possible; this will prove the work as it advances.

The tracing of the shores of rivers, creeks, roads, fences, &c., may safely be trusted to the compass, after having determined several of their prominent points by triangulating the ground with the theodolite. The compass, however, is a rude

instrument, and cannot be relied on, unless used in conjunction with the theodelite. It is, nevertheless, used to determine the area of ground by the methods explained in Chapter V.; yet, if the land were valuable, greater accuracy would certainly be necessary.

The plain table is used to great advantage when only a plot of the ground is wanted. It ought not to be used for the determination of long lines, nor can it be relied on in determining extended areas.

CHAPTER VII.

OF LEVELLING.

195. Ir all the points of the earth's surface were equidistant from the centre, it would be perfectly even, and present to the eye an unbroken level.

Intersected, however, as it is, by valleys and ridges of mountains, it becomes an important problem to ascertain the difference between the distances of given points from the centre of the earth; such difference is called the difference of level; and a line, all the points of which are equally distant from the centre, the line of true level.

196. One point is said to be above another, when it is farther from the centre of the earth; and below it, when it is nearer.

197. Let C (Pl. 9, Fig. 1,) represent the centre of the earth. A a point of its surface, and AEF the line of true level. If, at the point A, a tangent line GABD be drawn to the surface, such line is called the line of apparent level.

198. Now, if an instrument were placed at A, which could be brought into a horizontal position to indicate a horizontal line, this line would be tangent to the earth at A, and would be the line GABD of apparent level.

199. When, therefore, we have ascertained the direction of a tangent, or horizontal line, we have found the line of apparent level only; the line of true level is yet to be determined.

If at the points E and F vertical staves be placed, the line of apparent level passing through A will cut them at B and D, while the line of true level cuts them at E and F.

^{*} The spheroidal form of the earth is not considered, as it affects the results too inconsiderably to be regarded in the common operations of levelling.

Therefore, BE and DF are, respectively, the differences between the apparent levels of the points E and F, as determined by the horizontal line passing through A, and the true levels of those points.

But AB²=BE (BE+2EC), and AD²=DF (DF+2FC) (228)*. In the common operations of levelling, the arcs AE, AF, are small; and since the difference between small arcs and their tangents is very inconsiderable, the arcs AE, AF may be substituted for the tangents AB, AD. And since the external parts of the secants BE and DF are very small in respect of the diameter of the earth, they may be neglected without sensible error: the expressions above will then become,

AE²=BE×2EC, and AF²=DF×2FC,
or, BE=
$$\frac{AE^2}{2EC}$$
; and DF= $\frac{AF^2}{2FC}$;

and since the diameter of the earth is constant, BE and DF are proportional to AE² and AF².

But BE and DF are respectively the differences between the true levels of the points E and F, and their apparent levels, as ascertained from the point A: hence, the difference between the apparent and true level of any point, is equal to the square of the distance of that point from the place where the apparent level was made, divided by the diameter of the earth; or, the diameter being constant, the rise of the apparent above the true level, is proportional to the square of the distance.

200. The mean diameter of the earth being about 7921 miles, if AE be taken equal to 1 mile, then, the excess BE= $\frac{AE^2}{2AC}$, becomes equal to $\frac{1}{7921}$ =8.001 inches.

If the excess FD, for any other distance AF, were required, AE²: AF²:: BE: FD; and by similar proportions, the following table is calculated.

Table showing the differences in inches between true and apparent level, for distances between 1 and 100 chains.

Chains.	Inches	Chains.	Inches.	Chains.	Inches.	Chains.	Inches.
1	.001	26	.845	51	3.255	76	7.221
2	.005	27	.911	52	3.380	77	7.412
3	.011	28	.981	53	3.511	78	7.605
4	.020	29	1.051	54	3.645	79	7.802
5	.031	30	1.125	55	3.781	80	8.001
6	.045	31	1.201	56	3.925	81	8.202
7	.061	32	1.280	57	4.061	82	8.406
8	.080	33	1.360	58	4.205	83	8.612
9	.101	34	1.446	59	4.351	84	8.832
10	.125	35	1.531	60	4.500	85	9.042
11	.151	36	1.620	61	4.654	86	9.246
12	.180	37	1.711	62	4.805	87	9.462
13	.211	38	1.805	63	4.968	88	9.681
14	.245	39	1.901	64	5.120	89	9.902
15	.281	40	2.003	65	5.281	90	10.126
16	.320	41	2.101	66	5.443	91	10.351
17	.361	42	2.208	67	5.612	92	10.587
18	.405	43	2.311	68	5.787	93	10.812
19	.451	44	2.420	69	5.955	94	11.046
20	.500	45	2.531	70	6.125	95	11.233
21	.552	46	2.646	71	6.302	96	11.521
22	.605	47	2.761	72	6.480	97	11.763
23	.661	48	2.880	73	6.662	98	12.017
24	.720	49	3.004	74	6.846	99	12.246
25	.781	50	3.125	75	7.032	100	12.502

We cannot proceed farther in the discussion of the principles of levelling, until we have described the instruments which are to be used, and explained the particular objects that they are to answer.

OF THE LEVEL.

201. The level is an instrument used to determine horizontal lines, and the difference of level of the different points on the surface of the earth.

The part of the instrument shown in Fig. 2, Pl. 9, rests on a tripod to which it is permanently attached at Z. HH is a horizontal brass plate, through which four levelling screws with milled heads are passed, and worked against a second horizontal plate GG. Two of these screws, K and I, are seen in the figure. S is a clamp screw, which, being loosened, allows the upper part of the instrument to turn freely around its axis. Q is a tangent screw, by means of which the upper part of the instrument is moved gently, after the clamp screw S has been EE is a horizontal bar, perpendicular to which are made fast. the wyes, designated Y, that support the telescope LB. This telescope is confined in the Y's by the loops r, r, which are fastened by the pins p and p. The object-glass B, is adjusted to its focus by the screw X; the eye-glass L slides out and in freely. The screws f, f, work the slide which carries the horizontal hair; and two horizontal screws, only one of which, a, is seen, work the slide that carries the vertical hair. CD is an attached spirit level. The screw N elevates and depresses the Y, nearest the eye-glass. In some instruments this Y is elevated and depressed by means of two screws at M and R.

Before using the level it must be adjusted. The adjustment consists in bringing the different parts to their proper places.

The line of collimation is the axis of the telescope. With this axis, the line drawn through the centre of the eye-glass, and the intersection of the spider's lines, within the barrel of the telescope, ought to coincide.

First adjustment. To fix the intersection of the spider's lines in the axis of the telescope.

Having screwed the tripod to the instrument, extend the legs, and place them firmly. Then loosen the clamp screw S, and direct the telescope to a small, well defined, and distant object. Then slide the eye-glass till the spider's lines are seen distinctly; after which, with the screw X, adjust the object-glass to its proper focus, when the object and the spider's lines

^{*}This, and some of the following adjustments, are so similar to those of the theodolite, that they would not be repeated, but that some may use the level without wishing to study a more complicated instrument.

will be seen distinctly. Note now the precise point covered by the intersection of the spider's lines.

Having done this, revolve the telescope in the Y's, half round, when the attached level CD will come to the upper side. See if in this position the horizontal hair appears above or below the point, and in either case, loosen the one, and tighten the other, of the two screws which work the horizontal slide, until the horizontal hair has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again, by the aid of the screw N, the intersection of the spider's lines to the point, and repeat the operation, till the horizontal hair neither ascends nor descends while the telescope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted.

Second adjustment. To make the axis of the attached level CD parallel to the line of collimation.

Turn the screw N, or the screws M and R, until the bubble of the level DC stands at the middle of the tube. Then open the loops, and reverse the telescope. If the bubble still stands at the middle of the tube, the axis of the level is horizontal; but if not, it is inclined, the bubble being at the elevated end. In such case, raise the depressed, or depress the elevated end, by means of the screw h, half the inclination; and then with the screw N, bring the level to a horizontal position. Reverse the telescope in the Y's, and make the same correction again; and proceed thus, until the bubble stands in the middle of the tube, in both positions of the telescope; the axis of the level is then horizontal.

Let the telescope be now revolved in the Y's. If the bubble continue in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recedes from the centre, the axis of the level is inclined to the line of collimation, and must be made parallel to it, by means of two small screws, which work horizontally; one of these screws is seen at q. By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation; and then, if the telescope

be revolved in the Y's, the bubble will continue at the middle point of the tube. It is, however, difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation: for, allowing the level to be truly horizontal in one position of the telescope, after it is reversed, there will be but one corresponding position in which the bubble will stand at the middle of the tube. This suggests the necessity of making the first part of the adjustment with tolerable accuracy; then, having made the second with care, re-examine the first, and proceed thus till the adjustment is completed.

Third adjustment. To make the level CD and the line of collimation perpendicular to the axis of the instrument, or parallel to the horizontal bar EE.

Loosen the clamp screw S, and turn the bar EE, until the level DC comes directly over two of the levelling screws. By means of these screws, make the level DC truly horizontal. Then, turn the level quite round; if, during the revolution, it be still horizontal, it must be at right angles to the axis of the instrument about which it has been revolved. But if after the revolution, the level DC be not horizontal, rectify half the error with the screw N, and half with the levelling screws. Then place the bar EE over the other two levelling screws. and make the same examinations and corrections as before: and proceed thus, until the level can be turned entirely around without displacing the bubble at the centre. When this can be done, it is obvious, that the level DC and the line of collimation, are at right angles to the axis of the instrument about which they revolve; and since the axis is carefully adjusted by the maker, at right angles to the bar EE, it follows, that the line of collimation, the level DC, and the bar EE, are parallel to each other.

These adjustments are, however, made on the supposition, that the parts of the telescope which come in contact with the Y's are portions of the same cylinder. To ascertain if they be so, let the telescope be reversed in the Y's, and then turned half round; if the level DC continue horizontal, and the intersection of the spider's lines is directed to the same point in

both positions of the telescope, the adjustments are accurate. If otherwise, such alterations must be made in the places of the spider's lines, by the screws which govern their slides, that, in both positions of the telescope, their intersection shall be directed to the same point, the level DC continuing at the same time horizontal.

The level is now adjusted. When used, however, it is best to re-examine it every day or two, as the work will be erroneous unless the adjustments are accurate.

OF LEVELLING STAVES.

202. The levelling staves are used to determine the points at which a given horizontal line intersects lines that are perpendicular to the surface of the earth, and the distance of such points of intersection from the ground.

They are thus constructed. AB (Pl. 9, Fig. 3) is a rectangular piece of wood, in the middle of which is a groove abcd. Into this groove a slide *lnst* enters, and is worked freely along the groove. At the upper end of the slide is a rectangular index fhgi, called a vane, six inches, in the direction hi. vane is divided into four equal parts, by the lines fg, hi: the two rectangles fh, ig, are usually painted black, and the other two, if, hg, white, so that the lines fg and hi may be distinguished with great accuracy. The slide from fg to ln is of the same length with the body of the staff AB: hence, when the line fg coincides with bc, the lower end of the slide ln will coincide with ad. The pins p and q, which work in grooves. and are largest at the ends p and q, are pressed in to hold the slide in any position at which it may be placed. The length of the staff is generally six feet, and it is usually divided into eighths or tenths of an inch. The slide is divided in the same way. The longer lines show the feet, the shorter the inches. object to be attained by these divisions is, to ascertain the distance of the line fg from the ground. When the line fg is brought to the top of the staff, to coincide with bc, the lower line wio. of the vane, coincides with the line marked 6, on the left of the staff: which shows, the staff standing upright, that the line fg is six feet above the ground. From the line marked 6, to the lower end of the staff, is, indeed, but 5 feet 9 inches; but the line fg is three inches above the line wio, so that fg is six feet from the ground.

If, from the last position, the slide be run up until the line win coincides with the division marked 1, on the left of the staff, the line fg will be six feet and one inch from the ground: if till it coincides with bc, it will be six feet and three inches, the inches being marked both on the staff and slide. If it be still run up, until 7 on the slide coincides with bc, the line fg will be seven feet from the ground. In the figure, the line fg is seven feet from the bottom of the staff. The count above 6 feet 3 inches is always made on the slide. The manner of counting off, for the parts of an inch, is too plain to require particular explanation.

Having run down the slide till the upper line h, of the vane, coincides with bc, place $b\mathbf{B}$ on the ground, and the staff vertical. It is now plain, that the line fg is three inches above the ground. These three inches are marked on the right of the staff. If the slide be run up till the lower line h coincides with 1 on the right of the staff, the line fg will be one foot from the ground, and similarly until six feet be shown at the other end of the staff.

The feet are marked 1, 2, 3, &c., from the upper end, and are reversed in the present position of the staff; but are upright when the staff is placed for use.—In this position of the staff, the count is made at the lower line of the vane.

203. There is yet a method of ascertaining if the level be truly adjusted, which ought not to be neglected, since all the results depend on the accuracy of the instrument. The method is this:—The line of collimation being first adjusted, place the level A (Fig. 4) at any convenient place, as G. At equal distances of about 100 yards, on either side, and in the same line with the level, place the levelling staves CE, BF. Make the level horizontal with the levelling screws. Then, turn it towards either staff, as BF, and run the vane up or down, as required, until the intersection of the hairs strikes its centre: then make the slide fast, and note carefully the height of the vane. Turn the level half round, and do the same in respect of the staff CE. Let the telescope be now reversed in the Y's.

Sight again to the staff BF, and move the vane, until the intersection of the hairs shows its centre; and note the exact height. Let the telescope be now turned half round, and the same done in respect of the staff CE.

If the staves are equidistant from the level, the difference between the two observed heights of the vane of the staff BF, will be equal to the difference of the observed heights on the staff CE; and if the staves are at unequal distances from the level, the differences of the observed heights will be proportional to those distances, BG, GC.

Let gAf be the true horizontal line, and Ad the first line of sight. When the level is turned half round, the corresponding line will be Ab. The level being reversed in the Y's, the line of sight becomes Aa, and turning the level half round, the corresponding line is AE. Now, Bd and Ba are the observed heights on one staff, and CE, Cb on the other. Moreover, if GB and GC are equal, it is evident, that the two triangles Ada, AEb will also be equal; and consequently, da = Eb.

It is also evident, that Aa is as much above the horizontal line Ag, as Ad is below it: so that, if da, the difference of the two heights, be divided by 2, the quotient will show how far the vane must be elevated from its first position, or depressed from its second, to bring it to the horizontal line passing through A. Let the index be so elevated, or depressed. Then turn the screw N (Fig. 2), until the intersection of the hairs rests on the centre of the vane: the axis of the telescope is then horizontal, and by means of the screw h, the level DC is made parallel to it. The line of collimation and the level CD are then to be made parallel to EE, as in the third adjustment. It is perhaps too obvious to be mentioned, that, if the level be truly adjusted in the beginning, the points d and a will coincide with g, and the points E and b with f.

204. Having described the instruments used in levelling, it remains to show the manner of using them in the practical operations on the field.

When it is proposed to find the difference of level of any two objects, or stations, all levels made in the direction of the station at which the work is begun, are, for the sake of distinction merely, called back-sights; and levels taken in the direction of the other station, fore-sights.

Before going on the field with the level, rule three columns, as below, and head them, Stations, Back-sights, Fore-sights.

Stations.	· Back-Sights.	Fore-sights.
1 2 3 4	10 11 6 6 8 3 9	3 0 4 9 8 3
	31 11	16 0

PROBLEM.

205. To find the difference of level between any two points, as A and G. (Pl. 9, Fig. 5.)

The level being adjusted, place it at any point B, as nearly in the line joining A and G as may be convenient. Place a levelling staff at A, and another at N, a point lying as near as may be in the direction of G. Make the level horizontal by means of the levelling screws; turn the telescope to the staff at A, and direct the person at the staff to slide up the vane until the horizontal line ab cuts its centre; then note the distance Ab, (equal to 10 feet in the present example,) and enter it in the column of back-sights, opposite station 1. Sight also to the staff at N, and enter the distance Na, equal to 3 feet, in the column of fore-sights, opposite station 1.

Take up the level, and place it at some other convenient station, as C, and remove the staff at A to M. Having levelled the instrument, sight to the staff at N, and enter the distance Nd, 11 feet 6 inches, in the column of back-sights, opposite station 2: sight also to the staff at M, and enter the distance Mf, equal 0, in the column of fore-sights, opposite station 2.

Let the level be now removed to any other station, as D, and the staff at N, to some other point, as P. Let the distance Mg, equal to 6 feet 8 inches, be entered in the column

of back-sights, opposite station 3, and the distance Ph, equal to 4 feet 9 inches, in the column of fore-sights. Let the instrument be now placed at E, and the distance Pm, equal to 3 feet 9 inches, and Gn, equal to 8 feet 3 inches, be entered opposite station 4, in their proper columns.

By adding up the columns, we find, that the sum of the backsights is equal to 31 feet 11 inches, and the sum of the foresights, 16 feet; the difference, 15 feet and 11 inches, is the difference of level of the points A and G.

Demonstration.—Let the back-sights be called plus, and the fore-sights, minus.

Then, having let fall the perpendiculars NF, MH, PI, and GL, on the horizontal line AL, it remains to be proved, that the difference of level,

GL=
$$Ab+Nd+Mg+Pm-Na-0-hP-nG$$
.
Now, $Ab+Nd-Na=Ab+ad=Fd$;
Therefore, GL= $Fd+Mg+Pm-hP-nG$.
But $Fd+Mg=Hg$, and $+Pm-hP=-hm$,
Therefore, GL= $Hg-hm-nG=hI-(hm+nG)=GL$.

As the same may be shown in every example, we conclude that, the difference between the sum of the fore-sights and the sum of the back-sights is, in all cases, equal to the difference of level.

It is also evident that, when the sum of the back-sights exceeds the sum of the fore-sights, the last station is more elevated than the first; and, conversely, if the sum of the back-sights is less than the sum of the fore-sights, the second station is lower than the first.

206. In this example, we have not regarded the difference between the true and apparent level. If it be necessary to ascertain the result with extreme accuracy, this difference must be considered; and then, the horizontal distances between the level, at each of its positions, and the staves, must be measured, and the apparent levels diminished by the differences of level; which differences can be found from the table.

Stat.	Back-sts.	Distances.	Fore-st.	Distances.	Cor. back sights.	Cor. fore-sights.
1 2 3 4 5	9 8 8 7 5 2 10 3 11 0	25 ch. 18 ch. 29 ch.	2 4 3 1 1 9	32 ch. 28 ch. 16 ch. 87 ch. 72 ch.	9 7.500 8 6.219 5 1.595 10 1.949 10 9.469	1 4.720 2 3.019 3 0.680 0 11.538 1 10.520
					44 2.732	9 6.477

The following is such an Example.

In this example, the first column shows the stations; the second, the back-sights; the third, the distances from the level in each of its positions to the back staff; the fourth, the foresights; the fifth, the distances from the level to the forward staff; the sixth and seventh, are the columns of back and foresights, corrected by the difference of level. The corrections are thus made:—The difference of level in the table corresponding to 20 chains, is .5 of an inch, which being subtracted from 9 feet 8 inches, leaves 9 feet 7.5 inches for the corrected back-sight; this is entered opposite station 1 in the sixth column. The difference of level corresponding to 32 chains, is 1.280 inches, which being subtracted from the apparent level, 1 foot 6 inches, leaves 1 foot 4.720 inches for the true fore-sight from station 1. The other corrections are made in the same manner.

The sum of the back-sights being 44 feet 2.732 inches, and the sum of the fore-sights 9 feet 6.477 inches, it follows, that the difference, 34 feet 8.255 inches, is the true difference of level.

207. In finding the true from the apparent level, we have not regarded the effect caused by refraction on the apparent elevation of objects, as well because the refraction is different in different states of the atmosphere, as because the corrections are inconsiderable in themselves.

208. The small errors that would arise from regarding the apparent as the true level, may be avoided, by placing the

levelling staves at equal distances from the level. In such case, it is plain, 1st, that equal corrections must be made in the fore and back-sights; and, 2dly, that when the fore and back-sights are diminished equally, the result, which is always the difference of their sums, will not be affected.

This method should always be followed if practicable, as it avoids the trouble of making corrections for the difference of true and apparent level.

The differences between the true and apparent level being very inconsiderable for short distances, if only ordinary accuracy be required, it will be unnecessary to make measurements at all. Care, however, ought to be taken, in placing the levelling staves, to have them as nearly at equal distances from the level as can be ascertained by the eye; and if the distances are unequal, let the next distances also be made unequal; that is, if the back-sight was the longest in the first case, let it be made proportionably shorter in the second, and the reverse.

CHAPTER VIII.

OF THE METHODS OF SHOWING THE CONTOUR AND ACCIDENTS OF GROUND.

- 209. Besides the surveys that are made to determine the area of land and the relative positions of objects, it is frequently necessary to make minute and careful examinations for the purpose of ascertaining the form and accidents of the surface, to distinguish the swelling hill from the sunken valley, and the course of the rivulet from the unbroken plain.
- 210. This branch of surveying is called Topography. In surveys made with a view to the location of extensive works, the slopes and irregularities of the ground are of the first importance: indeed, the examinations would be useless without them.
- 211. The manner of ascertaining these irregularities is, to intersect the surface of the ground by a system of horizontal planes at equal distances from each other; the curves determined by these secant planes, being lines of the surface, will indicate its form at the places of section, and, as the curves are more or less numerous, the form of the surface will be more or less accurately ascertained.

If such a system of curves be determined, and then projected or let fall on a horizontal plane, it is obvious, that the curves on such plane will be nearer together or farther apart, as the ascent of the hill is steep or gentle.

If, therefore, such intersections be made, and the curves so determined accurately delineated on paper, the map will present such a representation of the ground as will show its form. its inequalities, and its striking characteristics.

212. The subject divides itself, naturally, into two parts.

First, to make the necessary examinations and measurements on the field. And, secondly, to make the delineations on paper. For the former of these objects, the theodolite is the best instrument; the common level, however, will answer all the purposes, though it is less convenient.

Before going on the field, it is necessary to provide a number of wooden stakes, about two feet in length, with heads. These stakes are used to designate particular points, and are to be driven to the surface of the ground. A nail should then be driven into the head of each of them, to mark its centre.

213. We shall, perhaps, be best understood, by giving an example or two, and then adding such general remarks, as will extend the particular cases to all others that can occur.

Let A (Pl. 9, Fig. 6,) be the summit of a hill, the contour of which it is required to represent. At A, let a stake be driven, and let the axis of the theodolite, or level, be placed directly over the nail which marks its centre. From A, measure any line down the hill, as AB, using the telescope of the theodolite or level to arrange all its points in the same vertical plane. Great care must be taken, to keep the measuring chain horizontal, for it is the horizontal distances that are required. At different points of this line, as a, b, c, d, &c, let stakes be driven, and let the horizontal distances Aa, ab, bc, and cd, be carefully measured. In placing the stakes, reference must be had to the abruptness of the declivity, and the accuracy with which the surface is to be delineated: their differences of level ought not to exceed once and a half or twice the difference between the horizontal planes of section.

Having placed stakes and measured all the distances along the line AB, run another line down the hill, as AC, placing stakes at the points e, f, g, and h, and measuring the horizontal distances Ae, ef, fg, and gh. Run also the line AD, placing stakes at i, l, m, and n, and measuring the horizontal distances Ai, il, lm, and mn.

Each line, AB, AC, AD, running down the hill from A, may be regarded as the intersection of the hill by a vertical plane; and these secant planes are to be continued over all the ground which is to be surveyed. If the work is done with a theodolite, or with a level having a compass, the angles DAB and BAC, contained by the vertical secant planes, can be measured; if it is done with a level, having no needle, let any of the distances ae, bf, ai, bl, &c. be measured with the chain, and there will be known the three sides of the triangles Aae, Abf, Aai, Abl.

Let now, the difference of level of the several points marked in each of the lines AB, AD, AC, be ascertained.

In the present example the results of the measurements and levelling, are—

Line	e AB.					
Distances.	Difference of Level.					
Aa = 40 feet,	A above a 12 feet,					
ab = 50 "	a above b 8 "					
bc = 30 "	b above c 9 "					
cd = 46 "	c above d II "					
Line	AC.					
Distances.	Difference of Level.					
Ae = 28 feet,	A above e 11 feet,					
ef = 45 "	e above f 9 "					
fg = 55 "	f above g 12 "					
gh = 49 "	g above h 14 "					
Line AD.						
Distances.	Difference of Level.					
Ai = 25 feet,	A above i 9 feet,					
il = 55 "	<i>i</i> above <i>l</i> 13 "					
lm = 38 "	l above m 7 "					
mn = 48 "	m above n 14 "					
$\angle CAB=25^{\circ}$,	$\angle DAB = 30^{\circ}$.					

These data are sufficient, not only to find the intersections of horizontal planes with the surface of the hill, but also to delineate such curves of section on paper

Having drawn on the paper the line AB, lay off the angle $BAC=25^{\circ}$, and the angle $BAD=30^{\circ}$. Then, from a convenient scale of equal parts, lay off the distances Aa, ab, bc, cd, Ae, ef, fg, gh, Ai, il, lm, and mn.

Let it be required that the horizontal planes be at a distance of eight feet from each other. Since A is the highest point of the hill, and the difference of level of the points A and a, is 12 feet, the first plane, reckoning downwards, will intersect the line traced on the ground from A to B, between A and a. Regarding the descent as uniform, which we may do for small distances without sensible error, we have this proportion; as the difference of level of the points A and a, is to the horizontal distance Aa, so is 8 feet to the horizontal distance from A at which the first horizontal plane will cut the line from A to B. This distance being thus found, and laid off from A to o, gives o, a point of the curve in which the first plane intersects the ground. The points at which it cuts the lines from A to C, and from A to D, are determined similarly, and three points in the first curve are thus found.

By the aid of the sector, the graphic operations are greatly facilitated. Let it be borne in mind, that the descent from A to a, is 12 feet, and that it is required, upon the supposition of the descent being uniform, to find that part of the distance corresponding to a descent of 8 feet. Take the distance from A to a, in the dividers, and open the arms of the sector until the dividers will reach from 12, on the line of equal parts, on the one side, to 12, on the line of equal parts, on the other. Then, without changing the angle, extend the dividers from 8 on the one side, to 8 on the other; the latter is obviously the proportional distance to be laid off from A to o. Or, if the dividers be extended from 4 to 4, the proportional distance may be laid off from a to o. If the distances to be taken from the sector fall too near the joint, let multiples of them be used; as for instance, on the French sectors, let the arms be extended until the dividers reach from 120 on the one, to 120 on the other, then 80 or 40 will be the proportional numbers. Other multiples may be used, though it is generally more convenient to multiply by IO.

The second plane is to pass 8 feet below the first, that is, 16 feet below A, or 4 feet below a, a being 12 feet below A. Take the distance ab in the dividers, and extend the sector, so that the dividers will reach from 8 to (the descent from a

to b being 8 feet) 8, or from 80 to 80; then, the distance from 4 to 4, or from 40 to 40, being laid off from a to p, gives p, a point of the second curve.

The difference of level between a and b being 8 feet, and the difference of level between a and p being 4 feet, the difference of level between p and b must also be 4 feet: hence, the third plane will pass 4 feet below b, and q, determined as above, is a point of the third curve.

The difference of level between b and c being 9 feet, and consequently between q and c, 5 feet, the fourth plane will pass 3 feet below c, and r is a point of the fourth curve.

The difference of level between c and d being 11 feet, the difference of level between r and d is 8 feet; so that the fifth plane will pass through d, which is consequently a point of the fifth curve.

The points at which the horizontal planes cut the lines drawn from A to C, and from A to D, are determined in a manner entirely similar. Having thus made as many diverging sections from the point A as may be necessary, and found the points in which they are cut by horizontal planes, the horizontal curves of section can be described through the several corresponding points. These curves being represented on paper, their curvature shows the form of the surface of the hill in the direction of a horizontal line traced around it; and the distances between them, the abruptness or gentleness of the declivity. The numbers (8), (16), &c. show the vertical distance of the respective planes below the point A.

214. If it were required to show a profile of the ground, let the vertical plane passing through A and B be revolved about its intersection with a horizontal plane passing through d. Erect perpendiculars at r, c, q, b, p, a, o, and A, to the line BA, and make them equal to the respective distances of these points above the horizontal plane passing through d, viz. at r, 8 feet, at c, 11, at q, 16, at b, 20, at p, 24, at a, 28, at o, 32, and at A, 40; and through the extremities of the perpendiculars so determined, let a curve be traced: this curve will be the curve of the hill from d to A. The curve is omitted in the figure because it would confuse it.

215. This method of finding the form of the surface of a hill, is, perhaps, the best, when the hill slopes gradually from its summit, and the declivity is sufficiently gentle to measure down it. If the surface were that of an undulating plain, the following method is preferable:—

Measure a horizontal line, as AB (Pl. 9, Fig. 7), running along one side of the ground to be surveyed. At the extremities A and B, erect the perpendiculars AD and BC, and produce them until all the land to be surveyed shall be included within the rectangle ABCD. On the line AB measure the horizontal distances AE, EF, FG, and GB; and on the line DC, the distances DH, HI, IL, and LC, respectively equal to the distances on AB: that is, DH=AE, H1=EF, &c. The distances AE, EF, &c. are regulated by the inequalities of the ground, being less if the changes in the surface are considerable, and greater if the changes are nearly uniform. In the present example, they are 100 feet each, which, upon ordinary ground, would render the work tolerably accurate. Let stakes be driven at A, E, F, G, B, C, L, I, H, and D. Measure now the line AD. and place stakes at convenient distances, as a, b, c, and d: place stakes also along the other lines EH, FI, GL, and BC, at suitable points, and measure the respective distances Ef, fg, &c. It is best to use the telescope of the theodolite or level, in order to run the lines and place the stakes truly. In placing the the stakes, it should be borne in mind, that the difference of level of either two that follow each other, ought not to be very great; and also, that they ought not to be on the same horizontal plane.

After the stakes are all placed, and the distances measured, let the difference of level of all the points so designated be found. In the present example, the results of the measurements are—

$$Aa = 80 \text{ ft.}$$
 $AE = 100 \text{ ft.}$ $EF = 100 \text{ ft.}$ $GB = 100 \text{ ft.}$ $ab = 60$ $bc = 90$ $fg = 85$ $ik = 115$ $mn = 76$ $mn = 76$

Of the Levelling.

Line A	D.	1	Line E	H.		Line I	FI.	I	ine G	L		I	ine	BO	; .
	Ft	_		Ft	_		_Ft.			_1	Pt.	_		_	Ft.
A above	a 5	$ \mathbf{E}$	below	A 3	F	below	$\mathbf{E2}$	G	below	\mathbf{F}	1	В	belo	wC	2
a "	b 6	E	above	f 9	F	above	i 3	G	above	m	2	В	abov	req	3
b "															
c below															
d above	D 4	h	below	H 3	l	below	13	p l	oelo w	L	4	t k	elov	v C	5

The heights of the points are here compared with each other, two and two. Before, however, we can conceive clearly their relative heights, we must assume some one point, and compare all the others with it. Let the point A be taken. The height of

This being done, a mere inspection shows us the highest and lowest points, as also the relative heights of the others, reckoning upwards or downwards. Let them be now written in the order of their heights above the lowest point, which is D. The difference of level between A and D being 20 feet, if the difference of level of each of the points below A be taken from 20 feet, the remainder will be the height above D. Arranging them in their order, we have

\boldsymbol{c}	abov	e D 2 ft	. H	abov	e D 7ft.	pa	bo.	ve D 9ft	. Ba	bov	reD 12ft.
\boldsymbol{d}	.66	D 4	k	66	D 7	q	66	D 9	L	66	D 13
h	"	D 4	8	"	D 7	$ \mathbf{C} $	"	D 9	G	"	D 14
ŧ	46	D 4	f	66	D 8	n	"	D 11	a	66	D 15
g	66	D 5	I	66	$\mathbf{D} 8$	i	66	D 12	F	"	D 15
ĩ.	66	D 5	b	66	D 9	m	"	D 12	E	"	D 17

Let the surface be now intersected by a system of horizontal planes at 3 feet from each other,—the first plane being 3 feet above the point D. The point b being 9 feet above D, and the point c, 2 feet, the first plane will intersect the line AD between b and c: let the proportional distance be found, as in the last example, and one point u, of the first curve, will be known. The point H being 7 feet above D, the plane will cut the line DC between H and D, and finding the proportional distance as before, a second point, v, of the first curve, is determined. Now, in drawing this curve, it will be borne in mind, that the point h is but $\overline{4}$ feet above D, and consequently, but 1 foot above the first curve, so that the curve must run from u near to h, and then turn around to the point v. The curve is marked (3), which is the number of feet that it is above the lowest point, and similarly for the other curves of the figure; their number showing their distance in feet above D. Around the point d. there is a small curve, also marked (3). By inspecting the table, it will be seen that d is 4 feet above D, and that the ground descends from d towards D and c: d is therefore a small knowl, the top of which is cut off by the first plane. show that the ground descends from d, even below the first curve, a plane is passed I foot below the first plane, or 2 feet above D: the curve of section is marked (2).

The second of the system of curves, or the one marked (6), must cut the line AD between b and c, the line EH between f and g, the line FI between k and l, and also between l and l; it also cuts EH again between l and l, and the line DC between l and l.

The third curve, or the one passing 9 feet above D, passes through b, cuts the line EH between E and f, the line FI between i and k; thence it passes to p, and thence to the line DC, crossing it between I and L. There is also another curve determined by this plane, since it passes through the points C and q, leaving the points t and t below it. This curve runs from C to t0, and from t0 to t0, as drawn in the figure.

The fourth curve, marked (12), intersects the line AD between a and b, EH between E and f, Fl at i, GL at m, and BC at B. There is also another curve lying around the point

L: for the plane cuts GL between p and L, the line DC between C and L, and again between I and L.

The fifth curve, marked (15), cuts AD at a, EH between E and f, and AB at F. The sixth curve, marked (18,, cuts AD between A and a, and AB between A and E. The proportional distances in all these cases are found as in the first example.

In looking on the little map that has been made, it is clearly indicated by the curves, that the ground slopes from A to c, thence rises to d, and then slopes to D. It also slopes from A along the line AB: from E in the directions f and i, from F in the directions i and m, from G in the directions m and B, and from B in the direction Bqs. The ground also slopes from L to p, thence to l and h, and along to curve (2), and the point D: and on the other side to t and s.

216. Thus far, we have said nothing of a plane of reference; it is any horizontal plane to which the levels of all the points are referred. In the first example, the plane of reference was assumed through the point A (Pl. 9, Fig. 6), and tangent to the surface of the hill: in the second example, it was taken through D, the lowest point of the work.

217. After having compared all the levels with any one point, the highest and the lowest points are at once discovered. and the plane of reference may be assumed through either of them. As, however, in comparing the heights of objects, the mind most readily refers the higher to the lower, it is considered preferable to take the plane of reference through the lowest point. We say, for example, that the summit of a hill is 200 feet above a given plain, and not that the plain is 200 feet below the summit of the hill; so we say that a plain is at a given distance above a river, and not that the river is below the plain. This habit of the mind, to refer the higher to the lower objects, suggests the propriety of taking the plane of reference through the lowest point, where there is no other circumstance to influence its selection. If, however, there are fixed and permanent objects, to which, as points of comparison. the mind readily refers all others, such as the court-house or church of a village, the market-house of a town, or any public

building or monument, it is best to assume the plane of reference through some such point; for, it must be kept in mind, that the ends proposed in the construction of maps, are, to present a clear view of the ground, its form, its accidents, and the relative positions of objects upon it.

- 218. When the plane of reference is so chosen that the points of the work fall on different sides of it, all the references on one side are called positive, and those on the other negative. Let the curves having a negative reference be distinguished by placing the *minus* sign before the number, thus —().
- 219. In these topographical surveys, great care should be taken to leave some permanent marks with their levels written upon them, in a durable manner. For example, if there are any rocks, let one or more of them be smoothed, and the vertical distance from the plane of reference be marked thereon: or, let the vertical distance of a point on some prominent building be ascertained and marked permanently upon the building with paint. Such points must also be noted on the map, so that a person, though unacquainted with the ground, could, by means of the map, go upon it, and trace out all the points, together with their differences of level.
- 220. The manner of shading the map, so as to indicate the eminences and slopes, although highly important, belongs to the department of drawing, rather than to that of practical mathematics.
- 221. In making topographical surveys, the great point is, to determine the curves which result from the intersection of the surface by horizontal planes. Besides the methods of diverging and parallel sections, we may assume a point on the surface of a hill, place the level there, and run a line of level round the hill, measuring the angles at every turn or change of direction: such a line is a horizontal curve. Then, levelling up or down the hill, a distance equal to the required distance between the horizontal curves, let a second horizontal curve be traced, passing through this point, and similarly for as many as may be necessary. This method, however, is not as good as the methods by sections, which will always afford accurate results.

CHAPTER IX.

OF SURVEYING HARBOURS.

- 222. There are two objects to be attained in the survey of a harbour.
- 1. To survey the shore along high or low-water mark,—to trace its windings, to note the points and inlets, and to ascertain and fix the places at which rivers and creeks discharge themselves. And,
- 2. To discover the channels, their direction, depth, and width, the position of shoals, the depth of water upon them, the nature of the bottom, and, in short, whatever may contribute to easy and safe navigation.
- 223. Having provided a boat and crew, row once or twice around the harbour—mark the more important and prominent points; at which, let station-staves with flags upon them be erected.

Then, measure a base-line, and form a series of triangles, having their angles at the stations before chosen. Let the angles of these triangles be measured with the theodolite, and their sides calculated; after which, the high or low-water mark may be traced along the shore with the compass, and the work plotted as in Chapter VI.

224. When a harbour is surveyed for the second object, viz. for the purpose of ascertaining the channels, their depth and width, the positions of shoals, and the depth of water thereon, other means must be used, and other examinations made, in addition to those already referred to.

Let buoys be anchored on the principal shoals and along the

edges of the channels, and using any of the lines already determined as a base, let the angles subtended by lines drawn from its extremities, to the buoys respectively, be measured with the theodolite. Then there will be known in each triangle the base and angles at the base, from which the distances to the buoys are easily found; and hence, their positions become known.

Having made the soundings, and ascertained the exact depth of the water at each of the buoys, several points of the harbour are established, at which the precise depth of the water is known; and by increasing the number of the buoys, the depth of the water can be found at as many points as may be deemed necessary.

225. If a person with a theodolite, or with any other instrument adapted to the measurement of horizontal angles, be stationed at each extremity of the base line, it will not be necessary to establish buoys. A boat, provided with an anchor, a sounding line, and a signal flag, has only to throw its anchor, hoist its signal flag, and make the sounding, while the persons at the extremities of the base line measure the angles;—from these data, the precise place of the boat can be determined.

226. There is also another method of determining the places at which the soundings are made, that admits of great despatch, and which, if the observations be made with care, affords results sufficiently accurate.

Having established, trigonometrically, three points which can be seen from all parts of the harbour, and having provided a sextant, let the sounding be made at any place in the harbour, and at the same time, the three angles subtended by lines drawn to the three fixed points, measured with the sextant.

The Problem, to find, from these data, the place of the boat at the time of the sounding, is the same as Example 6, p. 57.

It is only necessary to measure two of the angles, but it is safest to measure the third also, as it affords a verification of the work.

The great rapidity with which angles can be measured with the sextant, by one skilled in its use, renders this a most expeditious method of sounding and surveying a harbour. The sextant is not described, nor are its uses explained, in these Elements, because its construction combines many philosophical principles, with which the surveyor cannot be supposed conversant.

227. There is yet another method of finding the soundings, which, although not as accurate as those already explained, will, nevertheless, afford results approximating nearly to the It is this:—Let a boat be rowed uniformly from one extremity to the other, of any of the lines determined trigonometrically. Let soundings be made continually, and let the precise time of making each be carefully noted. Then, knowing the length of the entire line, the time spent in passing over it, as also the time of making each of the soundings, we can easily find the points of the line at which the several soundings were made; and hence the depth of water at those points be-Soundings may thus be made along any numcomes known. ber of known lines, and a comparison of the depths found on different lines, at or near their points of intersection, will show with what degree of accuracy the work has been done.

228. If the soundings are made in tide-waters, the time of high tide must be carefully noticed, as also the precise time of making the sounding, so that the exact depth at high or low water may be known. It is considered preferable to reduce the soundings to high-water mark, and the number of feet which the tide rises and falls should be noted on the map.

229. Having plotted the work done with the theodolite, as also the outline of the harbour traced with the compass, (223) it remains to delineate the bottom of the harbour; and this is done by means of horizontal curves (Chap. VIII.) which have already been used to represent broken and undulating ground.

Let the plane of reference be taken through high-water mark, or to coincide with the surface of the water at high tide. The accuracy with which the bottom of the harbour is to be delineated, will guide us in fixing the distance between the horizontal planes of section

The first horizontal plane is to be passed at a distance below the shallowest point that has been sounded, equal to the number of feet fixed upon for the distance between the planes of section; and the curve in which it intersects the bottom of the harbour determined as in Chapter VIII. And similarly, for the other horizontal planes of section.

Having thus delineated the bottom of the harbour, and noted on the map the distance of each intersecting plane below the plane of reference, let such lines be drawn, as will indicate the channels, shoals, sunken rocks, and direction of the current.

THE END.

A TABLE

· OF

LOGARITHMS OF NUMBERS

FROM 1 TO 10,000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.
ī	0.000000	26	1.414973	51	1.707570	76	1.880814
2	0.301030	27	1.431364	52	1.716003	77	1.886491
3	0.477121	28	1.447158	53	1.724276	78	1.892095
4	0.602060	29	1.462398	54	1.732394	79	1.897627
5	0.698970	30	1.477121	55	1.740363	80	1.903090
6	0.778151	31	1.491362	56	1.748188	81	1.908485
7	0.845098	32	1.505150	57	1.755875	82	1.913814
8	0.903090	33	1.518514	58	1.763428	83	1.919078
9	0.954243	34	1.531479	59	1.770852	84	1.924279
10	1.000000	35	1.544068	60	1.778151	85	1.929419
īī	1.041393	36	1.556303	61	1.785330	86	1.934498
12	1.079181	37	1.568202	62	1.792392	87	1.939519
13	1.113943	38	1.579784	63	1.799341	88	1.944483
14	1.146128	39	1.591065	64	1.806180	89	1.949390
15	1.176091	40	1.602060	65	1.812913	90	1.954243
16	1,204120	41	1.612784	66	1.819544	91	1.959041
17	1.230449	42	1.623249	67	1.826075	92	1.963788
18	1.255273	43	1.633468	68	1.832509	93	1.968483
19	1.278754	44	1.643453	69	1.838849	94	1.973128
20	1.301030	45	1.653213	70	1.845098	95	1.977724
21	1.322219	46	1.662758	71	1.851258	96	1.982271
22	1.342423	47	1.672098	72	1.857333	97	1.986772
23	1.361728	48	1.681241	73	1.863323	98	1.991226
24	1.380211	49	1.690196	74	1.869232	99	1.995635
25	1.397940	50	1.698970	75	1.875061	100	2.000000
				_			

N.B. In the following table, in the last nine columns of each page, where the first or leading figures change from 9's to 0's, points or dots are introduced instead of the 0's through the rest of the line, to catch the eye, and to indicate that from thence the annexed first two figures of the Logarithm in the second column stand in the next lower line.

N.	0	1	2	3	4	5	6	7	8	9	D.
100	1000000	0434	0868	1301	1734	2166	2598	3029	3461	3891	(432
101	4321	4751	5181	5609	6038	6466	6894	7321	7748	8174	428
102	8600	9026		9876	.300	.724	1147	1570	1993	2415	424
103	012837	3259			4521	4940	5360	5779		6616	
104	7033	7451	7868		8700	9116	9532	9947	.361	.775	
105	021189	1603			2841	3252	3664	4075	4486	4896	
106	5306	5715			6942	7350	7757	8164	8571	8978	408
107	9384	9789	.195		1004	1408		2216	2619		404
108	033424	3826	4227	4628	5029	5430	5830	6230	6629	7028	400
109	7426	7825	8223	8620	9017	9414	9811	.207	.602	.998	396
110	041393	1787	2182	2576	2969	3362	3755	4148	4540	4932	393
111	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830	389
112	9218	9606	9993	.380	.766	1153	1538	1924	2309	2694	386
113	053078	3463	3846	4230	4613	4996	5378	5760	6142	6524	382
114	6905	7286	7666	8046	8426	8805	9185	9563	9942	.320	379
115	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083	376
116	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815	372
117	8186	8557	8928	9298	9668	38	.407	.776	1145	1514	369
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
119	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819	363
120	079181	9543	9904	.266	.626	.987	1347	1707	2067	2426	360
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
122	6360	6716	7071	7426	7781	8136	8490	8845	9198	9552	355
123	9905	.258	.611	.963	1315	1667	2018	2370	2721	3071	351
124	093422	3772	4122	4471	4820	5169	5518	5866	6215	6562	349
125	6910	7257	7604	7951	8298	8644	8990	9335	9681	26	346
126	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462	343
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	340
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	.253	338
129	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609	335
130	113943	4277	4611	4944	5278	5611	5943	6276	6608	6940	333
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	.245	330
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
133	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781	325
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	12	323
135	130334	0655	.0977	1298	1619	1939	2260	2580	2900	3219	321
136	3539	3858	4177	4496	4814	5133	5451	5769	6086	6403	318
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	315
138	9879	.194	.508	.822	1136	1450	1763	2076	2389	2702	314
139	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140	146128	6438	6748	7058	7367	7676	7985	8294	8603	8911	309
141	9219	9527	9835	.142	.449	.756	1063	1370	1676	1982	307
142	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032	305
143	5336	5640	5943	6246	6549	6852	7154	7457	7759	8061	303
144	8362	8664	8965	9266	9567	9868	.168	.469	.769	1068	301
145	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055	299
146	4353	4650	4947	5244	5541	5838	6134	6430	6726	7022	297
147	7317	7613	7908	8203	8497	8792	9086	9380	9674	9968	295
148	170262	0555	0848	1141	1434	1726	2019	2311	2603	2895	293
149	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802	291
150	176091	$\frac{6381}{6381}$	6670	6959	7248	$\frac{7536}{7536}$	7825	-	-		_
151	8977	9264	9552	9839	.126			8113	8401	8689	289
152	181844	2129	2415	2700	2985	$\frac{.413}{3270}$.699	985	1272	1558	287
153	4691	4975	5259	5542	5825	6108	3555	3839	4123	4407	285
154	7521	7803	8084	8366	8647	8928	6391	6674	6956	7239	283
155	190332	0612	0892	1171	1451	1730	9209	9490	9771	51	281
156	3125	3403	3681	3959	4237		2010	2289	2567	2846	279
157	5899	6176	6453	6729	7005	4514 7281	4792 7556	5069	5346	5623	278
158	8657	8932	9206	9481	9755	29		7832	8107	8382	276
159	201397	1670	1943	2216	2488	2761	$\frac{.303}{3033}$	3305	$\frac{.850}{3577}$	1124 3848	$\frac{274}{272}$
-		-	2			2.01	5000	2000	2017	00101	212

N.	0	1	2	3	4	5	6	7	8	9	D.
160	204120	4391	4663	4934	5204	5475	5746	6016	6286	6556	127
161	6826	7096	7365	7634	7904	8173	8441	8710	8979		
162	9515	9783	51	.319	.586	.853	1121	1388	1654	1921	26
163	212188	2454	2720	2986	3252	3518	3783	4049	4314	4579	26
164	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221	
165	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846	
166	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456	
167	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051	25
168	5309	5568	5826	6084	6342	6600	6858	7115	7372	7630	
169	7887	8144	8400	8657	8913	9170	9426	9682	9938	.193	
170	230449	0704	0960	1215	1470	1724	1979	2234	2488	2742	25
171	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276	25
172	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795	
173	8046	8297	8548	8799	9049	9299	9550	9800			25
174	240549	0799	1048	1297	1546	1795			50	.300	25
175	3038	3286	3534	3782	4030	4277	2044	$\frac{2293}{4772}$	2541	2790	24
176	5513	5759	6006	6252	6499	6745	4525		5019	5266	24
177	7973	8219	8464				6991	7237	7482	7728	24
178	250420	0664	0908	8709	8954	9198	9443	9687	9932	.176	24
				1151	1395	1638	1881	2125	2368	2610	24
179	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031	24
180	255273	5514	5755	5996	6237	6477	6718	6958	7198	7439	24
181	7679	7918	8158	8398	8637	8877	9116	9355	9594	9833	23
182	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	23
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	23
184	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	23
185	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	23
186	9513	9746	9980	.213	.446	.679	.912	1144	1377	1609	23:
187	271842	2074	2306	2538	2770	3001	3233	3464	3696	3927	235
88	4158	4389	4620	4850	5081	5311	5542	5772	6002	6232	230
189	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229
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191	281033	1261	1488	1715	1942	2169	2396	2622	2849	3075	227
192	3301	3527	3753	3979	4205	4431	4656	4882	5107	5332	226
193	5557	5782	6007	6232	6456	6681	6905	7130	7354	7578	225
194	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812	223
195	290035	0257	0480	0702	0925	1147	1369	1591	1813	2034	222
96	2256	2478	2699	2920	3141	3363	3584	3804	4025	4246	221
97	4466	4687	4907	5127	5347	5567	5787	6007	6226	6446	220
198	6665	6884	7104	7323	7542	7761	7979	8198	8416	8635	219
199	8853	9071	9289	9507	9725	9943	.161	.378	.595	.813	218
200	301030	1247	1464	1681	1898	2114	2331	2547	2764	2980	217
201											
202	3196	3412 5566	3628	3844	4059	4275	4491	4706	4921	5136	216
02	5351		5781	5996	6211	6425	6639	6854	7068	7282	218
	7496	7710	7924	8137	8351	8564	8778	8991	9204	9417	213
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300	3867	4078	4289	4499	4710	4920	5130	5340	5551	5760	210
07	5970	6180	6390	6599	6809	7018	7227	7436	7646	7854	209
808	8063	8272	8481	8689	8898	9106	9314	9522	9730	9938	208
209	320146	0354	0562	0769	0977	1184	1391	1598	1805	2012	207
10	322219	2426	2633	2839	3046	3252	3458	3665	3871	4077	206
11	4282	4488	4694	4899	5105	5310	5516	5721	5926	6131	20
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13	8380	8583	8787	8991	9194	9398	9601	9805		.211	203
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215	2438	2640	2842	3044	3246	3447	3649	3850	4051		
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222	6353	6549	6744	6939	7135	7330	7525	7720	7915	8110	195
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226	4108	4301	4493	4685	4876	5068	5260	5452	5643	5834	192
227	6026	6217	6408	6599	6790	6981	7172	7363	7554	7744	191
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231	3612	3800	3988	4176	4363	4551	4739	4926	5113	5301	188
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237	4748	4932	5115	5298	5481	5664	5846	6029	6212	6394	18:
238	6577	6759	6942	7124	7306	7488	7670	7852	8034	8216	183
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241	2017	2197	2377	2557	2737	2917	3097	3277	3456	3636	180
242	3815	3995	4174	4353	4533	4712	4891	5070	5249	5428	179
243	5606	5785	5964	6142	6321	6499	6677	6856	7034	7212	178
244	7390	7568	7746	7923	8101	8279	8456	8634	8811	8989	178
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246	390935	1112	1288	1464	1641	1817	1993	2169	2345	2521	170
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248	4452	4627	4802	4977	5152	5326	5501	5676	5850	6025	17
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250	397940	8114	8287	8461	8634	8808	8981	9154	9328	9501	173
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252	401401	1573	1745	.192	2089	2261	$\frac{.711}{2433}$.883 2605		$\frac{1228}{2949}$	173
253	3121	3292	3464	1917		3978			2777		
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257	9933	.102	.271	.440	.609	.777	.946	1114	1283	1451	169
258	411620	1788	1956	2124	2293	2461	2629	2796	2964	3132	168
259	3300	3467	3635	3803	3970	4137	4305	4472	4639	4806	167
260	414973	5140	-5307	5474	5641	5808	5974	6141	6308	6474	167
261	6641	6807	6973	7139	7306	7472	7638	7804	7970	8135	166
262	8301	8467	8633	8798	8964	9129	9295	9460	9625	9791	165
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264	421604	1768	1933	2097	2261	2426	2590	2754	2918	3082	164
265	3246	3410	3574	3737	3901	4065	4228	4392	4555	4718	164
266	4882	5045	5208	5371	5534	5697	5860	6023	6186	6349	163
267	6511	6674	6836	6999	7161	7324	7486	7648	7811	7973	162
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270	431364	1525	1685	1846	2007	$\frac{1}{2167}$	2328	2488	2649	2809	161
271	2969	3130	3290	3450	3610	3770					
272							3930	4090	4249	4409	160
	4569	4729	4888	5048	5207	5367	5526	5685	5844	6004	159
273	6163	6322	6481	6640	6798	6957	7116	7275	7433	7592	159
274	7751	7909	8067	8226	8384	8542	8701	8859	9017	9175	158
275	9333	9491	9648	9806	9964	.122	.279	.437	.594	.752	158
276	440909	1066	1224	1381	1538	1695	1852	2009	2166	2323	157
277	2480	2637	2793	2950	3106	3263	3419	3576	3732	3889	157
278	4045	4201	4357	4513	4669	4825	4981	5137	5293	5449	156
279	5604	5760	5915	6071	6226	6382	6537	6692	6848	7003	155

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	1786	1940	2093	2247	2400	2553	2706	2859	3012	3165	153
284	3318	3471	3624	3777	3930	4082	4235	4387	4540	4692	153
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293	6868	7016	7164	7312	7460	7608	7756	7904	8052	8200	148
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295	9822	9969	.116	.263	.410	.557	.704	.851	.998	1145	147
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297	2756	2903	3049	3195	3341	3487	3633	3779	3925	4071	146
298	4216	4362	4508	4653	4799	4944	5090	5235	5381	5526	146
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301	8566	8711	8855	8999	9143	9287	9431	9575	9719	9863	144
302	480007	0151	0294	0438	0582	0725	0869	1012	1156	1299	144
303	1443	1586	1729	1872	2016	2159	2302	2445	2588	2731	143
304	2874	3016	3159	3302	3445	3587	3730	3872	4015	4157	143
305	4300	4442	4585	4727	4869	5011	5153	5295	5437	5579	145
		5863	6005	6147	6289	6430	6572	6714	6855	6997	145
306	5721				7704			8127			
307	7138	7280	7421	7563		7845	7986		8269	8410	14
308	8551	8692	8833	8974	9114	9255	9396	9537	9677	9818	14
309	9958	.:99	.239	.380	.520	.661	.801	.941	1081	1222	140
310	491362	1502	1642	1782	1922	2062	2201	2341	2481	2621	140
311	2760	2900	3040	3179	3319	3458	3597	3737	3876	4015	139
312	4155	4294	4433	4572	4711	4850	4989	5128	5267	5406	139
313	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791	139
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394	5496	5606	5717	5827	5937	6047	6157	6267	6377	6487	110
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118	1176					1695	1799	1903	2007	2110	104
119	2214	2318	2421	2525		2732	2835	2939	3042	3146	104
120	623249	3353	3456	3559	3663	3766	3869	3973	4076	4179	103
121	4282	4385	4488	4591	4695	4798	4901	5004		5210	103
122	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238	103
123	6340		6546			6853	6956	7058	7161	7263	103
124	7366		7571	7673		7878	7980	8082	8185	8287	102
125	8389		8593			8900	9002	9104	9206	9308	102
426 427	$9410 \\ 630428$		9613 0631	9715 0733	9817	9919	21	.123	.224	.326	102
128	1444		1647	1748	$0835 \\ 1849$	$0936 \\ 1951$	$\frac{1038}{2052}$	1139	1241 2255	1342	102
129	2457	2559	2660	2761	2862	2963	3064	2153 3165	3266	2356 3367	101 101
130	633468	3569	3670	3771	3872	3973	4074	_	-	-	-
131	4477	4578	4679	4779	4880	4981	5081	4175 5182	4276 5283	4376 5383	100
132	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388	100
133	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390	100
134	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389	99
135	8489	8589	8689	8789	8888	8988	9088	9188	9287	9387	99
136	9486	9586	9686	9785	9885	9984	84	.183	.283	.382	99
137	640481	0581	0680	0779	0879	0978	1077	1177	1276	1375	99
138 139	1474 2465	$\frac{1573}{2563}$	$\frac{1672}{2662}$	1771	1871	1970	2069	2168	2267	2366	99
_	-	-		2761	2860	2959	3058	3156	3255	3354	99
140	643453	3551	3650	3749	3847	3946	4044	4143	4242	4340	98
141 142	4439 5422	4537 5521	4636 5619	4734	4832	4931	5029	5127	5226	5324	98
143	6404	6502	6600	5717 6698	5815 6796	5913 6894	$6011 \\ 6992$	$6110 \\ 7089$	$6208 \\ 7187$	6306	98
144	7383	7481	7579	7676	7774	7872	7969	8067	8165	7285 8262	98
145	8360	8458	8555	8653	8750	8848	8945	9043	9140	9237	97
146	9335	9432	9530	9627	9724	9821	9919	16	.113	.210	97
147	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181	97
148	1278	1375	1472	1569	1666	1762	1859	1956	2053	2150	97
149	2246	2343	2440	2536	2633	2730	2826	2923	3019	3116	97
150	653213	3309	3405	3502	3598	3695	3791	3888	3984	4080	96
151	4177	4273	4369	4465	4562	4658	4754	4850	4946	5042	96
152	5138	5235	5331	5427	5523	5619	5715	5810	5906	6002	96
153	6098	6194	6290	6386	6482	6577	6673	6769	6864	6960	96
154	7056 8011	7152 8107	7247 8202	7343	7438	7534	7629	7725	7820	7916	96
156	8965	9060	9155	8298 9250	8393	8488	8584	8679	8774	8870	95
157	9916	11	.106	.201	9346	9441	$9536 \\ .486$	9631	9726	9821	95 95
158	660865	0960	1055	1150	1245	1339	1434	1529	1623	.771 1718	95
159	. 1813	1907	2002	2096	2191		2380	2475	2569	2663	95
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176	0	and and	2	3	4	5	6	7	8	9	D.

A TABLE OF LOGARITHMS FROM 1 TO 10,000.

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460	662758	2852	2947	3041	3135	3230	3324	3418	3512	3607	94
461	3701	3795	3889	3983	4078	4172	4266	4360	4454	4548	94
462	4642	4736	4830	4924	5018	5112	5206	5299	5393	5487	-94
463	5581	5675	5769	5862	5956	6050	6143	6237	6331	6424	94
464	6518	6612	6705	6799	6892	6986	7079	7173	7266	7360	94
165	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293	93
466	8386	8479	8572	8665	8759	8852	8945	9038	9131	9224	93
467	9317	9410	9503	9596	9689	9782	9875	9967	60	.153	93
468	670241	0339					0802	0895	0988	1080	
469			0431	0524	0617	0710				2005	93
	1173	1265	1358	1451	1543	1636	1728	1821	1913	-	93
470	672098	2190	2283	2375	2467	2560	2652	2744	2836	2929	92
471	3021	3113	3205	3297	3390	3482	3574	3666	3758	3850	92
472	3942	4034	4126	4218	4310	4402	4494	4586	4677	4769	92
473	4861	4953	5045	5137	5228	5320	5412	5503	5595	5687	92
474	5778	5870	5962	6053	6145	6236	6328	6419	6511	6602	92
475	6694	6785	6876	6968	7059	7151	7242	7333	7424	7516	91
476	7607	7698	7789	7881	7972	8063	8154	8245	8336	8427	91
477	8518	8609	8700	8791	8882	8973	9064	9155	9246	9337	91
478	9428	9519	9610	9700	9791	9882	9973	63	.154	.245	91
479	680336	0426	0517	0607	0698	0789	0879	0970	1060	1151	91
480	681241	1332	1422	1513	1603	1693	1784	1874	1964	2055	90
			0206	2416			2686				
481	2145	2235	2326		2506	2596		2777	2867	2957	90
482	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857	90
483	3947	4037	4127	4217	4307	4396	4486	4576	4666	4756	90
484	4845	4935	5025	5114	5204	5294	5383	5473	5563	5652	90
485	5742	5831	5921	6010	6100	6189	6279	6368	6458	6547	88
486	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440	88
487	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331	88
488	8420	8509	8598	8687	8776	8865	8953	9042	9131	9220	89
489	9309	9398	9486	9575	9664	9753	9841	9930	19	.107	89
490	690196	0285	0373	0462	0550	0639	0728	0816	0905	0993	89
491	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877	88
492	1965	2053	2142	2230	2318	2406	2494	2583	2671	2759	88
493	2847	2935	3023	3111	3199	3287	3375	3463	3551	3639	88
494	3727	3815	3903	3991	4078	4166	4254	4342	4430	4517	88
495	4605	4693	4781	4868	4956	5044	5131	5219	5307	5394	88
496	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269	87
497	6356	6444	6531	6618	6706	6793	6880	6968	7055	7142	87
498	7229	7317	7404	7491	7578	7665	7752	7839	7926	8014	87
499	8101	8188	8275	8362	8449						
				_		8535	8622	8709	8796	8883	87
500	698970	9057	9144	9231	9317	9404	9491	9578	9664	9751	87
501	9838	9924	11	98	.184	.271	.358	.444	.531	.617	87
502	700704	0790	0877	0963	1050	1136	1222	1309	1395	1482	86
503	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344	86
504	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205	86
505	3291	3377	3463	3549	3635	3721	3807	3895	3979	4065	86
506	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922	86
507	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778	86
508	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632	8
509	6718	6803	6888	6974	7059	7144	2229	7315	7400	7485	8
510	707570	7655	7740	7826	7911	7996	8081	8166	8251	8336	8
511	8421	8506	8591	8676	8761						
512	9270					8846	8931	9015	9100	9185	8
513	710117	9355	9440	9524	9609	9694	9779	9863	9948	33	8
514		0202	0287	0371	0456	0540	0625	0710	0794	0879	88
515	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723	84
	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566	84
516	2650	2734	2818	2902	2986	3070	3154	3238	3323	3407	84
517	3491	3575	3650	3742	3826	3910	3994	4078	4162	4246	84
518	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084	84
519	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920	84
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520	716003	6087	6170	6254	6337	6421	6504	6588	6671	6754	83
521	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587	83
522	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419	83
523	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248	83
524	9331	9414	9497	9580	9663	9745	9828	9911	9994	77	83
525	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903	83
526	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728	82
527	1811	1893	1975	2058	2140	2222	2305	2387	2469	2552	82
528	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374	82
529	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194	82
	-		-	7	-	_			-	120/27	-
530	724276	4358	4440	4522	4604	4685	4767	4849	4931	5013	82
531	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830	82
532	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646	82
533	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460	81
534	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273	81
535	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084	81
536	9165	9246	9327	9408	9489	9570	9651	9732	9813	9893	81
37	9974	55	.136	.217	.298	.378	.459	.540	.621	.702	81
538	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508	81
	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313	81
539		_	_		-	-	-	-		-	-
540	732394	2474	2555	2635	2715	2796	2876	2956	3037	3117	80
541	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919	80
542	3999	4.079	4160	4240	4320	4400	4480	4560	4640	4720	. 80
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519	80
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317	80
545	6397	6476	6556	6635	6715	6795	6874	6954	7034	7113	80
546	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908	79
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701	79
	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493	79
548								.126			79
549	9572	9651	9731	9810	9889	9968	47	-	.205	.284	-
550	740363	0442	0521	0600	0678	0757	0836	0915	0994	1073	79
551	1152	1230	1309	1388	1467	1546	1624	1703	1782	1860	79
552	1939	2018	2096	2175	2254	2332	2411	2489	2568	2646	79
553	2725	2804	2882	2961	3039	3118	3196	3275	3353	3431	78
554	3510	3588	3667	3745	3823	3902	3980	4058	4136	4215	78
555	4293	4371	4449	4528	4606	4684	4762	4840	4919	4997	78
556	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777	78
557	5855	5933	6011	6089	6167	6245	6323	6401	6479	6556	78
	6634	6712	6790	6868	6945	7023	7101	7179	7256	7334	78
558					7722	7800	7878	7955	8033	8110	78
559	7412	7489	7567	7645		_	-	-		-	_
560	748188	8266	8343	8421	8498	8576	8653	8731	8808	8885	77
561	8963	9040	9118	9195	9272	9350	9427	9504	9582	9659	77
562	9736	9814	9891	9968	45	.123	.200	.277	.354	.431	77
563	750508	0586	0663	0740	0817	0894	0971	1048	1125	1202	77
564	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972	77
565	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740	77
566	2816	2893	2970	3047	3123	3200	3277	3353	3430	3506	7
	3583	3660	3736	3813	3889	3966	4042	4119	4195	4272	7
567			4501		4654	4730	4807	4883	4960	5036	76
568	4348	4425		4578							
569	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799	70
570	755875	5951	6027	6103	6180	6256	6332	6408	6484	6560	71
571	6636	6712	6788	6864	6940	7016	7092	7168	7244	7320	7
572	7396	7472	7548	7624	7700	7775	7851	7927	8003	8079	71
573	8155	8230	8306	8382	8458	8533	8609	8685	8761	8836	70
574	8912	8988	9063	9139	9214	9290	9366	9441	9517	9592	7
						45	.121	.196	.272	.347	7
575	9668	9743	9819	9894	9970						
576	760422	0498	0573	0649	0724	0799	0875	0950	1025	1101	7
577	1176	1251	1326	1402	1477	1552	1627	1702	1778	1853	7
578	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604	7
579	2679	2754	2829	2904	2978	3053	3128	3203	3278	3353	7.
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580	763428	3503	3578,	3953	3727.	3802	3877	3952	4027	4101	75
581	4176	4251	4326	4400	4475	4550	4624	4699	4774	4848	75
582	4923	4998	5072	5147	5221	5296	5370	5445	5520	5594	75
583	5669	5743	5818	5892	5966	6041	6115	6190	6264	6338	74
584	6413	6487	6562	6636	6710	6785	6859	6933	7007	7082	74
585	7156	7230	7304	7379	7453	7527	.7601	7675	7749 8490	7823 8564	74 74
586	7898	7972	8046	8120	8194	8268 9008	8342 9082	8416 9156	9230	9303	74
587	8638	8712	8786	8860 9599	8934 9673	9746	9820	9894	9968	42	74
588	9377	9451	9525 0263	0336	0410	0484	0557	0631	0705	0778	74
589	770115	0189					1293	$\frac{3367}{1367}$	1440	1514	74
590	770852	0926	0999	1073	1146	$1220 \\ 1955$		2102	2175	2248	73
591	1587	1661	1734	$1808 \\ 2542$	$\frac{1881}{2615}$	2688		2835	2908	2981	73
592	2322	2395 3128	2468 3201	3274	3348	3421	3494	3567	3640	3713	73
593 594	3055 3786	3860	3933	4006	4079	4152	4225	4298	4371	4444	73
595	4517	4590	4663	4736	4809	4882		5028	5100	5173	73
596	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902	73
597	5974	6047	6120	6193	6265	6338	6411	6483	6556	6629	73
598	6701	6774	6846	6919	6992	7064	7137	7209	7282	7354	73
599	7427	7499	7572	7644	7717	7789	7862	7934	8006	8079	72
600	778151	8224	8296	8368	8441	8513	8585	8658	8730	8802	72
601	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524	72
602	9596	9669	9741	9813	9885	9957	29	.101	.173	.245	72
603	780317	0389	0461	0533	0605	0677	0749	0821	0893	0965	72
604	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684	72
605	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401	72
606	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117	72 71
607	3189	3260	3332	3403	3475	3546	3618	3689 4403	3761 4475	3832 4546	71
608	3904	3975	4046	4118 4831	4189 4902	$\frac{4261}{4974}$	4332 5045	5116	5187	5259	71
609	4617	4689	4760							5970	71
610	785330	5401	5472	5543	5615	5686	5757 6467	5828 6538	5899 6609	6680	71
611	6041	6112	6183	$6254 \\ 6964$	6325 7035	6396 7106	7177	7248	7319	7390	71
612 613	6751	6822 7531	6893 7602	7673	7744	7815	7885	7956	8027	8098	71
614	7460	8239	8310	8381	8451	8522	8593	8663	8734	8804	71
615	8168 8875	8946	9016	9087	9157	9228	9299	9369	9440	9510	71
616	9581	9651	9722	9792	9863	9933	4	74	.144	.215	70
617	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918	70
618	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620	70
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322	70
620	792392	2462	2532	2602	2672	2742	2812	2882	2952	3022	70
621	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721	70
622	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418	70
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115	70
624	5185	5254	5324	5393	5463	5532	5602	5672	5741	5811	70
625	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505	69
626	6574	6644	6713	6782	6852	6921	6990	7060	7129 7821	7198 7890	69 69
627	7268	7337	7406	7475	7545 8236	$7614 \\ 8305$	$7683 \\ 8374$	7752 8443	8513	8582	69
628	7960	8029 8720	$8098 \\ 8789$	8167 8858	8927	8996	9065	9134	9203	9272	69
$\frac{629}{629}$	8651								9892	9961	69
630	799341	9409	9478	9547	9616	9685 0373	9754 0442	9823 0511	0580	0648	69
631	800029	0098	0167	$0236 \\ 0923$	0305 0992	1061	1129	1198	1266	1335	69
632 633	0717 1404	0786 1472	0854 1541	1609	1678	1747	1815	1884	1952	2021	69
634	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705	69
635	2774	2842	2910	2979	3047	3116	3184	3252	3321	3389	68
636	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071	68
637	4139	4208	4276	4344		4480	4548	4616	4685	4753	68
638	4821	4889	4957	5025	5093	5161	5229	5297	5365	5433	68
639	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112	68
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640	806180	6248	6316	6384	6451	6519	6587	6655	6723	.67901	68
641	6858	6926	6994	7061	7129	7197	7264	7332	7400	7467	68
642	7535	7603	7670	7738	7806	7873	7941	8008	8076	8143	68
643	8211	8279	8346	8414	8481	8549	8616	8684	8751	8818	67
644	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492	67
645	9560	9627	9694	9762	9829	9896	9964	31	98	.165	67
646	810233	0300	0367	0434	0501	0569	0636	0703	0770	0837	67
647	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508	67
648	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178	67
649	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847	67
650	812913	2980	3047	3114	3181	3247	3314	3381	3448	3514	67
	3581	3648	3714	3781	3848	3914	3981	4048	4114	4181	67
651											
652	4248	4314	4381	4447	4514	4581	4647	4714	4780	4847	6
653	4913	4980	5046	5113	5179	5246	5312	5378	5445	5511	66
654	5578	5644	5711	5777	5843	5910	5976	6042	6109	6175	60
655	6241	6308	6374	6440	6506	6573	6639	6705	6771	6838	66
656	6904	6970	7036	7102	7169	7235	7301	7367	7433	7499	66
657	7565	7631	7698	7764	7830	7896	7962	8028	8094	8160	66
658	8226	8292	8358	8424	8490	8556	8622	8688	8754	8820	66
659	8885	8951	9017	9083	9149	9215	9281	9346	9412	9478	66
660	819544	9610	9676	9741	9807	9873	9939	4	70	.136	66
	820201	0267				0530	0595	0661	0727	0792	66
661			0333	0399	0464				1382		
662	0858	0924	0989	1055	1120	1186	1251	1317		1448	66
663	1514	1579	1645	1710	1775	1841	1906	1972	2037	2103	6
664	2168	2233	2299	2364	2430	2495	2560	2626	2691	2756	64
665	2822	2887	2952	3018	3083	3148	3213	3279	3344	3409	6
666	3474	3539	3605	3670	3735	3800	3865	3930	3996	4061	64
667	4126	4191	4256	4321	4386	4451	4516	4581	4646	4711	6
668	4776	4841	4906	4971	5036	5101	5166	5231	5296	5361	6
669	5426	5491	5556	5621	5686	5751	5815	5880	5945	6010	65
670	826075	6140	6204	6269	6334	6399	6464	6528	6593	6658	65
671	6723	6787	6852	6917	6981	7046	7111	7175	7240	7305	64
672	7369	7434	7499	7563	7628	7692	7757	7821	7886	7951	6
673	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595	64
674	8660	8724	8789	8853	8918	8982	9046	9111	9175	9239	64
675	9304	9368	9432	9497	9561	9625	9690	9754	9818	9882	64
676				.139		.268	.332	.396	.460	.525	64
	9947	11	75		.204		0973	1037	1102	1166	64
677	830589	0653	0717	0781	0845	0909					
678	1230	1294	1358	1422	1486	1550	1614	1678	1742	1806	64
679	1870	1934	1998	2062	2126	2189	2253	2317	2381	2445	64
680	832509	2573	2637	2700	2764	2828	2892	2956	3020	3083	64
681	3147	3211	3275	3338	3402	3466	3530	3593	3657	3721	64
682	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357	64
683	4421	4484	4548	4611	4675	4739	4802	4866	4929	4993	64
684	5056	5120	5183	5247	5310	5373	5437	5500	5564	5627	6:
685	5691	5754	5817	5881	5944	6007	6071	6134	6197	6261	6:
686	6324	6387	6451	6514	6577	6641	6704	67.67	6830	6894	6
687	6957	7020	7083	7146	7210	7273	7336	7399	7462	7525	6:
688	7588	7652	7715	7778	7841	7904	7967	8030	8093	8156	68
689	8219	8282	8345	8408	8471	8534	8597	8660	8723	8786	68
-		_	-		-	-	-		-	-	
690	838849	8912	8975	9038	9101	9164	9227	9289	9352	9415	6
691	9478	9541	9604	9667	9729	9792	9855	9918	9981	43	63
692	840106	0169	0232	0294	0357	0420	0482	0545	0608	0671	63
693	0733	0796	0859	0921	0984	1046	1109	1172	1234	1297	63
694	1359	1422	1485	1547	1610	1672	1735	1797	1860	1922	63
695	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547	65
696	2609	2672	2734	2796	2859	2921	2983	3046	3108	3170	65
697	3233	3295	3357	3420	3482	3544	3606	3669	3731	3793	65
698	3855	3918	3980	4042	4104	4166	4229	4291	4353	4415	65
699	4477	4539	4601		4726			4912	4974		65
200		1000			-	21001				-	-
N.	0	1	2	3	4	5	6	7	8	9	D.

N.	0	1	2	3	1.4	5	6	7	8	9	D.
700	1845098	5160	5222	5284	5346	1.5408	5470	5532	5594	15656	62
701	5718					6028	6090	6151	6213		62
702	6337			6523			6708	6770	6832	6894	62
703	6955		7079		7202		7326	7388	7449		62
704	7573		7696			7881	7943	8004	8066	8128	62
705	8189	8251	8312			8497	8559	8620	8682	8743	62
706	8805		8928			9112	9174	9235	9297	9358	61
707	9419	9481	9542			9726	9788	9849	9911	9972	61
708	850033	0095	0156			0340	0401	0462	0524		61
709	0646	0707	0769		-	0952	1014	1075	1136	1197	61
710	851258	1320	1381	1442	1503	1564	1625	1686	1747	1809	61
711	1870	1931	1992	2053	2114	2175	2236	2297	2358	2419	61
712	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029	61
713	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637	61
714	3698	3759	3820	3881	3941	4002	4063	4124	4185		61
715	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852	61
716	4913	4974	5034	5095	5156	5216	5277	5337	5398		61
717	5519	5580	5640	5701	5761	5829	5882	5943	6003		61
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668	.60
719	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272	60
720	857332	7393	7453	7513	7574	7634	7694	7755	7815	7875	60
721	7935	7995	8056	8116	8176	8236	8297	8357	8417	8477	60
722	8537	8597	8657	8718	8778	8838	8898	8958	9018	9078	60
723	9138	9198	9258	9318	9379	9439	9499	9559	9619	9679	60
724	9739	9799	9859	9918	9978	38	98	.158	.218	.278	60
725	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877	60
726	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475	60
727	1534	1594	1654	1714	1773	1833	1893	1952	2012	2072	60
728	2131	2191	2251	2310	2370	2430	2489	2549	2608	2668	60
729	2728	2787	2847	2906	2966	3025	3085	3144	3204	3263	.60
730	863323	3382	3442	3501	3561	3620	3680	3739	3799	3858	59
731	3917	3977	4036	4096	4155	4214	4274	4333	4392	4452	59
732	4511	4570	4630	4689	4748	4808	4867	4926	4985	5045	59
733	5104	5163	5222	.5282	5341	5400	5459	5519	5578	5637	59
734	5696	5755	5814	5874	5933	5992	6051	6110	6169	6228	59
735	6287	6346	6405	6465	6524	6583	6642	6701	6760	6819	59
736	6878	6937	6996	7055	7114	7173	7232	7291	7350	7409	59
737	7467	7526	7585	7644	7703	7762	7821	7880	7939	7998	59
738	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586	59
739	8644	8703	8762	8821	8879	8938	8997	9056	9114	9173	59
740	869232	9290	9349	9408	9466	9525	9584	9642	9701	9760	59
741	9818	9877	9935	9994	53	.111	.170	.228	.287	.345	59
742	870404	0462	0521	0579	0638	0696	0755	0813	0872	0930	58
743	0989	1047	1106	1164	1223	1281	1339	1398	1456	1515	58
744	1573	1631	1690	1748	1806	1865	1923	1981	2040	2098	58
745	2156	2215	2273	2331	2389	2448	2506	2564	2622	2681	58
746	2739	2797	2855	2913	2972	3030	3088	3146	3204	3262	58
747	3321	3379	3437	3495	3553	3611	3669	3727	3785	3844	58
748	3902	3960	4018	4076	4134	4192	4250	4308	4366	4424	58
749	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003	58
750	875061	5119	5177	5235	5293	5351	5409	5466	5524	5582	58
751	5640	5698	5756	5813	5871	5929	5987	6045	6102	6160	58
752	6218	6276	6333	6391	6449	6507	6564	6622	6680	6737	58
753	6795	6853	6910	6968	7026	7083	7141	7199	7256	7314	58
754	7371	7429	7487	7544	7602	7659	7717	7774	7832	7889	58
755	7947	8004	8062	8119	8177	8234	8292	8349	8407	8464	57
756	8522	8579	8637	8694	8752	8809	8866	8924	8981	9039	57
757	9096	9153	9211	9268	9325	9383	9440	9497	9555	9612	57
758	9669	9726	9784	9841	9898	9956	13	70	.127	.185	57
759	8802421	0299	0356	0413	0471	0528	0585	0642	0699	0756	57
N.	0	1	2	3	4	5	6	7	8	9 1	D.

761 1985 1442 1499 1556 1613 1670 1727 763 2525 2581 2609 2126 2183 2240 2297 266 764 3093 3150 3207 3264 3321 3377 3434 266 4229 4285 4342 4399 4455 4512 4569 4666 4229 4285 4342 4399 4455 4512 4569 4666 767 4795 4852 4909 4965 5022 5078 5135 6676 668 5661 5418 5474 5531 5587 5644 5700 4666 6716 6773 6829 682 6666 6716 6773 6829 682 6784 7891 7894 7881 8874 8731 7882 7892 7883 8909 8965 9921 9077 7976 7882 8918 9974 .30 .86 141 1.97 7777	0 1797 17707 17709 17709 2896 2997 334 344 45700 5775 681 1997 1314 137 1415 1415 1415 1415 1415 1415 1415 141	7 8	9	D.
762 1955 2012 2069 2126 2183 2240 2297 264 764 3093 3150 3207 3264 3321 3377 3434 265 2661 3718 3775 3832 3888 3945 4002 4767 4795 4852 4909 4655 5022 5078 5135 567 664 5700 5986 6039 6096 6152 6209 6265 667 6716 6773 6829 6829 6860 6716 6773 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 6829 683 8944 9470 9526 9582 9638 9414 9470 9526 9582 9638 941 9470 9526 9582 9638 941 9470 9526 9582 9638 941 9470	9 2297 234 9 3296 299 9 3434 34 5 4002 406 2 4569 465 8 5135 519 9 6265 63 6 629 688 6 7392 744 8 7955 80 1 19077 91 2 9638 968 6 1872 24 9 2985 304 4 3540 358 2 429 24 4 3540 358 1 6306 630 2 7407 746 1 6306 630 2 7407 746 1 7957 80 1 8506 856 1 6306 630 2 7407 746 1 8506 856 1 6306 630 2 7407 746 1 8506 856 1 6306 630 2 7407 746 1 8506 856 1 6306 630 2 7407 746 1 8506 856 1 6504 965 1 6504 965 1 7734 775 7 9827 80 1 3416 347 4 3958 40 1 6658 67 3 7196 72 2 757 80 1 1 774 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	213 1271	1328	57
763 2525 2581 2688 2695 2752 2809 2866 2866 3207 3264 3321 3377 3434 3321 3377 3434 4002 4 4666 4229 4285 4342 4399 4455 54512 4569 4667 667 4795 4852 4909 4965 5022 5078 5135 6676 6676 6660 6660 6676 6776 5700 6265 6676 6776 6773 6829 6862 6660 66716 6776 6829 6265 66776 6773 6829 770 771 7054 7111 7167 7722 76617 7674 7730 7786 7842 7899 7336 7392 7360 7392 7362 7392 7360 8862 9918 9974 .30 .861 861 811 .197 777 789421 4477 0533 5899 9645 0700 7756 9821	9			57
763 2525 2581 2638 2695 2752 2809 2864 3 3377 3434 3 3377 3434 4 3321 3377 3434 4 3321 3377 3434 4 3661 3718 3775 3832 3888 3945 4002 4 4 4795 4852 4909 4965 5022 5078 5135 6 6676 6660 6660 6676 6776 5700 5 5022 5078 5135 6 6660 6676 6767 6773 6829 6 6660 66716 6776 6829 6 6660 6716 6773 6829 7 7777 7617 7674 7730 7786 7842 7898 7955 8 8 8404 8460 8516 8 7957 7777 7841 8777 70533 5589 9642 7898 7955 8 9638 9974 30 .864<	98 2866 299 7 3434 344 5 4402 409 5 4669 465 8 5135 515 9 6265 633 6 6829 668 8 7955 807 0 8516 857 0 9754 809 1 1197 .25 9 638 965 1 .197 .25 9 638 965 1 .197 .25 9 638 965 1 .197 .25 9 638 965 1 .197 .25 9 638 965 1 .197 .25 1	354 2411	2468	57
764 3093 3150 3207 3264 3321 3377 3434 5766 4229 4285 4342 4399 4455 4512 4569 4 666 4229 4285 4342 4399 4455 4512 4569 4 666 667 6767 5361 5418 5474 5531 5587 5644 5700 6 669 66152 6209 6265 6 6 660 6716 673 6829 6 6660 6716 6773 6829 6 6772 7836 7392 736 7392 736 7392 736 7392 736 7392 736 7392 736 7392 736 7392 736 7842 7898 7895 884 8404 8460 8516 8 781 8741 8797 7583 9899 9865 9921 9077 777 7778 89621 9918 9974 .30 .86 <	73 3434 344 74 3402 406 75 4002 406 75 4002 406 75 4002 406 75 4000 575 75 400 77 91 75 200 6754 75 400 77 91 75 200 6754 75 600 77 91 75 600 77 91 75 600 77 91 75 70 77 80 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 77 827 0 77 77 827 0 77 77 77 827 0 77 77 78 827 0 77 74 77 78 827 0 77 74 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 77 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 78 827 0 77 77 77 827 0 77 77 78 827 0 77 77 77 827 0 77 77 78 827 0 77 77 77 827 0 77 77 78 827 0 77 77 78 827 0 77 77 77 827 0 77 77 827 0 77 77 77 827 0 77 77 827 0 77 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 827 0 77 77 77 827 0 77 7			57
766 4229 4285 4342 4399 4455 4512 4569 768 5361 5418 5474 5531 5587 5644 5700 8 769 5926 5983 6039 6096 6152 6209 6265 6 770 86491 6547 6604 6660 6716 6773 6829 6 772 7617 7674 7730 7786 7842 7898 7955 8 774 8741 8797 8853 8909 8965 9021 9077 9 775 9302 9358 9414 9470 9526 9582 9638 9 9682 9918 9974 .30 .861 141 197 1977 7778 890421 0477 0533 5589 6645 0700 0756 6 9829 5206 2262 2317 2373 2429 2 7881 2651 2707	2 4569 465 8 5135 513 8 6226 683 8 6829 688 8 7955 801 0 1516 7992 744 8 7955 802 0 1516 91314 137 6 1872 1993 2 2429 248 9 2985 304 4 3540 355 9 4094 415 3 4648 477 6 5201 525 9 5754 586 6 5040 505 1 1785 184 5 2429 148 8 7957 801 1 8506 856 6 1240 122 1 1785 184 5 2529 238 8 2873 292 1 3416 347 4 3958 401 4 3958 401 6 658 67 7 9602 966 6 5580 566 6 6119 61 6 6140 509 6 6 6140 509 6 6 619 7 9602 966 7 9602 966 8 2873 292 8 2873 292 8 2873 293 8 2874 293 8 2875 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293			57
766 4229 4285 4342 4399 4455 4512 4569 768 5361 5418 5474 5531 5587 5644 5700 8 769 5926 5983 6039 6096 6152 6209 6265 6 770 86491 6547 6604 6660 6716 6773 6829 6 772 7617 7674 7730 7786 7842 7898 7955 8 774 8741 8797 8853 8909 8965 9021 9077 9 775 9302 9358 9414 9470 9526 9582 9638 9 9682 9918 9974 .30 .861 141 197 1977 7778 890421 0477 0533 5589 6645 0700 0756 6 9829 5206 2262 2317 2373 2429 2 7881 2651 2707	2 4569 465 8 5135 513 8 6226 683 8 6829 688 8 7955 801 0 1516 7992 744 8 7955 802 0 1516 91314 137 6 1872 1993 2 2429 248 9 2985 304 4 3540 355 9 4094 415 3 4648 477 6 5201 525 9 5754 586 6 5040 505 1 1785 184 5 2429 148 8 7957 801 1 8506 856 6 1240 122 1 1785 184 5 2529 238 8 2873 292 1 3416 347 4 3958 401 4 3958 401 6 658 67 7 9602 966 6 5580 566 6 6119 61 6 6140 509 6 6 6140 509 6 6 619 7 9602 966 7 9602 966 8 2873 292 8 2873 292 8 2873 293 8 2874 293 8 2875 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293 8 2877 293			57
767 4795 4852 4909 4965 5022 5078 5135 8 769 5926 5983 6039 6096 6152 6209 6265 6 770 7054 7111 7167 7223 7280 7336 7392 7 772 7617 7674 7730 7786 7842 7898 7925 8 773 8179 8236 8292 8348 8404 8460 8516 8 775 9302 9358 9414 9470 9526 9582 9638 9 974 .30 .86 .141 .197 .90 .776 9862 9918 9974 .30 .86 .141 .197 .90 .777 7890421 10477 533 0589 0645 0700 0756 688 9918 9974 .30 .86 .141 .197 .93 141 .197 .93 .818 .381	8 5135 514 4 5700 573 3 6829 688 6 7392 744 8 7955 801 0 8516 857 1 9077 913 2 9638 968 1 .197 .25 0 0 756 081 1 872 192 3 2429 244 3 2409 244 3 3540 358 9 4094 415 3 4648 757 9 5754 586 6 5201 525 9 5754 586 6 5201 525 9 5754 586 1 6306 633 2 6857 691 1 8506 856 9 9054 916 1 1785 184 1 149 .22 0 0 695 077 6 1240 128 1 1785 184 1 3416 347 4 3958 401 1 1785 184 1 3416 347 1 3416			57
769 5361 5418 5474 5531 5644 5700 6209 6209 6209 6209 6209 6209 6209 6209 6209 6205 6209 6205 6209 6205 6209 6209 6205 6209 6205 6209 6205 6209 6205 6209 6205 6209 6205 6209 7736 7822 7842 7898 7936 7336 7392 7736 7730 7786 7842 7898 7955 8516 88 7844 8460 8516 8516 88 7842 7898 7955 9638 9645 9021 9077 990 9862 9918 9974 30 86 141 197 777 776 9862 9918 9974 30 86 141 197 777 778 99042 1047 70533 0589 0645 0700 0756 06 782 7831 141 1203 1	4 5700 577 9 6265 632 6826 682 688 687392 744 87955 801 9077 913 29638 968 11977 22 29838 968 314 137 32 2429 2429 248 3404 3540 35 3648 470 65201 525 7407 27957 801 1 8506 856 2 7407 744 2 7957 801 1 1795 724 2 7957 801 1 1795 184 2 2398 2873 3 81 2873 3 828 2873 3 828 2873 3 844 344 4 3958 405 6 619 617 7 734 37196 3 7196 <td></td> <td></td> <td>57</td>			57
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	- 14	823	5	400	545			5030 5558	50		5136	51	89	5241	52	94 5	347	53
		824		927	5980			6085	56 61:		6664			5769		22 5	875	53
		825	6	454	6507	65		6612	666		717			6296	634	19 6	401	53
		326		980	7033		85	7138	719		243	72		$6822 \\ 7348$	68		927	53
		28		506	7558	1		7663	771	16 7	768	78		7873	740		453	53
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		_	9190		-	-		712	876	_	816	88	69 8	3921	897		026	52 52
		31			$\frac{9130}{9653}$	918		235	928		340	939		1444	949		549	52
			9201		0176	970	0 9	$\begin{array}{c} 758 \\ 280 \end{array}$	981		862	991		967	1	4	.71	52
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		34		66	1218	127			137		$906 \\ 126$	095		010	106	2 1	114	52
		35 36			1738	179	0 1		189		946	147 199		530	158		334	52
		37			2258	231	0 2	362	241			251		050 570	210: 262:		54	52
		38	27 32		2777	282			293	3 29	185	303			314(74 92	52
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	84		242		331			-	3969	_		407	2 4		4176		28	52
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	84		585	28 5		593			034			562			725		76	52
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	84		685			6959		11 7	062		- 21	16:			$\begin{array}{c} 754 \\ 268 \end{array}$		05	51
	84		737 788			7473			576	76	27 7	678	3 77		781	73 78:		51
	84		839			7986 3498		-	880	814	10 8	191	82		293	834		51
	84	9	890			0010			601	86		703	87	54 8	805	885		51 51
- 1	85		2941	_		521	95		112	916	_	215		66 9	317	936	- 1	51
	85	1	993	0 99	81	.32	95		$\frac{623}{134}$	967		725			827	987		51
	85		044	0 04		542	059		343	069		236			338	.38		51
	853 854		094			051	110		153	120		$\frac{745}{254}$			847	089	8	51
ı	855		145			560	161	0 16	661	171	2 1	763	130		356	140		51
1	856		$\frac{1960}{2474}$			068	211		69	229	0 96	271	232		365 372	$\frac{191}{242}$		51
1	857		298	30		$\begin{array}{c} 575 \\ 082 \end{array}$	$\frac{262}{313}$		77	272	7 27	778	282			293	-	1
1	858		3487			589	363		83 90	323		285	333	5 33		343		1
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	365		016	706			666		15 6	6765	68	15	686			6463		
	366		518	756			7167			7267	73	17	736			7468		
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	369		020	907	0 91		170		- 1 -	270	932		8870 9369			3970	50	
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8	74		511	156			163	121	3 1	263	131		362	141		$\frac{964}{462}$	50	1
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N.	0	1	2	3	4	5	6	7	8	9	D.
880	944483	4532	4581	4631	4680	14729	4779	4828	4877	4927	49
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	4
882	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912	4
883	5961	6010	6059	6108	6157	6207	6256	6305	6354	6403	4
884	6452	6501	6551	6600	6649	6698	6747	6796	6845	6894	4
885	6943	6992	7041	7090	7140	7189	7238	7287	7336	7385	4
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	4
887	7924	7973	8022	8070	8119	8168	8217	8266	8315	8364	4
888	8413	8462	8511	8560	8609	8657	8706	8755	8804	8853	4
889	8902	8951	8999	9048	9097	9146	9195	9244	9292	9341	
200.00	-	-	-	107	1	-	Commence of	-	-	(months	4
890	949390	9439	9488	9586	9585	9634	9683	9731	9780	9829	4
891	9878	9926	9975	24	73	.121	.170	.219	.267	.316	4
892	950365	0414	0462	0511	0560	0608	0657	0706	0754	0803	4
893	0851	0900	0949	0997	1046	1095	1143	1192	1240	1289	4
894	1338	1386	1435	1483	1532	1580	1629	1677	1726	1775	4
895	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260	4
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	4
897	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228	4
898	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711	4
899	3760	3808	3856	3905	3953	4001	4049	4098	4146	4194	4
900	954243	4291	4339	4387	$\frac{3435}{4435}$	4484	4532	4580	4628	-	-
901	4725									4677	4
		4773	4821	4869	4918	4966	5014	5062	5110	5158	4
902	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640	4
903	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120	4
904	6168	6216	6265	6313	6361	6409	6457	6505	6553	6601	4
905	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080	4
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559	4
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	4
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516	48
909	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994	48
910	959041	9089	9137	9185	9232	9280	9328	9375	_	-	-
911	9518	9566	9614	9661	9709	9757	9804		9423	9471	48
912	9995	42	90					9852	9900	9947	48
913	960471	0518		.138	.185	.233	.280	.328	.376	.423	48
914	0946		0566	0613	0661	0709	0756	0804	0851	0899	48
		0994	1041	1089	1136	1184	1231	1279	1326	1374	4
915	1421	1469	1516	1563	1611	1658	1706	1753	1801	1843	4
916	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322	4
917	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795	4
918	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268	4
919	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741	4'
920	963788	3835	3882	3929	3977	4024	4071	4118	4165	4212	4
921	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684	4
922	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155	4
923	5202	5249	5296	5343	5390	5437	5484	5531			
924	5672	5719	5766	5813	5860	5907			5578	5625	4
925	6142	6189					5954	6001	6048	6095	4
926			6236	6283	6329	6376	6423	6470	6517	6564	4
920	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033	4
	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501	4
928	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969	4
929	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436	4
930	968483	8530	8576	8623	8670	8716	8763	8810	8856	8903	4
931	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369	4
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835	4
933	9882	9928	9975	21	68	.114	.161	.207	.254	.300	4
934	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765	
935	0812	0858	0904								4
936	1276			0951	0997	1044	1090	1137	1183	1229	4
937		1322	1369	1415	1461	1508	1554	1601	1647	1693	4
	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157	4
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619	4
939	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082	4
	V		-	-		-		-	-		

940 941 942 943 944 945 946 947 948	973128 3590 4051 4512 4972 5432 5891	3174 3636 4097 4558	3220 3682 4143	3266 3728	3313	3359	3405	3451	3497	3543	D. 46
942 943 944 945 946 947	4051 4512 4972 5432 5891	4097 4558		3728							
943 944 945 946 947	4512 4972 5432 5891	4558	4143		3774	3820	3866	3913	3959	4005	46
944 945 946 947	4972 5432 5891			4189	4235	4281	4327	4374	4420	4466	46
945 946 947	5432 5891		4604	4650	4696	4742	4788	4834	4880	4926	46
946 947	5891	5018	5064	5110	5156	5202	5248	5294	5340	5386	46
947		5478	5524	5570	5616	5662	5707	5753	5799	5845	46
		5937	5983	6029	6075	6121	6167	6212	6258	6304	46
948	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763	46
040	6808	6854	6900	6946	6992	7037	7083	7129	7175	7220	46
949	7266	7312	7358	7403	7449	7495	7541	7586	7632	7678	46
950	977724	7769	7815	7861	7906	7952	7998	8043	8089	8135	46
951	8181	8226	8272	8317	8363	8409	8454	8500	8546	8591	46
952	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047	46
953	9093	9138	9184	9230	9275	9321	9366	9412	9457	9503	46
954	9548	9594	9639	9685	9730	9776	9821	9867	9912	9958	46
955	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412	45
956	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867	45
957	0912	0957	1003	1048	1093	1139	1184	1229	1275	1320	45
958	1366	1411	1456	1501	1547	1592	1637	1683	1728	1773	45
959	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226	45
960	982271	2316	2362	2407	2452	2497	2543	2588	2633	2678	45
961	2723	2769	2814	2859	2904	2949	2994	3040	3085	3130	45
962	3175	3220	3265	3310	3356	3401	3446	3491	3536	3581	45
963	3626	3671	3716	3762	3807	3852	3897	3942	3987	4032	45
964	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482	45
965	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932	45
966	4977	5022	.5067	5112	5157	5202	5247	5292	5337	5382	45
967	5426	5471	5516	5561	5606	5651	5696	5741	5786	5830	45
968	5875	5920	5965	6010	6055	6100	6144	6189	6234	6279	45
969	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727	45
970	986772	6817	6861	6906	6951	6996	7040	7085	7130	7175	45
971	7219	7264	7309	7353	7398	7443	7488	7532	7577	7622	45
972	7666	7711	7756	7800	7845	7890	7934	7979	8024	8068	45
973	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514	45
974	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960	45
975	9005	9049	9094	9138	9183	9227	9272	9316	9361	9405	45
976	9450	9494	9539	9583	9628	9672	9717	9761	9806	9850	44
977	9895	9939	9983	28	72	.117	.161	.206	.250		44
978	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738	44
979	0783	0827	0871	0916	0960	1004	1049	1093	1137	1182	44
980	991226	1270	1315	1359	1403	1448	$\overline{1492}$	$\frac{1536}{1536}$	1580	1625	44
981	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067	
982	2111	2156	2200	2244	2288	2333	2377	2421	2465	2509	44
983	2554	2598	2642	2686	2730	2774	2819	2863	2907	2951	44
984	2995	3039	3083	3127	3172	3216	3260	3304	3348	3392	44
985	3436	3480	3524	3568	3613	3657	3701	3745	3789	3833	44
986	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273	44
987	4317	4361	4405	4449	4493	4537	4581	4625	4669	4713	44
988	4757	4801	4845	4889	4933	4977	5021	5065	5108	5152	44
989	5196	5240	5284	5328	5372	5416	5460	5504	5547	5591	44
990	995635	5679	$\frac{5723}{5723}$	5767	5811			-	_	_	_
991	6074	6117				5854	5898	5942	5986	6030	44
992	6512	6555	6161 6599	$6205 \\ 6643$	6249	6293	6337	6380	6424	6468	44
993	6949	6993	7037	7080	$\frac{6687}{7124}$	6731	6774	6818	6862	6906	44
994	7386	7430	7474		7124	7168	7212	7255	7299	7343	44
995	7823	7867	7910	7517 7954	7998	7605	7648	7692	7736	7779	44
996	8259	8303	8347	8390		8041	8085	8129	8172	8216	44
997	8695	8739	8782	8826	8434 8869	8477	8521	8564	8608	8652	44
998	9131	9174	9218	9261	9305	8913	8956	9000	9043	9087	44
999		9609	9652	9696	9739	$\frac{9348}{9783}$	9392 9826	9435	9479	9522	44
		-		0000	16010	31001	9020	9870	9913	9957	43
N.	0	1	2	3	4	5	6	7	8	9	D.

A TABLE

OF

LOGARITHMIC

SINES AND TANGENTS.

FOR EVERY

DEGREE AND MINUTE

OF THE QUADRANT.

N.B. The minutes in the left-hand column of each page, increasing downwards, belong to the degrees at the top; and those increasing upwards, in the right-hand column, belong to the degrees below.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	0.000000		10.000000	0.0	0.000000		Infinite.	60
1	6.463726	501717	000000	00	6.463726		13.536274	59
2	764756	293485	000000	00		293483	235244	58
3 4	940847	208231	000000	00	940847	208231	059153	57
	7.065786	161517	000000	00	7.065786	131969	12.934214	56
5	$162696 \\ 241877$	131968 111575	9.999999	01	241878	111578	837304	55 54
7	308824	96653	9999999	01	308825	99653	758122 691175	53
8	366816	85254	999999	01	366817	85254	633183	52
9	417968	76263	999999	01	417970	76263	582030	51
10	463725	68988	999998	01	463727	68988	536273	50
11	7.505118	62981	9.999998	$\overline{01}$	7.505120	62981	12.494880	49
12	542906	57936	999997	01	542909	57933	457091	48
13	577668	53641	999997	01	577672	53642	422328	47
14	609853	49938	999996	01	609857	49939	390143	46
15	639816	46714	999996	01	639820	46715	360180	45
16	667845	43881	999995	01	667849	43882	332151	44
17	694173	41372	999995	01	694179	41373	305821	43
18	718997	39135	999994	01	719003	39136	280997	42
19	742477	37127	999993	01	742484	37128	257516	41
20	764754	35315	999993	01	764761	35136	235239	40
21	7.785943	33672	9.999992	01	7.785951	33673	12.214049	39
22	806146	32175	999991	01	806155	32176	193845	38
23	825451	30805	999990	01	825460	30806	174540	37
24	843934	29547	999989	02	843944	29549	156056	36
25	861662	28388	999988	02	861674	28390	138326	35
26	878695	27317	999988	02	878708	27318	121292	34
27	895085	26323	999987	02	895099	26325	104901	33
28 29	910879 926119	25399	999986	$\frac{02}{02}$	910894	25401	089106	32
30	940842	24538 23733	999985	02	$926134 \\ 940858$	24540	073866	31
			999983	_		23735	059142	30
31	7.955082	22980	9.999982	02	7.955100	22981	12.044900	29
32	968870	22273	999981	$\frac{02}{02}$	968889	22275	031111	28
34	982233 995198	21608 20981	999980 999979	02	982253 995219	$21610 \\ 20983$	017747	27 26
35	8.007787	20390	999977	02	8.007809	20392	004781	25
36	020021	19831	999976	02	020045	19833	$11.992191 \\ 979955$	24
37	031919	19302	999975	02	031945	19305	968055	23
38	043501	18801	999973	02	043527	18803	956473	22
39	054781	18325	999972	02	054809	18327	945191	21
40	065776	17872	999971	02	065806	17874	934194	20
$\frac{1}{41}$	8.076500	17441	9.999969	$\frac{0}{0}$	8.076531	17444	11.923469	19
42	086965	17031	999968	02	086997	17034	913003	18
43	097183	16639	999966	02	097217	16642	902783	17
44	107167	16265	999964	03	107202	16268	892797	16
45	116926	15908	999963	03	116963	15910	883037	15
46	126471	15566	999961	03	126510	15568	873490	14
47	135810	15238	999959	03	135851	15241	864149	13
48	144953	14924	999958	03	144996	14927	855004	12
49	153907	14622	999956	03	153952	14627	846048	11
50	162681	14333	999954	03	162727	14336	837273	10
51	8.171280	14054	9.999952	$\overline{03}$	8.171328	14057	11.828672	9
52	179713	13786	999950	03	179763	13790	820237	8
53	187985	13529	999948	03	188036	13532	811964	7
54	196102	13280	999946	03	196156	13284	803844	6
55	204070	13041	999944	03	204126	13044	795874	5
56	211895	12810	999942	04	211953	12814	788047	4
	219581	12587	999940	04	219641	12590	780359	3
57		12372	999938	04	227195	12376	772805	2
58	227134							
58 59	234557	12164	999936	04	234621	12168	765379	1
58							765379	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	8.241855	11963	9.999934			11967	11.758079	60
1	249033	11768	999932	04	249102	11772	750898	59
2	256094	11580	999929	04	256165	11584	743835	58
3	263042	11398	999927	04	263115	11402	736885	57
4	269881	11221	999925	04	269956	11225	730044	56
5	276614	11050	999922	04	276691	11054	723309	5
6	283243	10883	999920	04	283323	10887	716677	54
7	289773	10721	999918	04	289856	10726	710144	5
8	296207	10565	999915	04	296292	10570	703708	55
9	302546	10413	999913	04	302634	10418	697366	51
10.	308794	10266	999910	04	308884	10270	691116	50
11	8.314954	10122	9.999907	04	8.315046	10126	11.684954	49
12	321027	9982	999905	04	321122	9987	678878	48
13	327016	9847	999902	04	327114	9851	672886	47
14	332924	9714	999899	05	333025	9719	666975	46
15	338753	9586	999897	05	3388561	9590	661144	45
16	344504	9460	999894	05	344610	9465	655390	44
17	350181	9338	999891	05	350289	9343	649711	43
18	355783	9219	999888	05	355895	9224	644105	42
19	361315	9103	999885	05	361430	9108	638570	41
20	366777	8990	999882	05	366895	8995	633105	40
21	8.372171	8880		_				-
22	377499		9.999879	05	8.372292	8885	11.627708	39
23		8772	999876	05	377622	8777	622378	38
	382762	8667	999873	05	382889	8672	617111	37
24	387962	8564	999870	05	388092	8570	611908	36
25	393101	8464	999867	05	393234	8470	606766	35
26	398179	8366	999864	05	398315	8371	601685	34
27	403199	8271	999861	05	403338	8276	596662	33
85	408161	8177	999858	05	408304	8182	591696	32
29	413068	8086	999854	05	413213	8091	586787	31
30	417919	7996	999851	06	418068	8002	581932	30
31	8.422717	7909	9.999848	06	8.422869	7914	11.577131	$\frac{1}{29}$
32	427462	7823	999844	06	427618	7830	572382	
33	432156	7740	999841	06	432315	7745	567685	28
34	436800	7657	999838	06	436962	7663		27
35	441394	7577	999834	06	441560	7583	563038	26
36	445941	7499	999831	06	446110	7505	558440	25
37	450440	7422	999827	06			553890	24
38	454893	7346			450613	7428	549387	23
39	459301	7273	999823 999820	06	455070	7352	544930	22
10	463665	7200		06	459481	7279	540519	21
		1 4 14 14 14	999816	06	463849	7206	536151	20
1	8.467985	7129	9.999812	06	8.468172	7135	11.531828	19
2	472263	7060	999809	06	472454	7066	527546	18
13	476498	6991	999805	06	476693	6998	523307	17
4	480693	6924	999801	06	480892	6931	519108	16
5	484848	6859	999797	07	485050	6865	514950	15
6	488963	6794	999793	07	489170	6801	510830	14
7	493040	6731	999790	07	493250	6738	506750	13
8	497078	6669	999786	07	497293	6676	502707	12
9	501080	6608	999782	07	501298	6615	498702	11
0	505045	6548	999778	07	505267	6555	494733	10
1	8.508974	6489	9.999774	07	8.509200	6496	11.490800	_
2	512867	6431	999769	07	513098	6439		9
3	516726	6375	999765	07	516961		486902	8
4	520551	6319	999761	07		6382	483039	7
5	524343			07	520790	6326	479210	6
6		6264	999757		524583	6272	475414	5
7	528102	6211	999753	07	528349	6218	471651	4
	531828	6158	999748	07	532080	6165	467920	3
8	535523	6106	999744	07	535779	6113	464221	2
9	539186	6055	999740	07	539447	6062	460553	1
60 1	542819	6004	999735	071	543084	6012	456916	0
-	Cosine	-	Sine 1	-	Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	-18
0	8.542819	6004	9.999735	07	8.543084	6012	11.456916	60
1	546422	5955	999731	07	546691	5962	453309	59
2	549995	5906	999726	07	550268	5914	449732	58
3	553539	5858	999722	08	553817	5866	446183	57
4	557054	5811	999717	08	557336	5819	442664	56
	560540	5765	999713	08	560828	5773	439172	55
5	563999	5719	999708	08	564291	5727	435709	54
6	567431	5674	999704	08	567727	5682	432273	53
7	570836	5630	999699	08	571137	5638	428863	52
8	574214			08	574520	5595	425480	51
9		5587	999694			5552	422123	50
10	577566	5544	999689	08	577877	_	-	400.0
11	8.580892	5502	9.999685	08	8.581208	5510	11.418792	49
12	584193	5460	999680	08	584514	5468	415486	48
13	587469	5419	999675	08	587795	5427	412205	47
14	590721	5379	999670	08	591051	5387	408949	46
15	593948	5339	999665	80	594283	5347	405717	45
16	597152	5300	999660	08	597492	5308	402508	44
17	600332	5261	999655	08	600677	5270	399323	43
18	603489	5223	999650	08	603839	5232	396161	42
19	606623	5186	999645	09	606978	5194	393022	41
20	609734	5149	999640	09	610094	5158	389906	40
_	-			$\frac{00}{09}$	8.613189	5121	11,386811	39
21	8.612823	5112	9.999635					
22	615891	5076	999629	09	616262	5085	383738	38
23	618937	5041	999624	09	619313	5050	380687	37
24	621962	5006	999619	09	622343	5015	377657	36
25	624965	4972	999614	09	625352	4981	374648	35
26	627948	4938	999608	09	628340	4947	371660	34
27	630911	4904	999603	09	631308	4913	368692	33
28	633854	4871	999597	09	634256	4880	365744	32
29	636776	4839	999592	09	637184	4848	362816	31
30	639680	4806	999586	09	640093	4816	359907	30
31	8.642563	4775	9.999581	09	8.642982	4784	11.357018	29
32	645428	4743	999575	09	645853	4753	354147	28
33	648274	4712	999570	09	648704	4722	351296	27
	651102	4682	999564	09	651537	4691	348463	26
34	653911	4652	999558	10	654352	4661	345648	25
35	656702		999553	10	657149	4631	342851	24
36		4622	999547	10	659928	4602	340072	23
37	659475	4592		10	662689	4573	337311	22
38	662230	4563	999541	10		4544	334567	21
39	664968	4535	999535		665433	4526		
40	667689	4506	999529	10	668160	-	331840	20
41	8.670393	4479	9.999524	10	8.670870	4488	11.329130	19
12	673080	4451	999518	10	673563	4461	326437	18
43	675751	4424	999512	10	676239	4434	323761	17
44	678405	4397	999506	10	678900	4417	321100	16
45	681043	4370	999500	10	681544	4380	318456	15
46	683665	4344	999493	10	684172	4354	315828	14
47	686272	4318	999487	10	686784	4328	313216	13
48	688863	4292	999481	10	689381	4303	310619	12
49	691438	4267	999475	10	691963	4277	308037	11
50	693998	4242	999469	10	694529	4252	305471	10
	The second secon	-		-		-	and the second second	7000
51	8.696543	4217	9.999463	11	8.697081	4228	11.302919	9
52	699073	4192	999456	11	699617	4203	300383	8
53	701589	4168	999450	11	702139	4179	297861	
54	704090	4144	999443	11	704646	4155	295354	(
55	706577	4121	999437	11	707140	4132	292860	1
56	709049	4097	999431	11	709618	4108	290282	4
57	711507	4074	999424	11	712083	4085	287917	
58	713952	4051	999418	11	714534	4062	285465	2
59	716383	4029	999411	11	716972	4040	283028	1
60	718800	4006	999404		719396	4017	280604	0
-	1000			7.5		-5000		-

0 8,718900 4006 9,999404 11 8,719396 4017 11,280604 12 723595 3962 999391 11 724204 3974 275796	-N		D.	Cosine	D	. Tang.	D.	Cotang.	T
1					111				1
1									
5 730688 38988 999371 11 729353 3909 258688 7 735354 3857 999367 12 733693 3886 26637 7 735354 3857 999357 12 733693 3886 266337 9 73999 3816 999336 12 738917 3848 261683 10 742259 3796 999336 12 749292 3807 257078 12 746802 3766 999322 12 744759 3787 259374 13 749053 3787 999310 12 749740 3749 252521 14 751297 3717 999308 12 754527 376 252521 16 755528 3698 999301 12 754227 3710 245773 245773 245773 245047 48017 2476227 3710 245773 243547 48017 2766823 3673 <	. 2	72359			4 -	* *******		W.OTOT	1
5 730688 38988 999371 11 729353 3909 258688 7 735354 3857 999367 12 733693 3886 26637 7 735354 3857 999357 12 733693 3886 266337 9 73999 3816 999336 12 738917 3848 261683 10 742259 3796 999336 12 749292 3807 257078 12 746802 3766 999322 12 744759 3787 259374 13 749053 3787 999310 12 749740 3749 252521 14 751297 3717 999308 12 754527 376 252521 16 755528 3698 999301 12 754227 3710 245773 245773 245773 245047 48017 2476227 3710 245773 243547 48017 2766823 3673 <	5	72597						275796	E
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22	(4	Degr	ees.) A	TAI	BLE OF LO	ga riti	imic	
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.843585	3005	9.998941	15	8.844644	3019	11.155356	60
1	845387	2992	998932	15	846455	3007	153545	59
2 3	847183	2980	998923	15	848260	2995	151740	58
4	848971 850751	2967 2955	998914 998905	15 15	850057 851846	2982 2970	149943 148154	57
5	852525	2943	998896	15	853628	2958	146372	56: 65
6	854291	2931	998887	15	855403	2946	144597	54
7	856049	2919	998878	15	857171	2935	142829	53
8	857801	2907	998869	15	858932	2923	141068	52
.9	859546 861283	2896	998860 998851	15 15	860686 862433	2911 2900	139314	51
$\frac{10}{11}$		2884		$\frac{15}{15}$		-	137567	50
11 12	8.863014 864738	2873	9.998841 998832	15	8.864173 865906	2888	11.135827	49
13	866455	2861 2850	998823	16	867632	2877 2866	134094 132368	48
14	868165	2839	998813	16	869351	2854	130649	46
15	869868	2828	998804	16	871064	2843	128936	45
16	871565	2817	998795	16	872770	2832	127230	44
17	873255	2806	998785	16	874469	2821	125531	43
18	874938	2795	998776	16	876162	2811	123838	42
19	876615	2786	998766	16	877849	2800	.122151	41
20	878285	2773	998757	16	879529	2789	120471	40
21	8.879949	2763	9.998747	16 16	8.881202	2779	11.118798	39
22 23	881607 883258	$2752 \\ 2742$	998738 998728	16	882869 884530	2768 2758	117131 11 54 70	38
24	884903	2731	998718	16	886185	2747	113815	37 36
25	886542	2721	998708	16	887833	2737	112167	35
26	888174	2711	998699	16	889476	2727	110524	34
27	889801	2700	998689	16	891112	2717	108888	33
28	891421	2690	998679	16	892742	2707	107258	32
29	893035	2680	998669	17	894366	2697	105634	31
30	894643	2670	998659	17	895984	2687	104016	30
31	8.896246 897842	2660	9.998649	17 17	8.897596	2677	11.102404	29 28
32 33	899432	2651 2641	998639 998629	17	899203 900803	2667 2658	100797 099197	27
34	901017	· 2631	998619	17	902398	2648	097602	26
35	902596	2622	998609	17	903987	2638	096013	25
36	904169	2612	998599	17	905570	2629	094430	24
37	905736	2603	998589	17	907147	2620	092853	23
38	907297	2593	998578	17	908719	2610	091281	22
39 40	908853 910404	2584 2575	998568	17 17	910285	2601	089715	21 20
			998558		911846	2592	088154	
41	8.911949	2566	9.998548	17	8.913401	2583	11.086599	19
42 43	913488 915022	2556 2547	998537 998527	17	914951 916495	2574 2565	085049 083505	18 17
44	916550	2538	998516	is	918034	2556	081966	16
45	918073	2529	998506	18	919568	2547	080432	15
46	919591	2520	998495	18	921096	2538	078904	14
47	921103	2512	998485	18	922619	2530	077381	13
48	922610	2503	998474	18	924136	2521	075864	12
49	924112	2494	998464	18 18	925649	2512	074351	11
50	925609	2486	998453		927156	2503	072844	10
51 52	8.927100 928587	2477 2469	9.998442 998431	18 18	8.928658	2495 2486	11.071342	9
53	930068	2469 2460	998431	18	930155 931647	2480 2478	069845 0683 5 8	8
54	931544	2452	998410	18	933134	2470	066866	6
55	933015	2443	998399	18	934616	2461	065384	. 5
56	934481	2435	998388	18	936093	2453	063907	4
57	935942	2427	998377	18	937565	2445	062435	3
58	937398	2419	998366	18	939032	2437	060968	2
59 60	938850	2411	998355	18	940494	2430	059506	1
QU.	940296	2403	998344	18	941952	2421	058048	0
	Cosine		Sine		Cotang.		Tang.	M.

85 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
01	8.940296	2403	9.998344	19	8.941952	2421	11.058048	60
1	941738	2394	998333	19	943404	2413	056596	59
3	943174	2387	998322	19	944852	2405	055148	58
3	944606	2379	998311	19	946295	2397	053705	5
4	946034	2371	998300	19	947734	2390	052266	5
5	947456	2363	998289	19	949168	2382	050832	5
6	948874	2355	998277	19	950597	2374	049403	5
7	950287	2348	998266	19	952021	2366	047979	5
8	951696	2340	998255	19	953441	2360	046559	5
9	953100	2332	998243	19	954856	2351	045144	5
10	954499	2325	998232	19	956267	2344	043733	5
11	8.955894	2317	9.998220	19	8.957674	2337	11.042326	4
12	957284	2310	998209	19	959075	2329	040925	4
13	958670	2302	998197	19	960473	2323	039527	4
14	960052	2295	998186	19	961866	2314	038134	4
15	961429	2288	998174	19	963255	2307	036745	4
16	962801	2280	998163	19	964639	2300	035361	4
17	964170	2273	998151	19	966019	2293	033981	4
18	965534	2266	998139	20	967394	2286	032606	4
19	966893	2259	998128	20	968766	2279	031234	4
	968249	2252	998116	20	970133	2271	029867	4
20	THE RESERVE AND ADDRESS OF THE PARTY.		The second second	20	8.971496	2265	11.028504	100
21	8.969600	2244	9.998104				027145	000
22	970947	2238	998092	20	972855	2257		0.00
23	972289	2231	998080	20	974209	2251	025791	9 00
24	973628	2224	998068	20	975560	2244	024440	
25	974962	2217	998056	20	976906	2237	023094	
26	976293	2210	998044	20	978248	2230	021752	
27	977619	2203	998032	20	979586	2223	020414	
28	978941	2197	998020	20	980921	2217	019079	
29	980259	2190	998008	20	982251	2210	017749	
30	981573	2183	997996	20	983577	2204	016423	
31	8.982883	2177	9.997984	20	8.984899	2197	11.015101	15
32	984189	2170	997972	20	986217	2191	013783	1
33	985491	2163	997959	20	987532	2184	012468	
34	986789	2157	997947	20	988842	2178	011158	15
35	988083	2150	997935	21	990149	2171	009851	1
36	989374	2144	997922	21	991451	2165	008549	1
	990660	2138	997910	21	992750	2158	007250	
37		2131	997897	21	994045	2152	005955	
38	991943		997885	21	995337	2146	004663	
39	993222	2125	997872	21	996624	2140	003376	
40	994497	2119		-			11.002092	
41	8.995768	2112	9.997860	21	8.997908	2134		
42	997036	2106	997847	21	999188	2127	000812	
43	998299	2100	997835		9.000465	2121	10.999535	1100
44	999560	2094	997822		001738	2115	998262	
45	9.000816	2087	997809		003007	2109	996993	
46	002069	2082	997797		.004272	2103	995728	
47	003318	2076	997784		005534	2097	994466	
48	004563	2070	997771	21	006792	2091	993208	
49	005805	2064	997758	21	008047	2085	991953	
50	007044	2058	997745		009298	2080	990702	
$\frac{51}{51}$	9.008278	2052	9.997732	-	9.010546	2074	10.989454	
	009510	2052	997719	200	011790	2068	988210	
52 53	010737	2040	997706		013031	2062	986969	
			997693		014268	2056	985732	
54	011962	2034			015502	2051	984498	
55	013182	2029	997680		016732	2045	983268	
56	014400	2023	997667		010732	2040	982041	
57	015613	2017	997654		017959	2033	980817	
58	016824	2012	997641		019183	2028	979597	
59	018031	2006	997628					
60	019235	2000	997614	22	021620	2023	978380	



M.	Sine	D.	Cosine	D,	Tang.	D,	Cotang.	1
0	19.019235	2000	9.997614	22	9.021620	2023	10.978380	60
1	020435	1995	997601	22	022834	2017	977166	59
2	021632	1989	997588	22	024044	2011	975956	58
3	022825	1984	997574	22	025251	2006	974749	57
4	024016	1978	997561	22	026455	2000	973545	56
5	025203	1973	997547	22	027655	1995	972345	5
6				23				
6	026386	1967	997534		028852	1990	971148	54
1	027567	1962	997520	23	030046	1985	969954	5
8 9	028744	1957	997507	23	031237	1979	968763	5
	029918	1951	997493	23	032425	1974	967575	5
10	031089	1947	997480	23	033609	1969	966391	50
11	9.032257	1941	9.997466	23	9.034791	1964	10.965209	49
12	033421	1936	997452	23	035969	1958	964031	48
3	034582	1930	997439	23	037144	1953	962856	4
4	035741	1925	997425	23				
					038316	1948	961684	40
15	036896	1920	997411	23	039485	1943	960515	4
16	038048	1915	997397	23	040651	1938	959349	44
17	039197	1910	997383	23	041813	1933	958187	4:
18	040342	1905	997369	23	042973	1928	957027	45
19	041485	1899	997355	23	044130	1923	955870	4
05	042625	1894	997341	23	045284	1918	954716	40
21	9.043762	1889	9.997327	$\overline{24}$			and the second s	1
					9.046434	1913	10.953566	3
22	044895	1884	997313	24	047582	1908	952418	38
23	046026	1879	997299	24	048727	1903	951273	3
24	047154	1875	997285	24	049869	1898	950131	3
25	048279	1870	997271	24	051008	1893	948992	3
65	049400	1865	997257	24	052144	1889	947856	34
27	050519	1860	997242	24	053277	1884	946723	3:
28	051635	1855	997228	24	054407	1879	945593	3
29	052749	1850	997214	24	055535	1874	944465	3
30	053859	1845	997199	24				
	-		and the same and the same as	_	056659	1870	943341	30
31	054966	1841	9.997185	24	9.057781	1865	10.942219	25
32	056071	1836	997170	24	058900	1869	941100	28
33	057172	1831	997156	24	060016	1855	939984	2
34	058271	1827	997141	24	061130	1851	938870	20
35	059367	1822	997127	24	062240	1846	937760	2
36	060460	1817	997112	24	063348	1842	936652	24
37	061551	1813	997098	24	064453	1837	935547	2:
38	062639	1808	997083	25	065556			
39	063724	1804	997068	25	066655	1833	934444	25
0	064806	1799		25		1828	933345	2
_		_	997053		067752	1824	932248	20
1	9.065885	1794	9.997039	25	9.068846	1819	10.931154	19
2	066962	1790	997024	25	069938	1815	930062	18
3	068036	1786	997009	25	071027	1810	928973	17
4	069107	1781	996994	25	072113	1806	927887	16
5	070176	1777	996979	25	073197	1802	926803	13
6	071242	1772	996964	25	074278		925722	
7	072306	1768		25		1797		14
8			996949		075356	1793	924644	1:
	073366	1763	996934	25	076432	1789	923568	1:
9	074424	1759	996919	25	077505	1784	922495	1
0	075480	1755	996904	25.	078576	1780	921424	10
1	9.076533	1750	9.996889	25	9.079644	1776	10.920356	-
2	077583	1746	996874	25	080710	1772	919290	
3	078631	1742	996858	25	081773	1767	918227	
4	079676	1738	996843	25	082833			
55						1763	917167	1
	080719	1733	996828	25	083891	1759	916109	1
6	081759	1729	996812	26	084947	1755	915053	1
7	082797	1725	996797	26	086000	1751	914000	
8	083832	1721	996782	26	087050	1747	912950	
59	084864	1717	996766	26	088098	1743	911902	
00	085894	1713	996751	26	089144	1738	910856	
	-		and the state of t	-			, 010000	100

M.	Sine	- D.	Cosine	D,	Tang.	D.	Cotang.	110
0	9.0858941	1713	9.996751	26	9.089144	1738	10.910856	60
1	086922	1709	996735	26	090187	1734	909813	59
2	087947	1704	996720	26	091228	1730	908772	58
3	088970	1700	996704	26	092266	1727	907734	57
4	089990	1696	996688	26	093302	1722	906698	56
5	091008	1692	996673	26	094336	1719	905664	55
6	092024	1688	996657	26	095367	1715	904633	54
7	093037			26	096395	1711		53
		1684	996641				903605	
8	094047	1680	996625	26	097422	1707	902578	5
9	095056	1676	996610	26	098446	1703	901554	5
10	096062	1673	996594	26	099468	1699	900532	50
11	9.097065	1668	9.996578	27	9.100487	1695	10.899513	45
2	098066	1665	996562	27	101504	1691	898496	48
3	099065	1661	996546	27	102519	1687	897481	4
4	100062	1657	996530	27	103532	1684	896468	46
5	101056		996514	27	104542	1680	895458	4
		1653						
6	102048	1649	996498	27	105550	1676	894450	44
7	103037	1645	996482	27	106556	1672	893444	4:
18	104025	1641	996465	27	107559	1669	892441	45
9	105010	1638	996449	27	108560	1665	891440	4
00	105992	1634	. 996433	27	109559	1661	890441	40
21	9.106973	1630	9.996417	27	9.110556	1658	10.889444	39
22	107951	1627	996400	27	111551	1654	888449	38
23					112543	1650	887457	3
	108927	1623	996384	27				
24	109901	1619	996368	27	113533	1646	886467	3
25	110873	1616	996351	27	114521	1643	885479	3
26	111842	1612	996335	27	115507	1639 -	884493	34
27	112809	1608	996318		116491	1636	883509	3
28	113774	1605	996302	28	117472	1632	882528	35
29	114737	1601	996285	28	118452	1629	881548	3
30	115698	1597	996269	28	119429	1625	880571	30
31	9.116656		-	-	9.120404	-	10.879596	2
32		1594	9.996252	28		1622		
	117613	1590	996235	28	121377	1618	878623	28
33	118567	1587	996219	28	122348	1615	877652	2
34	119519	1583	996202	28	123317	1611	876683	2
35	120469	1580	996185	28	124284	1607	875716	2
36	121417	1576	996168	28	125249	1604	874751	2
37	122362	1573	996151	28	126211	1601	873789	2
38	123306	1569	996134	28	127172	1597	872828	2
39	124248	1566	996117	28	128130	1594	871870	2
10	125187	1562	996100	28	129087	1591	870913	2
41	-	-		-		-		-
	9.126125	1559	9.996083		9.130041	1587	10.869959	1
12	127060	1556	996066		130994	1584	869006	1
43	127993	1552	996049		131944	1581	868056	1
14	128925	1549	996032		132893	1577	867107	1
15	129854	1545	996015	29	133839	1574	866161	1
16	130781	1542	995998		134784	1571	865216	1
17	131706	1539	995980		135726	1567	864274	
18	132630	1535	995963		136667	1564	863333	
19	133551	1532	995946		137605	1561	862395	
50	. 134470		995940		138542	1558	861458	
100		1529		-				-
51	9.135387	1525	9.995911	29	9.139476	1555	10.860524	13
52	136303	1522	995894	29	140409	1551	859591	13
53	137216	1519	995876		141340	1548	858660	
54	138128	1516	995859		142269	1545	857731	13
55	139037	1512	995841		143196	1542	856804	
56	139944				144121	1539	855879	
57		1509	995823					
	140850	1506	995806		145044	1535	854956	
58	141754	1503	995788		145966	1532	854034	1
59	142655	1500	995771		146885	1529	853115	FX
60	143555	1496	995753	29	147803	1526	852197	1
-					and the same of th			IN

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.143555	1496	19.995753	130	9.147803	1526	10.852197	60
1	144453	1493	995735	30	148718	1523	851282	5
3	145349	1490	995717	30	149632	1520	850368	58
3	146243	1487	995699	30	150544	1517	849456	5
4	147136	1484	995681	30	151454	1514	848546	56
5	148026	1481.	995664	30	152363	1511	847637	5.
6	148915	1478	995646	30	153269	1508	846731	54
7	149802	1475	995628	30	154174	1505	845826	5
8	150686	1472	995610	30	155077	1502	844923	55
9	151569	1469	995591	30	155978	1499	844022	2
10	152451	1466	995573	30	156877	1496	843123	5
11	9 153330	1463	9.995555	30	9.157775	1493	10.842225	4
12	154208	1460	995537	30	158671	1490	841329	4
13	155083	1457	995519	30	159565	1487	840435	4
14	155957	1454	995501	31	160457	1484	839543	4
15	156830	1451	995482	31	161347	1481	838653	4
16	157700	1448	995464	31	162236	1479	837764	4
17	158569	1445	995446	31	163123	1476	836877	4
18	159435	1442	995427	31	164008	1473	835992	4
19	160301	1439	995409	31	164892	1470	835108	4
05	161164	1436	995390	31	165774	1467	834226	4
21	9.162025	1433	9.995372	31	9.166654	1464	10.833346	3
22	162885	1430	995353	31	167532	1461	832468	
23	163743	1427	995334	31	168409	1458		3
24	164600	1424	995316	31	169284	1455	831591 830716	3
25	165454	1424	995297	31	170157			3
26	166307	1419	995278	31	171029	1453	829843	3
27	167159	1416	995260			1450	828971	3
8	168008	1413	995241	31 32	171899 172767	1447	828101	3
29	168856	1410	995222	32	173634	1444	827233 826366	3
30	169702	1407	995203	32	174499	$\frac{1442}{1439}$	825501	3
31			-	-			And the second s	
32	9.170547	1405	9.995184	32	9.175362	1436	10.824638	2
	171389	1402	995165	32	176224	1433	823776	2
33	172230	1399	995146	32	177084	1431	822916	2
34	173070	1396	995127	32	177942	1428	822058	2
35 36	173908	1394	995108	32	178799	1425	821201	2
	174744	1391	995089	32	179655	1423	820345	2
37	175578	1388	995070	32	180508	1420	819492	2
88	176411	1386	995051	32	181360	1417	818640	2
	177242	1383	995032	32	182211	1415	817789	2
0	178072	1380	995013	32	183059	1412	816941	2
1	9.178900	1377	9.994993	32	9.183907	1409	10.816093	1
2	179726	1374	994974	32	184752	1407	815248	1
3	180551	1372	994955	32	185597	1404	814403	1
4	181374	1369	994935	32	186439	1402	813561	1
5	182196	1366	994916	33	187280	1399	812720	1
6	183016	1364	994896	33	188120	1396	811880	14
7	183834	1361	994877	33	188958	1393	811042	1
8	184651	1359	994857	33	189794	1391	810206	1:
9	185466	1356	994838	33	190629	1389	809371	1
0	186280	1353	994818	33	191462	1386	808538	10
1	9.187092	1351	9.994798	33	9.192294	1384	10.807706	-
2	187903	1348	994779	33	193124	1381	806876	
3	188712	1346	994759	33	193953	1379	806047	
4	189519	1343	994739	33	194780	1376	805220	-
5	190325	1341	994719	33	195606	1374	804394	1
6	191130	1338	994700	33	196430			1
7	191933	1336	994680	33	197253	1371	803570	-
8	192734	1333	994660	33		1369	802747	
9	193534	1330	994640	33	198074	1366	801926	-
٥l	194332	1328	994620	33	198894 199713	1364	801106 800287	(

81 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	-
0	9.194332	1328	9.994620	33	9.1997131	1361	10.800287	60
1	195129	1326	994600	33	200529	1359	799471	59
2	195925	1323	994580	33	201345	1356	798655	58
3	196719	1321	994560	34	202159	1354	797841	57
	197511	1318	994540	34	202971	1352	797029	56
4				34				55
5	198302	1316	994519		203782	1349	796218	
6	199091	1313	994499	34	204592	1347	795408	54
7	199879	1311	994479	34	205400	1345	794600	53
8	200666	1308	994459	34	206207	1342	793793	52
9	201451	1306	994438	34	207013	1340	792987	51
0	202234	1304	994418	34	207817	1338	792183	50
1	9.203017	1301	9.994397	34	9.208619	1335	10.791381	49
								48
2	203797	1299	994377	34	209420	1333	790580	
13	204577	1296	994357	34	210220	1331	789780	47
4	205354	1294	994336	34	211018	1328	788982	46
5	206131	1292	994316	34	211815	1326	788185	45
6	206906	1289	994295	34	212611	1324	787389	44
7	207679	1287	994274	35	213405	1321	786595	43
8	208452	1285	994254	35	214198	1319	785802	42
9	209222	1282	994233	35	214989	1317	785011	41
			994212	35	215780		784220	40
05	209992	1280				1315		-
21	9.210760	1278	9.994191	35	9.216568	1312	10.783432	38
22	211526	1275	994171	35	217356	1310	782644	38
23	212291	1273	994150	35	218142	1308	781858	37
24	213055	1271	994129	35	218926	1305	781074	36
25	213818	1268	994108	35	219710	1303	780290	35
26	214579	1266	994087	35	220492	1301	779508	34
	215338	1264	994066	35	221272	1299	778728	33
27								
28	216097	1261	994045	35	222052	1297	777948	32
29	216854	1259	994024	35	222830	1294	777170	31
30	217609	1257	994003	35	223606	1292	776394	30
31	9.218363	1255	9.993981	35	9.224382	1290	10.775618	29
32	219116	1253	993960	35	225156	1288	774844	28
				35	225929		774071	2
33	219868	1250	993939			1286		26
34	220618	1248	993918	35	226700	1284	773300	
35	221367	1246	993896	36	227471	1281	772529	2
36	222115	1244	993875	36	228239	1279	771761	24
37	222861	1242	993854	36	229007	1277	770993	2:
38	223606	1239	993832	36	229773	1275	770227	25
39	224349	1237	993811	36	230539	1273	769461	2
40.	225092	1235	993789	36	231302	1271	768698	20
-		C 4.000.0		36			1	1
11	9.225833	1233	9.993768	0.0	9.232065	1269	10.767935	
12	226573	1231	993746		232826	1267	767174	18
13	227311	1228	993725		233586	1265	766414	T
14	228048	1226	993703		234345	1262	765655	1
15	228784	1224	993681	36	235103	1260	764897	14
16	229518	1222	993660	36	235859	1258	764141	14
17	230252	1220	993638	36	236614	1256	763386	1:
18	230984	1218	993616	36	237368	1254	762632	15
19	231714	1216	993594	37	238120	1252	761880	1
							761128	10
50	232444	1214	993572	37	238872	1250	The second secon	1
51	9.233172	1212	9.993550	37	9.239622	1248	10.760378	
52	233899	1209	993528	37	240371	1246	759629	1
53	234625	1207	993506	37	241118	1244	758882	- 3
54	235349	1205	993484	37	241865	1242	758135	1
55	236073	1203	993462	37	242610	1240	757390	
				37		1238		1
56	236795	1201	993440		243354		756646	1
57	237515	1199	993418	37	244097	1236	755903	
58	238235	1197	993396	37	244839	1234	755161	1
59	238953	1195	993374		245579	1232	754421	10
60	239670	1193	993351	37	246319	1230	753681	1

M	. Sine	D.	Cosine	1	O. Tang.	D.	Cotan	g.
0			3 9.9933	5113	7 9.2463	19(123		1
1	24038		1 9933					
2	24110	1189						43
3	241814							
4	242526						- I SOTE	
5								
6	243947				10000			02
7	244656							70
8		1179						39
9					- Govern		7478	09 4
						0 121:	74708	
10	246775	1173	99312	7 38	25364	8 121		
11	9.247478	1171	9.99310	4 38	9.25437	4 1209		200
12	248181	1169	99308	1 38				
13	248883	1167	99305					00 4
14	249583	1165	99303					
15	250282	1163	99301					
16	250980	1161	99299					
7	251677	1159			10000			0 4
8	252373		99296					0 4
9	253067	1158	99294					1 4
9		1156	99292				73985	
-	253761	1154	992898	8 38	260863	3 1192	73913	
1	9.254453	1152	9.99287	5 38	9.261578	1190	- Acceptance	
2	255144	1150	99285		262292		73770	
3	255834	1148	992829		263005			
4	256523	1146	992806		263717		73699	
5	257211	1144	992783		264428		73628	-
6	257898	1142	992759				73557	
7	258583	1141	992736		265138		73486	
8	259268	1139			265847		73415	
9	259951		992713		266555		73344	
0	260633	1137	992690		267261	1176	73273	9 31
E 1	The state of the s	1135	992666		267967	1174	73203	
1	9.261314	1133	9.992643	39	9.268671	1172	10.731329	9 29
2	261994	1131	992619	39	269375	1170	73062	
3	262673	1130	992596		270077	1169	72992	
1	263351	1128	992572	39	270779	1167	72922	
5	264027	1126	992549		271479	1165	728521	20
3	264703	1124	992525		272178	1164		
7	265377	1122	992501	39	272876	1162	727822	
3	266051	1120	992478	40	273573		727124	
9	266723	1119	992454	40	274269	1160	726427	
1	267395	1117	992430	40		1158	725731	
- 1	9.268065		Actions bester to the second	-	274964	1157	725036	10000
		1115	9.992406	40	9.275658	1155	10.724342	19
	268734	1113	992382	40	276351	1153	723649	
1	269402	1111	992359	40	277043	1151	722957	17
1	270069	1110	992335	40	277734	1150	722266	
1	270735	1108	992311	40	278424	1148	721576	
1	271400	1106	992287	40	279113	1147	720887	14
1	272064	1105	992263	40	279801	1145	720199	
1	272726	1103	992239	40	280488	1143		13
1	273388	1101	992214	40	281174	1141	719512	12
	274049	1099	992190	40	281858	1140	718826	11
17	9.274708	1098		-			718142	10
1	275367		9.992166	40	9.282542	1138	10.717458	9
1	276024	1096	992142	40	283225	1136	716775	8
1		1094	992117	41	283907	1135	716093	7
1	276681	1092	992093	41	284588	1133	715412	6
1	277337	1091		41	285268	1131	714732	5
14	277991	1089		41	285947	1130	714053	4
1	278644	1087		41	286624	1128	713376	3
1	279297	1086		41	287301	1126	712699	
1	279948	1084		41	287977	1125		2
	280599	1082		41	288652	1123	713023 711348	1 0

79 Degrees.

М.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1-6
0	9.280599	1082	9.991947	411	9.288652	1123	10.711348	60
1	281248	1081	991922	41	289326	1122	710674	59
0	281897	1079	991897	41	289999	1120	710001	58
2 3				41	290671	1118	709329	57
3	282544	1077	991873		291342	1117	708658	56
4	283190	1076	991848	41				
5	283836	1074	991823	41	292013	1115	707987	55
6	284480	1072	991799	41	292682	1114	707318	54
7	285124	1071	991774	42	293350	1112	706650	53
8	285766	1069	991749	42.	294017	1111	705983	52
	286408	1067	991724	42	294684	1109	705316	51
9					295349	1107	704651	50
0	287048	1066	991699	42				-
1	9.287687	1064	9.991674	42	9.296013	1106	10.703987	49
2	288326	1063	991649	42	296677	1104	703323	48
			991624	42	297339	1103	702661	47
3	288964	1061			298001	1101	701999	46
4	289600	1059	991599	42			701338	45
5	290236	1058	991574	42	298662	1100		
6	290870	1056	991549	42	299322	1098	700678	44
7	291504	1054	991524	42	299980	1096	700020	43
8	292137	1053	991498	42	300638	1095	699362	42
			991473	42	301295	1093	698705	41
9	292768	1051			301951	1092	698049	40
0.	293399	1050	991448	42				
21	9.294029	1048	9.991422	42	9.302607	1090	10.697393	39
22	294658	1046	991397	42	303261	1089	696739	38
		1045	991372	43	303914	1087	696086	37
23	295286			43	304567	1086	695433	36
4	295913	1043	991346			1084	694782	35
25	296539	1042	991321	43	305218			34
26	297164	1040	991295	43	305869	1083	694131	
27	297788	1039	991270	43	306519	1081	693481	33
28	298412	1037	991244	43	307168	1080	692832	32
29	299034	1036	991218	43	307815	1078	692185	31
				43	308463	1077	691537	30
30	299655	1034	991193	_		-		_
31	9.300276	1032	9.991167	43	9.309109	1075	10.690891	29
32	300895	1031	991141	43	309754	1074	690246	28
33	301514	1029	991115	43	310398	1073	689602	27
	302132	1028	991090	43	311042	1071	688958	26
34				43	311685	1070	688315	25
35	302748	1026	991064			1068	687673	24
36	303364	1025	991038	43	312327		687033	28
37	303979	1023	991012	43	312967	1067		
38	304593	1022	990986	43	313608	1065	686392	22
39	305207	1020	990960	43	314247	1064	685753	21
	305819	1019	990934		314885	1062	685115	20
40	The Property of the Party of th	_		-	-		10.684477	19
41	9.306430	1017	9.990908		9.315523	1061		
42	307041	1016	990882		316159	1060	683841	18
43	307650	1014	990855	44	316795	1058	683205	1
	308259	1013	990829		317430	1057	682570	1
44			990803		318064	1055	681936	1
45	308867	1011			318697	1054	681303	î
46	309474	1010	990777				680671	1
47	310080	1008	990750		319329	1053		
48	310685	1007	990724	44	319961	1051	680039	1
49	311289	1005	990697	44	320592	1050	679408	1
	311893	1004	990671	7.7	321222	1048	678778	1
50	and the second	-	100000000000000000000000000000000000000				10,678149	-
51	9.312495	1003	9.990644		9.321851	1047	0.070149	
52	313097	1001	990618	44	322479	1045	677521	1.
53	313698	1000	990591		323106	1044	676894	
		998	990565	1 77		1043	676267	
54	314297					1041	675642	
55	314897	997	990538				675017	
56	315495	996	990511			1040		
57	316092	994	990485	45		1039	674393	
58		993	990458	3 45	326231	1037	673769	
59		991	990431			1036	673147	1
60			99040		and the latest the second	1035	672525	
D.U	317879	990	99040	r to	001210	1000	0.000	- 1

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	9.317879	990	19.990404	145	19.3274741	1035	10.672526	60
ĭ	-318473	988	990378	45	328095	1033	671905	59
2	319066	987	990351	45	328715	1032	671285	58
3	319658	986	990324	45	329334	1030	670666	57
4	320249	984	990297	45	329953	1029	670047	56
5	320840	983	990270	45	330570	1028	669430	56
6	321430	982	990243		331187	1026		
							668813	54
7	322019	980	990215	45	331803	1025	668197	5
8	322607	979	990188	45	332418	1024	667582	55
9	323194	977	990161	45	333033	1023	666967	5]
10	323780	976	990134	45	333646	1021	666354	50
11	9.324366	975	9,990107	46	9.334259	1020	10.665741	40
12	324950	973	990079	46	334871	1019	665129	48
13	325534	972	990052	46	335482	1017	664518	47
14	326117	970	990025	46	336093	1016		
							663907	46
15	326700	969	989997	46	336702	1015	663298	4
16	327281	968	989970	46	337311	1013	662689	44
17	327862	966	989942	46	337919	1012	662081	4:
18	328442	965	989915	46	338527	1011	661473	45
19	329021	964	989887	46	339133	1010	660867	4
20	329599	962	989860	46	339739	1008	660261	40
21	9.330176	961	9.989832	46	9.340344	1007	10.659656	39
	330753	960	989804	46	340948	1006		
22							659052	38
23	331329	958	989777	46	341552	1004	658448	37
24	331903	957	.989749	47	342155	1003	657845	36
25	332478	956	989721	47	342757	1002	657243	3
26	333051	954	. 989693	47	343358	1000	656642	34
27	333624	953	989665	47	343958	999	656042	33
28	334195	952	989637	47	344558	998	655442	35
29	334766	950	989609	47	345157	997	654843	3
30	335337	949	989582	47	345755	996	654245	30
-	-	-	-		-	-		
31	9.335906	948	9.989553	47	9.346353	994	10.653647	25
32	336475	946	989525	47	346949	993	653051	28
33	337043	945	989497	47	347545	992	652455	2
34	337610	944	989469	47	348141	991	651859	26
35	338176	943	989441	47	348735	990	651265	2
36	338742	941	989413	47	349329	988	650671	24
37	339306	940	989384	47	349922	987	650078	2:
38	339871	939.	989356	47	350514	986	649486	25
39	340434	937	989328	47	351106		648894	
						985		2]
10	340996	936	989300	47	351697	983	648303	20
11	9.341558	935	9.989271	47	9.352287	982	10.647713	19
12	342119	934	989243	47	352876	981	647124	18
13	342679	932	989214	47	353465	980	646535	17
14	343239	931	989186	47	354053	979	645947	16
15	343797	930	989157	47	354640	977	645360	18
16	344355	929	989128	48	355227	976	644773	14
17			989100	48				
	344912	927			355813	975	644187	13
18	345469	926	989071	48	356398	974	643602	15
19	346024	925	989042	48	356982	973	643018	11
50	346579	924	989014	48	357566	971	642434	10
51	9.347134	922	9.988985	48	9.358149	970	10.641851	-
52	347687	921	988956	48	358731	969	641269	
53	348240	920	988927	48	359313	968	640687	,
54	348792			48				
		919	988898		359893	967	640107	(
55	349343	917	988869	48	360474	966	639526	
56	349893	916	988840	48	361053	965	638947	1
57	350443	915	988811	49	361632	963	638368	
58	350992	914	988782	49	362210	962	637790	
59	351540	913	988753	49	362787	961	637213	-53
60	352088	911	988724	49	363364	960	636636	(
100	Control of the Contro	1000						

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.352088	911	9.988724	49	9.363364	960	10.636636	60
1	352635	910	988695	49	363940	959	636060	59
2 3	353181 353726	909 908	988666 988636	49 49	364515 365090	958 957	635485 634910	58 57
4	354271	907	988607	49	365664	955	634336	56
5	354815	905	988578	49	366237	954	633763	55
6	355358	904	988548	49 49	366810	953	633190	54
7 8	355901 356443	903 902	988519 988489	49	367382 367953	952 951	632618 632047	53 52
ğ	356984	901	988460	49	368524	950	631476	51
10	357524	899	988430	49	369094	949	630906	50
11	9.358064	898	9.988401	49	9.369663	948	10.630337	49
12 13	358603 359141	897 896	988371 988342	49	370232 370799	946 945	629768 629201	48 47
14	359678	895	988312	50	371367	943	628633	46
15	360215	893	988282	50	371933	943	628067	45
16	360752	892	988252	50	372499	942	627501	44
17 18	361287 361822	891 890	988223 988193	50 50	373064 373629	941 940	626936 626371	43
19	362356	889	988163	50	374193	939	625807	41
20	362889	888	988133	50	374756	938	625244	40
21	9.363422	887	9.988103	50	9.375319	937	10.624681	39
22	363954	885	988073	50	375881	935	624119	38
23 24	364485 365016	884 883	988043 988013	50 50	376442 377003	934	623558 622997	37 36
25	365546	882	987983	50	377563	933 932	622437	35
26	366075	881	987953	50	378122	931	621878	34
27	366604	880	987922	50	378681	930	621319	33
28 29	367131 367659	879 877	987892 987862	50 50	379239 379797	929 928	620761 620203	32 31
30	368185	876	987832	51	380354	927	619646	30
$\frac{3}{31}$	9.368711	875	9.987801	$\frac{51}{51}$	9.380910	926	10.619090	29
32	369236	874	987771	51	381466	925	618534	28
33	369761	873	987740	51	382020	924	617980	27
34 35	370285 370808	872 871	987710 987679	51 51	382575 383129	923 922	617425 616871	26 25
36	37133 0	870	987649	51	383682	921	616318	24
37	371852	869	987618	51	384234	920	615766	23
38	372373	867	987588	51	384786	919	615214	22
39 40	372894 373414	866 865	987557 987526	51 51	385337 385888	918 917	614663 614112	21 20
41	9.373933	864	9.987496	$\frac{31}{51}$	$\frac{363666}{9.386438}$	915	10.613562	19
42	374452	863	987465	51	386987	914	613013	18
43	374970	862	987434	51	387536	913	612464	17
44 45	375487	861 860	987403 987372	52 52	388084	912	611916 611369	16 15
46	376003 376519	859	987341	52	388631 389178	911 910	610822	14
47	377035	858	997310	52	389724	909	610276	13
48	377549	857	987279	52	390270	908	609730	12
49 50	378063 378577	856	987248	52	390815	907	609185 608640	11 10
$\frac{50}{51}$		854	$\frac{987217}{9.987186}$	$\frac{52}{52}$	$\frac{391360}{9.391903}$	906	10.608097	10
52	9.379089 379601	853 852	9.987186	52 52	392447	905	607553	8
53	380113	851	987124	52	392989	903	607011	8
54	380624	850	987092	52	393531	902	606469	6
55 56	381134	849	987061	52	394073	901	605927	5 4
57	381643 382152	848 847	987030 986998	52 52	394614 395154	900 899	605386 604846	8
58	382661	846	986967	52	395694	898	604306	2
59	383168	845	986936	52	396233	897	603767	1
60	383675	844	986904	52	396771	896	603229	0
	. Cosine		Sine		Cotang.		l'ang.	M.

	Sine	D.	Cosine	I). Tang	g.	D.	Cotang	1
	0 9.38367				2 9.396	7711	896	10.603	- 1
					3 397		896	602	
2		-			3 397		895	602	
3				9 5			894	6016	
4							893	6010	
5	38620			16 5			892	6005	100
0				4 5	3999	990	891	6000	
7		-1 ,			3 400		890	5994	
8							889	5989	
9		-0.00		9 53			888	5984	
10	400.7		98658	7 53			887	5978	
11	9.38921	1 833	9.98655	5 53			_	Marine Committee	
12							886	10.5973	
13	39021			1 53			885	5968	
14	39070			9 53			884	5962	
15	39120	828					883	5957	
16	39170						882	5952	
17	392199				2000		881	5946	
18	39269	825	98633		4058 4063		880	5941	
19	393191		98629				879	5936	
20	393685				4068		878	5931	
21	9.394179				4074	-	377	59258	31 4
22	394673		9.986234	-100	9.4079		376	10.5920	55 3
23	395166	820	986202		4084		375	59159	
24	395658		986169		4089		374	59100	
25	396150		986137		4095		374	59047	9 3
26.	396641		986104	10 4	41004	15 8	373	58995	
27	397132		986072		41056		72	58943	
8	397621	816	986039		41109	92 8	71	58890	
29	398111	815	986007	100	4116		70	58838	
30	398600	814	985974		41213		69	58786	
N I	The second second		985942		41268	8 8	68	58734	
12	9.399088	813	9.985909		9.41317	9 8	67	10.58682	
3	399575	812	985876		41369		66	58630	
4	400062	811	985843	55	41421	- 1	65	58578	
5	400549	810	985811	55	41473		64	58526	
6	401035	809	985778	55	41525		64	58474	
7	401520	808	985745	55	41577		63	58422	
8	402005	807	985712	55	41629		62	58370	
3	402489	806	985679	55	41681		61	58319	
0	402972	805	985646	55	41732		60	58267	
- 1	403455	804	985613	55	41784		59		
	9.403938	803	9.985580	55	9.41835	-		582158	
2	404420	802	985547	55	41887	- 0		10.581649	
3	404901	801	985514	55	41938		57	581127	
1	405382	800	985480	55	41990			580613	
5	405862	799	985447	55	42041			580099	
3	406341	798	985414	56	42092			579585	
	406820	797	985380	56	421440			579073	
	407299	796	985347	56	421952	00		578560	
	407777	795		56	422463			578048	
	408254	794		56	422974			577537	
1 9	0.408731	794						577026	10
1	409207	793			9.423484			0.576516	9
1	409682	792		56	423993		8	576007	8
Tie	410157	791		56	424503			575497	7
1	410632	790		56	425011	84		574989	6
1	411106	789		56	425519	84		574481	6 5
1	411579	788	00=01-	56	426027	84.		573973	4
1	412052	787	0000-	56	426534	84		573466	3
1	412524	786		56	427041	84:		572959	2
		.00	2042161	(10	427547	046	1 1		- 10
13	412996	785		66	428052	843		572453	1

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1.7
0	9.412996	785	9.984944	57	9.428052	842	10.571948	60
1	413467	784	984910	57	428557	841	571443	5
2	413938	783	984876	57	429062	840	570938	58
3	414408	783	984842	57	429566	839	570434	5
4	414878	782	984808	57	430070	838	569930	56
5	415347	781	984774	57	430573	838	569427	5.
6	415815	780	984740	57	431075	837	568925	54
7	416283	779	984706	57	431577	836	568423	55
.8	416751	778	984672	57	432079	835	567921	55
9	417217	777	984637	57	432580	834	567420	5
10	417684	776	984603	57	433080	833	566920	50
11	9.418150	775	9.984569	57	9.433580	832	10.566420	45
12	418615	774	984535	57	434080	832	565920	48
13	419079	773	984500	57	434579	831	565421	4
14	419544	773	984466	57	435078	830	564922	46
15	420007	772	984432	58	435576	829	564424	45
16	420470	771	984397	58	436073	828	563927	44
17	420933	770	984363	58	436570	828	563430	4:
18	421395	769	984328	58	437067	827	562933	45
19	421857	768	984294	58	437563	826	562437	4]
20	422318	767	984259	58	438059	825	561941	40
21	9 422778	767	9.984224	58	9.438554	824	10.561446	39
22	423238	766	984190	58	439048	823	560952	38
23	423697	765	984155	58	439543	823	560457	37
24	424156	764	984120	58	440036	822	559964	36
25	424615		984085				559471	35
26		763		58	440529	821		34
	425073	762	984050	58	441022	820	558978	
27	425530	761	984015	58	441514	819	558486	38
85	425987	760	983981	58	442006	819	557994	35
29	426443	760	983946	58	442497	818	557503	31
30	426899	759	983911	58	442988	817	557012	30
31	9.427354	758	9.983875	58	9.443479	816	10.556521	29
32	427809	757	983840	59	443968	816	556032	28
33	428263	756	983805	59	444458	815	555542	27
34	428717	755	983770	59	444947	814	555053	26
35	429170	754	983735	59	445435	813	554565	25
36	429623	753	983700	59	445923	812	554077	24
37	430075	752	983664	59	446411	812	553589	23
38	430527	752	983629	59	446898	811	553102	22
39	430978	751	983594	59	447384	810	552616	21
10	431429	750	983558	59	447870	809	552130	20
11	9.431879	749	9.983523	59	9.448356	809	10.551644	19
12	432329	749	983487	59	448841		551159	18
3	432778	748	983452	59	449326	808	550674	17
4	433226	747	983416	59	449320	807	550190	16
						806		
5	433675	746	983381	59	450294	806	549706	15
6	434122	745	983345	59	450777	805	549223	14
7	434569	744	983309	59	451260	804	548740	13
8	435016	744	983273	60	451743	803	548257	12
9	435462	743	983238	60	452225	802	547775	11
0	435908	742	983202	60	452706	802	547294	10
	9.436353	741	9.983166	60	9.453187	801	10.546813	9
2	436798	740	983130	60	453668	800	546332	8
3	437242	740	983094	60	454148	799	545852	7
64	437686	739	983058	60	454628	799	545372	6
55	438129	738	983022	60	455107	798	544893	. 5
6	438572	737	982986	60	455586	797	514414	4
57	439014	736	982950	60	456064	796	543936	9
8	439456	736	982914	60	456542	796	543458	2
59	439897	735	982878	60	457019	795	542981	î
30	440338	734	982842	60	457496	794	542504	Ô
			000000	Se 40 1	TOLITOO	· JT	OXAUUT	- 4

74 Degrees.

T V	gi-a l	D.	,	D.	Tang.	D.	Cotang.	7.
М.			Cosine	60	9.457496	794	10.542504	60
0	9.440338 440778	734 733	9.982842 982805	60	457973	794	542027	59
2	441218	732	982769	61	458449	793	541551	58
3	441658	731	982733	61	458925	792	541075	57
4	442096	731	982696	61	459400	791	540600	56
5	442535	730	982660	61	459875	790	540125	55 54
6	442973 443410	729 728	982624 982587	61 61	460349 460823	790 789	539651 539177	53
8	443847	727	982551	61	461297	788	538703	52
9	444284	727	982514	61	461770	788	538230	5 1
10	444720	726	982477	61	462242	787	537758	<u>50</u>
11	9.445155	725	9.982441	61	9.462714	786	10.537286	49
12 13	445590	724 723	982404 982367	61 61	463186 463658	785 785	536814 536342	48 47
14	446025 446459	723	982331	61	464129	784	535871	46
15	446893	722	982294	ői	464599	783	535401	45
16	447326	721	982257	61	465069	783	534931	44
17	447759	720	982220	62	465539	782	534461	43
18 19	448191 448623	720 719	982183 982146	62 62	466008 466476	781 780	533992 533524	42 41
20	449054	718	982109	62	466945	780	533055	40
$\frac{20}{21}$	9.449485	717	9.982072	62	$\frac{163313}{9.467413}$	779	10.532587	39
22	449915	716	982035	62	467880	778	532120	38
23	450345	716	981998	62	468347	778	531653	37
24	450775	715	981961	62	468814	777	531186	36
25 26	451204 451632	714 713	981924 981886	62 62	469280 469746	776 775	530720 530254	35 34
27	452060	713	981849	62	470211	775	529789	33
28	452488	712	981812	62	470676	774	529324	32
29	452915	711	981774	62	471141	773	528859	31
30	453342	710	981737	62	471605	773	528395	30
31	9.453768	710	9.981699	63	9.472068	772	10.527932	29
32 33	454194 454619	709 708	981662 981625	63 63	472532 472995	771	527468 527005	28 27
34	455044	707	981587	63	473457	770	526543	26
35	455469	707	981549	63	473919	769	526081	25
36	455898	706	981512	63	474381	769	525619	24
37 38	456316 456739	705 704	981474 981436	63 63	474842 475303	768 767	525158 524697	23 22
39	457162	704	981399	63	475763	767	524237	21
40	457584	703	981361	63	476223	766	523777	20
41	9.458006	702	9.981323	63	9.476683	765	10.523317	19
42	458427	701	981285	63	477142	765	522858	100
43	458848	701	981247	63	477601	764	522399	17
44	459268 459688	700 699	981209 981171	63	478059 478517	763 763	521941 521483	16 15
46	460108	698	981133	64	478975	762	521025	14
47	460527	698	981095	64	479432	761	520568	13
48	460946	697	981057	64	479889	761	520111	12
49	461364	696	981019	64	480345	760	519655	11
50	461782	695	980981	64	480801	759	519199	10
51 52	9.462199 462616	695 694	9.980942 980904	64 64	9.481257 481712	759 758	10.518743 518288	8
53	463032	693	980866	64	482167	757	517833	9
54	463448	693	980827	64	482621	757	517379	6
55	463864	692	980789	64	483075	756	516925	5
56	464279	691	980750	64	483529	755	516471	4
57 58	464694 465108	690 690	980712 980673	64 64	483982 484435	755 754	516018 515565	3 2
59	465522	689	980635	64	484887	753	515113	î
60	465935	688	980596	64	485339	753	514661	lō,
	Cosine		Sine	Ī	Cetung.		Tang.	M.

73 Degrees.

-	4		ND TANGE	-		egrees		
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	9.465935	688	9.980596	64	9.485339	755	10.514661	60
1	466348	688	980558	64	485791	752	514209	59
2	466761	687	980519	65	486242	751	513758	58
3	467173	686	980480	65	486693	751	513307	57
4	467585	685	980442	65	487143	750	512857	56
5	467996	685	980403	65	487593	749	512407	55
6	468407	684	980364	65	488043	749	511957	54
7	468817	683	980325	65	488492	748	511508	53
8	469227	683	980286	65	488941	747	511059	52
9	469637	682	980247	65	489390	747	510610	51
10	470046	681	980208	65	489838	746	510162	50
_				_	-		-	-
11	9.470455	680	9.980169	65	9.490286	746	10.509714	49
12	470863	680	980130	65	490733	745	509267	48
13	471271	679	980091	65	491180	744	508820	47
14	471679	678	980052	65	491627	744	508373	46
15	472086	678	980012	65	492073	743	507927	45
16	472492	677	979973	65	492519	743	507481	44
17	472898	676	979934	66	492965	742	507035	43
18	473304	676	979895	66	493410	741	506590	42
19	473710	675	979855	66	493854	740	506146	41
20	474115	674	979816	66	494299	740	505701	40
21	9.474519	674	9.979776	66	9.494743	740	10.505257	39
22	474923	673	979737	66	495186	739	504814	38
23	475327	672	979697	66	495630	738	504370	37
24	475730	672	979658	66	496073	737	503927	36
25	476133	671	979618	66	496515	737	503485	35
26	476536	670	979579	66	496957	736	503043	34
27	476938	669	979539	66	497399	736	502601	33
28	477340	669	979499	66	497841	735	502159	32
	477741	668	979459	66	498282	734	501718	31
29					498722	734		30
30	478142	667	979420	66			501278	
31	9.478542	667	9.979380	66	9.499163	733	10.500837	29
32	478942	666	979340	66	499603	733	500397	28
33	479342	665	979300	67	500042	732	499958	27
34	479741	665	979260	67	500481	731	499519	26
35	480140	664	979220	67	500920	731	499080	25
36	480539	663	979180	67	501359	730	498641	24
37	480937	663	979140	67	501797	730	498203	23
38	481334	662	979100	67	502235	729	497765	22
39	481731	661	979059	67	502672	728	497328	21
						728		20
40	482128	661	979019	67	503109		496891	
41	9.482525	660	9.978979	67	9.503546	727	10.496454	19
42	482921	659	978939	67	503982	727	496018	18
43	483316	659	978898	67	504418	726	495582	17
44	483712	658	978858	67	504854	725	495146	16
45	484107	657	978817	67	505289	725	494711	15
46	484501	657	978777	67	505724	724	494276	14
47	484895	656	978736	67	506159	724	493841	13
						723	493407	12
48	485289	655	978696	68	506593			
49	485682	655	978655	68	507027	722	492973	11
50	486075	654	978615	68	507460	722	492540	10
51	9.486467	653	9.978574	68	9.507893	- 721	10.492107	
52	486860	653	978533	68	508326	721	491674	1 8
53	487251	652	978493	68	508759	720	491241	1
54	487643	651	978452	68	509191	719	490809	
55	488034	651	978411	68	509622	719	490378	1
56	488424	650	978370	68	510054	718	489946	1 4
57	488814	650	978329	68	510485	718	489515	
58	489204	649	978288	68	510916	717	489084	1 5
59	489593	648	978247	68	511346	716	488654	1
60	489982	648	978206	68	511776	716	488224	1 (

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
1	0	9.4899821					716	10.488224	60
3 491147 646 978083 69 513064 714 486307 4 491535 646 978042 69 513493 714 486307 5 491922 645 978001 69 513921 713 486079 6 492308 644 9777918 69 514349 713 485651 7 492695 644 9777876 69 515204 712 484796 8 493861 642 9777876 69 515204 712 484796 10 493851 642 977794 69 516057 710 483948 11 9.494236 641 9.77752 69 516057 710 483943 12 494621 641 9.77766 9 516057 710 483943 12 494588 639 977768 69 517335 709 482239 14 495388 639	1		648	978165		512206	716	487794	59
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53 510065 616 975974 72 534092 687 465908 54 510434 615 975930 72 534504 687 465496 55 510803 615 975887 72 534916 686 465084 56 511172 614 975844 72 535328 686 464672 57 511540 613 975800 72 535739 685 464261 58 511907 613 975757 72 536150 685 463850 59 512275 612 975714 72 536561 684 463439									10
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55 510803 615 975887 72 534916 686 465084 56 511172 614 975844 72 535328 686 464672 57 511540 613 975800 72 535739 685 464261 58 511907 613 975757 72 536160 685 463850 59 512275 612 975714 72 536561 684 463439									1 8
56 511172 614 975844 72 535328 686 464672 57 511540 613 975800 72 535739 685 464261 58 511907 613 975757 72 536150 685 463850 59 512275 612 975714 72 536561 684 463439									1
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Cosine Sine Cotang. Tang.					. ~				I M

71 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
01	9.512642	612	9.975670	73	9.536972	684	10.463028	60
1	513009	611	975627	73	537382	683	462618	59
2	513375	611	975583	73	537792	683	462208	58
3	513741	610	975539	73	538202	682	461798	57
4	514107	609	975496	73	538611	682	461389	56
5	514472	609	975452	73	539020	681	460980	55
6	514837	608	975408	73	539429	681	460571	54
7	515202	608	975365	73	539837	680	460163	53
8	515566	607	975321	73	540245	680	459755	52
9	515930	607	975277	73	540653	679	459347	51
10	516294	606	975233	73	541061	679	458939	50
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11	9.516657	605	9.975189	73	9.541468	678	10.458532	49
12	517020	605	975145	73	541875	678	458125	48
13	517382	604	975101	73	542281	677	457719	47
14	517745	604	975057	73	542688	677	457312	46
15	518107	603	975013	73	543094	676	456906	45
16	518468	603	974969	74	543499	676	456501	44
17	518829	602	974925	74	543905	675	456095	43
18	519190	601	974880	74	544310	675	455690	42
19	519551	601	974836	74	544715	674	455285	41
20	519911	600	974792	74	545119	674	454881	40
_		_		1				
21	9.520271	600	9.974748	74	9.545524	673	10.454476	39
22	520631	599	974703	74	545928	673	454072	38
23	520990	599	974659	74	546331	672	453669	37
24	521349	598	974614	74	546735	672	453265	36
25	521707	598	974570	74	547138	671	452862	35
26	522066	597	974525	74	547540	671	452460	34
27	522424	596	974481	74	547943	670	452057	33
28	522781	596	974436	74	548345	670	451655	35
29	523138	595	974391	74	548747	669	451253	31
30	523495	595	974347	75	549149	669	450851	30
								100
31	9.523852	594	9.974302	75	9.549550	668	10.450450	29
32	524208	594	974257	75	549951	668	450049	28
33	524564	593	974212	75	550352	667	449648	27
34	524920	593	974167	75	550752	667	449248	26
35	525275	592	974122	75	551152	666	448848	25
36	525630	591	974077	75	551552	666	448448	24
37	525984	591	974032	75	551952	665	448048	23
38	526339	590	973987	75	552351	665	447649	25
39	526693	590	973942	75	552750	665	447250	2
40	527046	589	973897	75	553149	664	446851	20
44.5				-			10.446452	19
41	9.527400	589	9.973852	75	9.553548	664		
42	527753	588	973807	75	553946	663	446054	18
43	528105	588	973761	75	554344	663	445656	1
44	528458	587	973716	76	554741	662	445259	1
45	528810	587	973671	76	555139	662	444861	1.
46	529161	586	973625	76	555536	661	444464	1
47	529513	586	973580	76	555933	661	444067	1:
48	529864	585	973535	76	556329	660	443671	1:
49	530215	585	973489	76	556725	660	443275	1
50	530565	584	973444	76	557121	659	442879	1
		10000		-			10,442483	-
51	9.530915	584	9.973398	76	9.557517	659		
52	531265	583	973352	76	557913	659	442087	
53	531614	582	973307	76	558308	658	441692	
54	531963	582	973261	76	558702	658	441298	
55	532312	581	973215	76	559097	657	440903	1
56	532661	581	973169	76	559491	657	440509	10
57	533009	580	973124	76	559885	656	440115	1.3
58	533357	580	973078	76	560279	656	439721	13
59	533704	579	973032	77	560673	655	439327	
	534052	578	972986		561066	655	438934	10
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	M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	Г
1 534399 577 972940 77 561459 654 438541 56 2 53745 577 972848 77 56244 653 437766 5 5 535783 576 972755 77 563028 653 436581 5 536129 575 972709 77 5633019 652 436581 65 436581 65 436581 652 436581 65 436581 653 436581 652 436581 653 436581 652 436581 652 436581 653 436581 653 436581 653 435798 56 661 435798 56 661 435798 56 661 436581 652 436581 652 436581 652 436581 652 436581 10 435798 56 661 438408 56 438408 4327 44 4342374 44 4342374 44 4343434 44 <	1==						655	10.438934	60
3 535092 577 972848 77 56244 653 437756 5 5 535783 576 972755 77 563028 653 436981 5 6 536129 575 972709 77 563419 652 436591 5 7 536474 574 972617 77 564320 651 435798 5 9 537163 573 972570 77 564592 651 435798 5 10 537507 573 972524 77 564933 650 435117 5 11 9.537851 672 972431 78 566153 649 434237 4 12 538194 572 972431 78 566153 649 434237 4 13 538538 671 972324 77 7664933 650 433347 4 14 5389807 579 972245	1	534 399	577						59
4 535438 576 972802 77 562636 653 4367364 5 5 535783 576 972709 77 563028 653 436792 56 6 536129 575 972709 77 563419 652 436189 56 7 538618 574 972570 77 5641202 651 435798 59 9 537163 573 972570 77 564592 651 435408 51 10 537507 573 972570 77 566493 650 435017 56 11 9.537851 572 9.72478 77 9.565373 650 10.434627 44 12 538194 572 9.72431 8 566573 649 433427 14 538800 571 972338 78 5665130 649 433434 14 14 538486 571 972245 78 566322									
5 535783 576 972755 77 5634028 653 436521 576 972709 77 563811 652 436581 67 9357163 573 972570 77 5641202 651 435798 535818 574 972617 77 5641202 651 435798 5351 972570 77 5641202 651 435408 5351 10 537507 573 972570 77 5645933 650 10 434627 44 435408 51 10 537507 573 9729247 77 564983 650 10 434627 44 11 9.537851 572 972931 78 5665373 669 10 434627 44 13 538538 571 972331 78 5665373 649 433487 44 15 539233 570 972215 78 566932 648 433068 44 17 34368 44 </td <td>3</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	3								
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8 536818 574 972617 77 564202 651 435708 55 9 537163 573 972570 77 564393 650 435408 51 10 537807 573 972570 77 564983 650 10.434627 43 11 9.537851 572 9.72473 77 565373 650 10.434627 44 13 538538 571 972385 78 5665432 649 4334548 45 15 539223 570 972291 78 566932 648 433688 46 16 539365 570 972291 78 567302 648 432680 44 17 539907 569 972195 78 567302 648 432680 44 18 540249 569 972151 78 568088 647 431902 431127 44 20 540331	6			972709			652		54
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14 539880 571 972338 78 566542 649 433458 44 16 539253 570 972245 78 566932 648 433608 44 17 539907 569 972198 78 567720 647 432291 42 18 540249 569 972151 78 568098 647 432291 42 19 540590 568 972105 79 568486 646 431514 42 20 540931 568 972017 78 5568473 646 431514 42 21 9.541272 567 9.972011 78 5569261 645 10.430739 32 22 541613 567 971964 78 570035 645 429965 37 23 541962 566 971870 78 570432 644 422957 42426293 566 971870 78 571956 <td>12</td> <td>538194</td> <td>572</td> <td>972431</td> <td></td> <td>565763</td> <td></td> <td></td> <td>48</td>	12	538194	572	972431		565763			48
15									
16 539565 570 972198 78 567709 648 432880 44 18 540249 569 972151 78 568098 647 431902 42 20 540931 568 972053 78 568493 646 431514 41 21 9.541272 567 9.972011 78 568493 646 431127 44 22 541613 567 9.972011 78 569649 645 430352 38 23 541953 566 971877 78 570422 644 429578 36 24 542293 565 971823 78 570809 644 429191 36 26 542971 565 971782 79 571581 643 428419 32 27 543310 564 971729 79 571581 643 428419 32 29 543987 563 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>									
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19								432291	43
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22 541613 567 971964 78 569648 645 490352 38 24 542293 566 971870 78 570035 645 429965 37 25 542632 565 971870 78 570809 644 429191 35 26 542971 565 971776 78 571195 643 428419 32 27 543310 564 971729 79 571581 643 428419 32 28 543649 564 971635 79 572352 642 428033 32 30 544325 563 971538 79 573323 641 10.426877 23 31 9.544663 562 9.971540 79 9.573123 641 426493 22 34 545388 561 971446 79 573607 641 426493 22 34 546674 561					_				
23 541953 566 971917 78 570035 645 429965 32 24 542293 566 971870 78 570432 644 429191 32 25 542632 565 971776 78 570490 644 429191 32 26 542971 565 971776 78 571195 643 428805 34 27 543310 564 971635 79 571967 642 428033 32 29 543987 563 971635 79 572738 642 427648 31 30 544325 563 971587 79 572738 642 4276628 33 32 545000 562 971493 79 573507 641 426493 28 34 545674 561 971398 79 574660 639 424576 24 35 546011 560 9713									
24 542893 566 971870 78 570422 644 429578 36 26 5428971 565 971873 78 570809 644 429191 32 27 543310 564 971729 79 571881 643 428419 32 28 543649 564 971682 79 571967 642 428033 33 29 543987 563 971635 79 572352 642 427648 31 30 544325 563 971580 79 573123 641 10.426877 22 32 545000 562 971493 79 573507 641 426493 22 34 545674 561 971398 79 574276 640 426724 26 35 546011 560 971351 79 574660 639 4245956 24 36 5460347 560 <td< td=""><td></td><td></td><td></td><td>971917</td><td></td><td></td><td></td><td></td><td>37</td></td<>				971917					37
26 542971 565 971776 78 571195 643 428805 34 27 543310 564 971729 79 571891 643 428805 34 28 543649 564 971692 79 571967 642 428033 32 29 543987 563 971635 79 572385 642 427648 31 30 544325 563 971580 79 572385 642 427628 33 34 546600 562 9.971540 79 573507 641 10.426877 22 33 54538 561 971446 79 573392 640 426108 22 34 545674 561 971303 79 574660 639 424574 24 35 546011 560 971303 79 575446 639 42456 24 37 546683 559 97		542293	566	971870	7.8	570422	644	429578	36
27 543310 564 971729 70 571581 643 428419 32 28 543987 563 971682 79 571967 642 428033 33 30 543925 563 971588 79 572352 642 427262 33 31 9.544663 562 9.971540 79 9.573123 641 10.426877 22 32 545000 562 9.971493 79 573507 641 426493 22 33 545338 561 971493 79 574276 640 426708 22 34 545674 561 971391 79 574276 640 426724 22 35 546011 560 971351 79 574660 639 424573 23 36 546847 560 971303 79 575427 639 424573 22 37 546883 559									
28 543649 564 971682 79 571967 642 428033 32 29 543987 563 971637 79 572352 642 427648 31 30 544325 563 971598 79 572372 642 427626 36 31 9.544663 562 9.971540 79 9.573123 641 10.426877 22 32 545000 562 9.971446 79 573807 641 426493 22 34 545674 561 971398 79 574276 640 426724 26 35 546011 560 971303 79 574660 639 424340 24 36 546347 560 971303 79 575427 639 4244573 23 37 546683 559 971208 79 575410 639 424373 23 38 547019 559									
29								428033	32
31 9.544663 562 9.971540 79 9.573123 641 10.426877 25 25 25 25 25 25 25	29								31
32 545000 562 971493 79 573507 641 426493 28 33 545338 561 971446 79 573507 641 426493 28 34 545674 561 971398 79 57426 640 426724 26 35 546011 560 971351 79 574660 639 424356 24 36 546347 560 971208 79 575427 639 424573 23 37 546683 559 971256 79 575427 639 424573 23 38 547019 559 971268 79 576310 638 424190 23 39 547354 558 971113 79 576576 637 423424 24 40 547689 558 971108 80 577341 636 422659 18 41 9.548024 557 9.79	_	544325	563	971588	79	572738	642	427262	30
38 545338 561 971446 79 573892 640 426108 27 34 545674 561 971398 79 574276 640 426704 24 35 546011 560 971303 79 575646 639 424340 22 36 546347 560 971303 79 575810 639 424956 24 37 546683 559 971208 79 575810 639 424956 24 38 547019 559 971208 79 575810 638 424902 23 39 547354 558 971113 79 576576 637 423424 20 41 9.548024 557 9.71068 80 5.75958 637 10.423041 14 42 548359 557 971018 80 577331 636 422277 17 43 548693 556 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>29</td></t<>									29
34 545674 561 971398 79 574276 640 425724 22 36 546347 560 971303 79 574660 639 425340 22 37 546683 559 971206 79 575427 639 424573 23 38 547019 559 971208 79 575810 638 42490 22 39 547354 558 971113 79 576576 637 423424 22 40 547689 558 971113 79 576576 637 423424 22 41 9.548024 557 9.971066 80 9.576958 637 10.423041 14 42 548359 557 971018 80 5778450 636 422277 17 44 549027 556 970922 80 578104 636 421896 16 45 549360 555									
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38 547019 559 971208 79 575810 638 424190 2239 39 547354 558 971161 79 576576 637 423807 24 40 547689 558 971113 79 576576 637 423424 22 41 9.548024 557 9.971066 80 9.576958 637 10.423041 15 42 548359 557 971018 80 577341 636 422659 16 43 548693 556 970970 80 5777341 636 422277 14 45 549360 555 970970 80 578486 635 421131 14 46 549693 555 970827 80 578486 635 421131 14 47 550026 554 970771 80 579248 634 420752 13 49 5504925 53					79		639	424956	24
39 547354 558 971161 79 576193 638 423807 21 40 547689 558 971113 79 576193 638 423807 21 41 9.549024 557 9.971066 80 9.576958 637 10.423041 18 43 548693 556 970970 80 577341 636 422277 14 45 549360 555 970874 80 578104 636 421514 15 46 549693 555 970874 80 578867 635 421514 16 47 550026 554 9707731 80 579248 634 420752 13 48 550359 553 970683 80 580099 634 420371 12 49 550692 553 970638 80 580399 633 419611 10 51 9.551356 522									
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41 9.548024 557 9.971066 80 9.576958 637 10.423041 15 42 548359 557 971018 80 577341 636 422659 18 43 548693 556 970970 80 577723 636 422277 17 44 549027 556 970972 80 578104 636 421896 16 45 549600 555 970874 80 578486 635 421133 14 46 549693 555 970827 80 578667 635 421133 14 47 550026 554 970773 80 579629 634 420371 12 49 550692 553 970638 80 580099 634 420371 12 50 551024 553 970638 80 580769 633 419611 10 51 9.551356 552									20
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52 551687 552 970538 80 581149 632 418851 8 53 552018 552 970490 80 581528 632 418472 7 54 552349 551 970442 80 581907 632 418093 6 55 552680 551 970394 80 582296 631 417714 5 56 553010 550 970345 81 582665 631 417335 4 57 553341 550 970297 81 583043 630 416957 3 58 553670 549 970249 81 583422 630 416578 2 59 554000 549 970200 81 583800 629 416200 1 60 554329 548 970152 81 584177 629 415823 0									_
54 552349 551 970442 80 581907 632 418093 655 55 552680 551 970394 80 582896 631 417714 56 56 553010 550 970345 81 582665 631 417714 56 57 553341 550 970297 81 583043 630 416957 3 58 553670 549 970249 81 583422 630 416578 2 59 554000 549 970200 81 583800 629 416200 1 60 554329 548 970152 81 584177 629 415823 0									8
54 552349 551 970442 80 581907 632 418093 655 55 552680 551 970394 80 582896 631 417714 56 56 553010 550 970345 81 582665 631 417714 56 57 553341 550 970297 81 583043 630 416957 3 58 553670 549 970249 81 583422 630 416578 2 59 554000 549 970200 81 583800 629 416200 1 60 554329 548 970152 81 584177 629 415823 0									7
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60 554329 548 970152 81 584177 629 415823 0		554000							1
Cosine Sine Cotang. Tang. M.	60	554329							0
		Cosine		Sine		Cotang.		Tang.	M.

69 Degrees.

615

612

53

 $\overline{49}$

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 $\overline{29}$

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Cotang.

415068

414314 413938 413561

413185 |

411309 48 410934 47 410560 46

410186 45 409812 44 409438 43 409065 42

408692

10.407946 407574 407202

400909 |

400173 18 399806 17 399438 16

399071 | 15

398704 | 14 398338 | 13

397605 | 11

Tang. | M.

10.396873

10.400541

10.404232

404602 30

10.411684

10.415823

SINES AND TANGENTS.

Cosine

9.970152 81

970103 81

970055 81

970006 81

969957 81

969909 81

969860 81

969762 81

 $\overline{82}$

9.968628 83

968678 83

968479 83

968278 83

968228 84

968178 84

9.968128 84 968078 84

967876 84

967826 84

967775 84

967725 84

967674 84

967573 84

967522 85

967421 85

967370 85

967268 85

967217 85

9.967624 84

969075 82 969025 82 968976 82 968926 83

9.969124

969518 82

969420 82 969370 82

969321 82

9.969616

D.

Tang.

19.584177

9.603127

9.599459

9.595768

9.592054

9.588316

М.

 $\overline{11}$

16

36

Sine

68856

9.570751

9.567587

9.564396

9.561178

9.557932

0 | 9.554329

D.

546

542

541 541

540 539

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523 523

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Cotang. 68 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.573575	521	9.967166	85	9.606410	606	10.393590	60
1	573888	520	967115	85	606773	606	393227	59
2 3	574200	520	967064	85	607137 607500	605 605	392863	58
1 4	574512 574824	519 519	967013 966961	85 85	607863	604	392500 392137	57 56
5	575136	519	966910	85	608225	604	391775	55
6	575447	518	966859	85	608588	604	391412	54
7	575758	518	966808	85	608950	603	391050	53
8	576069 576379	517 517	966756 966705	86	609312 609674	603 603	390688 390326	52 51
10	576689	516	966653	86	610036	602	389964	50 50
iii	9.576999	516	9.966602	$\frac{86}{86}$	9.610397	602	10.389603	49
12	577309	516	966550	86	610759	602	389241	48
13	577618	515	966499	86	611120	601	388880	47
14	577927	515	966447	86	611480	601	388520	46
15 16	578236 578545	514 514	966395 966344	86	611841 612201	601 600	388159 387799	45 44
17	578853	513	966292	86	612561	600	387439	43
18	579162	513	966240	86	612921	600	387079	42
19	579470	513	966188	86	613281	599	386719	41
20	579777	512	966136	86	613641	599	386359	40
21	9.580085	512	9 966085	87	9.614000	598	10.386000	39
22 23	580392 580699	511 511	966033 965981	87 87	614359 614718	598 598	385641 385282	38 37
24	581005	511	965928	87	615077	597	384923	36
25	581312	510	965876	87	615435	597	384565	35
26	581618	510	965824	87	615793	597	384207	34
27 28	581924 582229	509	965772	87	616151	596	383849	33
20 29	582535	509 509	965720 965668	87 87	616509 616867	596 596	383491 383133	32 31
3 0	582840	508	965615	87	617224	595	382776	30
$\overline{31}$	9.583145	508	9.965563	87	9 617582	595	10.382418	29
32	583449	507	965511	87	617939	595	382061	28
33	583754	507	965458	87	618295	594	381705	27
34 35	584058 584361	506 506	965406 965353	87	618652 619008	594	381348 380992	26
36	584665	506	965301	88	619364	594 593	380636	25 24
37	584968	505	965248	88	619721	593	380279	23
38	585272	505	965195	88	620076	593	379924	22
39	585574	504	965143	88	620432	592	379568	21
40	585877	504	965090	88	620787	592	379213	20
41 42	9.586179 586482	503 503	9.965037 - 964984	88 88	9.621142 621497	592 591	10.378858 378503	19 18
43	586783	503	964931	88	621852	591	378148	17
44	587085	502	964879	88	622207	590	377793	16
45	587386	502	964826	88	622561	590	377439	15
46	587688	501	964773	88	622915	590	377085	14
47 48	587989 588289	501 501	964719 964666	88 89	623269 623623	589 589	376731 376377	13 12
49	588590	500	964613	89	623976	589	376024	11
50	588890	500	964560	89	624330	588	375670	10
51	9.589190	499	9.964507	89	9.624683	588	10.375317	9
52	589489	499	964454	89	625036	588	374964	8
53 54	589789	499	964400	89 89	625388	587	374612	7
55	590088 590387	498 498	964347 964294	89	625741 626093	587 587	374259 373907	6 5
56	590686	497	964240	89	626445	586	373555	4
57	590984	497	964187	89	626797	586	373203	3
58 59	591282 591580	497	964133	89	627149	586	372851	2
60	591878	496 496	964080 964026	89 89	627501 627852	585 585	372499 372148	1 0
Ë	Cosine	200				000		
	Cosine		Sine		Cotang.		Tang.	M.

0			Cosine	D.	Tang.	D.	Cotang.	: 1
		496	9.964026	89	9.627852	585	10.372148	60
	592176 592473	495 495	963972 963919	89 89	628203 628554	585 585	371797 371446	59 58
2 3	592770	495	963865	90	628905	584	371095	57
4	593067	494	963811	90	629255	584	370745	56
5	593363	494	963757	90	629606	583	370394	55
6	593659	493	963704	90	629956	583	370044	54
7 8	593955 594251	493 493	963650 963596	90 90	630306 630656	583	369694 369344	53 52
9	594547	492	963542	90	631005	583 582	368995	51
1Ŏ	594842	492	963488	90	631355	582	368645	50
11	9.595137	491	9.963434	90	9.631704	582	10.368296	49
12	595432	491	963379	90	632053	581	367947	48
13 14	595727 596021	491	963325 963271	90	632401 632750	581	367599 367250	47 46
15	596315	490 490	963217	90	633098	581 580	366902	45
16	596609	489	963163	90	633447	580	366553	44
17	596903	489	963108	91	633795	580	366205	43
18	597196	489	963054	91	634143	579	365857	42
19 20	597490 597783	488	962999	91	634490 634838	579	365510 365162	41 40
$\frac{20}{21}$		488	962945	$\frac{91}{91}$	9.635185	579	10.364815	39
22	9.598075 598368	487 487	9.962890 962836	91	635532	578 578	364468	38
23	598660	487	962781	91	635879	578	364121	37
24	598952	486	962727	91	636226	577	363774	36
25	599244	486	962672	91	636572	577	363428	35
26	599536	485	962617	91	636919	577	363081	34
27 28	599827 600118	485 485	962562 962508	91 91	637265 637611	577	362735 362389	33 32
29	600409	484	962453	91	637956	576 576	362044	31
30	600700	484	962398	92	638302	576	361698	30
31	9.600990	484	9.962343	92	9.638647	575	10.361353	29
32	601280	483	962288	92	638992	575	361008	28
33	601570	483	962233	92	639337	575	360663	27
34 35	601860 602150	482	962178	92 92	639682	574	360318 359973	26 25
36	602439	482 482	962123 962067	92	640027 640371	574 574	359629	24
37	602728	481	962012	92	640716	573	359284	23
38	603017	481	961957	92	641060	573	3 58940	22
39	603305	481	961902	92	641404	573	358596	21
40	603594	480	961846	92	641747	572	358253	20
41	9.603882	480	9.961791	92	9.642091	572	10.357909	19
42 43	604170 604457	479 479	961735 961680	92 92	642434 642777	572 572	357566 357223	18 17
44	604745	479	961624	93	643120	571	356880	16
45	605032	478	961569	93	643463	571	356537	15
46	605319	478	961513	93	643806	571	856194	14
47 48	605606	478	961458	93 93	644148	570	355852	13
48	605892 606179	477 477	961402 961346	93	644490 644832	570 570	355510 355168	12 11
50	606465	476	961290	93	645174	569	354826	iö
51	9,606751	476	9.961235	$\frac{55}{93}$	9.645516	569	10.354484	9
52	607036	476	961179	93	645857	569	354143	8
53	607322	475	961123	93	646199	569	353801	7
54	607607	475	961067	93	646540	568	353460	6
55 56	607892	474 474	961011	93 93	646881	568	353119	5
57	608177 608461	474	960955 960899	93	647222 647562	568 567	352778 352438	3
53	608745	473	960843	94	647903	567	352097	2
59	609029	473	960786	94	648243	567	351757	ĩ
60 !	609318	473	960730	94	648583	56 6	851417	0
1	Cosine		Sine		Cotang.		Tang.	M.

1	Sine		1 0 :					_
		D.	Cerine	D.	Tang.	D.	Cotang.	
0	9.609313 609597	473 472	9.960730 960674	94 94	$9.645583 \\ 648923$		10.351417 351077	60
2	609880	472	960618		649263	566	350737	59 58
ã	610164	472	960561		649602		350398	57
4	610447	471	960505	94	649942	565	350058	56
5	610729	471	960448		650281	565	349719	55
6	611012	470	960392		650620		349380	54
7 8	611294 611576	470 470	960335 960279		650959 651297	564 564	349041 348703	53
9	611858	469	960222	94	651636	564	348364	52 51
10	612140	469	960165		651974		348026	50
$\overline{11}$	9.612421	469	9.960109		9.652312	563	10.347688	49
12	612702	468	960052	95	652650	563	347350	48
13	612983	468	9 59995		652988	563	347012	47
14	613264	467	959938	95	653326	562	346674	46
15 16	613545 613825	467 467	959882 959825	95 95	653663 654000	562 562	346337 346000	45
17	614105	466	959768	95	654337	561	345663	44
18	614385	466	959711	95	654674	561	345326	42
19	614665	466	959654	95	655011	561	344989	41
20	614914	465	9 59596	95	655348	561	344652	40
21	9.615223	465	9.959539	95	9.655684	560	10.344316	39
22	615502	465	959482	95	656020	560	343980	38
23 24	615781	464	959425 959368	95	656356	560	343644	37
25	616060 616338	464 464	959310	95 96	656692 657028	559 559	343308 342972	36 35
26	616616	463	959253	96	657364	559	342636	34
27	616894	463	959195	96	657699	559	342301	33
28	617172	462	959138	96	658034	558	341966	32
29	617450	462	959081	96	658369	558	341631	31
$\frac{30}{2}$	617727	462	959023	96	658704	558	341296	30
31 32	9.618004 618281	461	9.958965	96	9.659039	558	10.340961	29
33	618558	461 461	958908 958850	96 96	659373 659708	557 557	340627 340292	28 27
34	618834	460	958792	96	660042	557	339958	26
35	619110	460	958734	96	660376	557	339624	25
36	619386	460	958677		660710	556	3 39290	24
37 38	619662	459	958619	96	661043	556	338957	23
39	619938 620213	459 459	958561 958503	96 97	661377 661710	556 555	338623 338290	22
40	620488	458	958445	97	662043	555	337957	21 20
$\frac{1}{41}$	9.620763	458	9.958387	$\frac{37}{97}$	9.662376	555	10.337624	19
42	621038	457	958329	97	662709	554	337291	18
43	621313	457	958271	97	663042	554	336958	17
44	621587	457	958213	97	663375	554	336625	16
45 46	621861	456	958154 958096	97	663707	554	336293	15
47	622135 622409	456 456	958096 958038	97 97	664039 664371	553 553	335961	14
48	622682	455	957979	97	664703	553	335629 335297	13 12
49	622956	455	957921	97	665035	553	334965	11
50	623229	455	957863	97	665366	552	334634	îô
51	9.623502	454	9.957804	97	9.665697	552	10.334303	9
52 53	623774	454	957746	98	666029	552	333971	8
53 54	624047	454	957687	98	666360	551	333640	7
55	624319 624591	453 453	957628 957570	98 98	666691 667021	551	333309	6
56	624863	453	957511	98	667352	551 551	332979 332648	5 4
57	625135	452	957452	98	667682	550	332318	3
58	625406	452	957393	98	668013	550	331987	2
59 60	625677	452	957335	98	668343	550	331657	1
00	625948	451	957276	98	668672	550	331328	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.6259481	451	9.957276		9.6686731	550	10.331327	60
1	626219	451	957217	98	669002	549	330998	59
2	626490	451	957158	98	669332	549	330668	58
3	626760	450	957099	98	669661	549	330339	57
4	627030	450	957040	98	669991	548		56
5	627300	450	956981	98	670320	548	329680	55
6	627570	449	956921	99	670649	548		54
7	627840	449	956862	99	670977	548		53
8	628109	449	956803	99	671306	547		52
9	628378	448	956744	99	671634	547		51
	628647	448	956684	99	671963	547		50
10				_		_	10.327709	$\frac{30}{49}$
11	9.628916	447	9.956625	99	9.672291	547	327381	49
12	629185	447	956566	99	672619	546	327053	47
13	629453	447	956506	99	672947	546		
14	629721	446	956447	99	673274	546	326726	46
15	629989	446	956387	99	673602	546	326398	45
16	630257	446	956327	99	673929	545	326071	44
17	630524	446	956268	99	674257	545	325743	43
18	630792	445	956208	100	674584	545	325416	42
19	631059	445	956148	100	674910	544	325090	41
20	631326	445	956089	100	675237	544	324763	40
21	9.631593	444	9.956029	100	9.675564	544	10.324436	39
22	631859	444	955969	100	675890	544	324110	38
23	632125	444	955909	100	676216	543	323784	37
	632392	443	955849	100	676543	543	323457	36
24			955789	100	676869	543	323131	25
25	632658	443	955729	100	677194	543	322806	34
26	632923	443		100		542	322480	33
27	633189	442	955669		677520			32
28	633454	442	955609	100	677846	542	322154	31
29	633719	442	955548	100	678171	542	321829	
30	633984	441	955488	100	678496	542	321504	30
31	9.634249	441	9.955428	101	9.678821	541	10.321179	29
32	634514	440	955368	101	679146	541	320854	28
33	634778	440	955307	101	679471	541	320529	27
34	635042	440	955247	101	679795	541	320205	26
35	635306	439	955186	101	680120	540	319880	25
36	635570	439	955126	101	680444	540	319556	24
37	635834	439	955065	101	680768	540	319232	25
38	636097	438	955005	101	681092	540	318908	25
39	636360	438	954944	101	681416	539	318584	
40	636623	438	954883	101	681740	539	318260	
_				-			10.317937	19
41	9.636886	437	9.954823	101	9.682063	539		
42	637148	437	954762	101	682387	539	317613	
43	637411	437	954701	101	682710	538	317290	
44	637673	437	954640	101	683033	538	316967	
45	637935	436	954579	101	683356	538	316644	
46	638197	436	954518	102	683679	538	316321	
47	638458	436	954457	102		537	315999	
48	638720	435	954396	102		537	315676	
49	638981	435	954335	102	684646	537	315354	
50	639242	435	954274	102	684968	537	315032	1
_		434	9.954213	102	9.685290	536	10.314710	
51	9.639503		954152			536	314388	
52	639764	434				536	314066	
53	640024	434	954090			536	31374	
54	640284	433	954029					
55	640544	433	953968			535	313423	
56	640804	433	953906			535	313109	
57	641064		953845			535	31278	
58	641324		953783			535	31246	
59		432	953722			534	31213	
60			953660	103	688182	534	31181	31

	M.	Sine	D.	Cosine	D.	Tanc.	D.	Cotang.	
Section Sect									
Same									
4 642877 430 953413 103 689463 533 310177 55 643393 430 953290 103 690103 533 309877 54 643690 429 953128 103 690423 533 309877 54 3098577 52 3099258 52 3099258 52 3099258 52 309938 51 10 644423 428 953104 103 691062 532 309819 50 308938 51 11 9.644680 428 9.552980 104 692019 531 3079818 52 308938 51 11 3044680 428 9.52980 104 692019 531 3079818 307981 48 645193 427 952851 104 6920338 531 307344 66 464519 427 9528731 104 692975 531 307344 46 6645962 426 952669 104 693293 530 308884 32 <th></th> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
6 6443993 430 953290 103 690103 533 309897 54 7 643650 429 9533228 103 690423 533 309557 53 8 643908 429 953104 103 690742 532 309358 52 9 644165 429 953104 103 69162 532 309838 51 10 644423 428 953042 103 691861 532 308619 50 11 9 644680 428 9532918 104 692338 531 307662 47 14 644430 428 9525918 104 692338 531 307662 47 14 645450 427 952731 104 692338 531 307662 47 14 645450 427 952731 104 692393 531 307662 47 15 645706 427 952731 104 693293 530 306707 44 16 6456218 426 952666 104 693393 530 306707 44 17 646218 426 952666 104 693393 530 306707 44 18 646474 426 952541 104 693303 530 306707 44 18 646474 426 952541 104 694565 520 306838 43 18 646474 426 95241 104 694566 529 305434 40 21 9 64729 425 952481 104 694566 529 305434 40 22 64494 424 952231 104 695261 852 305412 40 23 646784 425 952419 104 695261 852 305412 40 24 64804 424 952231 104 695261 852 305412 304799 38 23 647749 424 952231 104 695501 528 303530 34 24 64804 424 952231 105 696470 528 303530 34 25 648512 423 951081 105 696470 528 303530 34 28 649020 423 951917 105 697103 528 303231 33 28 649020 423 951917 105 697403 528 303231 33 28 649020 423 951910 105 696470 528 303530 34 28 649020 423 951910 105 697420 527 302264 30 29 649527 422 95168 105 697420 527 302264 30 31 9 649521 422 951584 105 699316 526 300388 32 33 650287 421 951602 105 699316 526 300388 34 35 650792 421 951602 105 699316 526 300388 34 36 651649 420 951349 106 69947 526 300368 24 37 65255 419 951529 105 699316 526 300388 24 38 651649 420 951326 106 700893 525 299737 22 36 650539 421 951600 105 699362 526 300388 24 39 65048 429 951666 106 706783 524 299107 20 40 652052 419 951529 106 70678 525 299737 22 36 65306 418 950968 106 706930 522 299471 16 46 653058 417 950778 106 702486 524 299584 10 39 65806 418 950968 106 702486 524 299584 10 40 652052 419 951600 107 706503 522 299427 11 50 654658 416 950330 107 704663 522 295964 10 50 654658 416 950394 107 705603 521 294397 55 50 656799 413 949845 107 706561 521 294484 4 50 657047 413 949845 107 707666 520 298848 0									
7 643650 429 953228 103 690423 532 309258 52 9 644165 429 953104 103 691062 532 308938 51 10 644423 428 953042 103 691881 532 308938 51 11 9.644680 428 952918 104 692019 531 10.308300 99 12 644936 428 952918 104 692019 531 307662 47 456193 427 952731 104 6922656 531 307624 47 15 645706 427 952731 104 693293 530 306707 44 17 646218 426 952606 104 693293 530 306707 42 18 646724 426 952641 104 693293 530 306707 42 20 646724 <	5								
8 644908 429 953166 103 690742 532 309258 52 9 644165 429 953104 103 691062 532 308619 50 10 644423 428 953042 103 691381 532 308619 50 11 9 644680 428 953042 103 692019 531 10.308300 49 12 644936 428 952518 104 692019 531 307364 46 13 645193 427 9525731 104 692338 531 307662 47 14 645450 427 952731 104 692398 531 307662 47 15 645766 427 952731 104 693293 530 306707 44 16 6456218 426 952669 104 693323 530 306707 44 17 646218 426 952660 104 693323 530 306707 44 18 646744 428 952544 104 693930 530 306707 42 19 646729 425 952491 104 694586 529 304634 40 19 646744 428 952241 104 694288 530 305752 41 20 646984 425 952419 104 694586 529 304534 40 21 9.647240 425 9.952356 104 964566 529 304482 37 22 647494 424 952231 104 695518 529 304482 37 23 647749 424 952231 104 695518 529 304482 37 24 648004 424 952168 105 695518 529 304482 37 25 648528 424 952168 105 695586 529 304464 36 25 648528 424 952168 105 695586 529 304462 37 26 648766 423 951980 105 696787 528 303230 34 27 648766 423 951980 105 696787 528 3032897 32 29 649274 422 951854 105 697420 528 303230 34 26 649527 422 9515917 105 697103 528 302897 32 29 649274 422 951656 105 697420 527 302580 31 30 649527 422 951650 106 697420 528 303280 34 31 9.649781 422 951656 105 699385 527 302580 31 30 649527 422 951650 106 699470 528 302897 32 32 650034 422 951650 105 699632 527 302580 31 32 650034 422 951650 105 699632 527 302580 31 34 650539 421 951539 105 699632 526 300684 25 35 650792 421 951696 106 999632 526 300684 25 36 651644 420 951412 105 699632 526 300684 25 36 652555 418 951032 106 700578 525 299422 11 36 65308 417 950778 106 700878 525 299427 10 36 65308 418 950841 106 702466 524 297534 15 36 656308 417 950778 106 702463 522 299422 11 36 654309 416 950580 106 702466 524 297534 15 36 656505 418 950980 107 704663 522 295650 19 37 965300 419 951529 106 700678 525 299422 11 36 655058 416 950984 107 705603 521 299497 52 38 655080 416 950984 107 705603 521 299497 55 38 65507 415 950980 107 704663 522 295953 75 38 65507 415 950980 107 704663 522 295533 75 38 65507 415	6								
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20 646984 425 952419 104 694566 529 305434 40 21 9.647240 425 9.952356 104 695201 529 304799 38 22 647749 424 952231 104 695518 529 304482 37 24 648004 424 952168 105 695836 529 304482 37 26 648258 424 952168 105 696153 528 303847 35 26 648512 423 952043 105 696787 528 303213 33 27 648766 423 951917 105 6977103 528 302287 32 29 649274 422 951854 105 697420 527 302580 31 30 649527 422 951651 105 698053 527 301491 29 31 9.649781 422									
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37 651297 420 951349 106 699947 526 300053 23 38 651549 420 951286 106 700263 525 299737 22 39 651800 419 951222 106 700893 525 299107 20 41 9.652304 419 9.951159 106 700893 525 299107 20 42 652555 418 951032 106 701523 524 298473 17 43 652806 418 950968 106 701523 524 298163 17 44 653057 418 950968 106 702152 524 297848 16 45 653088 417 950778 106 702466 524 297848 16 46 653558 417 950741 106 703095 523 297220 14 47 653808 417									
38 651549 420 951286 106 700263 525 299737 22 39 651800 419 951222 106 700578 525 299427 20 41 9.652304 419 951122 106 700893 525 299107 20 41 9.652304 419 9.951096 106 701523 524 298477 19 42 652555 418 950932 106 701523 524 298477 19 44 653057 418 950905 106 702152 524 298163 17 45 653308 418 9509451 106 702466 524 297534 16 46 653558 417 950778 106 702780 523 297534 16 48 654059 416 9505861 106 703495 523 296591 13 49 654309 416									
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57 656302 414 950074 107 706228 521 293772 8 58 656551 414 950010 107 706541 521 293452 59 656799 413 949945 107 706854 521 293146 1 60 657047 413 949881 107 707166 520 292834 0		655805							
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59 656799 413 949945 107 706854 521 293146 1 60 657047 413 949881 107 707166 520 292834 0									
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Cosine Sine Cotang. Tang. M.	60	657047	413	949881					
		Cosine		Sine	Ī	Cotang.		Tang.	M.

63 Degrees.

45

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.657047	413	9.949881	107		520	10.292834	6
1	657295	413	949816	107	707478	520	292522	5
2	657542	412	949752	107	707790	520	292210	5
3	657790	412	949688	108	708102	520	291898	5
4	658037	412	949623	108	708414	519	291586	5
5	658284	412	949558	108	708726	519	291274	5
6	658531	411	949494	108	709037	519	290963	5
7	658778	411	949429	108	709349	519	290651	5
8	659025	411	949364	108	709660	519	290340	5
9	659271	410	949300	108	709971	518	290029	5
0	659517	410	949235	108	710282	518	289718	5
1	9.659763	410	9.949170	108	9.710593	518	10.289407	4
2	660009	409	949105	108	710904	518	289096	4
3	660255	409	949040	108	711215	518	288785	4
4	660501	409	948975	108	711525	517	288475	4
5	660746	409	948910	108	711836	517	288164	4
6	660991	408	948845	108	712146		287854	4
7	661236	408	948780	109	712456	517	287544	
		408	948715	109	712766	517		4
8	661481		948650	109	713076	516	287234	4
9	661726	407				516	286924	4
05	661970	407	948584	109	713386	516	286614	4
1	9.662214	407	9.948519	109	9.713696	516	10.286304	3
22	662459	407	948454	109	714005	516	285995	3
23	662703	406	948388	109	714314	515	285686	3
24	662946	406	948323	109	714624	515	285376	3
25	663190	406	948257	109	714933	515	285067	3
26	663433	405	948192	109	715242	515	284758	3
27	663677	405	948126	109	715551	514	284449	3
28	663920	405	948060	109	715860	514	284140	3
29	664163	405	947995	110	716168	514	283832	3
30	664406	404	947929	110	716477	514	283523	3
31	-		9.947863	$\frac{110}{110}$	9.716785			2
	9.664648	404		110		514	10.283215	
32	664891	404	947797		717093	513	282907	2
33	665133	403	947731	110	717401	513	282599	2
34	665375	403	947665	110	717709	513	282291	2
35	665617	403	947600	110	718017	513	281983	2
36	665859	402	947533	110	718325	513	281675	2
37	666100	402	947467	110	718633	512	281367	2
38	666342	402	947401	110	718940	512	281060	2
39	666583	402	947335	110	719248	512	280752	2
10	666824	401	947269	110	719555	512	280445	2
11	9.667065	401	9.947203	110	9.719862	512	10.280138	1
12	667305	401	947136	111	720169	511	279831	1
13	667546	401	947070	111	720476	511	279524	î
14	667786	400	947004	111	720783	511	279217	î
5	668027	400	946937	111	721089	511	278911	î
16	668267	400	946871	iii	721396	511	278604	i
17	668506	399	946804	111	721702	510	278298	i
18	668746	399	946738	111	722009	510	277991	i
19	668986		946671	111	722315	510	277685	1
50		399	946604	111			277379	1
-	669225	399			722621	510		12
1	9.669464	398	9.946538	111	9.722927	510	10.277073	
52	669703	398	946471	111	723232	509	276768	
53	669942	398	946404	111	723538	509	276462	
54	670181	397	946337	111	723844	509	276156	
55	670419	397	946270	112	724149	509	275851	
56	670658	397	946203	112	724454	509	275546	
57	670896	397	946136	112	724759	508	275241	
58	671134	396	946069	112	725065	508	274935	
59	671372	396	946002	112	725369	508	274631	
	671609	396	945935	112	725674	508	274326	
60								

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.671609	396	9.945935	112	9.725674	508	10.274326	60
i.	671847	395	945868	112	725979	508	274021	59
2	672084	395	945800	112	726284 726588	507 507	273716 273412	58 57
3	672321	395	945733	$\frac{112}{112}$	726892	507	273108	56
4	672558 672795	395 394	945666 945598	112	727197	507	272803	55
5 6	673032	394	945531	112	727501	507	272499	54
7	673268	394	945464	113	727805	506	272195	53
8	673505	394	945396	113	728109	506	271891	52
9	673741	393	945328	113	728412	506	271588	51
10	673977	393	945261	113	728716	506	271284	50
11	9.674213	393	9.945193	113	9.729020	506	10.270980	49
12	674448	392	945125	113	729323	505	270677 270374	48 47
13	674684	392	945058 944990	113 113	729626 729929	505 505	270071	46
14 15	674919 675155	$\frac{392}{392}$	944990	113	730233	505	269767	45
16	675390	391	944854	113	730535	505	269465	44
17	675624	391	944786	113	730838	504	2 69162	43
18	675859	391	944718	113	731141	504	268859	42
19	676094	391	944650	113	731444	504	268556	41
20	676328	390	944582	114	731746	504	268254	40
21	9.676562	390	9.944514	114	9.732048	504	10.267952	39
22	676796	390	944446	114	732351	503	267649 267347	38 37
23	677030	390	944377 944309	114 114	732653 732955	503 503	267045	36
24	677264 677498	389	944309	114	733257	503	266743	35
25 26	677731	389 389	944172	114	733558	503	266442	34
27	677964	388	944104	114	733860	502	266140	33
28	678197	388	944036	114	734162	502	265838	32
29	678430	388	943967	114	734463	502	265537	31
30	678663	388	943899	114	734764	502	265236	30
31	9 678895	387	9.943830	114	9.735066	502	10.264931	29
32	679128	387	943761	114	735367	502	264633	28
33	679360	387	943693	115	735668	501	264332 264031	27 26
34	.679592	387	943624 943555	115	735969 736269	501 501	263731	25
35 36	679824 680056	386 386	943486	115 115	736570	501	263430	24
37	680288	386	943417	115	736871	501	263129	23
38	680519	385	943348	115	737171	500	262829	22
39	680750	385	943279	115	737471	500	262529	21
40	680982	385	943210	115	737771	500	262229	20
41	9.681213	385	9.943141	115	9.738071	500	10.261929	19
42	681443	384	943072	115	738371	500	261629	18
43	681674	384	943003	115	738671	499	261329	17 16
44	681905	384	942934 942864	115	738971	499 499	261029 260729	15
45 46	682135 682365	384 383	942864	115 116	739271 739570	499	260430	14
47	682595	383	942726	116	739870	499	260130	13
48	682825	383	942656	116	740169	499	259831	12
49	683055	383	942587	116	740468	498	259532	11
50	683284	382	942517	116	740767	498	259233	10
$\overline{51}$	9.683514	382	9.942448	116	9.741066	498	10.258934	9
62	683743	382	942378	116	741365	498	258635	8
53	683972	382	942308	116	741664	498	258336	7
54 55	684201 684430	381	942239 942169	116 116	741962 742261	497 497	258038 257739	5
56	684658	381 381	942169	116	742261 742559	497	257441	4
57	684887	380	942099	116	742858	497	257142	3
58	685115	380	941959	116	743156	497	256844	2
59	685343	380	941889	117	743454	497	256546	1
60	685571	380	941819	117	743752	496	256248	0
	Cosine		Sine	1	Cotang.		Tang.	M.

61 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.685571	380	9.941819	117	9.743752	496	10.256248	60
1	685799	379	941749	117	744050	496	255950	59
3	686027	379	941679	117	744348	496	255652	58
3	686254	379	941609	117	744645	496	255355	57
4	686482	379	941539	117	744943	496	255057	56
5	686709	378	941469	117	745240	496	254760	55
6	686936	378	941398	117	745538	495	254462	54
7	687163	378	941328	117	745835	495	254165	53
8	687389	378	941258	117	746132	495	253868	52
9	687616	377	941187	117	746429	495	253571	51
10	687843	377	941117	117	746726	495	253274	50
11	9.688069	377	9.941046			494	10.252977	49
				118	9.747023			
12	688295	377	940975	118	747319	494	252681	48
13	688521	376	940905	118	747616	494	252384	47
14	688747	376	940834	118	747913	494	252087	46
15	688972	376	940763	118	748209	494	251791	45
16	689198	376	940693	118	748505	493	251495	44
17	689423	375	940622	118	748801	493	251199	45
18	689648	375	940551	118	749097	493	250903	45
19	689873	375	940480			493		41
				118	749393		250607	
20	690098	375	940409	118	749689	493	250311	40
21	9.690323	374	9.940338	118	9.749985	493	10.250015	35
22	690548	374	940267	118	750281	492	249719	38
23	690772	374	940196	118	750576	492	249424	37
24	690996	374	940125			492	249128	36
25				119	750872			
	691220	373	940054	119	751167	492	248833	35
26	691444	373	939982	119	751462	492	248538	34
27	691668	373	939911	119	751757	492	248243	33
28	691892	373	939840	119	752052	491	247948	35
29	692115	372	939768	119	752347	491	247653	3
30	692339	372	939697	119	752642	491	247358	30
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31	9.692562	372	9.939625	119	9.752937	491	10.247063	29
32	692785	371	939554	119	753231	491	246769	28
33	693008	371	939482	119	753526	491	246474	2
34	693231	371	939410	119	753820	490	246180	20
35	693453	371	939339	119	754115	490	245885	2!
36	693676	370	939267	120	754409	490	245591	24
37	693898	370	939195	120	754703	490	245297	2:
38	694120	370						25
			939123	120	754997	490	245003	
39	694342	370	939052	120	755291	490	244709	2
40	694564	369	938980	120	755585	489	244415	20
41	9.694786	369	9.938908	120	9.755878	489	10.244122	19
42	695007	369	938836	120	756172	489	243828	1
43	695229	369	938763	120	756465	489	243535	i
44								1
	695450	368	938691	120	756759	489	243241	
45	695671	368	938619	120	757052	489	242948	1
46	695892	368	938547	120	757345	488	242655	1
47	696113	368	938475	120	757638	488	242362	1
48	696334	367	938402		757931	488	242069	1
49	696554	367	938330		758224	488	241776	1
50	696775	367	938258		758517	488	241483	
_				-	-		-	-
51	9.696995	367	9.938185		9.758810	488	10.241190	
52	697215	366	938113		759102	487	240898	
53	697435	366	938040	121	759395	487	240605	
54	697654	366	937967		759687	487	240313	
55	697874	366	937895		759979	487	240021	
56	698094	365	937822		760272	487	239728	
57								
	698313	365	937749			487	239436	18
58	698532	365	937676			486	239144	
59	698751	365	937604	121	761148	486	238852	
60	698970	364	937531			486	238561	

48 ' (30 Degrees.) A TABLE OF LOGARITHMIC

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.698970	364	9.937531	121	9.761439	486	10.238561	1 6
1	699189	364	937458	122	761731	486	238269	
2	699407	364	937385	122	762023	486	237977	58
3	699626	364	937312	122	762314	486	237686	5
4	699844	363	937238	122	762606	485	237394	56
5	700062	363	937165	122	762897	485	237103	5
6	700280	363	937092	122	763188	485	236812	54
7	700498	363	937019	122	763479	485	236521	53
8	700716	363	936946	122	763770	485	236230	55
9	700933	362	936872	122	764061	485	235939	51
10	701151	362	936799	122	764352	484	235648	50
11	9.701368	362	9.936725	122	9.764643	484	10,235357	49
12	701585	362	936652	123	764933	484	235067	48
13	701802	361	936578	123	765224	484	234776	4
14	702019	361	936505	123	765514	484	234486	46
15	702236	361	936431	123	765805	484	234195	45
16	702452	361	936357	123	766095	484	233905	44
17	702669	360	936284	123	766385	483	233615	43
18	702885	360	936210	123	766675	483	233325	42
19	703101	360	936136	123	766965	483	233035	41
20	703317	360	936062	123	767255	483	232745	40
21	9.703533	359	9.935988	123	9.767545	483	10.232455	39
22	703749	359	935914	123	767834	483	232166	
23	703964	359	935840	123	768124	482	231876	38
24	704179	359	935766	124	768413	482	231587	37 36
25	704395	359	935692	124	768703	482	231297	35
26	704610	358	935618	124	768992	482	231008	
27	704825	358	935543	124	769281	482	230719	34
28	705040	358	935469	124	769570	482	230430	33
29	705254	358	935395	124	769860	481	230140	31
30	705469	357	935320	124	770148	481	229852	
31	9.705683	357		_			The second secon	30
32	705898	357	9.935246	124	9.770437	481	10.229563	29
33	706112		935171	124	770726	481	229274	28
34	706326	357 356	935097 935022	124	771015	481	228985	27
35	706539			124	771303	481	228697	26
36	706753	356	934948	124	771592	481	228408	25
37	706967	356	934873	124	771880	480	228120	24
38	707180	356	934798	125	772168	480	227832	23
39	707393	355	934723	125	772457	480	227543	22
40	707606	355	934649	125	772745	480	227255	21
_		355	934574	125	773033	480	226967	20
41	9.707819	355	9.934499	125	9.773321	480	10.226679	19
12	708032	354	934424	125	773608	479	226392	18
13	708245	354	934349	125	773896	479	226104	17
14	708458	354	934274	125	774184	479	225816	16
15	708670	354	934199	125	774471	479	225529	15
16	708882	353	934123	125	774759	479	225241	14
17	709094	353	934048	125	775046	479	224954	13
18	709306	353	933973	125	775333	479	224667	12
19	709518	353	933898	126	775621	478	224379	11
50	709730	353	933822	126	775908	478	224092	10
51	9.709941	352	9.933747	126	9.776195	478	10.223805	9
52	710153	352	933671	126	776482	478	223518	8
53	710364	352	933596	126	776769	478	223231	7
54	710575	352	933520	126	777055	478	222945	6
55	710786	351	933445	126	777342	478	222658	5
66	710997	351	933369	126	777628	477	222372	4
57	711208	351	933293	126	777915	477	222085	3
58	711419	351	933217	126	778201	477	221799	2
59	711629	350	933141	126	778487	477	221512	ĩ
30	711839	350	933066	126	778774	477	221226	Ô

M.	Sine	D.	Cosine	D.	. Tang.	D.	Cotang.	
01	9 711839	350	9.933066	126	9.778774	477	10.221226	60
1	712050	350	932990	127	779060	477	220940	59
2	712260	350	932914	127	779346	176	220654	58
3	712469	349	932838	127	779632	476	220368	57
4	712679	349	932762	127	779918	476	220082	56
5	712889	349	932685	127	780203	476	219797	55
6	713098	349	932609	127	780489	476	219511	54
7	713308	349	932533	127	780775	476	219225	5:
8	713517	348	932457	127	781060	476	218940	52
9	713726	348	932380	127	781346	475	218654	5
10	713935	348	932304	127	781631	475	218369	50
11	9.714144	348	9.932228	127	9.781916	475	10.218084	49
2	714352	347	932151	127	782201	475	217799	48
3	714561	347	932075	128	782486	475	217514	4
4	714769	347	931998	128	782771	475	217229	4
15	714978			128	783056		216944	4
	715186	347	931921 931845	128	783341	475	216659	4
16						475	216374	4:
17	715394	346	931768	128	783626	474		
18	715602	346	931691	128	783910	474	216090	4
19	715809	346	931614	128	784195	474	215805	4
20	716017	346	931537	128	784479	474	215521	4
21	9.716224	345	9.931460	128	9.784764	474	10.215236	3
22	716432	345	931383	128	785048	474	214952	3
23	716639	345	931306	128	785332	473	214668	3
24	716846	345	931229	129	785616	473	214384	3
25	717053	345	931152	129	785900	473	214100	3
26	717259	344	931075	129	786184	473	213816	3
27	717466	344	930998	129	786468	473	213532	3
28	717673	344	930921	129	786752	473	213248	3
29	717879			129	787036		212964	3
	718085	344	930843			473	212681	3
30		343	930766	129	787319	472		100
31	9.718291	343	9.930688	129	9.787603	472	10.212397	2
32	718497	343	930611	129	787886	472	212114	2
33.	718703	343	930533	129	788170	472	211830	2
34	718909	343	930456	129	788453	472	211547	2
35	719114	342	930378	129	788736	472	211264	2
36	719320	342	930300	130	789019	472	210981	2
37	719525	342	930223	130	789302	471	210698	2
38	719730	342	930145	130	789585	471	210415	2
39	719935	341	930067	130	789868	471	210132	2
40	720140	341	929989	130	790151	471	209849	2
41	9.720345	341	9.929911	130	9.790433	471	10.209567	ī
				130			209284	lî
42	720549	341	929833		790716	471	209204	1
43	720754	340	929755	130	790999	471	209001	
14	720958	340	929677	130	791281	471		
45	721162	340	929599	130	791563	470	208437	1
16	721366	340	929521	130	791846	470	208154	
47	721570	340	929442	130	792128	470	207872	
48	721774	339	929364	131	792410	470	207590	
19	721978	339	929286	131	792692	470	207308	
50	722181	339	929207	131	792974	470	207026	1
51	9.722385	339	9.929129	131	9.793256	470	10.206744	1
52	722588	339	929050	131	793538	469	206462	198
53	722791	338	928972	131	793819	469	206181	1
54	722994	338	928893	131	794101	469	205899	1
55	723197	338	928815	131	794383	469	205617	
56	723400	338	928736	131	794664	469	205336	
	40000000					469	205055	1
57	723603	337	928657	131	794945	469	204773	1
58	723805	337	928578	131	795227			
59 60	724007 724210	337	928499	131	795508	468	204492 204211	
		337	928420	131	795789	468	204211	1

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.724210	337	9.928420	132	9.795789	468	10.204211	60
ĭ	724412	337	928342	132	796070	468	203930	59
2	724614	336	928263	132	796351	468	203649	58
ã	724816	336	928183	132	796632	468	203368	57
4	725017	336	928104	132	796913	468	203087	56
5	725219	336	928025	132	797194	468	202806	55
ě	725420	335	927946	132	797475	468	202525	54
7	725622	335	927867	132	797755	468	202245	53
8	725823	335	927787	132	798036	467	201964	52
9	726024	335	927708	132	798316	467	201684	51
10	726225	335	927629	132	798596	467	201404	50
$\overline{11}$	9.726426	334	9.927549	132	9.798877	467	10.201123	49
12	726626	334	927470	133	• 799157	467	200843	48
13	726827	334	927390	133	799437	467	200563	47
14	727027	334	927310	133	799717	•467	200283	46
15	727228	334	927231	133	799997	466	200003	45
16	727428	333	927151	133	800277	466	199723	44
17	727628	333	927071	133	800557	466	199443	43
18	727828	833	926991	133	800836	466	199164	42
19	728027	333	926911	133	801116	466	198884	41
20	728227	333	926831	133	801396	466	198604	40
21	9.728427	332	9.926751	133	9.801675	466	10.198325	39
22	728626	332	926671	133	801955	466	198045	38
23	728825	332	926591	133	802234	465	197766	87
24	729024	332	926511	134	802513	465	197487	36
25	729223	331	926431	134	802792	465	13,008	85
26	729422	331	926351	134	803072	465	1 966 28 196649	34
27	729621	331	926270	134	803351	465		33 32
28	729820	331	926190	134	803630	465	196370 196092	31
29	730018	330	926110	134 134	803908	465 465	195813	30
30	730216	330	926029		804187			
31	9.730415	330	9.925949	134	9.804466	464	10.195534	29
32	730613	330	925868	184	804745	464	195255	28 27
83	730811	330	925788	134	805023 805302	464 464	194977 194698	26
84	731009	829	925707	134 134	805580	464	194420	95
35	731206 731404	329 329	925626 9255 4 5	135	805859	464	194141	24
36 37	731602	329	925465	135	806137	464	193863	28
38	731799	829	925384	135	806415	463	193585	22
39	731996	328	925303	135	806693	463	193307	21
40	732193	328	925222	135	806971	463	193029	20
41	9.732390	328	9.925141	135	9.807249	463	10.192751	19
42	732587	328	925060	135	807527	463	192473	iš
43	732784	328	924979	135	807805	463	192195	17
44	732980	327	924897	135	808083	463	191917	iė
45	733177	327	924816	135	808361	463	191639	15
46	733373	327	924735	136	808638	462	191362	14
47	733569	327	924654	136	808916	462	191084	18
48	733765	327	924572	136	809193	462	190807	12
49	733961	326	924491	136	809471	462	190529	11
50	734157	326	924409	136	809748	462	190252	10
51	9.734353	326	9.924328	136	9.810025	462	10,189975	9
52	734549	326	924246	136	810302	462	189698	8 7
53	734744	325	924164	136	810580	462	189420	7
54	734939	325	924083	136	810857	462	189143	6
55	735135	325	924001	136	811134	461	188866	5
56	735330	325	923919	136	811410	461	188590	4
57	735525	325	923837	136	811687	461	188313	3
58	735719	324	923755	137	811964	461	188036	2
59	735914	324	923673	137	812241	461	187759	1
60	736109	324	923591	137	812517	461	187483	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D	Tang.	D.	Cotang.	- 4
0	9.736109	324	9.923591	137	9.812517	461	10.187482	60
1	736303	324	923509	137	812794	461	187206	59
2	736498	324	923427	137	813070	461	186930	58
3	736692	323	923345	137	813347	460	186653	57
4	736886	323	923263	137	813623	460	186377	56
5	737080	323	923181	137	813899	460	186101	55
6	737274	323	923098	137	814175	460	185825	54
7	737467	323	923016	137	814452	460	185548	53
8	737661	322	922933	137	814728	460	185272	5:
9	737855	322	922851	137	815004	460	184996	5
10	738048	322	922768	138	815279	460	184721	
100	Contract of the second							50
11	9.738241	322	9.922686	138	9.815555	459	10.184445	45
2	738434	322	922603	138	815831	459	184169	48
3	738627	321	922520	138	816107	459	183893	4
4	738820	321	922438	138	816382	459	183618	4
5	739013	321	922355	138	816658	459	183342	4
6	739206	321	922272	138	816933	459	183067	4
7	739398	321	922189	138	817209		182791	4:
8	739590					459		
		320	922106	138	817484	459	182516	45
9	739783	320	922023	138	817759	459	182241	4
05	739975	320	921940	138	818035	458	181965	40
1	9.740167	320	9.921857	139	9.818310	458	10.181690	39
22	740359	320	921774	139	818585	458	181415	38
3	740550	319	921691	139	818860		181140	3
						458		
4	740742	319	921607	139	819135	458	180865	3
25	740934	319	921524	139	819410	458	180590	3.
26	741125	319	921441	139	819684	458	180316	3
27	741316	319	921357	139	819959	458	180041	3
28	741508	318	921274	139	820234	458	179766	35
29	741699	318	921190	139	820508	457	179492	3
30	741889	318	921107	139	820783	457	179217	30
-		-		-				-
31	9.742080	318	9.921023	139	9.821057	457	10.178943	25
32	742271	318	920939	140	821332	457	178668	28
33	742462	317	920856	140	821606	457	178394	2
34	742652	317	920772	140	821880	457	178120	2
35	742842	317	920688	140	822154	457	177846	2
36	743033	317	920604	140	822429	457	177571	2
37	743223	317	920520	140	822703	457	177297	2:
38	743413		920436	140	822977	456	177023	2
39		316						2
	743602	316	920352	140	823250	456	176750	
01	743792	316	920268	140	823524	456	176476	2
11	9.743982	316	9.920184	140	9.823798	456	10.176202	1
12	744171	316	920099	140	824072	456	175928	i
3	744361	315	920015	140	824345	456	175655	i
4	744550	315	919931	141	824619	456	175381	i
5	744739		919846	141	824893	456	175107	1
6		315						
	744928	315	919762	141	825166	456	174834	1
7	745117	315	919677	141	825439	455	174561	1
8	745306	314	919593	141	825713	455	174287	1
9	745494	314	919508	141	825986	455	174014	1
0	745683	314	919424	141	826259	455	173741	1
1	9.745871	314	9.919339	141	9.826532	455	10.173468	3
2	746059	314	919254	141	826805	455	173195	
								2
3	746248	313	919169	141	827078	455	172922	
4	746436	313	919085	141	827351	455	172649	7
55	746624	313	919000	141	827624	455	172376	
6	746812	313	918915	142	827897	454	172103	
7	746999	313	918830	142	828170	454	171830	
8	747187	312	918745	142	828442	454	171558	19
59	747374	312	918659	142	828715	454	171285	1
30	747562		918574					
JUI	141002	312	910014	144	828987	454	171013	. '

M. Sine D. Cosine D. Tang. D. Cotang.								<u> </u>	
1 747749 312 918489 142 829502 454 170740 59 2 774936 312 918491 142 829505 454 170468 58 3 748123 311 918318 142 829905 454 170195 57 6 748683 311 918062 142 830621 453 169651 55 7 748870 311 917976 143 830893 452 169107 53 8 749056 310 917891 143 83165 453 168685 52 10 749423 310 9176631 143 831437 453 168685 51 12 749801 310 9177548 143 832525 453 167475 47 13 749997 309 917462 143 832525 453 167475 47 14 750123 309 9	M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
1									60
Table									
4 748310 311 918233 142 830077 454 169923 56 5 748670 311 918062 142 830621 453 169679 54 7 748870 311 917976 143 830893 453 169379 54 8 749056 310 917891 143 8311437 453 168863 52 9 749243 310 917761 143 8318709 453 168863 51 11 9.749615 310 9.917681 143 832253 453 167747 43 12 749801 310 9.917681 143 832253 453 167747 44 13 749987 309 917264 143 832525 453 167744 47 14 750172 309 917186 143 833339 452 166661 44 15 750585 309	2								
6 748497 311 918147 142 830621 453 169379 54 7 748870 311 917976 143 830893 453 168107 53 8 748950 310 917891 143 831497 453 168835 52 10 749429 310 9177891 143 831497 453 168563 51 11 9.749615 310 9177548 143 8331981 453 168291 50 12 749801 310 9175748 143 832255 453 167747 47 13 749987 309 917376 143 832555 453 167747 48 15 750358 309 917290 143 833304 452 166932 45 16 75043 309 917376 143 833339 452 166932 45 18 750729 308									
66 7448683 311 918062 142 830621 453 169379 54 7 74870 310 917891 143 830893 453 168855 52 9 749243 310 917891 143 831165 453 168856 51 10 749429 310 917719 143 831709 453 168856 51 11 9.749615 310 917749 143 832525 453 167747 48 13 749987 309 917462 143 832253 453 1677475 48 14 750172 309 917290 143 833068 452 166932 45 16 750543 309 917290 143 83368 452 166932 45 17 750729 309 917118 144 833681 452 166389 31 18 750914 308 916946 144 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>									
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Cosine Sine Cotang. Tang. M.	<u> </u>		001		T.F.		770		
		Cosine		Sine		Cotang.		Tang.	M.

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M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.758591	301	9.913365	147	9.845227	448	10.154773	60
1	758772	300	913276	147	845496	448	154504	59
2	758952	300	913187	148	845764	448	154236	58
3	759132	300	913099	148	846033	448	153967	57
4	759312	300	913010	148	846302	448	153698	56
5	759492	300	912922	148	846570	447	153430	55
6	759672	299	912833	148	846839	447	153161	54
7	759852	299	912744	148	847107	447	152893	
8	760031	299	912655	148		447		53
					847376		152624	5%
9	760211	299	912566	148	847644	447	152356	51
10	760390	299	912477	148	847913	447	152087	50
11	9.760569	298	9.912388	148	9.848181	447	10.151819	49
12	760748	298	912299	149	848449	447	151551	48
13	760927	298	912210	149	848717	447	151283	47
14	761106	298	912121	149	848986	447	151014	46
15	761285	298	912031	149	849254	447	150746	45
16	761464	298	911942	149	849522	447	150478	44
17	761642	297	911853	149	849790	446	150210	43
18	761821	297	911763	149	850058	446		
						446	149942	42
19	761999	297	911674	149	850325		149675	4
20	762177	297	911584	149	850593	446	149407	4(
21	9.762356	297	9.911495	149	9.850861	446	10.149139	39
22	762534	296	911405	149	851129	446	148871	38
23	762712	296	911315	150	851396	446	148604	3
24	762889	296	911226	150	851664	446	148336	36
25	763067	296	911136	150	851931	446	148069	3
26	763245	296	911046	150	852199	446	147801	34
27	763422	296				446		
			910956	150	852466		147534	33
28	763600	295	910866	150	852733	445	147267	35
29	763777	295	910776	.150	853001	445	146999	3
30	763954	295	910686	150	853268	445	146732	30
31	9.764131	295	9.910596	150	9.853535	445	10.146465	29
32	764308	295	910506	150	853802	445	146198	28
33.	764485	294	910415	150	854069	445	145931	2
34	764662	294	910325	151	854336	445	145664	26
35	764838	294	910235	151	854603	445	145397	2
								2
36	765015	294	910144	151	854870	445	145130	
37	765191	294	910054	151	855137	445	144863	2
38	765367	294	909963	151	855404	445	144596	25
39	765544	293	909873	151	855671	444	144329	2
40	765720	293	909782	151	855938	444	144062	2
41	9.765896	293	9.909691	151	9.856204	444	10.143796	1
42	766072	293	909601	151	856471	444	143529	1
43	766247	293	909510	151	856737	444	143263	1
							142996	1
44	766423	293	909419	151	857004	444		
45	766598	292	909328	152	857270	444	142730	1
46	766774	292	909237	152	857537	444	142463	1
47	766949	292	909146	152	857803	444	142197	1
48	767124	292	909055	152	858069	444	141931	1
49	767300	292	908964	152	858336	444	141664	1
50	767475	291	908873	152	858602	443	141398	1
51	9.767649	291	9.908781	152	9.858868	443	10.141132	3
52	767824	291	908690	152	859134	443	140866	
					859400	443	140600	3
53	767999	291	908599	152				
54	768173	. 291	908507	152	859666	443	140334	2
55	768348	290	908416	153	859932	443	140068	100
56	768522	290	908324	153	860198	443	139802	10
57	768697	290	908233	153	860464	443	139536	
58	768871	290	908141	153	860730	443	139270	1
59	769045	290	908049	153	860995	443	139005	1
60	769219	290	907958	153	861261	443	138739	
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М.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.769219	290	9.907958	153		443	10.138739	60
1	769393	289 289	907866	153 153	861527	443 442	138473	59
3	769566 769740	289	907774 907682	153	861792 862058	442	138208 137942	58 57
4	769913	289	907590	153	862323	442	137677	56
5	770087	289	907498	153	862589	442	137411	55
6	770260	288	907406	153	862854	442	137146	54
7 8	770433 770606	288 288	907314 907222	154 154	863119 863385	442 442	136881 136615	53 52
9	770779	288	907129	154	863650	442	136350	51
10	770952	288	907037	154	863915	442	136085	50
$\overline{11}$	9.771125	288	9.906945	154	9.864180	442	10.135820	49
12	771298	287	906852	154	864445	442	135555	48
13 14	771470 771643	287 287	906760 906667	154 154	864710 864975	442 441	135290 135025	47
15	771815	287	906575	154	865240	441	134760	45
16	771987	287	906482	154	865505	441	134495	44
17	772159	287	906389	155	865770	441	134230	43
18	772331	286	906296	155	866035	441	133965	42
19 20	772503 772675	286 286	906204 906111	155 155	866300 866561	441 441	133700 133436	41 40
$\frac{20}{21}$	9.772847	286	9.906018	155	9.866829	441	10.133171	39
22	773018	286	905925	155	867094	441	132906	38
23	773190	286	905832	155	867358	441	132642	37
24	773361	. 285	905739	155	867623	441	132377	36
25 26	773533 773704	285 285	905645	155	867887	441 440	132113	35 34
27	773875	285	905552 905459	155 155	868152 868416	440	131848 131584	33
28	774046	285	905366	156	868680	440	131320	32
29	774217	285	905272	156	868945	440	131055	31
30	774388	284	905179	156	869209	440	130791	30
31	9.774558	284	9.905085	156	9.869473	440	10.130527	29
32 33	774729 774899	284 284	904992 904898	156 156	869737 870001	440 440	130263 129999	28 27
34	775070	284	904804	156	870265	440	129735	26
35	775240	284	904711	156	870529	440	129471	25
36	775410	283	904617	156	870793	440	129207	24
37 38	775580 775750	283 283	904523 904429	156 157	871057 871321	440 440	128943 128679	23 22
39	775920	283	904335	157	871585	440	128415	21
40	776090	283	904241	157	871849	439	128151	20
41	9.776259	283	9.904147	157	$9.87\overline{2112}$	439	10.127888	19
42	776429	282	904053	157	872376	439	127624	18
43 44	776598	282 282	903959	157	872640	439	127360	17 16
45	776768 776937	282 282	903864 9 0 3770	157 157	872903 873167	439 439	127097 126833	15
46	777106	282	903676	157	873430	439	126570	14
47	777275	281	903581	157	873694	439	126306	13
48	777444	281	903487	157	873957	439	126043	12
49 50	777613 777781	281 281	903392 903298	158 158	874220 874484	439 439	125780 125516	11 10
51	9.777950	281	9.903203	$\frac{158}{158}$	9.874747	439	$\frac{125310}{10.125253}$	10
52	778119	281 281	903108	158	875010	439	124990	8
53	778287	280	903014	158	875273	438	124727	7
54	778455	280	902919	158	875536	438	124464	6
55 56	778624 778792	280 280	902824 902729	158	875800 876063	438 438	124200 123937	5
57	778960	280 280	902729	158 158	876003 876326	438	123937	3
58	779128	280	902539	159	876589	438	123411	2
59	779295	279	902444	159	876851	438	123149	1
60	779463	279	902349	159	877114	438	122886	
	Cosine		Sine		Cotang.		Tang.	M.
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M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.779463	279	9.902349	159	9.877114	438	10.122886	60
1	779631	279	902253	159	877377	438	122623	59
23	779798	279	902158	159	877640	438	122360	5
3	779966	279	902063	159	877903	438	122097	5
4	780133	279	901967	159	878165	438	121835	5
5	780300	278	901872	159	878428	438	121572	5
6	780467	278	901776	159	878691	438	121309	5
7	780634	278	901681	159	878953	437	121047	5
8	780801	278	901585	159	879216	437	120784	5
9	780968	278	901490	159	879478	437	120522	5
10	781134	278	901394	160	879741	437		5
_				-			120259	
11	9.781301	277	9.901298	160	9.880003	437	10.119997	4
12	781468	277	901202	160	880265	437	119735	4
13	781634	277	901106	160	880528	437	119472	4
14	781800	277	901010	160	880790	437	119210	4
15	781966	277	900914	160	881052	437	118948	4
16	782132	277	900818	160	881314	437	118686	4
17	782298	276	900722	160	881576	437	118424	4
18	782464	276	900626	160	881839	437	118161	4
19	782630	276	900529	160	882101		117899	4
20	782796					437		4
-		276	900433	161	882363	436	117637	-
115	9.782961	276	9.900337	161	9.882625	436	10.117375	3
22	783127	276	900240	161	882887	436	117113	3
23	783292	275	900144	161	883148	436	116852	3
24	783458	275	900047	161	883410	436	116590	3
25	783623	275	899951	161	883672	436	116328	3
26	783788	275	899854	161	883934	436	116066	3
27	783953	275	899757	161	884196		115804	3
28						436		3
	784118	275	899660	161	884457	436	115543	
29	784282	274	899564	161	884719	436	115281	3
30	784447	274	899467	162	884980	436	115020	3
31	9.784612	274	9.899370	162	9.885242	436	10.114758	2
32	784776	274	899273	162	885503	436	114497	2
33	784941	274	899176	162	885765	436	114235	2
34	785105	274	899078	162	886026	436	113974	2
35	785269	273	898981	162	886288	436	113712	2
36	785433	273	898884	162	886549	435	113451	2
37		273	898787				113190	2
	785597			162	886810	435		2
38	785761	273	898689	162	887072	435	112928	2
39	785925	273	898592	162	887333	435	112667	
40	786089	273	898494	163	887594	435	112406	2
41	9.786252	272	9.898397	163	9.887855	435	10.112145	1
42	786416	272	898299	163	888116	435	111884	1
43	786579	272	898202	163	888377	435	111623	ī
44	786742	272	898104	163	888639	435	111361	î
45			898006	163				î
	786906	272			888900	435	111100	1
46	787069	272	897908	163	889160	435	110840	1
47	787232	271	897810	163	889421	435	110579	
48	787395	271	897712	163	889682	435	110318	1
49	787557	271	897614	163	889943	435	110057	1
50	787720	271	897516	163	890204	434	109796	1
51	9.787883	271	9.897418	164	9.890465	434	10.109535	
52	788045	271	897320	164	890725	434	109275	
53	788208		897222			. 434	109213	13
		271		164	890986			
54	788370	270	897123	164	891247	434	108753	
55	788532	270	897025	164	891507	434	108493	16
56	788694	270	896926	164	891768	434	108232	
57	788856	270	896828	164	892028	434	107972	
58	789018	270	896729	164	892289	434	107711	1
59	789180	270	896631	164	892549	434	107451	1
60	789342	269	896532	164	892810	434	107190	N.
3.50	1	400			00.010	202	10.100	1.11

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M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.789342	269	9.896532	164	9.892810	434	10.107190	60
	789504	269 269	896433	165	893070	434	106930	50
1	789665	269	896335	165	893331	434	106669	58
23	789827	269	896236	165	893591	434	106409	57
4	789988	269	896137	165	893851	434	106149	56
ă.	790149	269	896038	165	894111	434	105889	55
5	790310	268	895939	165	894371	434	105629	54
7	790471	268	895840	165	894632	433	105368	53
8	790632	268	895741	165	894892	433	105108	52
. 9	790793	268	895641	165	895152	433	104848	51
10	790954	268	895542	165	895412	433	104588	50
$\overline{11}$	9.791115	268	9.895443	166	9.895672	433	10.104328	49
12	791275	267	895343	166	895932	433	104068	48
13	791436	267	895244	166	896192	433	103808	47
14	791596	267	895145	166	896452	433	103548	46
15	791757	267	895045	166	896712	433	103388	45
16	791917	267	894945	166	896971	433	103029	44
17	792077	267	894846	166	897231	433	102769	48
18	792237	266	894746	166	897491	433	102509	42
19	792397	266	894646	166	897751	433	102249	41
20	792557	266	894546	166	898010	433	101990	40
21	9.792716	. 266	9.894446	167	9.898270	433	10.101730	39
22	792876	266	894346	167	893530	433	101470	38
23	793035	266	894246	167	898789	433	101211	37
24	793195	265	894146	167	899049	432	100951	36
25	793354	265	894046	167	899308	432	100692 100432	35 34
26	793514	265	893946	167	899568 899827	432	100432	33
27 28	793673 793832	265 265	893846 893745	167 167	900086	432 432	099914	32
29	793991	265	893645	167	990346	432	099654	31
30	794150	264	893544	167	900605	432	099395	30
							10.099136	29
31	9.794308	264	9.893444	168	9.900864	432 432	098876	28
32 33	794467 794626	264 264	893343 893243	168 168	901124 901383	432	098617	27
34	794784	264 264	893142	168	901642	432	098358	26
35	794942	264	893041	168	901901	432	098099	25
36	795101	264	892940	168	902160	432	097840	24
37	795259	263	892839	168	902419	432	097581	23
38	795417	263	892739	168	902679	432	097321	22
39	795575	263	892638	168	902938	432	097062	31
40	795733	263	892536	168	903197	431	096803	20
41	9.795891	263	9.892435	169	9.903455	431	10.096545	19
42	796049	263	892334	169	903714	431	096286	18
43	796206	263	892233	169	903973	431	096027	17
44	796364	262	892132	169	904232	431	095768	16
45	796521	262	892030	169	904491	431	095509	15
46	796679	262	891929	169	904750	431	095250	14
47	796836	262	891827	169	905008	431	094992	13
48	796993	262	891726	169	905267	431	094733	12
49	797150	261	891624	169	905526	431	094474	11
50	797307	261	891523	170	905784	431	094216	10
51	9.797464	261	9.891421	170	9.906043	431	10.093957	9
52	797621	261	891319	170	906302	431	093698	8
53	797777	261	891217	170	906560	431	093440	7
54	797934	261	891115	170	906819	431	093181	6
55 56	798091	261	891013	170	907077	431	092923	5
50 57	798247 798403	261 260	890911 890809	170 170	907336 907594	431 431	092664 092406	3
58	798560	260 260	890707	170	907594	431	092148	9
59	798716	260 260	890605	170	907852	430	091889	2
60	798872	260	890503	170	908369	430	091681	ō
	Cosine		Sine	1 1 1	Cotang.	1	Tang.	M.
~				·	Cottains.			

51 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	1
0	9.798872	260	9.890503	170	9.908369	430	10.091631	60
1	799028	260	890400	171	908628	430	091372	59
2	799184	260	890298	171	908886	430	091114	58
3	799339	- 259	890195	171	909144	430	090856	57
4	799495	259	890093	171	909402	430	090598	56
5	799651	259	889990	171	909660	430	090340	55
				171		430	090082	54
6	799806	259	889888		909918			
7	799962	259	889785	171	910177	430	089823	53
8	800117	259	889682	171	910435	430	089565	52
9	800272	258	889579	171	910693	430	089307	51
10	800427	258	889477	171	910951	430	089049	50
1	9.800582	258	9.889374	172	9.911209	430	10.088791	49
2	800737	258	889271	172	911467	430	088533	48
	800892	258	889168	172	911724	430	088276	47
13							088018	46
4	801047	258	889064	172	911982	430		
5	801201	258	888961	172	912240	430	087760	45
6	801356	257	888858	172	912498	430	087502	44
7	801511	257	888755	172	912756	430	087244	43
18	801665	257	888651	172	913014	429	086986	42
9	801819	257	888548	172	913271	429	086729	41
0	801973	257	888444	173	913529	429	086471	40
-				-			10.086213	39
21	9.802128	257	9.888341	173	9.913787	429		
22	802282	256	888237	173	914044	429	085956	38
23	802436	256	888134	173	914302	429	085698	37
24	802589	256	888030	173	914560	429	085440	36
25	802743	256	887926	173	914817	429	085183	35
26	802897	256	887822	173	915075	429	084925	34
27	803050	256	887718	173	915332	429	084668	33
28	803204	256	887614	173	915590	429	084410	32
					915847	429	084153	31
29	803357	255	887510	173				30
30	803511	255	887406	174	916104	429	083896	-
31	9.803664	255	9.887302	174	9.916362	429	10.083638	29
32	803817	255	887198	174	916619	429	083381	28
33	803970	255	887093	174	916877	429	083123	27
34	804123	255	886989	174	917134	429	082866	26
35	804276	254	886885	174	917391	429	082609	25
36			886780	174	917648	429	082352	24
	804428	254			917905	429	082095	2:
37	804581	254	886676	174				25
38	804734	254	886571	174	918163	428	081837	
39	804886	254	886466	174	918420	428	081580	21
40	805039	254	886362	175	918677	428	081323	20
41	9.805191	254	9.886257	175	9.918934	428	10.081066	19
42		253	886152	175	919191	428	080809	18
	805343				919191	428	080552	1
43	805495	253	886047	175			080295	1
44	805647	253	885942	175	919705	428		
45	805799	253	885837	17.5	919962	428	080038	13
46	805951	253	885732	175	920219	428	079781	14
47	806103	253	885627	175	920476	428	079524	13
48	806254	253	885522	175	920733	428	079267	15
49	806406	252	885416	175	920990	428	079010	1
50	806557	252	885311	176	921247	428	078753	10
-	-			-		-		=
51	9.806709	252	9.885205	176	9.921503	428	10.078497	
52	806860	252	885100	176	921760	428	078240	1
53	807011	252	884994	176	922017	428	077983	13
54	807163	252	884889	176	922274	428	077726	1
55	807314	252	884783	176	922530	428	077470	1
56	807465	251	884677	176		428	077213	
						428	076956	13
57	807615	251	884572	176				
58	807766	251	884466	176		428	076700	
59	807917	251	884360	176		427	076443	
60	808067	251	884254	177	923813	427	076187	1.4
-							Tang.	1 M

M	. Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0			19.88425	4 17	719.92381	3 427		371 6
1			88414	8 17				
2	808368	251						
3	808519			6 17	7 92458			
4		250						
5		250						
6								14 5
7	00000	250				2 427	07464	8 5
1	809119	250			7 925609	427	07439	
8	809269	250	883404	1 17	7 925865	427		
9	809419	249	883297					
10	809569	249						
11	-	1000	_		-	-	07362	_
12	9.809718	249			9.926634	427	10.07336	6 4
	809868	249		178	926890	427	07311	
13	810017	249	882871	178	927147		07285	
14	810167	249	882764					
15	810316	248	882657				07259	
16	810465	248			0.000		07234	1 4
17	810614		882550				07208	5 4
18		248	882443				07182	9 4
	810763	248	882336			427	07157	
19	810912	248	882229	179	928683		07131	
20	811061	248	882121				07106	
21	9.811210		_	-	-			
22		248	9.882014	179	0.040100		10.07080	4 3
	811358	247	881907	179	929452	427	07054	
23	811507	247	881799	179	929708	427	07029	
24	811655	247	881692	179	929964	426	07003	6 3
25	811804	247	881584	179				
26	811952	247	881477	179		426	069780	
27	812100	247	881369		000110	426	06952	
8	812248			179	000.01	426	069269	
29		247	881261	180	930987	426	069013	3 35
30	812396	246	881153	180	931243	426	068757	
_	812544	246	881046	180	931499	426	06850	
31	9.812692	246	9.880938	180				100
32	812840	246			9.931755	426	10.068245	
33	812988		880830	180	932010	426	067990	28
4		246	880722	180	932266	426	067734	27
	813135	246	880613	180	932522	426	067478	
15	813283	246	880505	180	932778	426	067222	
6	813430	245	880397	180	933033	426	066967	
7	813578	245	880289	181	933289			
8	813725	245	880180	181		426	066711	
9	813872	245	880072		933545	426	066455	
0				181	933800	426	066200	21
- 1	814019	245	879963	181	934056	426	065944	20
1	9.814166	245	9.879855	181	9.934311	426	10.065689	19
2	814313	245	879746	181				
3	814460	244	879637	181	934567	426	065433	18
4	814607	244			934823	426	065177	17
5			879529	181	935078	426	064922	16
6	814753	244	879420	181	935333	426	064667	15
	814900	244	879311	181	935589	426	064411	14
7	815046	244	879202	182	935844	426	064156	13
8	815193	244	879093	182	936100	426		
9	815339	244	878984	182			063900	12
0	815485	243	878875	182	936355	426	063645	11
ī					936610	426	063390	10
	9.815631	243	9.878766	182	9.936866	425	10.063134	9
15	815778	243	878656	182	937121	425	062879	9
3	815924	243		182	937376			8
1	816069	243		182		425	062624	1
5	816215	243			937632	425	062368	6
1	816361			182	937887	425	062113	5
		243		183	938142	425	061858	4
	816507	242		183	938398	425	061602	3
3 1	816652	242	877999	183	938653	425	061347	2
)	816798	242		183	938908			
1	816943	242		183	020160	425	061092	1 0
	Cosine	-		100	939163	425	060837	U
			Sine 1		Cotang.		Tang.	M.

49 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
01	9.816943	242	9.877780	183	9.939163	425	10.060837	60
1	817088	242	877670	183	939418	425	060582	59
2	817233	242	877560	183	939673	425	060327	58
3	817379	242	877450	183	939928	425	060072	57
4	817524	241	877340	183	940183	425	059817	56
5	817668	241	877230	184	940438	425	059562	55
6	817813	241	877120	184	940694	425	059306	54
7	817958	241	877010	184	940949	425	059051	53
8	818103	241	876899	184	941204	425	058796	52
9	818247	241	876789	184	941458	425	058542	51
10	818392	241	876678	184	941714	425	058286	50
11	9.818536	240	9.876568	184	9.941968	425	10.058032	49
12	818681	240	876457	184	942223	425	057777	48
13	818825	240	876347	184	942478	425	057522	47
14	818969	240	876236	185	942733	425	057267	46
15	819113	240	876125	185	942988	425	057012	45
16	819257	240	876014	185	943243	425	056757	44
17	819401	240	875904	185	943498	425	056502	43
18	819545	239	875793	185	943752	425	056248	42
19	819689	239	875682	185	944007	425	055993	41
20	819832	239	875571	185	944262	425	055738	40
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21	9.819976	239	9.875459	185	9.944517	425	10.055483	39
22	820120	239	875348	185	944771	424	055229	38
23	820263	239	875237	185	945026	424	054974	37
24	820406	239	875126	186	945281	424	054719	36
25	820550	238	875014	186	945535	424	054465	35
26	820693	238	874903	186	945790	424	054210	34
27	820836	238	874791	186	946045	424	053955	33
28	820979	238	874680	186	946299	424	053701	35
29	821122	238	874568	186	946554	424	053446	31
30	821265	238	874456	186	946808	424	053192	30
31	9.821407	238	9.874344	186	9.947063	424	10.052937	29
32	821550	238	874232	187	947318	424	052682	28
33	821693	237	874121	187	947572	424	052428	27
34	821835	237	874009	187	947826	424	052174	26
	821977	237	873896	187	948081	424	051919	25
35 36	822120	237	873784	187	948336	424	051664	24
37	822262	237	873672	187	948590	424	051410	2:
			873560	187	948844	424	051156	25
38	822404	237	873448	187	949099	424	050901	2
39	822546	237	873335	187	949099	424	050647	20
40	822688	236						-
41	9.822830	236	9.873223	187	9.949607	424	10.050393	15
42	822972	236	873110	188	949862	424	050138	18
43	823114	236	872998	188	950116	424	049884	17
44	823255	236	872885	188	950370	424	049630	16
45	823397	236	872772	188	950625	424	049375	1
46	823539	236	872659	188	950879	424	049121	14
47	823680	235	872547	188	951133	424	048867	1:
48	823821	235	872434	188	951388	424	048612	15
49	823963	235	872321	188	951642	424	048358	1.
50	824104	235	872208	188	951896	424	048104	10
51	9.824245	235	9.872095	189	9.952150	424	10.047850	-
52	824386	235	871981	189	952405	424	047595	1
			871868	189	952659	424	047341	1
53	824527	235		189	952913	424	047087	
54	824668	234	871755			424	046833	
55	824808	234	871641	189	953167			1
56	824949	234	871528	189		423	046579	
57	825090	234	871414			423	046325	
58	825230	234	871301	189	953929	423	046071	3
59	.825371	234	871187			423	045817	
60	825511	234	871073	190	954437	423	045563	
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52 832697 227 865068 195 967629 422 032371 8 53 832833 227 864950 195 967883 422 03217 7 54 832969 226 864833 196 968136 422 031864 6 55 833105 226 864716 196 968389 422 031611 5 56 833241 226 864598 196 968643 422 031857 4 57 833377 226 864481 196 96896 422 031104 3 58 833512 226 864363 196 969149 422 030851 3 59 833648 226 864245 196 969403 422 030597 1 60 833783 226 864127 196 969656 422 030844 0									
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54 832969 226 864833 196 968136 422 031864 6 55 833105 226 864716 196 968389 422 031611 5 56 833241 226 864598 196 968643 422 031357 4 57 833377 226 864481 196 968969 422 031104 3 58 833512 226 864363 196 969149 422 030851 2 59 833648 226 864245 196 969403 422 030851 2 60 833783 226 864127 196 969656 422 030844 0									
55 833105 226 864716 196 968389 422 091611 5 56 833241 226 864598 196 968643 422 031857 4 57 833377 226 864481 196 968896 422 03104 03104 2 58 833512 226 864363 196 969149 422 030851 3 59 833648 226 864245 196 969403 422 030597 1 60 833783 226 864127 196 969656 422 030844 0									
56 833241 226 864598 196 968643 422 031857 4 57 833377 226 864481 196 968896 422 031104 3 58 833512 226 864363 196 969149 422 030851 3 59 833648 226 864245 196 969403 422 030857 1 60 833783 226 864127 196 969656 422 030344 0									
57 833377 226 864481 196 968996 422 031104 3 58 833512 226 864363 196 969149 422 030851 2 59 833648 226 864245 196 969403 422 030597 1 60 833783 226 864127 196 969656 422 030844 0									
59 833648 226 864245 196 969403 422 030597 1 60 833783 226 864127 196 969656 422 030844 0	57	833377					422		3
60 833783 226 864127 196 969656 422 030844 0			226		196				
Cosine Sine Cotang. Tang. M.	60		226		196	969656	422		
		Cosine		Sine		Cotang.		Tang.	M.

47 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.833783	226	9.864127	196	9.969656	422	10.030344	60
1	833919	225	864010	196	969909	422	030091	59
23	834054	225	863892	197	970162	422	029838	58
3	834189	225	863774	197	970416	422	029584	5
4	834325	225	863656	197	970669	422	029331	50
5	834460	225	863538	197	970922	422	029078	
6	834595	225	863419	197	971175	422		5
7	834730	225	863301	197	971429	422	028825	54
8	834865	225	863183	197	971682		028571	5
9	834999	224				422	028318	5
			863064	197	971935	422	028065	5
10	835134	224	862946	198	972188	422	027812	50
11	9.835269	224	9.862827	198	9.972441	422	10.027559	4
12	835403	224	862709	198	972694	422	027306	48
13	835538	224	862590	198	972948	422	-027052	4
14	835672	224	862471	198	973201	422	026799	4
15	835807	224	862353	198	973454	422	026546	4
16	835941	224	862234	198	973707	422	026293	4
17	836075	223	862115	198	973960	422		
18	836209	223	861996	198	974213	422	026040	4:
19	836343	223	861877	198			025787	45
20	836477				974466	422	025534	4]
_		223	861758	199	974719	422	025281	40
21	9.836611	223	9.861638	199	9.974973	422	10.025027	39
22	836745	223	861519	199	975226	422	024774	38
23	836878	223	861400	199	975479	422	024521	3
24	837012	222	861280	199	975732	422	024268	36
25	837146	222	861161	199	975985	422	024015	3
26	837279	222	861041	199	976238	422		
27	837412	222	860922	199	976491		023762	34
28	837546	222	860802	199		422	023509	35
29					976744	422	023256	35
	837679)	222	860682	200	976997	422	023003	31
30	837812	222	860562	200	977250	422	022750	30
31	9.837945	222	9.860442	200	9.977503	422	10.022497	29
32	838078	221	860322	200	977756	422	022244	28
33	838211	221	860202	200	978009	422	021991	27
34	838344	221	860082	200	978262	422	021738	26
35	838477	221	859962	200	978515	422	021485	25
36	838610	221	859842	200	978768	422		
37	838742	221	859721	201			021232	24
					979021	422	020979	23
38	838875	221	859601	201	979274	422	020726	25
39	839007	221	859480	201	979527	422	020473	21
10	839140	220	859360	201	979780	422	020220	20
11	9.839272	220	9.859239	201	9.980033	422	10.019967	19
12	839404	220	859119	201	980286	422	019714	18
13	839536	220	858998	201	980538	422	019462	17
14	839668	220	858877	201	980791	421	019209	10
15	839800	220	858756	202	981044			
16	839932	220	858635	202	981297	421	018956	14
						421	018703	14
17	840064	219	858514	202	981550	421	018450	13
18	840196	219	858393	202	981803	421	018197	15
19	840328	219	858272	202	982056	421	017944	1
50	840459	219	858151	202	982309	421	017691	1
51	9.840591	.219	9.858029	202	9.982562	421	10.017438	-
52	840722	219	857908	202	982814	421	017186	-
53	840854	219	857786	202	983067	421	016933	
54	840985	219	857665	203	983320			
						421	016680	1
55	841116	218	857543	203	983573	421	016427	1
56	841247	218	857422	203	983826	421	016174	4
57	841378	218	857300	203	984079	421	015921	
58	841509	218	857178	203	984331	421	015669	1
59	841640	218	857056	203	984584	421	015416	11
60	841771	218	856934	203	984837	421	015163	
	A STATE OF THE PARTY OF THE PAR		N					

7.	, G1: -	-	Coster	T.	m _{arr} -	P	Coto	
M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	<u> </u>
0	9.841771 841902	218 218	9.856934 856812	203 203	9.984837 985090	421 421	10.015163 014910	60 59
9	842033	218	856690	204	985343	421	014657	58
ã	842163	217	856568	204	985596	421	014404	57
4	842294	217	856446	204	985848	421	014152	56
5	842424	217	856323 856201	204 204	986101 986354	421 421	013899	55
6	842555 842685	217 217	856078	204	986607	421	013646 013393	54 53
8	842815	217	855956	204	986860	421	013140	52
9	842946	217	855833	204	987112	421	012888	51
10	843076	217	855711	205	987365	421	012635	50
11	9.843206	216	9.855588	205	9.987618	421	10.012382	49
12	843336	216	855465 855342	205 205	987871 988123	421 421	012129	48
13 14	843466 843595	216 216	855219	205	988376	421	011877 011624	47 46
15	843725	216	855096	205	988629	421	011371	45
16	843855	216	854973	205	988882	421	011118	44
17	843984	216	854850	205	989134	421	010866	43
18	844114	215	854727	206	989387	421	010613	42
19 20	844243 844372	215 215	854603 854480	206 206	989640 989893	421 421	010360 010107	41
$\frac{20}{21}$	9.844502	215	9.854356	206	9.990145	421	10.009855	$\frac{40}{20}$
22	844631	215 215	854233	206	990398	421	009602	39 38
23	844760	215	854109	206	990651	421	009349	37
24	844889	215	853986	206	990903	421	009097	36
25	845018	215	853862	206	991156	421	008844	35
26 27	845147	215 214	853738 853614	206	991409	421	008591	34
28	845276 845405	214	853490	207 207	991662 991914	421 421	008338 008086	33 32
29	845533	214	853366	207	992167	421	007833	31
30	845662	214	853242	207	992420	421	007580	30
31	9.845790	214	9.853118	207	9.992672	421	10.007328	$\overline{29}$
32	845919	214	852994	207	992925	421	007075	28
33	846047	214	852869	207	993178	421	006822	27
34 35	846175 846304	214 214	852745 852620	207 207	993430 993683	421 421	006570	26
36	846432	213	852496	208	993936	421	006317 006064	25 24
37	846560	213	852371	208	994189	421	005811	23
38	846688	213	852247	208	994441	421	005559	22
39	846816	213	852122	208	994694	421	005306	21
40	846944	213	851997	208	994947	421	005053	20
41 42	9.847071	213	9.851872	208	9.995199	421	10.004801	19
43	847199 847327	213 213	851747 851622	208 208	995452 995705	421 421	004548 004295	18 17
44	847454	212	851497	209	995957	421	004043	16
45	847582	212	851372	209	996210	421	003790	15
46	847709	212	851246	209	996463	421	003537	14
47 48	847836 847964	212 212	851121 850996	209	996715	421	003285	13
49	848091	212	850870	209 209	996968 997221	421 421	003032 002779	12 11
50	848218	212	850745	209	997473	421	002527	10
51	9.848345	212	9.850619	209	9.997726	421	10.002274	9
52	848472	211	850493	210	997979	421	002021	8
53	848599	211	850368	210	998231	421	001769	7
54 55	848726 848852	211	850242	210	998484	421	001516	6
56	848979	211 211	850116 849990	210 210	998737 998989	421 421	001263	5 4
57	849106	211	849864	210	999242	421	001011 000758	3
58	849232	211	849738	210	999495	421	000505	2
59	849359	211	849611	210	999748	421	000253	1
60	849485	211	849485	210	10.000000	421	000000	0
	Cosine		Sine		Cotang.		Tang.	M.

45 Degrees

A TRAVERSE TABLE,

SHOWING THE DIFFERENCE OF

LATITUDE AND DEPARTURE

FOR DISTANCES BETWEEN 1 AND 100, AND FOR ANGLES TO QUARTER DEGREES BETWEEN $1^{\rm O}$ AND $90^{\rm O}$.

Distance.	₫ I	Deg.	<u> 1</u>]	Deg.	₽ D	eg.	Dist
псе	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	1.00	0.00	1.00	0.01	1.00	0.01	
2 3 4 5 6 7	3.00	0.01	3.00	0.03	3.00	0.04	2 3 4 5 6
1 4	4.00	0.02	4.00	0.03	4.00	0.05	4
6.	5.00 6.00	0.02 0.03	5.00 6.00	0.04 0.05	5.00 6.00	0.07 0.08	6
7	7.00	0.03	7.00	0.06	7.00	0.09	7
8	8.00 9.00	0.03 0.04	8.00 9.00	0.07 0.08	8.00 9.00	0.10 0.12	8 9
10	10.00	0.04	10.00	0.09	10.00	0.13	10
11	11.00	0.05	11.00	0.10	11.00	0.14	1:1
12 13	12.00 13.00	0.05 0.06	12.00 13.00	0.10 0.11	12.00 13.00	0.16 0.17	12 13
14	14.00	0.06	14.00	0.12	14.00	0.18	14
15 16	15.00	0.07	15.00 16.00	0.13 0.14	15.00 16.00	0.20 0.21	15 16
17	16.00 17.00	0.07	17.00	0.14	17.00	0.22	17
18	18.00	0.08	18.00	0.16	18.00	0.24	18
19 20	19.00 20.00	0.08	19.00 20.00	0.17 0.17	19.00 20.00	$0.25 \\ 0.26$	19 20
21	21.00	0.09	21.00	0.18	21.00	0.27	21
22 23	22.00	0.10	22.00	0.19	22.00	0.29	22
23	23.00 24.00	0.10 0.10	23.00 24.00	$0.20 \\ 0.21$	23.00 24.00	0.30 0.31	23 24
25	25.00	0.11	25.00	0.22	25.00	0.33	25
26 27	26.00 27.00	0.11 0.12	26.00 27.00	$\begin{array}{c} \textbf{0.23} \\ \textbf{0.24} \end{array}$	26.00 27.00	$0.34 \\ 0.35$	26 27
28	28.00	0.12	28.00	0.24	28.00	0.37	28
29 30	29.00	0.13 0.13	29.00	0.25	29.00	0.38	29
30	$\frac{30.00}{31.00}$	0.13	$\frac{30.00}{31.00}$	$\frac{0.26}{0.27}$	$\frac{30.00}{31.00}$	$\frac{0.39}{0.41}$	$\frac{30}{31}$
32	32.00	0.14	32.00	0.28	32.00	0.42	32
33	33.00	0.14 0.15	33.00	0.29	33.00	0.43	33
34 35	34.00 35.00	0.15	34.00 35.00	0.30 0.31	34.00 35.00	0.45 0.46	34 35
36	36.00	0.16	36.00	0.31	36.00	0.47	36
37 38	37.00 38.00	$0.16 \\ 0.17$	37.00 38.00	$0.32 \\ 0.33$	37.00 38.00	0.48 0.50	37 38
39	39.00	0.17	39.00	0.34	39.00	0.51	39
40	40.00	0.17	40.00	0.35	40.00	0.52	40
41 42	41.00 42.00	0.18 0.18	41.00 42.00	$0.36 \\ 0.37$	41.00 42.00	0.54	41 42
43	43.00	0.19	43.00	0.38	43.00	0.56	43
44	44.00	0.19 0.20	44.00	0.38	44.00	0.58	44 .
45 46	45.00 46.00	0.20	45.00 46.00	0.39	45.00 46.00	0.59	· 45 46
47	47.00	0.21 0.21	47.00	0.41	47.00	0.62	47
48 49	48.00 49.00	0.21	48.00 49.00	0.42 0.43	48.00 49.00	0.63	48 49
_60	50.00	0.22	50.00	0.44	50.00	0.65	_50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Ä	893	Deg.	89 <u>1</u>	Deg.	891	Deg.	Dist
<u></u>			ii		H		

Die	4 I	Deg.	1 2	Deg.	1 1	Deg.	Di
tance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	51.00	0.22	51.00	0.45	51.00	0.67	51
53	52.00 53.00	0.23	52.00 53.00	0.45 0.46	52.00 53.00	0.68	52 53
54 55	54.00 55.00	0.24 0.24	54.00 55.00	0.47 0.48	54.00 55.00	0.71 0.72	54 55
56	56.00	0.24	56.00	0.49	56.00	0.73	56
57 58	57.00 58.00	0.25 0.25	57.00 58.00	0.50 0.51	57.00 57.99	0.75	57 58
59	59.00	0.26	59.00	0.51	58.99	0.76 0.77	59
$\frac{60}{61}$	61.00	$\frac{0.26}{0.27}$	60.00	0.52	59.99	$\frac{0.79}{0.80}$	60
62	62.00	0.27	61.00 62.00	0.53 0.54	60.99 61.99	0.80	62
63 64	63.00 64.00	0.27 0.28	63.00	0.55	62.99	0.82 0.84	63 64
65	65.00	0.28	64.00 65.00	0.56 0.57	63.99 64.99	0.85	65
66	66.00 67.00	0.29 0.29	66.00 67.00	0.58 0.58	65.99 66.9 9	0.86 0.88	66 67
. 68	68.00	0.30	68.00	0.59	67.99	0.89	68
69 70	69.00 70.00	$\begin{array}{c} 0.30 \\ 0.31 \end{array}$	69.00 70.00	0.60 0.61	68.99 69.99	0.90 0.92	69 70
71	71.00	0.31	71.00	0.62	70.99	0.93	71
72 73	72.00 73.00	$0.31 \\ 0.32$	72.00 73.00	0.63	71.99	0.94 0.96	72 73
74	74.00	0.32	73.00	0.64 0.65	72.99 73.99	0.97	74
, 75 76	75.00	0.33	75.00	0.65	74.99	0.98 0.99	75 76
77	76.00 77.00	0.33 0.34	76.00 77.00	0.66 0.67	75.99 76.99	1.01	77
77 78 79	78.00	0.34	78.00	0.68 0.69	77.99 78.99	$\begin{array}{c} 1.02 \\ 1.03 \end{array}$	78 79
80	79.00 80.00	$\begin{array}{c} \textbf{0.34} \\ \textbf{0.35} \end{array}$	79.00 80.00	0.70	79.99	1.05	80
81	81.00	0.35	81.00	0.71	80.99	1.06	81
82 83	82.00 83.00	0.36	82.00 83.00	0.72 0.72	81.99 82.99	1.07 1.09	82 83
84	84.00	0.36	84.00	0.73	83.99	1.10	84
85 86	85.00 86.00	0.37 0.38	85.00 86.00	0.74 0.75	84.99 85.99	1.11 1.13	85 86
87	87.00	0.38	87.00	0.76 0.77 0.78	86.99	1.14	87
88 89	88.00 89.00	0.38 0.39	88.00 89.00	0.77	87.99 88.99	1.15 1.16	88 89
90	90.00	0.39	90.00	0.79	89.99	1.18	90
91	91.00 92.00	0.40 0.40	91.00 92.00	0.79 0.80	90.99 91.99	1.19	91 92
92 93	93.00	0.41	93.00 94.00	0.81	92.99	1.22	93
94	94.00 95.00	0.41 0.41	94.00 95.00	0.82 0.83	93.99 94.99	1.23 1.24	94 95
95 96	96.00	0.42	96.00	0.84	95.99	1.26	96
97 98	97.00 98.00	$\begin{array}{c} \textbf{0.42} \\ \textbf{0.43} \end{array}$	97.00 98.00	0.85 0.86	96.99 97.99	1.27 1.28	97 98
99	99.00	0.43	99.00	0.86	97.99 98.99	1.30	99
100	100.00	0.44	100.00	0.87	99.99	1.31	100
ruce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Distance.	891	Deg.	89 <u>‡</u> I	Deg.	. 891 I	Deg.	Dist
				I			

Dist	1 D	eg.	1 1 I	Deg,	1½]	Deg.	14	Deg.	Distance
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 29 30 31	1.00 3.00 4.00 5.00 6.00 7.00 10.00 11.00 12.00 14.00 15.00 16.00 17.00 20.00 21.00 22.00 23.00 24.00 25.00 28.00 29.00 30.00 31.00	0.02 0.03 0.05 0.07 0.09 0.10 0.12 0.14 0.16 0.17 0.21 0.23 0.24 0.35 0.35 0.35 0.35 0.35 0.35 0.35 0.35	1.00 2.00 3.00 4.00 7.00 8.00 9.00 11.00 112.00 13.00 14.00 15.00 16.00 17.00 20.00 21.00 21.99 22.99 24.99 24.99 24.99 28.99 29.99 30.99	0.02 0.04 0.07 0.09 0.11 0.13 0.15 0.22 0.26 0.28 0.33 0.35 0.37 0.41 0.46 0.48 0.50 0.50 0.55 0.57 0.65 0.65 0.65 0.65	1.00 2.00 3.00 4.00 6.00 7.00 8.00 9.00 11.00 112.00 14.00 14.99 15.99 16.99 20.99 21.99 22.99 22.99 24.99 24.99 26.99 27.99 30.99	0.03 0.05 0.08 0.10 0.16 0.21 0.24 0.28 0.31 0.34 0.37 0.39 0.42 0.47 0.50 0.55 0.60 0.65 0.65 0.65 0.71 0.76 0.76 0.76 0.76	1.00 2.00 3.00 4.00 6.00 7.00 8.00 9.00 10.90 11.99 12.99 13.99 14.99 16.99 20.99 21.99 22.99 22.99 24.99 24.99 26.99 27.99 28.99 27.99 28.99 29.99 30.99	0.03 0.06 0.09 0.12 0.18 0.21 0.25 0.31 0.34 0.37 0.40 0.49 0.55 0.56 0.61 0.67 0.70 0.70 0.70 0.83 0.86 0.89 0.92	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22 24 25 26 27 28 29 30 31
32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50	32.00 32.99 33.99 34.99 35.99 36.99 37.99 40.99 41.99 42.99 44.99 44.99 46.99 47.99 48.99 49.99	0.56 0.58 0.69 0.63 0.66 0.68 0.70 0.72 0.75 0.77 0.79 0.80 0.82 0.84 0.86	31. 99 32. 99 33. 99 34. 99 35. 99 36. 99 38. 99 40. 99 41. 99 42. 99 44. 99 44. 99 46. 99 47. 99 48. 99 49. 99	0.70 0.72 0.76 0.79 0.81 0.85 0.87 0.98 0.94 0.96 0.98 1.03 1.05 1.07	31.99 32.99 33.99 34.99 35.99 36.99 37.99 40.99 41.99 42.99 42.99 44.99 46.99 47.98 48.98	0.84 0.86 0.89 0.92 0.94 0.97 0.99 1.05 1.07 1.10 1.13 1.26 1.28 1.26 1.31	31.99 32.98 33.98 34.98 35.98 36.98 37.98 39.98 40.98 41.98 43.98 44.98 45.98 46.98 47.98 48.98 49.98	1.01 1.04 1.07 1.10 1.13 1.16 1.19 1.22 1.25 1.28 1.31 1.34 1.37 1.40 1.47 1.53	32 33 34 35 36 37 38 39 40 41 42 43 445 46 47 48 49 50
Distance.	Dep. 89 1	Lat. Deg.	Dep.	Lat. Deg.	Dep. 88½	Lat.	Dep.	Lat.	Distance.

Distance.	-1 D	eg:	1 1 1	Deg.	. 11/2	Deg.	12]	Deg.	Distance.
nce.	.Ļat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	шсе.
100 100	Lat. 50.99 51.99 52.99 54.99 55.99 60.99 61.99 60.99 6	Dep. 0.89 0.91 0.92 0.96 0.96 0.98 1.01 1.05 1.06 1.08 1.10 1.12 1.13 1.15 1.17 1.19 1.22 1.24 1.26 1.31 1.34 1.34 1.36 1.40 1.41 1.45 1.47 1.45 1.50 1.55 1.57 1.59 1.66 1.68 1.68 1.69 1.71	50.99 51.99 52.99 552.99 552.99 552.99 552.99 552.99 552.99 60.99 61.99 62.99 62.99 63.98 64.98 65.98 66.98 66.98 67.98 67.98 77.98 77.98 77.98 77.98 78.98 78.98 79.98 80.98	Dep. 1.11 1.13 1.16 1.20 1.22 1.24 1.27 1.39 1.35 1.35 1.37 1.40 1.42 1.44 1.45 1.53 1.55 1.57 1.61 1.66 1.68 1.70 1.77 1.77 1.79 1.81 1.83 1.85 1.90 1.92 1.94 1.96 1.99 2.03 2.05 2.09 2.12	Lat. 50.98 51.98 52.98 53.98 54.98 56.98 56.98 56.98 60.98 61.98 62.98 62.98 63.98 64.98 65.98 66.98 67.98 67.98 70.98 77.97 77.97 77.97 77.97 78.97 78.97 78.97 78.97 78.97 78.97 78.97 79.97	Dep. 1.34 1.36 1.39 1.41 1.47 1.52 1.54 1.60 1.62 1.68 1.70 1.68 1.73 1.86 1.88 1.79 1.89 1.89 1.94 1.99 2.02 2.04 2.12 2.04 2.15 2.28 2.30 2.33 2.36 2.34 2.446 2.51 2.57	50.98 51.98 51.98 52.98 53.97 54.97 55.97 56.97 56.97 60.97 61.97 62.97 66.97 70.97 71.97 73.97 77.97 73.97 74.97 75.96 76.96 77.96 80.96 81.96 81.96 82.96 83.96 84.96 85.96 85.96 87.96 90.96 90.96 91.96	Dep. 1.56 1.59 1.62 1.68 1.71 1.77 1.80 1.89 1.92 2.02 2.08 2.11 2.17 2.23 2.26 2.32 2.35 2.34 2.47 2.53 2.66 2.69 2.72 2.75 2.84 2.99 2.94 2.99	100. 5122345567890 612234656678690 7122374576778790 81223845568990 912239455999999999999999999999999999999999
99 100	98.98 99.98	1.73 1.75	98.98 99.98	2.16 2.18	98.97 99.97	2.59 2.62	98.95 99.95	3.02 3.05	99 100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	89 1	Deg.	883	Deg.	881	Deg.	881	Deg.	Distance.

TRAVERSE TABLE.

Distance	2 I	Deg.	21]	Deg.	21 1	Deg.	21	Deg.	Distance.
mos.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
1 9	1.00 2.00	0.03	1.00 2.00	0.04	1.00	0.04	1.00 2.00	0.05	1
2 3	8.00	0.10	3.00	0.12	3.00	0.13	3.00	0.14	2 3 4
4 5	4.00 5.00	0.14 0.17	4.00 5.00	0.16 0.20	4.00 5.00	0.17	4.00	0.19	5 6
6	6.00	0.21 0.24	6.00	0.24 0.27	5.99	0.26 0.31	5.99	0.29	6
8	7.00 7.99	0.28	7.99	0.81	6.99 7.99	0.35	6.99 7.99	0.34 0.38	8
9 10	8.99 9.99	0.31 0.35	8.99 9.99	0.35 0.39	8.99 9.99	0.39	8.99 9.99	0.43 0.48	9 10
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53	11
12 13	11.99 12.99	0.42	11.99 12.99	0.47 0.51	11.99 12.99	0.52 0.57	11.99 12.99	0.58 0.62	12 13
14	13.99	0.49	13.99	0.55	13.99	0.61	13.98	0.67	14
15 16	14.99 15.99	0.52 0.56	14.99 15.99	0.59 0.63	14.99 15.99	0.65 0.70	14.98 15.98	0.72 0.77	15 16
17	16.99	0.59	16.99	0.67 0.71	16.98	0.74	16.98	0.82	17
18 19	17.99 18.99	0.63 0.66	17.99 18.99	0.75	17.98 18.98	0.79	17.98 18.98	0.86	18 19
20	19.99	0.70	19.98	0.79	19.98	0.87	19.98	0.96	20
21 22	20.99 21.99	0.73 0.77	20.98 21.98	0.82 0.86	20.98 21.98	0.92 0.96	20.98	1.01	21 22
23 24	22.99 23.99	0.80	22.98	0.90 0.94	22.98	1.00 1.05	22.97 23.97	1.10	23 24
24 25	24.98	0.84 0.87	23.98 24.98	0.98	23.98 24.98	1.09	24.97	1.15	25
26 27	25.98 26.98	0.91 0.94	25.98 26.98	1.02	25.98 26.97	1.13	25.97 26.97	1.25	26 27
28	27.98	0.98	27.98	1.10	27.97	1.22	27.97	1.34	28
29 30	28.98 29.98	1.01	28.98 29.98	1.14	28.97 29.97	1.26	28.97 29.97	1.39	29 30
31	30.98	.1.08	30.98	1.22	30.97	1.35	30.96	1.49	31
32 33	31.98 32.98	1.12	31.98 32.97	1.26	31.97 32.97	1.40 1.44	31.96 32.96	1.54 1.58	32 33
34	33.98	1.19	33.97	1.33	33.97	1.48	33.96	1.63	84
35 36	34.98 35.98	1.22 1.26	34.97 35.97	1.37	34.97 35.97	1.53 1.57	34.96 35.96	1.68	35 36
37	36.93	1.29	36.97	1.45	36.96	1.61	36.96	1.78	37
38 39	37.98 38.98	1.33 1.36	37.97 38.97	1.49	37.96 38.96	1.66	37.96 38.96	1.82 1.87	38 39
40	39.98	1.40	39.97	1.57	39.96	.1.75	39.95	1.92	40
41 42	40.98 41.97	1.43	40.97	1.61 1.65	40.96 41.96	1.77	40.95 41.95	1.97 2.02	41 42
43	42.97	1.50	42.97	1.69	42.96	1.88	42.95	2.06	43
44 45	43.97	1.54	43.97 44.97	1.73	43.96 44.96	1.92 1.96	43.95 44.95	2.11 2.16	44 45
46	45.97	1.61	45.96	1.81	45.96	2.01	45.95	2.21	46
47 48	46.97 47.97	1.64	46.96	1.85	46.96 47.95	2.05 2.09	46.95 47.95	2.25 2.30	47 48
49 50	48.97 49.97	1.71 1.74	48.96 49.96	1.92 1.96	48.95 49.95	2.14 2.18	48.94	2.35 2.40	49 50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	88 1	Deg.	873	Deg.	87 <u>1</u>	Deg.	871	Deg.	Distance.

Distance	2 D	eg.	21	Deg.	21	Deg.	21	Deg.	Distance.
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	noe.
51	50.97	1.78	50.96	2.00	50.95	2.22	50.94	2.45	51
52	51.97 52.97	1.81 1.85	51.96 52.96	2.04 2.08	51.95	2.27 2.31	51.94 52.94	2.50 2.54	52 53
53 54	53.97	1.88	53.96	2.12	52.95 53.95	2.36	53.94	2.59	54
55	54.97	1.92	54.96	2.16	54.95	2.40	54.94	2.64	55
56	55.97	1.95	55.96	2.20	55.95	2.44	55.94	2.69	56
57	56.97	1.99 2.02	56.96	2.24	56.95	2.49	56.93 57.93	2.73 2.78	57 58
58 59	57.96 58.96	2.06	57.96 58.95	2.28 2.32	57.94 58.94	2.53 2.57	58.93	2.83	59
60	59.96	2.09	59.95	2.36	59.94	2.62	59.93	2.88	60
61	60.96	2.13	60.95	2.39	60.94	2.66	60.93	2.93	61
62	61.96	2.16	61.95	2.43	61.94	2.70	61.93	2.97	62
63 64	62.96 63.96	2.20 2.23	62.95 63.95	2.47 2.51	62.94 63.94	2.75 2.79	62.93 63.93	3.02 3.07	63 64
65	64.96	2.27	64.95	2.55	64.94	2.79	64.93	3.12	65
66	65.96	2.30	65.95	2.59	65.94	2.88	65.92	3.17	66
67	66.96	2.34	66.95	2.63	66.94	2.92	66.92	3.21	67
68 69	67.96 68.96	2.37 2.41	67.95 68.95	2.67 2.71	67.94 68.93	2.97 3.01	67.92 68.92	3.26 3.31	68 69
70	69.96	2.44	69.95	2.75	69.93	3.05	69.92	3.36	70
71	70.96	2.48	70.95	2.79	70.93	3.10	70.92	3.41	71
72	71.96	2.51	71.94	2.83	71.93	3.14	71.92	3.45	72
73	72.96	2.55	72.94	2.87	72.93	3.18	72.92	3.50	73 74
74	73.95 74.95	2.58 2.62	73.94 74.94	2.91 2.94	73.93 74.93	3.23 3.27	73.91 74.91	3.55 3.60	75
75 76	75.95	2.65	75.94	2.98	75.93	3.31	75.91	3 65	76
77	76.95	2.69	76.94	3.02	76.93	3.36	76.91	3.70	77
78	77.95	2.72	77.94	3.06	77.93	3.40	77.91	3.74 3.79	78 79
79	78.95 79.95	2.76 2.79	78.94 79.94	3.10 3.14	78.92 79.92	3.45 3.49	78.91 79.91	3.79	80
80	80.95	2.83	80.94	3.18	80.92	3.53	80.91	3.89	81
82	81.95	2.86	81.94	3.22	81.92	3.58	81.91	3.93	82
83	82.95	2.90	82.94	3.26	82.92	3.62	82,90	3.98	83
84	83.95	2.93	83.94	3.30	83.92	3.66	83.90 84.90	4.03 4.08	84 85
85 86	84.95 85.95	2.97 3.00	84.93 85.93	3.34 3.38	84.92 85.92	3.71 3.75	85.90	4.13	86
87	86.95	3.04	86.93	3.42	86.92	3.79	86.90	4.17	87
88	87.95	8.07	87.93	8.45	87.92	3.84	87.90	4.22	88
89	88.95 89.95	3.11 3.14	88.93 89.93	3.49 3.53	88.92 89.91	3.88 3.93	88.90 89.90	4.27	89 90
90	90.95	3.14	90:93	3.57	90.91	3.97	90.90	4.37	91
91 92	91.94	3.18	91.93	3.61	91.91	4.01	91.89	4.41	92
93	92.94	3.25	92.93	3.65	92.91	4.06	92.89	4.46	93
94	98.94	3.28	93.93	3.69	93.91	4.10	93.89	4.51	94
95	94.94 95.94	3.32 3.35	94.93 95.93	3.73 3.77	94.91 95.91	4.14 4.19	94.89 95.89	4.56 4.61	95 96
96 97	96.94	3.39	96.93	3.81	96.91	4.23	96.89	4.65	97
08	97.94	3.42	97.92	8.85	97.91	4.27	97.89	4.70	98
99	98.94	8.46	98.92	3.89	98.91	4.32	98.89 99.88	4.75 4.80	99 100
100	99.94	3.49	99.92	3.93	99.91	4.36	ļ		
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
ä	88 1	Deg.	.87‡	Deg.	87 <u>1</u>	Deg.	871	Deg.	ä
					<u> </u>		X		

Table Tabl	Dist	3 E	eg.	3}]	Deg.	3½]	Deg.	31 1	Deg.	Distance.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
9	1		0.10	2.00	0.11	2.00			0.13	1 2
9	3 4	3.00	0.16	3.00	$0.17 \\ 0.23$	2.99 3.99		2.99	0.20	3
9	Š	4.99	0 26	4.99	0.28	4.99	0.31	4.99	0.33	5 6
9	7	6.99	0.37	6.99	0.40	6.99	0.43	6.99	0.46	7
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	9	8.99	0.47	8.99	0.51	8.98	0.55	8.98	0.59	9
12 11.98 0.63 11.98 0.68 11.98 0.73 12.98 0.73 12.97 0.78 12.97 0.85 13 14 13.98 0.79 13.98 0.79 13.97 0.92 14.97 0.92 14 16 14.98 0.79 14.98 0.89 16.97 0.91 15.97 0.98 15.97 1.05 16 17 16.98 0.89 16.97 0.96 16.97 1.04 16.96 1.11 17 18 17.98 0.94 17.97 1.02 17.97 1.10 17.96 1.18 18 19 18.98 0.99 18.97 1.08 18.96 1.16 18.96 1.21 19.96 1.31 20 20 19.97 1.05 19.97 1.13 19.96 1.22 19.96 1.31 20 21 20.97 1.15 21.96 1.30 22.96 1.30 22.96									0.72	11
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12 13	11.98	0.68		$0.68 \\ 0.73$	12.98			0.78	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	13.98	0.73	13.98	0.79	13.97	0.85	13.97	0.92	14
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	16	15.98	0.84	15.97	0.91	15.97	0.98	15.97	1.05	16
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	17.98	0.94	17.97	1.02	17.97	1.10	17.96	1.18	18
22 21.97 1.15 21.96 1.25 21.96 1.34 21.95 1.44 22 23 22.97 1.20 22.96 1.30 22.96 1.47 22.95 1.50 23 24 23.97 1.26 23.96 1.36 23.96 1.47 23.95 1.57 24 25 24.97 1.31 24.96 1.42 24.95 1.53 24.95 1.53 24.95 1.64 25 26.96 1.41 26.96 1.57 25.95 1.59 25.94 1.70 26 27 26.96 1.41 26.96 1.57 27.95 1.59 27.95 1.65 26.94 1.77 27 28 27.96 1.57 28.95 1.64 28.95 1.77 27.94 1.83 28 29.96 1.57 29.95 1.70 29.94 1.83 29.94 1.90 30 29.96 1.57 29.95 1.70 29.94 1.83 29.94 1.96 30 31 30.96 1.62 30.95 1.76 30.94 1.89 30.93 2.03 31 32.95 1.78 33.95 1.81 31.94 1.95 31.93 2.09 32 33 32.95 1.78 33.95 1.87 32.94 2.01 32.93 2.16 33 34.95 1.78 33.95 1.93 33.94 2.08 33.93 2.22 34 35.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 36.95 1.94 36.94 2.10 36.93 2.26 36.92 2.35 36 36.95 1.94 36.94 2.10 36.93 2.26 36.92 2.35 36 37.95 1.99 37.94 2.15 37.93 2.32 37.92 2.49 38 39.95 2.09 39.94 2.27 39.93 2.44 39.91 2.62 40 41.94 2.20 41.93 2.38 41.92 2.56 41.91 2.75 44 43.94 2.26 44.93 2.38 41.92 2.63 42.91 2.81 43 44 43.94 2.36 44.93 2.49 43.92 2.69 43.91 2.88 44 44.94 2.36 44.93 2.55 44.92 2.63 42.91 2.81 43 44 43.94 2.36 44.93 2.55 44.92 2.63 44.93 2.16 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 44.94 2.36 44.93 2.55 44.92 2.63 44.91 2.81 43 44 43.94 2.36 44.93 2.66 46.91 2.87 46.90 3.07 47 48.94 2.36 44.93 2.56 44.93 2.66 46.91 2.87 46.90 3.07 47 48.94 2.36 44.93 2.56 44.93 2.66 46.91 2.87 46.90 3.07 47 48.94 2.36 44.93 2.56 44.93 2.66 46.9			1.05			19.96	1.22	19.96	1.31	20
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	21 22	20.97 21.97								
25 24.97 1.31 24.96 1.42 24.95 1.53 24.95 1.64 25.96 1.76 25.96 1.47 25.95 1.59 25.94 1.70 26 27 26.96 1.41 26.96 1.53 26.95 1.65 26.94 1.77 27 28 27.96 1.47 27.95 1.59 27.95 1.71 27.94 1.83 28 29 28.96 1.57 29.95 1.60 28.95 1.77 28.94 1.90 29 30 29.94 1.96 30 29.95 1.70 29.94 1.83 29.94 1.90 29 30 29.94 1.96 30 30 30 31 30.96 1.67 31.95 1.76 30.94 1.89 30.93 2.03 31 33 32.95 1.73 32.95 1.73 32.95 2.16 33 33 34 34.95 1.83 34.94 2.01 32.93 2.21 33 35	23	22.97	1.20	22.96	1,30	22.96	1.40	22.95	1.50	23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	24.97	1.31	24.96	1.42	24.95	1.53	24.95	1.64	25
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	26.96	1.41	26.96	1.53	26.95	1.65	26.94	1.77	27
31 30.96 1.62 30.95 1.76 30.94 1.89 30.93 2.03 31 32 31.96 1.67 31.95 1.81 31.94 1.95 31.93 2.09 32 33 32.95 1.73 32.95 1.87 32.94 2.01 32.93 2.16 33 34 35 34.95 1.83 34.94 1.98 34.93 2.14 34.92 2.22 34 35 36.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 35.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 37 36.95 1.94 36.94 2.10 36.93 2.26 36.92 2.42 37 38 37.95 1.99 37.94 2.15 37.93 2.32 37.92 2.49 38 39 38.95 2.04 38.94 2.21 38.93 2.38 39.95 2.09 39.94 2.27 39.93 2.44 39.91 2.62 40 41.94 2.20 41.93 2.38 41.92 2.56 41.91 2.75 42 41.94 2.20 41.93 2.38 41.92 2.63 42.91 2.81 43 44.94 2.30 43.93 2.49 43.92 2.69 43.91 2.88 44 43.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 46.94 2.46 44.93 2.56 44.93 2.56 45.94 2.41 47.92 2.76 47.91 2.81 45.90 3.01 46 47.98 2.56 48.92 2.78 48.91 2.87 48.90 3.20 49 49.93 2.55 48.92 2.78 48.91 2.99 48.90 3.20 49 49.93 2.62 49.92 2.83 49.91 3.05 49.89 3.27 50	29	28.96	1.52	28.95	1.64	28.95	1.77	28.94	1.90	29
32 31.96 1.67 31.95 1.81 31.94 1.95 31.93 2.09 32 33 32.95 1.73 32.95 1.87 32.94 2.01 32.93 2.16 33 34 33.95 1.78 33.95 1.93 33.94 2.01 33.93 2.22 34 35 34.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 36 35.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 37 36.95 1.94 36.94 2.15 37.93 2.22 37.92 2.42 37 38 37.95 1.99 37.94 2.21 38.93 2.32 37.92 2.42 37 39 38.95 2.04 38.94 2.21 38.93 2.38 38.92 2.55 39 40 39.95 2.09 39.94 2.27 3					1.76					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	32	31.96	1.67	31.95	1.81				2.09	32
36 35.95 1.88 35.94 2.04 35.93 2.20 35.92 2.35 36 37 36.95 1.94 36.94 2.10 36.93 2.26 36.92 2.42 37 38 37.95 1.99 37.94 2.15 37.93 2.32 37.92 2.49 38 39 38.95 2.04 38.94 2.21 38.93 2.38 38.92 2.55 39 40 39.95 2.09 39.94 2.27 39.93 2.44 39.91 2.62 40 41 40.94 2.15 40.93 2.32 40.92 2:50 40.91 2.68 41 42 41.94 2.25 42.93 2.44 42.92 2.63 42.91 2.81 43 44 43.94 2.36 44.93 2.55 44.92 2.63 42.91 2.81 43 45 44.94 2.36 44.93 2.55 4	34	33.95	1.78	33.95	1.93	33.94	2.08	33.93	2.22	34
38 37.95 1.99 37.94 2.15 37.93 2.32 37.92 2.49 38 39 38.95 2.09 39.94 2.21 38.93 2.38 38.92 2.55 38 41 40.94 2.15 40.93 2.32 40.92 2:50 40.91 2.62 40 42 41.94 2.25 42.93 2.44 42.92 2:56 41.91 2.75 42 43 42.94 2.25 42.93 2.44 42.92 2.63 42.91 2.81 43 44 43.94 2.36 44.93 2.49 43.92 2.69 43.91 2.88 44 45 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 46 45.94 2.41 45.93 2.61 45.91 2.81 45.90 3.01 46 47 46.94 2.46 46.92 2.66 46.91 2.87 46.90 3.07 47 49 48.93 2.56 48.91 2.93 47.90 3.14 48 49 48.93 2.56 48.91 2.93 47.90 3.14 48 <td>36</td> <td>35.95</td> <td>1.88</td> <td>35.94</td> <td>2.04</td> <td>35.93</td> <td>2.20</td> <td>35.92</td> <td>2.35</td> <td>36</td>	36	35.95	1.88	35.94	2.04	35.93	2.20	35.92	2.35	36
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	38	37.95	1.99	37.94	2.15	37.93	2.32	37.92	2.49	38
42 41.94 2.20 41.93 2.38 41.92 2.56 41.91 2.75 42 43 42.94 2.25 42.93 2.44 42.92 2.63 42.91 2.81 43 44 43.94 2.36 44.93 2.55 44.92 2.69 43.91 2.88 44 45 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 46 45.94 2.41 45.93 2.61 45.91 2.81 45.90 3.01 46 47 46.94 2.46 46.92 2.66 46.91 2.87 46.90 3.07 47 48 47.93 2.51 47.92 2.72 47.91 2.93 47.90 3.14 48 49 48.93 2.56 48.91 2.99 48.90 3.20 49 50 49.93 2.62 49.92 2.83 49.91 3.05 4			2.09		2.27	39.93				
44 43.94 2.30 43.93 2.49 43.92 2.69 43.91 2.88 44.94 45 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 46 45.94 2.41 45.93 2.61 45.91 2.81 45.90 3.01 46 47 46.94 2.46 46.92 2.66 46.91 2.87 46.90 3.07 47 48 47.93 2.51 47.92 2.72 47.91 2.93 47.90 3.14 48 49 48.93 2.56 48.92 2.78 48.91 2.99 48.90 3.20 49 50 49.93 2.62 49.92 2.83 49.91 3.05 49.89 3.27 60	41		2.15 2.20		2.32				2.68	
45 44.94 2.36 44.93 2.55 44.92 2.75 44.90 2.94 45 46 45.94 2.41 45.93 2.61 45.91 2.81 45.90 3.01 46 47 46.94 2.46 46.92 2.66 46.91 2.87 46.90 3.07 47 48 47.93 2.51 47.92 2.72 47.91 2.93 47.90 3.14 48 49 48.93 2.56 48.92 2.78 48.91 2.99 48.90 3.20 49 50 49.93 2.62 49.92 2.83 49.91 3.05 49.89 3.27 50	43	42.94	2.25	42.93	2.44	42.92	2.63	42.91	2.81	43
47 48.94 2.46 46.92 2.66 46.91 2.87 46.90 3.07 47 48 47.93 2.51 47.92 2.72 47.91 2.93 47.90 3.14 48 49 48.93 2.56 48.92 2.78 48.91 2.99 48.90 3.20 49 50 49.93 2.62 49.92 2.83 49.91 3.05 49.89 3.27 50	45	44.94	2.36	44.93	2.55	44.92	2.75	44.90	2.94	45
49 48.93 2.56 48.92 2.78 48.91 2.99 48.90 3.20 49 50 49.93 2.62 49.92 2.83 49.91 3.05 49.89 3.27 50	47	46.94	2.46	46.92	2.66	46.91	2.87	46.90	3.07	47
	49	48.93	2.56	48.92	2.78	48.91	2.99	48.90	3.20	49
87 Deg. 861 Deg. 861 Deg. 861 Deg. 861 Deg.										
87 Deg. 861 Deg. 861 Deg. 5	tanc	Dah.	Liat.	Deb.	Lat.	Dep.	Lat.	Dep. Lat.		tanc
	ä	87 I	Deg.	.863	Deg.	.861	Deg.	861	861 Deg.	

Dist	3 D	eg.	31 I	Deg.	3½ I	Deg.	3¾ I	eg.	DISI
tance	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.93	2.67	50.92	2.89	50.90	3.11	50.89	3.34	5
52	51.93	2.72 2.77	51.92	2.95	51.90	3.17	51.89	3.40	55
53	52.93	2.77	52.91	3.00	52.90	3.24	52.89	3.47	5
54	53.93	2.83	53.91	3.06	53.90	3.30	53.88	3.53	5
55	54.92	2.88	54.91	3.12	54.90	3.36	54.88	3.60	5
56	55.92	2.93	55.91	3.17 3.23	55.90	3.42	55.88	3.66	5
57	56.92	2.98	56.91	3.23	56.89	3.48	56.88	3 73 3.79	5
58	57.92	3.04	57.91	3.29	57.89	3.54	57.88	3.86	5
59 60	58.92	3.09	58.91	$\frac{3.34}{3.40}$	58.89 59.89	3.66	59.87	3.92	60
-	59.92	3.14	59.90			3.72	60.87	3.99	6
61	60.92	3.19 3.24	60.90	$\frac{3.46}{3.51}$	60.89	3.79	61.87	4.05	6
62 63	61.92	3.30	62.90	3.57	62.88	3.85	62,87	4.12	6
64	62.91 63.91	3.35	63.90	3.63	63.88	3.91	63.86	4.19	6
65	64.91	3.40	64.90	3.69	64.88	3.97	64.86	4.25	6
66	65.91	3.45	65.89	3.74	65.88	4.03	65.86	4.32	6
67	66.91	3.51	66.89	3.80	66.88	4 09	66.86	4.38	6
68	67.91	3.56	67.89	3.86	67.87	4.15	67.85	4.45	6
69	68.91	3.61	68.89	3.91	68.87	4.21	68.85	4.51	6
70	69.90	3.66	69.89	3.97	69.87	4.27	69.85	4.58	7
71	70.90	3.72	70.89	4.03	70.87	4.33	70.85	4.64	7
72	71.90	3.77	71.88	4.08	71.87	4.40	71.85	4.71	7
73	72.90	3.82	72.88	4.14	72.86	4.46 4.52	72.84 73.84	4.84	7
74	73.90	3.87	73.88	4.20	73.86	4.58	74.84	4.91	7
75 76	74.90 75.90	3.98	74.88 75.88	4.25	75.86	4 64	75.84	4.97	7
77	76.89	4.03	76.88	4.37	76.86	4.70	76.84	5.04	7
78	77.89	4.08	77.87	4.42	77.85	4.76	77.83	5.10	7
79	77.89 78.89	4.13	78.87	4.48	78.85	4.82	78.83	5.17	7
80	79.89	4.19	79.87	4.54	79.85	4.88	79.83	5.23	- 8
81	80.89	4.24	80.87	4.59	80.85	4.94	80.83	5.30	8
82	81.89	4.29	81.87	4.65	81.85	5.01	81.82	5.36	8
83	82.89	4.34	82.87	4.71 4.76	82.85	5.07	82.82	5.43 5.49	8
84	83.88	4.40	83.86	4.76	83.84	5.13 5.19	83.82	5.56	8
85	84.88	4.45	84.86 85.86	4.82	84.84	5.25	85.82	5.62	8
86	85.88	4.55	86.86	4.93	86.84	5.31	86.81	5.69	8
88	87.88	4.61	87.86	4.99	87.84	5.37	87.81	5.76	8
89	88.88	4.66	88.86	5.05	88.83	5.43	88.81	5.82	8
90	89.88	4.71	89.86	5.10	89.83	5.49	89.81	5.89	9
91	90.88	4.76	90.85	5.16	90.83	5.56	90.81	5.95	9
92	91.87	4.81	91.85	5.22	91,83	5.62	91.80	6.02	9
93	92.87	4.87	92.85	5.27	92.83	5.68	92.80	6.08	9
94	93.87	4.92	93.85	5.33	93.82	5.74	93.80 94.80	6.21	9
95	94.87	4.97	94.85	5.39	94.82 95.82	5.80		6.28	g
96	95.87	5.02 5.08	95.85	5.44 5.50	96.82	5.92	95.79 96.79	6.34	9
97 98	97.87	5.13	97.84	5.56	97.82	5.98	97.79	6.41	9
99	98.86	5.18	97.84 98.84	5.61	98.82	6.04	98.79	6.47	9
100	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	10
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	3000
Distance.	.87]	Deg.	863	Deg.	861	Deg.	861	Deg.	

Distance.	4 D	eg.	41 I	Deg.	4½ I	Deg.	41 I	eg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
1 2 3 4 5 6 7 8 9	1.00 2.00 2.99 3.99 4.99 5.99 6.98 7.98	0.07 0.14 0.21 0.28 0.35 0.42 0.49 0.56	1.00 1.99 2.99 3.99 4.99 5.98 6.98 7.98	0.07 0.15 0.22 0.30 0.37 0.44 0.52 0.59	1.00 1.99 2.99 3.99 4.98 5.98 6.98 7.98	0.08 0.16 0.24 0.31 0.39 0.47 0.55 0.63	1.00 1.99 2.99 3.98 4.98 5.98 6.97 7.97	0.08 0.17 0.25 0.33 0.41 0.50 0.58 0.66	1 2 3 4 5 6 7 8
10	8.98 9.98	0.63	8.98 9.97	0.67 0.74	8.97 9.97	$\begin{array}{c} 0.71 \\ 0.78 \end{array}$	8.97 9.97	0.75 0.83	10
11 12 13 14 15 16 17 18	10.97 11.97 12.97 13.97 14.96 15.96 16.96 17.96	0.77 0.84 0.91 0.98 1.05 1.12 1.19 1.26 1.33	10.97 11.97 12.96 13.96 14.96 15.96 16.95 17.95	0.82 0.89 0.96 1.04 1.11 1.19 1.26 1.33	10.97 11.96 12.96 13.96 14.95 15.95 16.95 17.94 18.94	0.86 0.94 1.02 1.10 1.18 1.26 1.33 1.41	10.96 11.96 12.96 13.95 14.95 15.95 16.94 17.94 18.93	0.91 0.99 1.08 1.16 1.24 1.32 1.41 1.49	11 12 13 14 15 16 17
19 20 21	18.95 19.95 20.95	$\frac{1.40}{1.46}$	18.95 19.95 20.94	$\frac{1.40}{1.48}$ 1.56	$\frac{18.94}{19.94}$ 20.94	$\frac{1.49}{1.57}$	$\frac{19.93}{20.93}$	$\frac{1.57}{1.66}$ 1.74	19 20 21
22 23 24 25 26	21.95 22.94 23.94 24.94 25.94	1.53 1.60 1.67 1.74 1.81	21.94 22.94 23.93 24.93 25.93	1.63 1.70 1.78 1.85 1.93	21.93 22.93 23.93 24.92 25.92	1.73 1.80 1.88 1.96 2.04	21.92 22.92 23.92 24.91 25.91	1.82 1.90 1.99 2.07 2.15	22 23 24 25 26
27 28 29 30	26.93 27.93 28.93 29.93	1.88 1.95 2.02 2.09	26.93 27.92 28.92 29.92	2.00 2.08 2.15 2.22	26.92 27.91 28.91 29.91	2.12 2.20 2.28 2.35	26.91 27.90 28.90 29.90	2.24 2.32 2.40 2.48	27 28 29 30
31 32 33 34 35	30.92 31.92 32.92 33.92 34.91	2.16 2.23 2.30 2.37 2.44	30.91 31.91 32.91 33.91 34.90	2.30 2.37 2.45 2.52 2.59	30.90 31.90 32.90 33.90 34.89	2.43 2.51 2.59 2.67 2.75	30.89 31.89 32.89 33.88 34.88	2.57 2.65 2.73 2.82 2.90	31 32 33 34 35
36 37 38 39	35.91 36.91 37.91 38.90	2.51 2.58 2.65 2.72 2.79	35.90 36.90 37.90 38.89	2.67 2.74 2.82 2.89	35.89 36.89 37.88 38.88	2.82 2.90 2.98 3.06 3.14	35.88 36.87 37.87 38.87	2.98 3.06 3.15 3.23	36 37 38 39
40 41 42 43 44	43.89	2.86 2.93 3.00 3.07	39.89 40.89 41.88 42.88 43.88	3.04 3.11 3.19 3.26	39.88 40.87 41.87 42.87 43.86	3.22 3.30 3.37 3.45	39.86 40.86 41.86 42.85 43.85	3.40 3.48 3.56 3.64	40 41 42 43 44
45 46 47 48 49 50	45.89 46.89 47.88 48.88	8.42	44.88 45.87 46.87 47.87 48.87 49.86	3.33 3.41 3.48 3.56 3.63 3.71	44.86 45.86 46.86 47.85 48.85 49.85	3.53 3.61 3.69 3.77 3.84 3.92	44.85 45.84 46.84 47.84 48.83 49.83	3.81 3.89 3.97 4.06	45 46 47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep. 851	Lat.	Dep.	Lat.	Distance.

Dist	4 I	eg.	41	Deg.	4½ I	Deg.	43	Deg.	DIST.
tance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.88	3.56	50.86	3.78	50.84	4.00	50.82	4.22	5
52	51.87	3.63	51.86	3.85	51.84	4.08	51.82	4.31	5
53	52.87	3.70	52.85	3.93	52.84	4.16	52.82	4.39	5
54 55	53.87	3.77 3.84	53.85	4.00	53.83	4.24	53.81	4.47	5
56	54.87 55.86	3.91	54.85	4.08	54.83	4.32	54.81	4.55	5
57	56.86	3.98	55.85 56.84	4.15	55.83	4.39	55.81 56.80	4.64	5
58	57.86	4.05	57.84	$\frac{4.22}{4.30}$	57.82	4.55	57.80	4.80	5
59	58.86	4.12	58.84	4.37	58.82	4.63	58.80	4.89	5
60	59.85	4.19	59.84	4.45	59.82	4.71	59.79	4.97	6
61	60.85	4.26	60.83	4.52	60.81	4.79	60.79	5.05	6
62	61.85	4.32	61.83	4.59	61.81	4.86	61.79	5.13	6
63	62.85	4.39	62.83	4.67	62.81	4.94	62.78	5.22	6
64	63.84	4.46	63.82	4.74	63.80	5.02	63.78	5.30	6
65	64.84	4.53	64.82	4.82	64.80	5.10 5.18	64.78	5.38 5.47	6
67	65.84	4.67	$65.82 \\ 66.82$	4.89	65.80	5.26	65.77	5.55	6
68	67.83	4.74	67.81	5.04	67.79	5.34	67.77	5.63	6
69	68.83	4.81	68.81	5.11	68.79	5.41	68.76	5.71	6
70	69.83	4.88	68.81 69.81	5.19	69.78	5.49	69.76	5.80	7
71	70.83	4.95	70.80	5.26	70.78	5.57	70.76	5.88	7
72	71.82	5.02	71.80	5.34	71.78	5.65	71.75	5.96	7
73	72.82	5.09	72.80	5.41	72.77	5.73	72.75	6.04	7
74 75	73.82 74.82	5.16 5.23	73.80	5.48	73.77	5.81	73.75	$6.13 \\ 6.21$	7
76	75.81	5.30	74.79	5.56 5.63	74.77	5.88	74.74	6.29	7
77	76.81	5.37	75.79 76.79 77.79	5.71	76.76	6.04	76.74	6.38	7
78	77.81 78.81	5.44	77.79	5.71 5.78	77.76	6.12	77.73	6.46	7
79		5.51	78.78	5.85	78.76	6.20	78.73	6.54	7
80	79.81	5.58	79.78	5.93	79.75	6.28	79.73	6.62	8
81	80.80	5.65	80.78	6.00	80.75	6.36	80.72	6.71	8
82	81.80 82.80	5.72 5.79	81.78 82.77	6.08	81.75	6.43	81.72	6.79	8
83 84	83.80	5.86	83.77	6.15	82.74	6.51	82.71	6.87	8
85	84.79	5.93	84.77	$6.23 \\ 6.30$	83.74	6.67	84.71	7.04	8
86	85.79	6.00	85.76	6.37	85.73	6.75	85,70	7.12	8
87	86.79	6.07	86.76	6.45	86.73	6.83	86.70	7.12 7.20	8
88	87.79	6.14	87.76 88.76	6.52	87.73	6.90	87.70	7.29	8
89	88.78	$\frac{6.21}{6.28}$	88.76	6.60	88.73	6.98	88.70	7.37	8
90	89.78		89.75	6.67	89.72	7.06	89.69	7.45	9
91	90.78	6.35	90.75	6.74	90.72	7.14	90.69	7.54	9
92 93	$91.78 \\ 92.77$	6.42 6.49	91.75	6.82	91.72	7.22 7.30	91.68	7.62 7.70	9 9
94	93.77	6.56	92.74 93.74	6.97	$92.71 \\ 93.71$	7.38	93.68	7.78	9
95	93.77 94.77	6.63	94.74	7.04	94.71	7.45	94.67	7.87	9
96	95.77	6.70	95.74	7.11	95.70	7.53	95.67	7.95	9
97	96.76	6.77	96.73 97.73	7.11 7.19 7.26	96.70	7.61	96.67	8.03	9
98	97.76 98.76	6.84	97.73	7.26	97.70	7.69	97.66	8.12	9
99	99.76	6.91	98.73 99.73	$7.34 \\ 7.41$	98.69	7.77	98.66 99.66	8.20	10
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	-
Distance.	86 I	Deg.	853	Deg.	851	Deg.	851	Deg.	Dietonoo

K

Distance.	5 D	eg.	5 1 I	eg.	5 <u>1</u>]	Deg.	51 1	Deg.	· Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
<u> </u>	1.00	0.09	1.00	0.09	1.00	0.10 0.19	0.99	0.10 0.20	1 2
2 3 4 5 6 7	2.99	0.26	2.99	0.27	2.99	0.29	2.98	0.30	2 3 4
4	3.98	0.35	3.98	0.37	3.98	0.38	3.98	0.40	4
5	4.98 5.98	0.44	4.98 5.97	0.46	4.98 5.97	0.48 0.58	4.97 5.97	0.50	5 6
7	6.97	0.61	6.97	0.64	6.97	0.67	6.96	0.70	7
В	7.97 8.97	0.70	7.97	0.73	7.96	0.76	7.96	0.80	- 8
9 10	9.96	0.78 0.87	8.96 9.96	$\begin{array}{c} 0.82 \\ 0.92 \end{array}$	8 96 9.95	0.86 0.96	8.95 9.95	0.90 1.00	9 10
11	10.96	0.96	10.95	1.01	10.95	1.05	10.94	1.10	11
12 13	11.95 12.95	1.05	11.95 12.95	1.10 1.19	11.94 12.94	1.15 1.25	11.94 12.93	1.20 1.30	12 13
14	13.95	1.22	13.94	1.28	13.94	1.34	13.93	1.40	14
15	14.94	1.31	14.94	1.37	14.93	1.44	14.92	1.50	15 16
16 17	15.94 16.94	1.48	15.93 16.93	1.46 1.56	15.93 16.92	1.53	15.92 16.91	1.60 1.70	17
18	17.93	1.57	17.92	1.65	17.92	1.73	17.91	1.80	18
19 20	18.93 19.92	1.66 1.74	18.92 19.92	1.74 1.83	18.91 19.91	1.82	18.90 19.90	1.90 2.00	19 20
21	20.92	1.83	20.91	1.92	20.90	2.01	20.89	2.10	21
22	21.92 22.91	1.92 2.00	21.91 22.90	2.01	21.90 22.89	2.11 2.20	21.89 22.88	2.20 2.30	22 23
23 24	23.91	2.09	23.90	2.10 2.20	23.89	2.30	23.88	2.40	24
25	24.90	2.18	24.90	2.29	24.88	2.40	24.87	2.50	25
26 27	25.90 26.90	$2.27 \\ 2.35$	25.89 26.89	2.38 2.47	25.88 26.88	2.49 2.59	25.87 26.86	2.60. 2.71	26 27
28	27.89	2.44	27.88	2.56	27.87	2.68	27.86	2.81	28
29	28.89	2.53	28.88	2.65	28.87	2.78	28.85	2.91	29
30 31	29.89 30.88	$\frac{2.61}{2.70}$	$\frac{29.87}{30.87}$	$\frac{2.75}{2.84}$	$\frac{29.86}{30.86}$	$\frac{2.88}{2.97}$	$\frac{29.85}{30.84}$	$\frac{3.01}{3.11}$	$\frac{30}{31}$
32	31.88	2.79	31.87	2.93	31.85	3.07	31.84	3.21	32
3 3	32.87	2.88	32.86	3.02	32.85	3.16	32.83	3.31	33
34 35	33.87 34.87	2.96 3.05	33.86 34.85	3.11 3.20	33.84 34.84	3.26 3.35	33.83 34.82	3.41	34 35
36	35.86	3.14	35.85	3.29	35.83	3.45	35.82	3.61	36
37	36.86	3.22	36.84	3.39	36.83	3.55	36.81	3.71	37
38 39	37.86 38.85	3.31 3.40	37.84 38.84	3.48 3.57	37.83 38.82	3.64	37.81 38.80	3.81	38 39
40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	4.01	40
41	40.84	3.57	40.83	3.75	40.81	3.93	40.79	4.11	41
42 43	41.84 42.84	3.66 3.75	41.82 42.82	3.84 3.93	41.81	4.03	41.79 42.78	4.21	42 43
43 44	48.83	3.75	43.82	4.03	42.80 43.80	4.12	42.78	4.31	43
45	44.83	3.92	44.81	4.12	44.79	4.31	44.77	4.51	45
46 47	45.82 46.82	4.01 4.10	45.81 46.80	4.21 4.30	45.79 46.78	4.41	45.77 46.76	4.61	46 47
48	47.82	4.18	47.80	4.39	47.78	4.60	47.76	4.81	48
49 50	48.81 49.81	4.27 4.36	48.79 49.79	14.48 4.58	48.77 49.77	4.70	48.75 49.75	4.91 5.01	49 50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep. Lat.		
Distance.		1				1 244	Dep. Lat.		Distance.
ĕ	85	Deg.	843	Deg.	841	Deg.	841	Deg.	1.5
Ι".	55				-3	5.	1		1-
نسيب									_

Distance.	, 5 I	eg.	51 1	Deg.	5 <u>1</u>	Deg.	5 1 1	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52 53 54 55 56 56 57 58 60 61 62 63 64 65 66 67 70 71 72 73 74 75 76 77 78 79 80 80	50.81 51.80 52.80 53.79 55.79 55.78 56.78 59.77 60.77 61.76 62.76 63.76 64.75 66.75 67.74 69.73 70.73 71.73 72.72 73.72 74.71 75.71 76.71 77.70 78.70 79.70 80.69 81.69	4.44 4.53 4.67 4.79 4.887 5.06 5.12 5.40 5.549 5.58 5.67 5.84 5.93 6.10 6.19 6.36 6.45 6.62 6.71 7.06 6.89 7.15	50.79 51.78 52.78 53.77 56.77 56.77 56.76 57.76 59.75 60.74 61.74 62.74 63.73 64.73 64.73 64.71 69.71 70.70 71.70 71.70 72.69 73.69 74.68 76.68 77.68 78.67 79.66 80.66 80.66 81.66	4.76 4.76 4.85 4.93 5.12 5.31 5.49 5.58 5.67 6.13 6.22 6.41 6.50 6.68 6.77 6.86 6.77 6.86 7.05 7.14 7.23 7.32	50.77 51.76 52.76 53.75 53.75 54.75 55.74 56.74 57.73 58.73 59.72 60.72 61.71 62.71 63.71 64.70 65.69 67.69 67.69 67.69 67.69 67.69 67.69 68.68 70.67 71.67 72.66 73.66 74.65 76.65 77.66 78.64 79.63 80.63 80.63 81.62	4.98 5.08 5.18 5.27 5.37 5.56 5.57 5.94 6.023 6.323 6.323 6.323 6.71 6.90 7.09 7.28 7.38 7.57 7.67 7.86	50.74 51.74 52.73 53.73 53.73 54.72 55.72 56.71 57.71 58.70 60.69 61.69 62.68 63.68 64.67 65.67 66.66 67.66 68.65 69.65 70.64 71.64 72.63 73.63 74.62 76.61 77.61 78.60 79.60 80.59 80.59 81.59	5.11 5.21 5.31 5.61 5.61 5.71 6.21 6.31 6.31 6.41 6.61 7.01 7.21 7.41 7.61 7.71 7.61 7.71 7.81 8.02 8.12	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 67 70 71 72 73 74 75 77 77 78 79 80 81
83 84 85 86 87 88 89 90	82.68 83.68 84.68 85.67 86.67 87.67 88.66 89.66	7.23 7.32 7.41 7.50 7.58 7.67 7.76 7.84	82.65 83.65 84.64 85.64 86.64 87.63 88.63 89.62	7.59 7.69 7.78 7.87 7.96 8.05 8.14 8.24	82.62 83.61 84.61 85.60 86.60 87.59 88.59 89.59	7.96 8.05 8.15 8.24 8.34 8.43 8.53 8.63	82.58 83.58 84.57 85.57 86.56 87.56 88.55 89.55	8.32 8.42 8.52 8.62 8.72 8.82 9.02	83 84 85 86 87 88 89 90
91 92 93 94 95 96 97 98 99	90.65 91.65 92.65 93.64 94.64 95.63 96.63 97.63 98.62 99.62	7.93 8.02 8.11 8.19 8.28 8.37 8.45 8.63 8.72	90.62 91.61 92.61 93.61 94.60 95.60 96.59 97.59 98.59 99.58	8.33 8.42 8.51 8.60 8.69 8.78 8.88 8.97 9.06 9.15	90.58 91.58 92.57 93.57 94.56 95.56 96.55 97.55 98.54 99.54	8.72 8.82 8.91 9.01 9.11 9.20 9.30 9.39 9.49 9.58	90.54 91.54 92.53 93.53 94.52 95.52 96.51 97.51 98.50 99.50	9.12 9.22 9.32 9.42 9.52 9.62 9.72 9.82 9.92 10.02	91 92 93 94 95 96 97 98 99 100
Distance.	Dep. 85 1	Lat.	Dep. 841	Lat. Deg.	Dep. 841	Lat. Deg.	Dep. 844	Lat. Deg.	Distance.

Distance	6 I	Deg.	61 1	Deg.	-6 <u>1</u> I	Deg.	6‡ 1	Deg.	Distance.
III Ce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	mce.
1	0.99	0.10	0.99	0.11	0.99	0.11	0.99	0.12	2 3
2	1.99	0.21	1.99	0.22	1.99	0.23	1.99	0.24	
3	2.98	0.31	2.98	0.33	2.98	0.34	2.98	0.35	
4 5 6	8.98 4.97 5.97	0.41 0.52 0.63	3.98 4.97 5.96	0.44 0.54 0.65	3.97 4.97 5.96	0.45 0.57 0.68	3.97 4.97 5.96	0.47 0.59 0.71	2 3 4 5 6
7	6.96	0.73	6.96	0.76	6.96	0.79	6.95	0.82	7
8	7.96	0.84	7.95	0.87	7.95	0.91	7.94	0.94	8
9	8.95	0.94	8.95	0.98	8.94	1.02	8.94	1.06	9
$\frac{10}{11}$	9.95	1.05	$\frac{9.94}{10.93}$	1.09	$\frac{9.94}{10.93}$	1.13	$\frac{9.93}{10.92}$	1.18	10
12	11.93	1.25	11.93	1.31	11.92	1.36	11.92	1.41	12
13	12.93	1.36	12.92	1.42	12.92	1.47	12.91	1.53	13
14	13.92	1.46	13.92	1.52	13.91	1.59	13.90	1.65	14
15	14.92	1.57	14.91	1.63	14.90	1.70	14.90	1.76	15
16	15.91	1.67	15.90	1.74	15.90	1.81	15.89	1.88	16
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00	17
18	17.90	1.88	17.89	1.96	17.88	2.04	17.88	2.12	18
19	18.90	1.99	18.89	2.07	18.88	2.15	18.87	2.23	19
20	19.89	2.09	19.88	2.18	19.87	2.26	19.86	2.35	20
21	20.88	2.20	20.88	2.29	20.87	2.38	20.85	2.47	21
22	21.88	2.30	21.87	2.40	21.86	2.49	21.85	2.59	22
23	22.87	2.40	22.86	2.50	22.85	2.60	22.84	2.70	23
24	23.87	2.51	23.86	2.61	23.85	2.72	23.83	2.82	24
25	24.86	2.61	24.85	2.72	24.84	2.83	24.83	2.94	25
26	25.86	2.72	25.85	2.83	25.83	2.94	25.82	3.06	26
27	26.85	2.82	26.84	2.94	26.83	3.06	26.81	3.17	27
28	27.85	2.93	27.83	3.05	27.82	3.17	27.81	3.29	28
29	28.84	3.03	28.83	3.16	28.81	3.28	28.80	3.41	29
30 31 32	30.83 31.82	3.14 3.24 3.34	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{3.27}{3.37}$	$\frac{29.81}{30.80}$ 31.79	$\frac{3.40}{3.51}$	$\frac{29.79}{30.79}$ 31.78	3.53 3.64 3.76	30 31 32
33 34 35	32.82 33.81 34.81	3.45 3.55 3.66	32.80 33.80 34.79	3.59 3.70 3.81	32.79 33.78	3.74 3.85 3.96	32.77 33.76 34.76	3.88 4.00 4.11	33 34 35
36 37 38	35.80 36.80 37.79	8.76 8.87 3.97	35.79 36.78 37.77	3.92 4.03 4.14	34.78 35.77 36.76 37.76	4.08 4.19 4.30	35.75 36.75	4.23 4.35 4.47	36 37 38
39 40	38.79 39.78	4.08 4.18	38.77 39.76	4.25 4.35	37.76 38.75 39.74	4.41 4.53	37.74 38.73 39.72	4.58 4.70	39 40
41	40.78	4.29	40.76	4.46	40.74	4.64	40.72	4.82	41
42	41.77	4.39	41.75	4.57	41.73	4.76	41.71	4.94	42
43	42.76	4.49	42.74	4.68	42.72	4.87	42.70	5.05	43
44	43.76	4.60	43.74	4.79	43.72	4.98	43.70	5.17	44
45	44.75	4.70	44.73	4.90	44.71	5.09	44.69	5.29	45
46	45.75	4.81	45.73	5.01	45.70	5.21	45.68	5.41	46
47	46.74	4.91	46.72	5.12	46.70	5.32	46.67	5.52	47
48	47.74	5.02	47.71	5.23	47.69	5.43	47.67	5.64	48
49	48.73	5.12	48.71	5.34	48.69	5.55	48.66	5.76	49
50	49.73	5.23	49.70	5.44	49.68	5.66	49.65	5.88	50
8	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	84]	Deg.	63 1	Deg.	831	Deg.	831	Deg.	Distance.

Distance.	6 D	eg.	·61 I	Deg.	6 <u>1</u>]	Deg	6 } I	eg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52 53 54 55 56 57 58 59 60 61 62 63 64 65	50.72 51.72 52.71 53.70 55.69 56.69 57.68 58.68 59.67 60.67 61.66 62.65 63.65 64.64	5.33 5.44 5.54 5.64 5.75 5.96 6.06 6.17 6.27 6.38 6.48 6.59 6.69 6.79	50.70 51.69 52.68 53.68 54.67 55.67 56.66 57.66 57.66 59.64 60.64 61.63 62.63 63.62 64.61	5.55 5.66 5.77 5.88 5.99 6.21 6.31 6.42 6.53 6.64 6.75 6.86 6.97 7.08	50.67 51.67 52.66 53.65 54.65 55.64 56.63 57.63 57.63 60.61 61.60 62.60 63.59 64.58	5.77 5.89 6.00 6.11 6.23 6.34 6.45 6.57 6.68 6.79 6.91 7.02 7.13 7.25 7.36	50.65 51.64 52.63 53.63 54.62 55.61 56.60 57.60 58.59 59.58 60.58 61.57 62.56 63.56 64.55	5.99 6.11 6.23 6.35 6.46 6.58 6.70 6.82 6.93 7.05 7.17 7.29 7.40 7.52 7.64	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65
66 67 68 69 70 71 72 73 74 75 76	65.64 66.63 67.63 68.62 69.62 70.61 71.61 72.60 73.59 74.59 75.58 76.58	6.90 7.00 7.11 7.21 7.32 7.42 7.53 7.63 7.74 7.84 7.94 8.05	65.61 66.60 67.60 68.59 69.58 70.58 71.57 73.56 74.55 75.55 76.54	7.19 7.29 7.40 7.51 7.62 7.73 7.84 7.95 8.06 8.17 8.27 8.38	65.58 66.57 67.56 68.56 69.55 70.54 71.54 72.53 73.52 74.52 75.51 76.51	7.37 7.58 7.70 7.81 7.92 8.04 8.15 8.26 8.38 8.49 8.60 8.72	65.54 66.54 67.53 68.52 69.51 70.51 71.50 72.49 74.48 75.47 76.47	7.76 7.88 7.99 8.11 8.23 8.35 8.46 8.58 8.70 8.82 8.93 9.05	66 67 68 69 70 71 72 73 74 75 76
78 79 80 81 82 83 84 85 86 87 88	77.57 78.57 79.56 80.56 81.55 82.55 83.54 84.53 85.53 86.52 87.52	8.15 8.26 8.36 8.47 8.57 8.68 8.78 8.88 9.09 9.20 9.30	77.54 78.53 79.53 80.52 81.51 82.51 83.50 84.50 85.49 86.48 87.48 88.47	8.49 8.60 8.71 8.82 8.93 9.04 9.14 9.25 9.36 9.47 9.58	77.50 78.49 79.49 80.48 81.47 82.47 83.46 84.45 86.44 87.43 88.43	8.83 8.94 9.06 9.17 9.28 9.40 9.51 9.62 9.74 9.85 9.96	77.46 78.45 79.45 80.44 81.43 82.42 83.42 84.41 85.40 86.40 87.39 88.38	9.17 9.29 9.40 9.52 9.64 9.76 9.87 9.99 10.11 10.23 10.34 10.46	78 79 80 81 82 83 84 85 86 87 88 89
90 91 92 93 94 95 96 97 98 99 100	89.51 90.50 91.50 92.49 93.49 94.48 95.47 96.47 97.46 98.46 99.45	9.41 9.51 9.62 9.72 9.83 9.93 10.03 10.14 10.24 10.35 10.45 Lat.	89.47 90.46 91.45 92.45 93.44 94.44 95.43 96.42 97.42 98.41 99.41	9.80 9.91 10.02 10.12 10.34 10.45 10.56 10.67 10.78 10.89	99.42 90.42 91.41 92.40 93.40 94.39 95.38 96.38 97.37 98.36 99.36	10.19 10.30 10.41 10.53 10.64 10.75 10.87 10.98 11.09 11.21 11.32	89.38 90.37 91.36 92.36 93.35 94.34 95.33 96.33 97.32 98.31 99.31	10.58 10.70 10.81 10.93 11.05 11.17 11.28 11.40 11.52 11.64 11.75	90 91 92 93 94 95 96 97 98 99 100
Distance	Dep.	Deg.	Dep.	Deg.	Bep. 83½	Lat. Deg.	Dep. 831	Lat. Deg.	Distance.

Die	7 D	eg.	7 <u>1</u> T	eg.	71/2	Deg.	73 1	Deg.	Distance
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
1 2 3	0.99	0.12 0.24	0.99	0.13 0.25	0.99 1.98	0.13 0.26	0.99	0.13 0.27	1 2
4	2.98 3.97	0.37 0.49	2.98 3.97	0.38 0.50	2.97 3.97	$0.39 \\ 0.52$	2.97 3.96	0.40	3 4
5 6	4.96 5.96	0.61 0.73	4.96 5.95	0.63 0.76	4.96 5.95	$\begin{array}{c} 0.65 \\ 0.78 \end{array}$	4.95 5.95	0.67	5 6
8	6.95 7.94	0.85	6.94 7.94	0.88 1.01	6.94 7.93	0.91 1.04	6.94 7.93	0.94 1.08	8
9 10	8.93 9.93	1.10 1.22	8.93 9.92	1.14 1.26	8.92 9.91	1.17	8.92 9.91	1.21 1.35	9 10
11 12	10.92	1.34	10.91	1.39	10.91 11.90	1.44	10.90 11.89	1.48	11 12
13 14	12.90 13.90	1.58	12.90 13.89	1.64	12.89 13.88	1.70	12.88 13.87	1.75	12 13 14
15 16	14.89	1.83	14.88 15.87	1.89 2.02	14.87 15.86	1.96 2.09	14.86 15.85	2.02 2.16	15 16
17 18	16.87	2.07 2.19	16.86 17.86	2.15	16.85 17.85	2.22 2.35	16.84 17.84	2.29 2.43	17 18
19 20	18.86	2.32	18.85 19.84	2.27 2.40 2.52	18.84 19.83	2.48 2.61	18.83 19.82	2.56 2.70	19 20
21	20.84 21.84	2.56 2.68	20.83 21.82	2.65 2.78	20.82 21.81	2.74 2.87	20.81 21.80	2.83 2.97	21 22
22 23 24	22.83 23.82	2.80 2.92	22.82 23.81	2.90 3.03	22.80 23.79	3.00 3.13	22.79 23.78	3.10 3.24	23 24
25 26	24.81 25.81	3.05 3.17	24.80 25.79	3.15 3.28	24.79 25.78	3.26 3.39	24.77 25.76	3.37	25 26
27 28	26.80 27.79	3.29 3.41	26.78 27.78	3.41 3.53	26.77 27.76	3.52 3.65	26.75 27.74	3.64 3.78	27
29 30	28.78 29.78	3.53 3.66	28.77 29.76	3.66 3.79	28.75 29.74	3.79 3.92	28.74 29.73	3.91 4.05	28 29 30
31 32	30.77 31.76	3.78 3.90	30.75 31.74	3.91 4.04	30.73 31.73	4.05	$\frac{30.72}{31.71}$	4.18 4.32	31
33 34	32.75	4.02	32.74 33.73	4.16 4.29	32.72 33.71	4.18	32.70	4.45 4.58	32 33
35 36	33.75 34.74 35.73	4.14 4.27 4.39	34.72	4.42	34.70	4.44	33.69 34.68	4.72	34 35
37	36.72 37.72	4.51 4.63	35.71 36.70 37.70	4.54	35.69 36.68	4.70 4.83	35.67 36.66	4.85	36 37
38 39	38.71	4.75	38.69	4.80 4.92	37.67 38.67	4.96 5.09	37.65 38.64	5.12 5.26	38 39
40	$\frac{39.70}{40.70}$	4.87 5.00	$\frac{39.68}{40.67}$	5.05	$\frac{39.66}{40.65}$	$\begin{array}{r r} 5.22 \\ \hline 5.35 \end{array}$	$\frac{39.63}{40.63}$	5.39	40
42 43	41.69 42.68	5.12 5.24	41.66 42.66	5.30 5.43	41.64 42.63	5.48 5.61	41.62 42.61	5.66 5.80	42 43
44 45	43.67 44.67	5.36 5.48	43.65 44.64	5.55 5.68	43.62 44.62	5.74 5.87	43.60 44.59	5.93 6.0°	44 45
46 47	45.66 46.65	5.61 5.73	45.63 46.62	5.81 5.93	45.61 46.60	6.00	45.58 46.57	6.20	46 47
48 49	47.64 48.63	5.85 5.97	47.62 48.61	6.06	47.59 48.58	6.27	47.56 48.55	6.47	48 49
50	49.63	6.09	49.60	6.31	49.57	6.53	49.54 6.74		50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Ö	83	Deg.	82]	Deg.	821	Deg.	821	Deg.	Dist
					 			821 Deg.	

Distance.	71	Deg.	71	Deg.	71/2	Deg.	73 1	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
52 53	51.61 52.60	6.34 6.46	51.58 52.58	6.56 6.69	51.56	6.79 6.92	51.53 52.52	7.01 7.15	52 53
54	53.60	6.58	53.57	6.81	52.55 53.54	7.05	53.51	7.28	54
55	54.59	6.70	54.56	6.94	54.53	7.18	54.50	7.42	- 55
56 57	55.58	6.82	55.55 56.54	7.07 7.19	55.52	7.31	55.49	7.55	56
58	57.57	7.07	57.54	7.19	56.51 57.50	7.44	56.48 57.47	7.69 7.82	57 58
59	58.56	7.19	58.53	7.45	58.50	7.70	58.46	7.96	59
60	59.55	7.31	59.52	7.57	59.49	7.83	59.45	8.09	60
61 62	60.55 61.54	7.43 7.56	60.51	7.70 7.82	60.48	7.96	60.44	8.23	61
63	62.53	7.68	61.50	7.95	61.47 62.46	8.09 8.22	61.43 62.42	8.36 8.50	62 63
64	63.52	7.80	63.49	8.08	63.45	8.35	63.42	8.63	64
65	64.52	7.92 8.04	64.48	8.20	64.44	8.48	64.41	8.77	65
66	65.51	8.04	65.47	8.33 8.46	65.44	8.61 8.75	65.40	8.90 9.04	66 67
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17	68
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	9.30	69
70	69.48	8.53	69.44	8.83	69.40	9.14	69.36	9.44	70
71 72	70.47	8.65 8.77	70.43 71.42	8.96 9.09	70.39	9.27	70.35	9.57	71
73	72.46	8.90	72.42	9.21	71.38	9.40 9.53	72.33	9.71	72 73
74	73.45	9.02	73.41	9.21 9.34	73.37	9,66	73.32	9.98	74
75 76	74.44 75.43	9.14 9.26	74.40 75.39	9.46 9.59	74.36	9.79	74.31	10.11	75
77	76.43	9.38	76.38	9.72	75.35 76.34	9.92 10.05	75.31 76.30	10.25 10.38	76 77
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29	10.52	78
79	78.41 79.40	9.63 9.75	78.37	9.97	78.32	10.31	78.28	10.65	79
80	80.40	$\frac{9.75}{9.87}$	79.36		79.32	10.44	79.27	10.79	80
81 82	81.39	9.99	80.35 81.34	$10.22 \\ 10.35$	80.31 81.30	10.57 10.70	80.26 81.25	10.92 11.06	81 82
83	82.38	10.12	82.34	10.47	82.29	10.83	82.24	11.19	83
84	83.37	10.24	83.33	10.60	83.28	10.96	83.23	11.33	84
85 86	84.37 85.36	10.36 10.48	84.32 85.31	10.73 10.85	84.27 85.26	11.09 11.23	84.22 85.21	11.46 11.60	85 86
87	86.35	10.60	86.30	10.98	86.26	11.36	86.21	11.73	87
88	87.34	10.72	87.30	11.11	87.25	11.49	87.20	11.87	88
89 90	88.34 89.33	10.85 10.97	88.29	11.23 11.36	88.24 89.23	11.62	88.19 89.18	12.00 12.14	89 90
91	90.32	11.09	90.27	$\frac{11.30}{11.48}$	$\frac{69.23}{90.22}$	11.75	$\frac{89.18}{90.17}$	$\frac{12.14}{12.27}$	91
92	91.31 92.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41	92
93	92.31	11.33	92.26	11.74	92.20	12.14	92.15	12.54	93
94 95	93.30 94.29	11.46 11.58	93.25 94.24	$\frac{11.86}{11.99}$	93.20	12.27	93.14 94.13	12.68 12.81	94
96	95.28	11.70	95.23	12.12	94.19 95.18	12.40 12.53	95.12	12.95	95 96
97	96.28	11.82	96.22	12.24	96.17	12.66	96.11	13.08	97
98 99	97.27 98.26	$11.94 \\ 12.07$	97.22 98.21	12.37 12.49	97.16	12.79	97.10 98.10	13.22	98
100	99.25	12.19	99.20	12.49	98.15 99.14	12.92 13.05	99.09	13.35 13.49	99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance	83 1	Deg.	824	Deg.	82 <u>1</u>	Deg.	821	Deg.	Distance.

Dist	7 D	eg.	7 <u>‡</u> [eg.	7 <u>1</u>	Deg.	71	Deg.	Distance.
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
$\overline{1}$	0.99	0.12	0.99	0.13 0.25	0.99	0.13	0.99	0.13	1 2
2 3	2.98	0.24 0.37	2.98	0.38	2.97	0.26 0.39	2.97	0.27 0.40	2 3
4	3.97 4.96	0.49 0.61	3.97 4.96	0.50 0.63	3.97 4.96	0.52 0.65	3.96 4.95	0.54	4 5
5 6	5.96	0.73	5.95	0.76	5.95	0.78	5.95	0.81	6
7 8	6.95 7.94	0.85 0.97	6.94	0.88	6.94 7.93	0.91 1.04	6.94 7.93	0.94 1.08	7 8
9	8.93	1.10	8.93	1.14	8.92	1.17	8.92	1.21	9
10	9.93	1.22	9.92	1.26	9.91	1.31	9.91	$\frac{1.35}{1.48}$	10
11 12	10.92 11.91	1.34	10.91 11.90	1.39	10.91	1.44	10.90 11.89	1.62	11 12
13	12.90	1.58	12.90	1.64	12.89	1.70	12.88	1.75	13
14 15	13.90 14.89	1.71 1.83	13.89 14.88	1.77 1.89	13.88 14.87	1.83	13.87 14.86	1.89 2.02	14 15
16	15.88	1.95	15.87	2.02	15.86	2.09	15.85	2.16	16
17 18	16.87 17.87	2.07 2.19	16.86 17.86	2.15 2.27	16.85 17.85	2.22 2.35	16.84 17.84	2.29 2.43	17 18
19	18.86	2.32	18.85	2.40	18.84	2.48	18.83	2.56	19
$\frac{20}{21}$	$\frac{19.85}{20.84}$	2.44	$\frac{19.84}{20.83}$	$\frac{2.52}{2.65}$	$\frac{19.83}{20.82}$	$\frac{2.61}{2.74}$	$\frac{19.82}{20.81}$	$\frac{2.70}{2.83}$	20 21
22 23	21.84	2.68	21.82	2.78	21.81	2.87	21.80	2.97	22
23 24	22.83 23.82	2.80 2.92	22.82 23.81	2.90 3.03	22.80 23.79	3.00 3.13	22.79 23.78	3.10 3.24	23 24
25	24.81	3.05	24.80	3.15	24.79	3.26	24.77	3.37	25
26 27	25.81 26.80	3.17 3.29	25.79 26.78	3.28 3.41	25.78 26.77	3.39 3.52	25.76 26.75	3.51 3.64	26 27
28	27.79	3.41	27.78	3.53	27.76	3.65	27.74	3.78	28
29 30	28.78 29.78	3.53 3.66	28.77 29.76	3.66 3.79	28.75 29.74	3.79 3.92	28.74 29.73	3.91 4.05	29 30
31	30.77	3.78	30.75	3.91	30.73	4.05	30.72	4.18	31
32	31.76	3.90	31.74	4.04	31.73	4.18	31.71	4.32	32
33 34	32.75 33.75	4.02 4.14	32.74 33.73	4.16 4.29	32.72 33.71	4.31 4.44	32.70 33.69	4.45	33 34
35	34.74	4.27	34.72	4.42	34.70	4.57	34.68	4.72	35
36 37	35.73 36.72	4.39 4.51	35.71 36.70	4.54 4.67	35.69 36.68	4.70	35.67 36.66	4.85	36 37
38	36.72 37.72	4.63	37.70	4.80	37.67	4.96	37.65	5.12	38
39 40	38.71 39.70	4.75 4.87	38.69 39.68	4.92 5.05	38.67 39.66	5.09 5.22	38.64 39.63	5.26 5.39	39 40
41	40.70	5.00	40.67	5.17	40.65	5.35	40.63	5.53	41
42	41.69	5.12	41.66 42.66	5.30	41.64	5.48	41.62	5.66	42
43 44	42.68 43.67	5.24 5.36	43.65	5.43 5.55	42.63 43.62	5.61	42.61 43.60	5.80	43
45	44.67	5.48	44.64	5.68	44.62	5.87	44.59	6.0	45
46 47	45.66	5.61 5.73	45.63 46.62	5.81 5.93	45.61 46.60	6.00	45.58	6.20	46 47
48	47.64	5.85	47.62	6.06	47.59	6.27	47.56	6.47	48
49 50	48.63 49.63	5.97 6.09	48.61 49.60	6.18	48.58 49.57	6.40 6.53	48.55 49.54	6.61 6.74	49 50
nce.	Dep.	Lat.	Dep.	 		- 		Lat.	nce.
Distance.	83	Deg.	82½ Deg.		821	Deg.	821	Deg.	Distance

Dist	7 D	eg.	.74 I	Deg.	$7\frac{1}{2}$ I	Deg.	7¾ I	eg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
52	51.61	6.34	51.58	6.56	51.56	6.79	51.53	7.01	52
53	52.60	6.46	52.58	6.69	52.55	6.92	52.52	7.15	53
54	53.60	6.58	53.57	6.81	53.54	7.05	53.51	7.28	54
55 56	54.59 55.58	6.82	55.55	6.94	54.53 55.52	7.18 7.31	54.50 55.49	7.42	56
57	56.58	6.95	56.54	7.19	56.51	7.44	56.48	7.69	57
58	57.57	7.07	57.54	7.32	57.50	7.57	57.47	7.82	58
59	58.56	7.19	58.53	7.45	58.50	7.57	58.46	7.96	59
60	59.55	7.31	59.52	7.57	59.49	7.83	59.45	8.09	60
61	60.55	7.43	60.51	7.70	60.48	7.96	60.44	8.23	6
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43	8.36	6:
63	62.53	7.68	62.50	7.95	62.46	8.22	62.42	8.50	6:
64	63.52	7.80	63.49	8.08	63.45	8.35	63.42	8.63	64
65	64.52	7.92	64.48	8.20	64.44	8.48	64.41	8.77	6
66	65.51	8.17	65.47	8.33	65.44	8.61	$65.40 \\ 66.39$	9.04	6'
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17	68
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	9.30	6
70	69.48	8.53	69.44	8.83	69.40	9.14	69.36	9.44	7
71	70.47	8.65	70.43	8.96	70.39	9.27	70.35	9.57	7
72	71.46	8.77	71.42	9.09	71.38	9.40	71.34	9.71 9.84	7
73	72.46	8.90	72.42	9.21	72.38	9.53	72.33	9.84	7
74	73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98	7
75	74.44	$9.14 \\ 9.26$	74.40	9.46	74.36	9.79	74.31	10.11	7
76	75.43 76.43	9.38	75.39	$9.59 \\ 9.72$	75.35 76.34	$9.92 \\ 10.05$	75.31 76.30	$10.25 \\ 10.38$	7
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29	10.52	7
79	78.41	9.63	78.37	9.97	78.32	10.31	78.28	10.65	7
80	79.40	9.75	79.36	10.10	79.32	10.44	79.27	10.79	8
81	80.40	9.87	80.35	10.22	80.31	10.57	80.26	10.92	8
82	81.39	9.99	81.34	10.35	81.30	10.70	81.25	11.06	8
83	82.38	10.12	82.34	10.47	82.29	10.83	82.24	11.19	8
84	83.37	10.24	83.33	10.60	83.28	10.96	83.23	11.33	8
85	84.37	10.36	84.32	$10.73 \\ 10.85$	84.27	11.09	84.22 85.21	11.46	8
86 87	86.35	$10.48 \\ 10.60$	85.31	10.98	85.26	11.23 11.36	86.21	11.73	8
88	87.34	10.72	87.30	11.11	87.25	11.49	87.20	11.87	8
89	88.34	10.85	88.29	11.23	88.24	11.62	86.21 87.20 88.19	12.00	8
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14	9
91	90.32	11.09	90.27	11.48	90.22	11.88	90.17	12.27	9
92	91.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41	9
93	92.31	11.33	92.26	11.74	92.20	12.14	92.15	12.54	9
94	93.30	11.46	93.25	11.86	93.20	12.27	93.14 94.13	12.68 12.81	9
95 96	94.29 95.28	11.58 11.70	94.24 95.23	11.99 12.12	94.19	$12.40 \\ 12.53$	95.19	12.95	9
97	96.28	11.82	96.22	12.12	95.18	12.66	95.12 96.11	13.08	9
98	97.27	11.94	97.22	12.37	97.16	12.79	97.10	13.22	9
99	97.27 98.26	12.07	98.21	12.49	98.15	12.92	98.10	13.35	9
100	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	10
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nee
Distance.	83 1	Deg.	823	Deg.	821	Deg.	821	Deg.	Distance.

Distance.	7 D	eg.	7 <u>‡</u> [Deg.	71/2	Deg.	73 1	Deg.	Distance.
500	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
1 2 3 4 5 6 7 8	0.99 1.99 2.98 3.97 4.96 5.96 6.95 7.94 8.93	0.12 0.24 0.37 0.49 0.61 0.73 0.85 0.97	0.99 1.98 2.98 3.97 4.96 5.95 6.94 7.94 8.93	0.13 0.25 0.38 0.50 0.63 0.76 0.88 1.01	0.99 1.98 2.97 3.97 4.96 5.95 6.94 7.93 8.92	0.13 0.26 0.39 0.52 0.65 0.78 0.91 1.04	0.99 1.98 2.97 3.96 4.95 5.95 6.94 7.93 8.92	0.13 0.27 0.40 0.54 0.67 0.81 0.94 1.08	1 2 3 4 5 6 7 8 9
10 11 12 13 14 15 16 17 18 19 20	9.93 10.92 11.91 12.90 13.90 14.89 15.88 16.87 17.87 18.86 19.85 20.84	1.22 1.34 1.46 1.58 1.71 1.83 1.95 2.07 2.19 2.32 2.44 2.56	9.92 10.91 11.90 12.90 13.89 14.88 15.87 16.86 17.86 18.85 19.84 20.83	1.26 1.39 1.51 1.64 1.77 1.89 2.02 2.15 2.27 2.40 2.52 2.65	9.91 10.91 11.90 12.89 13.88 14.87 15.86 16.85 17.85 18.84 19.83	1.31 1.44 1.57 1.70 1.83 1.96 2.09 2.22 2.35 2.48 2.61 2.74	9.91 10.90 11.89 12.88 13.87 14.86 15.85 16.84 17.84 18.83 19.82	1.35 1.48 1.62 1.75 1.89 2.02 2.16 2.29 2.43 2.56 2.70 2.83	10 11 12 13 14 15 16 17 18 19 20
22 23 24 25 26 27 28 29 30	21.84 22.83 23.82 24.81 25.81 26.80 27.79 28.78 29.78	2.68 2.80 2.92 3.05 3.17 3.29 3.41 8.53 3.66	21.82 22.82 23.81 24.80 25.79 26.78 27.78 28.77 29.76	2.78 2.90 3.03 3.15 3.28 3.41 3.53 3.66 3.79	21.81 22.80 23.79 24.79 25.78 26.77 27.76 28.75 29.74	2.87 3.00 3.13 3.26 3.52 3.65 3.79 3.92	21.80 22.79 23.78 24.77 25.76 26.75 27.74 28.74 29.73	2.97 3.10 3.24 3.37 3.51 8.64 3.78 3.91 4.05	22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	30.77 31.76 32.75 33.75 34.74 35.73 36.72 37.72 38.71 39.70	3.78 3.90 4.02 4.14 4.27 4.39 4.51 4.63 4.75	30.75 31.74 32.74 33.73 34.72 35.71 36.70 37.70 38.69 39.68	3.91 4.04 4.16 4.29 4.42 4.54 4.67 4.80 4.92 5.05	30.73 31.73 32.72 33.71 34.70 35.69 36.68 37.67 38.67 39.66	4.05 4.18 4.31 4.44 4.57 4.70 4.83 4.96 5.09 5.22	30.72 31.71 32.70 33.69 34.68 35.67 36.66 37.65 38.64 39.63	4.18 4.32 4.45 4.58 4.72 4.85 4.99 5.12 5.26 5.39	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	40.70 41.69 42.68 43.67 44.67 45.66 46.65 47.64 48.63 49.63	5.00 5.12 5.24 5.36 5.48 5.61 5.73 5.85 5.97 6.09	40.67 41.66 42.66 43.65 44.64 45.63 46.62 47.62 48.61 49.60	5.17 5.30 5.43 5.55 5.68 5.81 5.93 6.06 6.18 6.31	40.65 41.64 42.63 43.62 44.62 45.61 46.60 47.59 48.58 49.57	5.35 5.48 5.61 5.74 5.87 6.00 6.13 6.27 6.40 6.53	40.63 41.62 42.61 43.60 44.59 45.58 46.57 47.56 48.55 49.54	5.53 5.66 5.80 5.93 6.0° 6.20 6.34 6.47 6.61 6.74	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat. Deg.	Dep. 821	Lat. Deg.	Dep.	Lat.	Distance.

Distance	7 D	eg.	71 1	Døg.	71/2	Deg.	7 <u>}</u> I	Deg.	Distance.
mce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52 53 54 55 56 57	50.62 51.61 52.60 53.60 54.59 55.58 56.58	6.22 6.34 6.46 6.58 6.70 6.82 6.95	50.59 51.58 52.58 53.57 54.56 55.55 56.54	6.44 6.56 6.69 6.81 6.94 7.07	50.56 51.56 52.55 53.54 54.53 55.52 56.51	6.66 6.79 6.92 7.05 7.18 7.31 7.44	50.53 51.53 52.52 53.51 54.50 55.49 56.48	6.88 7.01 7.15 7.28 7.42 7.55 7.69	51 52 53 54 55 56 57
58 59 60 61 62	57.57 58.56 59.55 60.55 61.54	6.95 7.07 7.19 7.31 7.43 7.56	57.54 58.53 59.52 60.51 61.50	7.32 7.45 7.57 7.70 7.82	57.50 58.50 59.49 60.48 61.47	7.57 7.70 7.83 7.96 8.09	57.47 58.46 59.45 60.44 61.43	7.82 7.96 8.09 8.23 8.36	58 59 60 61 62
63 64 65 66 67	62.53 63.52 64.52 65.51 66.50	7.68 7.80 7.92 8.04 8.17	62.50 63.49 64.48 65.47 66.46	7.95 8.08 8.20 8.33 8.46	62.46 63.45 64.44 65.44 66.43	8.22 8.35 8.48 8.61 8.75	62.42 63.42 64.41 65.40 66.39	8.50 8.63 8.77 8.90 9.04	63 64 65 66 67
68 69 70 71 72	67.49 68.49 69.48 70.47 71.46	8.29 8.41 8.53 8.65 8.77	67.46 68.45 69.44 70.43 71.42	8.58 8.71 8.83 8.96 9.09	$\begin{array}{r} 67.42 \\ 68.41 \\ 69.40 \\ \hline 70.39 \\ 71.38 \end{array}$	8.88 9.01 9.14 9.27 9.40	67.38 68.37 69.36 70.35 71.34	9.17 9.30 9.44 9.57 9.71	68 69 70 71 72
73 74 75 76 77	72.46 73.45 74.44 75.43 76.43	8.90 9.02 9.14 9.26 9.38	72.42 73.41 74.40 75.39 76.38	9.21 9.34 9.46 9.59 9.72	72.38 73.37 74.36 75.35 76.34	9.53 9.66 9.79 9.92 10.05	72.33 73.32 74.31 75.31 76.30	9.84 9.98 10.11 10.25 10.38	73 74 75 76 77
78 79 80 81 82 83	77.42 78.41 79.40 80.40 81.39 82.38	9.51 9.63 9.75 9.87 9.99 10.12	77.38 78.37 79.36 80.35 81.34 82.34	9.84 9.97 10.10 10.22 10.35 10.47	77.33 78.32 79.32 80.31 81.30 82.29	10.18 10.31 10.44 10.57 10.70 10.83	77.29 78.28 79.27 80.26 81.25 82.24	10.52 10.65 10.79 10.92 11.06 11.19	78 79 80 81 82 83
84 85 86 87 88	83.37 84.37 85.36 86.35 87.34	10.24 10.36 10.48 10.60 10.72	83.33 84.32 85.31 86.30 87.30	10.60 10.73 10.85 10.98	83.28 84.27 85.26 86.26 87.25 88.24	10.96 11.09 11.23 11.36 11.49	83.23 84.22 85.21 86.21 87.20	11.33 11.46 11.60 11.73 11.87	84 85 86 87 88
90 91 92 93	88.34 89.33 90.32 91.31 92.31	10.85 10.97 11.09 11.21 11.33	88.29 89.28 90.27 91.26 92.26	11.23 11.36 11.48 11.61 11.74	$\begin{array}{r} 89.23 \\ \hline 90.22 \\ 91.21 \\ 92.20 \\ \end{array}$	11.62 11.75 11.88 12.01 12.14	88.19 89.18 90.17 91.16 92.15	12.00 12.14 12.27 12.41 12.54	90 91 92 93
94 95 96 97 98 99	93.30 94.29 95.28 96.28 97.27 98.26	11.46 11.58 11.70 11.82 11.94 12.07	93.25 94.24 95.23 96.22 97.22 98.21	11.86 11.99 12.12 12.24 12.37 12.49	93.20 94.19 95.18 96.17 97.16 98.15	12.27 12.40 12.53 12.66 12.79 12.92	93.14 94.13 95.12 96.11 97.10 98.10	12.68 12.81 12.95 13.08 13.22 13.35	94 95 96 97 98 99
100	99.25 Dep.	12.19 Lat.	99.20 Dep.	12.62 Lat.	99.14 Dep.	13.05 Lat.	99.09 Dep.	13.49 Lat.	100
Distance.		Deg.		Deg.	<u>-</u> -	Deg.	821	Deg.	Distance.

Die	7 D	eg.	7 <u>1</u> T	eg.	7 <u>1</u>]	Deg.	73 1	Deg.	Distance
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2	0.99	0.12 0.24	0.99 1.98	0.13 0.25	0.99	0.13 0.26	0.99	0.13 0.27	1 2
3 4 5 6	2.98 3.97	0.37 0.49	2.98 3.97	0.38	2.97 3.97	0.39 0.52	2.97 3.96	0.40 0.54	3 4
5	4.96	0.61	4.96	0.63	4.96	0.65	4.95	0.67	5
6	5.96 6.95	0.73 0.85	5.95 6.94	0.76 0.88	5.95 6.94	0.78 0.91	5.95 6.94	0.81 0.94	6 7
8 9	7.94 8.93	0.97 1.10	7.94 8.93	1.01	7.93 8.92	1.04	7.93 8.92	1.08	8
10	9.93	1.10	9.92	1.26	9.91	1.31	9.91	1.35	10
11	10.92 11.91	1.34	10.91 11.90	1.39	10.91 11.90	1.44	10.90 11.89	1.48	11
12 13	12.90	1.58	12.90	1.64	12.89	1.70	12.88	1.75	12 13
14 15	13.90 14.89	1.71	13.89 14.88	1.77	13.88 14.87	1.83	13.87 14.86	1.89 2.02	14 15
16 17	15.88 16.87	1.95 2.07	15.87 16.86	2.02 2.15	15.86 16.85	2.09 2.22	15.85 16.84	2.16 2.29	16 17
18	17.87	2.19	17.86	2.27 2.40	17.85	2.35	17.84	2.43	18
19 20	18.86	2.32 2.44	18.85 19.84	2.40 2.52	18.84 19.83	2.48 2.61	18.83 19.82	2.56 2.70	19 20
21	20.84	2.56	20.83	2.65	20.82	2.74	20.81	2.83	21
22 23	21.84 22.83	2.68 2.80	21.82 22.82	2.78 2.90	$ 21.81 \\ 22.80$	2.87 3.00	21.80 22.79	2.97 3.10	22 23
24 25	23.82 24.81	2.92 3.05	23.81 24.80	3.03 3.15	23.79 24.79	3.13 3.26	23.78 24.77	3.24	24 25
26 27	25.81 26.80	3.17 3.29	25.79 26.78	3.28 3.41	25.78 26.77	3.39 3.52	25.76 26.75	3.51 3.64	26
28	27.79	3.41	27.78	3.53	27.76	3.65	27.74	3.78	27 28
29 30	28.78 29.78	3.53 3.66	28.77 29.76	3.66 3.79	28.75 29.74	3.79 3.92	28.74	3.91 4.05	29 30
31	30.77	3.78	30.75	3.91	30.73	4.05	30.72	4.18	31
32 33	31.76 32.75	8.90 4.02	31.74 32.74	4.04 4.16	31.73 32.72	4.18 4.31	31.71 32.70	4.32 4.45	32 33
34 35	33.75 34.74	4.14 4.27	33.73 34.72	4.29	32.72 33.71 34.70	4.44	33.69 34.68	4.58	34 35
36	95 73	4.39	35.71	4.54	35.69	4.70	35.67	4.85	36
37 38	36.72 37.72	4.51 4.63	36.70 37.70	4.67 4.80	36.68 37.67	4.83	36.66 37.65	4.99 5.12	37 38
39 40	38.71 39.70	4.75 4.87	38.69 39.68	4.92 5.05	38.67 39.66	5.09 5.22	38.64 39.63	5.26 5.39	39 40
41	40.70	5.00	40.67	5.17	40.65	5.35	40.63	5.53	41
42 43	41.69 42.68	5.12 5.24	41.66	5.30 5.43	41.64 42.63	5.48 5.61	41.62 42.61	5.66 5.80	42 43
44	43.67	5.36 5.48	43.65 44.64	5.55 5.68	43.62 44.62	5.74 5.87	43.60 44.59	5.93	44
45 46	45.66	5.61	45.63	5.81	45.61	6.00	45.58	6.20	46
47 48	46.65	5.73 5.85	46.62	5.93 6.06	46.60 47.59	6.13	46.57 47.56	6.34	47 48
49 50	48.63 49.63	5.97 6.09	48.61 49.60	6.18	48.58 49.57	6.40	48.55 49.54	6.61	49 50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	1
Distance.	83	Deg.	82]	Deg.	821	Deg.	821	Deg.	Distance

Dist	7 D	eg.	.74 I	Deg.	$7\frac{1}{2}$ I	Deg.	73 I	eg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
52	51.61	6.34	51.58	6.56	51.56	6.79	51.53	7.01	52
53	52.60	6.46	52.58	6.69	52.55	6.92	52.52	7.15	53
54	53.60	6.58	53.57	6.81	53.54	7.05	53.51	7.28	54
55	54.59	6.70	54.56	6.94	54.53	7.18	54.50	7.42	55
56	55.58	6.82	55.55	7.07	55.52	7.31	55.49	7.55	56
57	56.58	6.95	56.54	7.19	56.51	7.44 7.57	56.48	7.69	57
58	57.57	7.07	57.54	7.32	57.50	7.57	57.47	7.82	58
59 60	58.56 59.55	7.19	58.53 59.52	7.45	$58.50 \\ 59.49$	7.70	58.46 59.45	7.96	59 60
61	60.55	7.43	60.51	7.70	60.48	7.96	60.44	8.23	61
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43	8.36	62
63	62.53	7.68	62.50	7.95	62.46	8.22	62.42	8.50	63
64	63.52	7.80	63.49	8.08	63.45	8.35	63.42	8.63	64
65	64.52	7.92	64.48	8.20	64.44	8.48	64.41	8.77	65
66	65.51	8.04	65.47	8.33	65.44	8.61	65.40 66.39	8.90	66
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39	9.04	67
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17	68
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	9.30	69
70	69.48	8.53	69.44	8.83	69.40	9.14	69.36	9.44	70
71 72	70.47	8.65 8.77	70.43	8.96 9.09	70.39 71.38	$9.27 \\ 9.40$	$70.35 \\ 71.34$	9.57	7:
73	72.46	8.90	72.42	9.21	72.38	9.53	72,33	9.84	7
74	73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98	7
75	74.44	9.14	74.40	9.46	74.36	9.79	74.31	10.11	7
76	75.43	9.26	75.39	9.59	75.35	9.92	75.31	10.25	70
77	76.43	9.38	76.38	9.72	76.34	10.05	76,30	10.38	7
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29 78.28	10.52	78
79	78.41	9.63	78.37	9.97	78.32	10.31	78.28	10.65	7
80	79.40	9.75	79.36	10.10	79.32	10.44	79.27	10.79	8
81	80.40	9.87	80.35	$\frac{10.22}{10.35}$	80.31	10.57	80.26 81.25	$10.92 \\ 11.06$	8
82	81.39 82.38	$9.99 \\ 10.12$	82.34	10.33	81.30	$10.70 \\ 10.83$	89 94	11.19	8
83	83.37	10.12	83.33	10.60	82.29	10.83	82.24 83.23	11.33	8
85	84.37	10.36	84.32	10.73	84.27	11.09	84.22	11.46	8
86	85.36	10.48	85.31	10.85	85.26	11.23	85.21	11.60	8
87	86.35	10.60	86.30	10.98	86.26	11.36	86.21	11.73	8
88		10.72	87.30	11.11	87.25	11.49	87.20	11.87	8
89	87.34 88.34	10.85	88.29	11.23	88.24	11.62	88.19	12.00	8
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14	9
91	90.32	11.09	90.27	11.48	90.22	11.88	90.17	12.27	9
92	91.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41	9
93	92.31	11.33	92.26	11.74	92.20	12.14	92.15 93.14	12.54 12.68	9
94	93.30 94.29	11.46	93.25 94.24	11.86	93.20	12.27 12.40	94.13	12.81	9
95 96	95.28	11.58 11.70	95.23	12.12	94.19 95.18	12.40	95.12	12.95	9
97	96 28	11.82	96.22	12.24	96.17	12.66	96.11	13.08	9
98	96.28 97.27	11.94	96.22 97.22	12.37	97.16	12.79	97.10	13.22	9
99	98.26	12.07	98.21	12.49	98.15	12.92	97.10 98.10	13.35	9
100	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	10
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	83	Deg.	823	Deg.	821	Deg.	821	Deg.	Distance.

Dist	. 8 I	Deg.	8 <u>1</u> I)eg.	8 1 I	Deg.	8 1	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7	0.99 1.98 2.97 3.96 4.95 5.94 6.93	0.14 0.28 0.42 0.56 0.70 0.84 0.97	0.99 1.98 2.97 3.96 4.95 5.94 6.93	0.14 0.29 0.43 0.57 0.72 0.86 1.00	0.99 1.98 2.97 3.96 4.95 5.93 6.92	0.15 0.30 0.44 0.59 0.74 0.89 1.03	0.99 1.98 2.97 3.95 4.94 5.93 6.92	0.15 0.30 0.46 0.61 0.76 0.91	1 2 3 4 5 6
8 9 10	7.92 8.91 9.90	1.11 1.25 1.39	7.92 8.91 9.90	1.15 1.29 1.43	7.91 8.90 9.89	1.18 1.33 1.48	7.91 8.90 9.88	1.22 1.37 1.52	8 9 10
11 12 13 14 15 16 17 18	10.89 11.88 12.87 13.86 14.85 15.84 16.83 17.82	1.53 1.67 1.81 1.95 2.09 2.23 2.37 2.51	10.89 11.88 12.87 13.86 14.85 15.84 16.83	1.58 1.72 1.87 2.01 2.15 2.30 2.44 2.58	10.88 11.87 12.86 13.85 14.84 15.82 16.81	1.63 1.77 1.92 2.07 2.22 2.36 2.51 2.66	10.87 11.86 12.85 13.84 14.83 15.81 16.80 17.79	1.67 1.83 1.98 2.13 2.28 2.43 2.59 2.74	11 12 13 14 15 16 17
19 20 21 22 23 24	18.82 19.81 20.80 21.79 22.78 23.77	2.64 2.78 2.92 3.06 3.20 3.34	18.80 19.79 20.78 21.77 22.76 23.75	2.73 2.87 3.01 3.16 3.30 3.44	$ \begin{array}{r} 18.79 \\ 19.78 \\ \hline 20.77 \\ 21.76 \\ 22.75 \\ 23.74 \end{array} $	2.81 2.96 3.10 3.25 3.40 3.55	18.78 19.77 20.76 21.74 22.73 23.72	3.04 3.19 3.35 3.50 3.65	19 20 21 22 23 24
25 26 27 28 29 30	24.76 25.75 26.74 27.73 28.72 29.71	3.48 3.62 3.76 3.90 4.04 4.18	24.74 25.73 26.72 27.71 28.70 29.69	3.59 3.73 3.87 4.02 4.16 4.30	24.73 25.71 26.70 27.69 28.68 29.67	3.70 3.84 3.99 4.14 4.29 4.43	24.71 25.70 26.69 27.67 28.66 29.65	3.80 3.96 4.11 4.26 4.41 4.56	25 26 27 28 29 30
31 32 33 34 35 36- 37 38	30.70 31.69 32.68 33.67 34.66 35.65 36.64 37.63	4.31 4.45 4.59 4.73 4.87 5.01 5.15 5.29	30.68 31.67 32.66 33.65 34.64 35.63 36.62 37.61	4.45 4.59 4.74 4.88 5.02 5.17 5.31 5.45	30.66 31.65 32.64 33.63 34.62 35.60 36.59 37.58	4.58 4.73 4.88 5.03 5.17 5.32 5.47 5.62	30.64 31.63 32.62 33.60 34.59 35.58 36.57 37.56	4.72 4.87 5.02 5.17 5.32 5.48 5.63 5.78	31 32 33 34 35 36 37 38
39 40 41 42 43	38.62 39.61 40.60 41.59 42.58	5.43 5.57 5.71 5.85 5.98	38.60 39.59 40.58 41.57 42.56	5.60 5.74 5.88 6.03 6.17	38.57 39.56 40.55 41.54 42.53	5.76 5.91 6.06 6.21 6.36	38.55 39.53 40.52 41.51 42.50	5.93 6.08 6.24 6.39 6.54	39 40 41 42 43
44 45 46 47 48	43.57 44.56 45.55 46.54 47.53	6.12 6.26 6.40 6.54 6.68	43.54 44.53 45.52 46.51 47.50	6.31 6.46 6.60 6.74 6.89	43.52 44.51 45.49 46.48 47.47	6.50 6.65 6.80 6.95 7.09	43.49 44.48 45.46 46.45 47.44	6.69 6.85 7.00 7.15 7.30	44 45 46 47 48
50 50	48.52 49.51	6.82	48.49	7.03	48.46 49.45	7.24	48.43 49.42	7.45	49 50
Distance	Вер. 82 1	Lat. Deg.	Dep.	Lat. Deg.	81½	Lat. Deg.	Dep.	Lat.	Distance.

TRAVERSE TABLE.

Dist	8 I	eg.	81	Deg.	81 I	Deg.	83 1	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	50.50	7.10	50.47	7.32	50.44	7.54	50.41	7.76	51
52	51.49	7.24 7.38	51.46	7.46	51.43	7.69	51.39	7.91	52
53	52.48	7.38	52.45	7.61	52.42	7.83	52.38	8.06	53
54	53.47	7.52	53.44	7.75	53.41	7.98	53.37	8.21	54
55	54.46	7.65 7.79	54.43	7.89	54.40	8.13	54.36	8.37	55
56	55.46 56.45	7.79	55.42	8.04	55.38	8.28	55.35	8.52	56
58	57.44	8.07	57.40	8.32	56.37	8.57	56.34 57.32	8.67	57 58
59	58.43	8.21	58.39	8.47	58.35	8.72	58.31	8.98	59
60	59.42	8.35	59.38	8.61	59.34	8.87	59.30	9.13	60
61	60.41	8.49	60.37	8.75	60.33	9.02	60.29	9.28	61
62	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43	62
63	62.39	8.77	62.35	9.04	62.31	9.31	62.27	9.58	63
64	63.38	8.91	63.34	9.18	63.30	9.46	63.26	9.74	64
65	64.37	9.05	64.33	9.33	64.29	9.61	64.24	9.89	65
66	65.36	9.19	65.32	9.47	65.28	9.76	65.23	10.04	66
67	66.35 67.34	9.32	66.31	9.61	66.26	9.90	66.22	10.19 10.34	67
68		9.46	67.30	9.76	67.25	10.05	67.21	10.34	68
69 70	68.33	$9.60 \\ 9.74$	68.29	9.90	68.24	10.20	68.20	10.50	69 70
_	69.32	-		10.04	69.23	10.35	69.19	10.65	11 44 54 55
71	70.31	9.88	70.27	10.19	70.22	10.49	70.17	10.80	71
72 73	71.30 72.29	10.02	71.25	10.33	71.21	10.64	71.16	10.95 11.10	72
74	73.28	$10.16 \\ 10.30$	73.23	10.47 10.62	72.20	$10.79 \\ 10.94$	72.15	11.26	74
75	74.27	10.44	74.22	10.76	74.18	11.09	74.13	11.41	75
76	75.26	10.58	75.21	10.91	75.17	11.23	75.12	11.56	76
77	76.25	10.72	76.20	11.05	76.15	11.38	76.10	11.71	77
78	77.24 78.23	10.86	77.19	11.19	77.14	11.53	77.09	11.87	78
79	78.23	10.99	78.18	11.34	78.13	11.68	78.08	12.02	79
80	79.22	11.13	79.17	11.48	79.12	11.82	79.07	12.17	80
81	80.21	11.27	80.16	11.62	80.11	11.97	80.06	12.32	81
82	81.20	11.41	81.15	11.77	81.10	12.12	81.05	12.47	82
83	82.19	11.55	82.14	11.91	82.09	12.27	82.03	12.63	83
84	83.18	11.69	83.13	12.05	83.08	12.42	83.02	12.78 12.93	84
86	84.17	$11.83 \\ 11.97$	84.12 85.11	$12.20 \\ 12.34$	84.07	12.56	84.01	13.08	86
87	86.15	12.11,	86.10	12.48	86.04	12.86	85.99	13.23	87
88	87.14	12.25	87.09	12.63	87.03	13.01	86.98	13.39	88
89	88.13	12.39	88.08	12.77	88.02	13.16	87.96	13.54	89
90	89.12	12.53	89.07	12.91	89.01	13.30	88.95	13.69	90
31	90.11	12.66	90.06	13.06	90.00	13.45	89.94	13.84	91
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14.00	92
93	92.09	12.94	92.04	13.34	91.98	13.75	91.92	14.15	98
94	93.09	13.08	93.03	13.49	92.97	13.89	92.91	14.30	94
95	94.08	13.22	94.02	13.63	93.96	14.04	93.89	14.45	95
$-\frac{96}{97}$	95.07	13.36	95.01	13.78	94.95	14.19	94.88	14.60 14.76	96
98	97.05	$13.50 \\ 13.64$	96.00	$13.92 \\ 14.06$	95.93 96.92	14.34 14.49	96.86	14.91	98
99	97.05 98.04	13.78	97.98	14.21	97.91	14.63	97.85	15.06	99
100	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	82]	Deg.	813	Deg.	8112	Deg.	811	Deg.	Distance.

Dist	9 D	eg.	9 <u>†</u> I	eg.	9 <u>1</u>]	Deg	9∄]	Deg.]	Distance.
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1	0.99	0.16	0.99	0.16	0.99	0.17	0.99	0.17	1
2	1.98	0.31	1.97	0.32	1.97	0.33	1.97	0.34	2
3	2.96	0.47	2.96	0.48	2.96	0.50	2.96	0.51	3
4	3.95	0.63	3.95	0.64	3.95	0.66	3.94	0.68	4
5	4.94	0.78	4.93	0.80	4.93	0.83	4.93	0.85	5
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02	6
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90	1.19	7
8	7.90	1.25	7.90	1.29	7.89	1.32	7.88	1.35	8
9	8.89	1.41	8.88	1.45	8.88	1.49	8.87	1.52	9
10 11 12	$\frac{9.88}{10.86}$	$\frac{1.56}{1.72} \\ 1.88$	$\frac{9.87}{10.86}$ 11.84	$\frac{1.61}{1.77}$ 1.93	9.86 10.85 11.84	$\frac{1.65}{1.82}$ 1.98	9.86 10.84 11.83	1.69 1.86 2.03	10 11 12
13	12.84	2.03	12.83	2.09	12.82	2.15	12.81	2.20	13
14	13.83	2.19	13.82	2.25	13.81	2.31	13.80	2.37	14
15	14.82	2.85	14.80	2.41	14.79	2.48	14.78	2.54	15
16	15.80	2.50	15.79	2.57	15.78	2.64	15.77	2.71	16
17	16.79	2.66	16.78	2.73	16.77	2.81	16.75	2.88	17
18	17.78	2.82	17.77	2.89	17.75	2.97	17.74	3.05	18
19 20 21	18.77 19.75 20.74	$\frac{2.97}{3.13}$	$\frac{18.75}{19.74}$ 20.73	$\frac{3.05}{3.21}$	$\frac{18.74}{19.73}$ 20.71	$\frac{3.14}{3.30}$	$\frac{18.73}{19.71}$ 20.70	$\frac{3.22}{3.39}$	19 20 21
22	21.73	3.44	21.71	3.54	21.70	3.63	21.68	3.73	22
23	22.72	3.60	22.70	3.70	22.68	3.80	22.67	3.90	23
24	23.70	3.75	23.69	3.86	23.67	3.96	23.65	4.06	24
25	24.69	3.91	24.67	4.02	24.66	4.13	24.64	4.23	25
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40	26
27	26.67	4.22	26.65	4.34	26.63	4.46	26.61	4.57	27
28	27.66	4.38	27.64	4.50	27.62	4.62	27.60	4.74	28
29	28.64	4.54	28.62	4.66	28.60	4.79	28.58	4.91	29
30	29.63	4.69	29.61	4.82	29.59	4.95	29.57	5.08	30
31	30.62	4.85	30.60	4.98	30.57	5.12	30.55	5.25	31
32	31.61	5.01	31.58	5.14	31.56	5.28	31.54	5.42	32
33	32.59	5.16	32.57	5.30	32.55	5.45	32.52	5.59	33
34	33.58	5.32	33.56	5.47	33.53	5.61	33.51	5.76	34
35	34.57	5.48	34.54	5.63	34.52	5.78	34.49	5.93	35
36	35.56	5.63	35.53	5.79	35.51	5.94	35.48	6.10	36
37 38 39	36.54 37.53 38.52	5.79 5.94 6.10	36.52 37.51 38.49	5.95 6.11 6.27	36.49 37.48 38.47	6.11 6.27 6.44 6.60	36.47 37.45 38.44 39.42	6.27 6.44 6.60 6.77	37 38 39 40
40 41 42	39.51 40.50 41.48	6.26 6.41 6.57	39.48 40.47 41.45	6.43 6.59 6.75	39.45 40.44 41.42	6.77	40.41 41.39	6.94	41 42
43 44 45	42.47 43.46 44.45	6.73 6.88 7.04 7.20	42.44 43.43 44.41	6.91 7.07 7.23 7.39	42.41 43.40 44.38	7.10 7.26 7.43 7.59	42.38 43.36 44.35 45.34	7.28 7.45 7.62 7.79	43 44 45 46
46 47 48 49	45.43 46.42 47.41 48.40	7.20 7.35 7.51 7.67	45.40 46.39 47.38 48.36	7.55 7.72 7.88	45.37 46.36 47.34 48.33	7.76 7.76 7.92 8.09	46.32 47.31 48.29	7.96 8.13 8.30	47 48 49
50	49.38 Dep.	7.82 Lat.	49.35 Dep.	8.04 Lat.	49.32 Dep.	8.25 Lat.	49.28 Dep.	8.47 Lat.	, 50
Distance,		Deg.	80}	Deg.		Deg.	<u> </u>	Deg.	Distance,

Distance.	1 [9]	Deg.	91	Deg.	91	Deg.	91 1	Deg.	Distance.
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dop.	ince.
51 52 53 54 55	50.37 51.36 52.35 53.34 54.32	7.98 8.13 8.29 8.45 8.60	50.34 51.32 52.31 53.30 54.28	8.20 8.36 8.52 8.68 8.84	50.30 51.29 52.27 53.26 54.25	8.42 8.58 8.75 8.91 9.08	50.26 51.25 52.23 53.22 54.21	8.64 8.81 8.98 9.14 9.31	51 52 53 54 55
56 57 58 59 60	55.31 56.30 57.29 58.27 59.26	8.76 8.92 9.07 9.23 9.39	55.27 56.26 57.25 58.23 59.22	9.00 9.16 9.32 9.48 9.64	55.23 56.22 57.20 58.19 59.18	9.24 9.41 9.57 9.74 9.90	55.19 56.18 57.16 58.15 59.13	9.48 9.65 9.82 9.99 10.16	56 57 58 59 60
61 62 63 64 65	60.25 61.24 62.22 63.21 64.20	9.54 9.70 9.86 10.01 10.17	60.21 61.19 62.18 63.17 64.15	9.81 9.97 10.13 10.29 10.45	60.16 61.15 62.14 63.12 64.11	10.07 10.23 10.40 10.56 10.73	60.12 61.10 62.09 63.08 64.06	10.33 10.50 10.67 10.84 11.01	61 62 63 64 65
66 68 69 70	65.19 66.18 67.16 68.15 69.14	10.32 10.48 10.64 10.79 10.95	65.14 66.13 67.12 68.10 69.09	10.61 10.77 10.93 11.09 11.25	65.09 66.08 67.07 68.05 69.04	10.89 11.06 11.22 11.39 -11.55	65.05 66.03 67.02 68.00 68.99	11.18 11.85 11.52 11.69 11.85	66 67 68 69 70
71 72 73 74 75 76	70.13 71.11 72.10 73.09 74.08 75.06	11.11 11.26 11.42 11.58 11.73 11.89	70.08 71.06 72.05 73.04 74.02 75.01	11.41 11.57 11.73 11.89 12.06 12.22	70.03 71.01 72.00 72.99 73.97 74.96	11.72 11.88 12.05 12.21 12.38 12.54	69.97 70.96 71.95 72.93 73.92 74.90	12.02 12.19 12.36 12.53 12.70 12.87	71 72 73 74 75 76
77 78 79 80 81	76.05 77.04 78.03 79.02 80.00	12.05 12.20 12.36 12.51	76.00 76.99 77.97 78.96	12.38 12.54 12.70 12.86 13.02	75.94 76.93 77.92 78.90	12.71 12.87 13.04 13.20	75.89 76.87 77.86 78.84 79.83	13.04 13.21 13.38 13.55	77 78 79 80 81
82 83 84 85 86	80.99 81.98 82.97 83.95 84.94	12.83 12.98 13.14 13.30 13.45	80.93 81.92 82.91 83.89 84.88	13.18 13.34 13.50 13.66 13.82	80.88 81.86 82.85 83.83 84.82	13.53 13.70 13.86 14.03 14.19	80.82 81.80 82.79 83.77 84.76	13.89 14.06 14.23 14.39 14.56	82 83 84 85 86
87 88 89 90 91	85.93 86.92 87.90 88.89	13.61 13.77 13.92 14.08	85.87 86.86 87.84 88.83	13.98 14.15 14.31 14.47	85.81 86.79 87.78 88.77	14.36 14.52 14.69 14.85	85.74 86.73 87.71 88.70	14.73 14.90 15.07 15.24	87 88 89 90
92 93 94 95 96	90.87 91.86 92.84 93.83 94.82	14.39 14.55 14.70 14.86 15.02	90.80 91.79 92.78 93.76 94.75	14.79 14.95 15.11 15.27 15.43	90.74 91.72 92.71 93.70 94.68	15.18 15.35 15.51 15.68 15.84	90.67 91.66 92.64 93.63 94.61	15.58 15.75 15.92 16.09 16.26	92 93 94 95 96
97 98 99 100	95.81 96.79 97.78 98.77 Dep.	15.17 15.33 15.49 15.64 Lat.	95.74 96.73 97.71 98.70	15.59 15.75 15.91 16.07	95.67 96.66 97.64 98.63	16.01 16.17 16.84 16.50	95.60 96.58 97.57 98.56 Dep.	16.43 16.60 16.77 16.93	97 98 99 100
Distance.	81 I	<u> </u>	Dep. Lat.		80½		80½ Deg.		Distance

Distance.	10 1	Dèg.	101	Deg.	10}	Deg.	101	Deg	Distance.
noe.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1	0.98 1.97	0.17 0.35	0.98 1.97	0.18 0.36	0.98 1.97	0.18 0.36	0.98	0.19	1 2
2 8 4	2.95	0.52	2.95	0.53	2.95	0.55	2.95	0.56	3
5	3.94 4.92	0.69 0.87	3.94 4.92	0.89	3.93 4.92	0.73 0.91	3.93 4.91	.0.75 0.93	4 5
5 6 7	5.91 6.89	1.04	5.90 6.89	1.07 1.25	5.90 6.88	1.09 1.28	5.89 6.88	1.12	5 6 7
8	7.88	1.30	7.87	1.42	7.87	1.46	7.86	1.49	8
10	8.86 9.85	1.56 1.74	8.86 9.84	1.60 1.78	8.85 9.83	1.64 1.82	8.84 9.82	1.68	10 10
11 12	10.83 11.82	1.91 2.08	10.82	1.96 2.14	10.82	2.00 2.19	10.81	2.05 2.24	11 12
13	12.80	2.26	12.79	2.31	12.78	2.37	12.77	2.42	13
14 15	18.79 14.77	2.43 2.60	13.78 14.76	2.49 2.67	13.77 14.75	2.55 2.73	13.75 14.74	2.61 2.80	14 15
16 17	15.76 16.74	2.78 2.95	15.74 16.73	2.85 3.03	15.73	2.92 3.10	15.72 16.70	2.98 3.17	16
18	17.73	3.13	17.71	3.20	16.72 17.70	3.28	17.68	3.36	17 18
19 20	18.71 19.70	3.30 3.47	18.70 19.68	3.38 3.56	18.68 19.67	3.46 3.64	18.67 19.65	3.54 3.73	19 20
21 22	20.68 21.67	3.65 3.82	20.66 21.65	3.74 3.91	20.65 21.63	3.83 4.01	20.63 21.61	3.92 4.10	21
23	22.65	3.99	22.63	4.09	22.61	4.19	22.60	4.29	22 23
24 25	23.64 24.62	4.17 4.34	23.62 24.60	4.27	23.60 24.58	4.37	23.58 24.56	4.48 4.66	24 25
26	25.61	4.51	25.59	4.63	25.56	4.74	25.54	4.85	26
27 28	26.59 27.57	4.69 4.86	26.57 27.55	4.80 4.98	26.55 27.53	4.92 5.10	26.53 27.51	5.04 5.22	27 28
29 30	28.56 29.54	5.04 5.21	28.54 29.52	5.16 5.34	28.51 29.50	5.28 5.47	28.49 29.47	5.41 5.60	29 30
31	30.53	5.38	30.51	5.52	30.48	5.65	30.46	5.78	31
32 33	31.51 32.50	5.56 5.73	31.49 32.47	5.69 5.87	31.46 32.45	5.83 6.01	31.44 32.42	5.97 6.16	32 33
34 35	33.48 34.47	5.90 6.08	33.46	6.05	33.43	6.20	33.40	6.34	34
36	35.45	6.25	34.44 35.43	6.23 6.41	34.41 35.40	6.38 6.56	34.39 35.37	6.53 6.71	35 36
37 38	36.44 37.42	6.42	36.41 37.39	6.58	36.38 37.36	6.74	36.35 37.33	6.90 7.09	37 38
39	38.41	6.77	38.38	6.94	38.35	7.11	38.32	7.27	39
40	$\frac{39.39}{40.38}$	$\frac{6.95}{7.12}$	$\frac{39.36}{40.35}$	$\frac{7.12}{7.30}$	$\frac{39.33}{40.31}$	$\frac{7.29}{7.47}$	39.30 40.28	$\frac{7.46}{7.65}$	40
42	41.36	7.29	41.33	7.47	41.30	7.65	41.26	7.88 8.02	41 42
43 44	42.35 43.33	7.47 7.64	42.31 43.30	7.65 7.83	42.28 43.26	7.84 8.02	42.25 43.23	8.02 8.21	43 44
45	44.32	7.81	44.28	8.01	44.25	8.20	44.21	8.39	45
46 47	45.30 46.29	7.99 8.16	45.27 46.25	8.19 8.36	45.23 46.21	8.38 8.57	45.19 46.18	8.58 8.77	46 47
48 49	47.27	8.34 8.51	47.23 48.22	8.54 8.72	47.20 48.18	8.75 8.93	47.16	8.95 9.14	48 49
50	49.24	8.68	49.20	8.90	49.16	9.11	49.12	9.33	50
Distance	Dep.	Lat.	Dep. Lat.		Dep.	Lat.	Dep.	Lat.	ince.
Dist	80 1	Deg.	793	Deg.	79 <u>1</u>	Deg.	791	Deg.	Distance.

51 50.23 8.86 50.19 9.08 50.15 9.29 50.10 9.51 52 51.21 9.03 51.17 9.25 51.13 9.48 51.09 9.70 53 52.19 9.20 52.15 9.43 52.11 9.66 52.07 9.89 54 53.18 9.38 53.14 9.61 53.10 9.84 53.05 10.07 55 54.16 9.55 54.12 9.79 54.08 10.02 54.03 10.26 56 55.15 9.72 55.11 9.96 56.00 10.21 55.02 10.22 55.06 10.21 55.02 10.26 56.09 10.22 57.03 10.27 56.00 10.63 58.01 10.75 56.98 10.82 59.80 10.23 57.96 11.00 60.59 10.42 59.04 10.68 59.00 10.93 58.95 11.19 61 60.07 10.59 60.03 10.82	Distance.	10	Deg.	101	Deg.	101	Deg.	103	Deg.	PIST
52 51.21 9.03 51.17 9.25 51.13 9.48 51.09 9.70 53 52.19 9.20 52.15 9.43 52.11 9.66 52.07 9.89 54 53.18 9.38 53.14 9.61 53.10 9.84 53.05 10.07 55 54.16 9.55 54.12 9.79 54.08 10.02 54.03 10.26 56 55.15 9.72 55.11 9.96 55.06 10.39 56.00 10.45 57 56.13 9.90 56.09 10.12 56.05 10.39 56.00 10.65 58 57.12 10.07 57.07 10.32 57.03 10.57 56.98 10.82 60 59.09 10.42 59.04 10.68 59.00 10.93 58.95 11.00 61 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.38 62.61.06 10.77 61	ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Taranco
52 51.21 9.03 51.17 9.25 51.13 9.48 51.09 9.70 54 53.18 9.38 53.14 9.61 53.10 9.84 53.05 10.07 55 54.16 9.55 54.12 9.79 54.08 10.02 54.03 10.26 56 55.15 9.72 55.11 9.96 55.06 10.21 55.02 10.45 58 57.12 10.07 57.07 10.32 57.03 10.57 56.98 10.22 59 58.10 10.25 58.06 10.50 58.01 10.75 57.63 11.03 61 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.38 62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.99 11.56 65 64.01 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>50.15</td> <td>9,29</td> <td>50,10</td> <td>9.51</td> <td>5</td>						50.15	9,29	50,10	9.51	5
34 93.18 9.38 53.14 9.61 53.10 9.84 53.05 10.07 56 55.15 9.72 55.11 9.96 55.06 10.21 55.02 10.45 57 56.13 9.90 56.09 10.14 56.05 10.39 56.00 10.63 58 57.12 10.07 57.07 10.32 57.03 10.57 56.98 10.82 59 58.10 10.25 58.06 10.50 58.01 10.75 57.96 11.00 60 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.30 61 60.07 10.94 61.99 11.21 61.95 11.48 61.89 11.36 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.57 64 63.03 11.11 63.96 11.18 61.99 11.81 66.91 12.10 64.89 12.03		51.21	9.03	51.17					9.70	5
55 54.16 9.55 54.12 9.79 54.08 10.02 54.03 10.26 56 55.15 9.72 55.11 9.96 55.06 10.21 55.02 10.45 57 56.13 9.90 56.09 10.14 56.05 10.39 56.00 10.63 59 58.10 10.25 58.06 10.50 58.01 10.75 57.96 11.00 60 59.09 10.42 59.04 10.68 59.00 10.93 58.95 11.00 61 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.38 62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.56 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 6		52.19		52.15						5
56 55.15 9.72 55.11 9.96 55.06 10.21 55.02 10.45 58 57.12 10.07 57.07 10.32 57.03 10.57 56.98 10.82 59 58.10 10.25 58.66 10.50 58.01 10.75 57.96 11.00 60 59.99 10.42 59.04 10.68 59.00 10.93 58.95 11.10 61 60.07 10.59 60.03 10.85 59.00 10.93 58.95 11.10 62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.56 64 63.03 11.11 62.98 11.30 60.91 11.56 66 65.90 11.46 64.95 11.74 64.89 12.03 64.84 12.16 67 65.98 11.66 <t< td=""><td></td><td></td><td></td><td>53.14</td><td></td><td>53.10</td><td>9.84</td><td></td><td></td><td>5</td></t<>				53.14		53.10	9.84			5
57 56.13 9.90 56.09 10.14 56.05 10.39 56.00 10.63 57.03 10.57 56.98 10.82 59.04 10.68 59.00 10.75 57.96 11.00 57.96 11.00 57.96 11.00 57.96 11.00 57.96 11.00 57.96 11.00 58.95 11.19 59.90 10.83 58.95 11.19 59.93 11.30 60.91 11.56 60.91 11.56 63.93 11.66 62.81 11.39 60.91 11.56 62.88 11.39 62.93 11.66 62.88 11.36 62.88 11.36 62.88 11.36 62.88 11.36 62.88 11.36 62.88 11.46 64.95 11.74 64.89 12.03 64.84 12.11 65.82 12.12 66.86 66.97 11.81 66.91 12.10 66.86 12.29 67.95 11.28 69.93 11.66 68.11 2.86 68.88 12.41 66.86 12.29 66.9			9.55		9.79		10.02			5
58 57.12 10.07 57.07 10.32 57.03 10.57 56.98 10.82 59 58.10 10.25 58.66 10.50 58.01 10.75 57.96 11.00 60 59.99 10.42 59.04 10.68 59.00 10.93 58.95 11.19 61 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.38 64 63.03 11.11 62.98 11.30 60.96 11.30 60.91 11.56 65 64.01 11.29 63.96 11.57 63.91 11.66 62.88 11.94 66 65.00 11.46 64.95 11.74 64.89 12.03 64.84 12.16 68.81 12.21 65.88 12.21 65.88 12.21 65.88 12.21 65.88 12.21 65.88 12.21 65.88 12.25 67.79 12.87 70.79 12.87 70.79 12.25 70.79 <t< td=""><td></td><td>55.15</td><td>9.72</td><td>55.11</td><td></td><td></td><td>10.21</td><td></td><td></td><td>5</td></t<>		55.15	9.72	55.11			10.21			5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		50.13				56.05				5
60 59.09 10.42 59.04 10.68 59.00 10.93 58.95 11.19 61 60.07 10.59 60.03 10.85 59.98 11.12 59.93 11.38 62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.76 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66.89 11.57 63.91 11.85 63.86 12.12 65.88 12.21 65.82 12.23 64.84 12.31 65.82 12.30 64.84 12.31 65.82 12.23 66.81 12.80 66.81 12.81 65.82 12.25 67.79 12.87 68.83 12.76 68.77 13.06 67.79 12.87 68.83 12.76 67.79 12.87 67.79 12.87 68.83 12.76 67.84 </td <td></td> <td>59 10</td> <td></td> <td>50.00</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td>		59 10		50.00						5
61 60.07 10.59 60.03 10.85 59.98 11.12 60.93 11.38 62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.56 64 63.03 11.11 62.98 11.57 63.91 11.66 62.88 11.94 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 65.90 11.48 66.91 12.10 66.86 12.21 65.82 12.56 82.72 12.88 67.90 12.28 67.84 12.57 67.79 12.87 67.79 12.88 70.79 13.12 70.74 12.50 70.85 12.81 70.79 13.12 70.74 13.49 72.70 13.62 73.80 13.37 71.78 13.39 71.78 13.49 72.70 13.80										5
62 61.06 10.77 61.01 11.03 60.96 11.30 60.91 11.56 63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.75 64 63.03 11.11 62.98 11.39 62.93 11.66 62.88 11.94 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 65.00 11.46 64.95 11.74 64.89 12.03 64.84 12.31 67 65.98 11.63 65.93 11.92 65.88 12.21 65.82 12.50 68 66.97 11.81 66.91 12.10 66.86 12.39 66.81 12.99 67.95 11.98 67.90 12.28 67.84 12.57 67.79 12.87 67.90 12.28 67.84 12.57 67.79 12.87 70 68.94 12.16 68.88 12.46 68.83 12.76 68.77 13.06 71 69.92 12.33 69.87 12.63 69.81 12.94 69.75 13.24 72 70.91 12.50 70.85 12.81 70.79 13.12 70.74 13.43 71.89 12.68 71.83 12.99 71.78 13.30 71.72 13.62 74 72.88 12.85 72.82 13.17 72.76 13.49 72.70 13.80 73.86 13.02 73.80 13.35 73.74 13.67 73.68 13.02 73.80 13.35 73.74 13.67 73.68 13.02 73.80 13.55 73.74 13.67 73.68 13.99 77.80 13.72 77.74 14.06 77.5.71 14.03 75.65 14.36 76.82 13.54 76.76 13.88 76.82 13.54 76.76 13.88 76.82 13.54 76.76 13.88 76.82 13.54 76.76 13.88 76.82 13.54 76.76 13.88 78.72 14.24 80.69 14.59 80.63 14.58 78.60 14.92 81 79.77 14.07 79.71 14.41 81.68 14.77 81.61 15.13 82.53 15.67 83.81 14.76 83.64 15.13 83.55 77.62 14.24 80.69 14.59 80.63 14.58 80.56 15.28 80.75 14.24 80.69 14.59 80.63 14.58 80.56 15.28 80.66 15.28 80.60 15.98 90.53 16.30 84.56 15.99 80.53 15.49 83.51 15.85 88.86 84.63 15.30 89.55 16.19 89.48 16.92 89.49 16.04 88.42 16.79 90.88 15.63 89.55 16.19 89.48 16.92 90.60 15.98 90.53 16.37 90.46 16.77 90.39 17.16 99.99 90.60 15.98 90.53 16.37 90.46 16.77 90.39 17.16 99.99 97.50 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.47 19.99 99.83 18.29 99.75 17.19 97.42 17.62 97.34 18.04 97.26 18.4				-			-	000000000000000000000000000000000000000		6
63 62.04 10.94 61.99 11.21 61.95 11.48 61.89 11.75 64 63.03 11.11 62.98 11.39 62.93 11.66 62.88 11.96 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 65.00 11.46 64.95 11.74 64.89 12.03 64.84 12.31 67 65.98 11.98 67.90 12.28 65.88 12.21 65.82 12.50 69 67.95 11.98 67.90 12.28 67.84 12.57 68.77 13.06 71 69.92 12.33 69.87 12.63 69.81 12.94 69.75 13.02 74 72.88 12.85 71.78 13.30 71.72 13.43 71 79.91 12.50 70.85 12.81 70.79 13.12 70.74 13.43 72 70.91 12.50										6
64 63.03 11.11 62.98 11.39 62.93 11.66 62.88 11.94 65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 65.00 11.46 64.95 11.74 64.89 12.03 64.84 12.31 67 65.98 11.63 65.93 11.92 65.88 12.21 65.82 12.50 69 67.95 11.98 67.90 12.28 67.84 12.57 67.79 12.87 70 68.94 12.16 68.88 12.46 68.83 12.76 68.77 13.06 71 69.92 12.33 69.87 12.63 69.81 12.94 69.75 13.24 70 70.91 12.50 70.85 12.81 70.79 13.12 70.74 13.43 73 71.89 12.68 71.83 12.97 71.78 13.30 72.70 13.80 75							11.30		11.56	6
65 64.01 11.29 63.96 11.57 63.91 11.85 63.86 12.12 66 65.00 11.46 64.95 11.74 64.89 12.03 64.84 12.31 67 65.98 11.63 65.93 11.92 65.88 12.21 65.82 12.50 68 66.97 11.81 66.91 12.10 66.86 12.39 66.81 12.68 70 68.94 12.16 68.88 12.46 68.83 12.76 67.79 12.86 71 69.92 12.33 69.87 12.63 69.81 12.94 69.75 13.26 74 72.88 12.55 70.85 12.81 70.79 13.12 70.74 13.43 71.72 13.24 75 73.86 13.02 73.80 13.35 73.74 13.67 77.70 13.80 76 74.85 13.20 73.80 13.35 73.74 13.67 77.61 14.84				69 00			11.48			6
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68 66.97 11.81 66.91 12.10 66.86 12.39 66.81 12.68 69 67.95 11.98 67.90 12.28 67.84 12.57 67.79 12.87 70 68.94 12.16 68.88 12.46 68.83 12.76 68.77 13.06 71 69.92 12.33 69.87 12.63 69.81 12.94 69.75 13.24 72 70.91 12.50 70.85 12.81 70.79 13.12 70.74 13.43 73 71.89 12.68 71.83 12.99 71.78 13.39 72.70 13.42 75 73.86 13.02 73.80 13.35 73.74 13.67 72.70 13.80 76 74.85 13.20 75.77 13.70 75.71 13.74 73.68 13.99 77 75.83 13.37 75.77 13.70 77.68 14.21 76.61 14.36 79									12.50	6
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		66.97								6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								67.79		6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	70	68.94	12.16					68.77		7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	71	69.92	12.33	69.87	12.63		_			7
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	73	71.89				71.78				7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	74	72.88				72.76		72.70		7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		73.86				73.74		73.68	13.99	7
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		76.82	13.54	76.76						7
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		87.65	15.45					87.44		8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							16.40	88.42		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	91	89.62	15.80	89.55	16.19	89.48			16.97	-
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	93	91.59	16.15	91.52	16.55			91.37	17.35	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		92.57	16.32		16.73			92.35	17.53	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					16.90	93.41	17.31			
98 96.51 17.02 96.44 17.44 96.36 17.86 96.28 18.28 99 97.50 17.19 97.42 17.62 97.34 18.04 97.26 18.47 100 98.48 17.36 98.40 17.79 98.33 18.22 98.25 18.65						94.39	17.49		17.91	1
98 96.51 17.02 96.44 17.44 96.36 17.86 96.28 18.28 99 97.50 17.19 97.42 17.62 97.34 18.04 97.26 18.47 100 98.48 17.36 98.40 17.79 98.33 18.22 98.25 18.65			16.84	95.45	17.26	95.38	17.68			
100 98.48 17.36 98.40 17.79 98.33 18.22 98.25 18.65			17.02				17.86			1
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Distance	11 I	Deg.	111	Deg.	11½	Deg.	117	Deg.	Distance
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
1 2 3 4 5 6 7	0.98 1.96 2.94 3.93 4.91 5.89	0.19 0.38 0.57 0.76 0.95 1.14	0.98 1.96 2.94 3.92 4.90 5.88	0.20 0.39 0.59 0.78 0.98 1.17	0.98 1.96 2.94 3.92 4.90 5.88	0.20 0.40 0.60 0.80 1.00 1.20	0.98 1.96 2.94 3.92 4.90 5.87	0.20 0.41 0.61 0.82 1.02 1.22	1 2 3 4 5 6
8 9 10	6.87 7.85 8.83 9.82 10.80	1.34 1.53 1.72 1.91 2.10	6.87 7.85 8.83 9.81 10.79	1.37 1.56 1.76 1.95	6.86 7.84 8.82 9.80 10.78	1.40 1.59 1.79 1.99 2.19	6.85 7.83 8.81 9.79	1.43 1.63 1.83 2.04	7 8 9 10
12 13 14 15 16 17	11.78 12.76 13.74 14.72 15.71 16.69	2.29 2.48 2.67 2.86 3.05 3.24 3.43	11.77 12.75 13.73 14.71 15.69 16.67 17.65	2.13 2.34 2.54 2.73 2.93 3.12 3.32 3.51	11.76 12.74 13.72 14.70 15.68 16.66 17.64	2.39 2.59 2.79 2.99 3.19 3.39 3.59	11.75 12.73 13.71 14.69 15.66 16.64 17.62	2.44 2.65 2.85 3.06 3.26 3.46 3.66	12 13 14 15 16 17
19 20 21 22	17.67 18.65 19.63 20.61 21.60	3.63 3.82 4.01 4.20	18.63 19.62 20.60 21,58	3.71 3.90 4.10 4.29	$ \begin{array}{r} 18.62 \\ 19.60 \\ \hline 20.58 \\ 21.56 \end{array} $	3.79 3.99 4.19 4.39	18.60 19.58 20.56 21.54	3.87 4.07 4.28 4.48	19 20 21 22
23 24 25 26 27 28 29	22.58 23.56 24.54 25.52 26.50 27.49 28.47	4.39 4.58 4.77 4.96 5.15 5.34 5.53	22,56 23,54 24,52 25,50 26,48 27,46 28,44	4,49 4,68 4.88 5.07 5.27 5.46 5.66	22.54 23.52 24.50 25.48 26.46 27.44 28.42	4.59 4.78 4.98 5.18 5.38 5.58 5.58 5.78	22.52 23.50 24.48 25.46 26.43 27.41 28.39	4.68 4.89 5.09 5.30 5.50 5.70 5.91	23 24 25 26 27 28 29
30 31 32 33 34 35 36 37 38	30.43 31.41 32.39 33.38 34.36 35.34 36.32 37.30	5.72 5.92 6.11 6.30 6.49 6.68 6.87 7.06 7.25	30.40 31.39 32.37 33.35 34.33 35.31 36.29 37.27	5.85 6.05 6.24 6.44 6.63 6.83 7.02 7.22 7.41	30.38 31.36 32.34 33.32 34.30 35.28 36.26 37.24	6.18 6.38 6.58 6.78 6.98 7.18 7.38 7.58	30.35 31.33 32.31 33.29 34.27 35.25 36.22	6.11 6.31 6.52 6.72 6.92 7.13 7.33 7.53	30 31 32 33 34 35 36 37
39 40 41 42 43 44	38.28 39.27 40.25 41.23 42.21 43.19	7.44 7.63 7.82 8.01 8.20 8.40	38.25 39.23 40.21 41.19 42.17 43.15	7.61 7.80 8.00 8,19 6.39 6.58	38.22 39.20 40.18 41.16 42.14 43.12	7.78 7.97 8.17 8.37 8.57 8.77	37.20 38.18 39.16 40.14 41.12 42.10 43.08	7.74 7.94 8.15 8.35 8.55 8.76 8.96	38 39 40 41 42 43 44
45 46 47 48 49 50	44.17 45.15 46.14 47.12 48.10 49.08	8.59 8.78 8.97 9.16 9.35 9.54	44.14 45.12 46.10 47.08 48.06 49.04	8,78 8,97 9,17 9,36 9,56 9,75	44.10 45.08 46.06 47.04 48.02 49.00	8.97 9.17 9.37 9.57 9.77 9.97	44.06 45.04 46.02 46.99 47.97 48.95	9.16 9.37 9.57 9.78 9.98 10.18	45 46 47 48 49 50
Distance.	Dep.	Lat. Dog.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep.	Lat.	Distance.

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Distance	- 11	Deg.	111	Deg.	114	Deg.	113	Deg.	Distance.
псе	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	8
51	50.06	9.73	50.02	9.95	49.98	10.17	49.93	10.39	
52 53	51.04 52.03	9.92	51.00 51.98	10.14 10.34	50.96 51.94	10.37	50.91 51.89	10.59	
54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00	54
55	53.99	10.49	53.94	10.73	53.90	10.97	53.85	11.20	55
56 57	54.97 55.95	10.69	54.92 55.90	10.93	54.88 55.86	11.16	54.83 55.81	11.40	56
58	56.93	11.07	56.89	11.32	56.84	11.56	56.78	11.81	58
59 60	57.92 58.90	11.26	57.87 58.85	11.51	57.82 58.80	11.76	57.76 58.74	12.01 12.22	60
61	59.88	11.64	59.83	11.90	59.78	$\frac{11.36}{12.16}$	59.72	12.42	61
62	60.86	11.83	60.81	12.10 12.29	60.76 61.74	12.36	60.70 61.68	12.63	62
63 64	61.84	12.02 12.21	61.79 62.77	12.29	62.72	12.56 12.76	62.66	12.83 13.03	63 64
65	63.81	12.40	63.75	12.68	63.70	12.96	63.64	13.24	65
66	64.79	12.59	64.73	12.88	64.68	13.16	64.62	13.44	66
67 68	65.77	12.78 12.98	65.71 66.69	13.07 13.27	65.66	13.36 13.56	65.60	13.64 13.85	68
69	67.73	13.17	67.67	13.46	67.61	13.76	67.55	14.05	69
70	68.71	13.36	68.66	13.66	69.59	13.96	68.53	14.25	70
$\frac{71}{72}$	69.70 70.68	13.55 13.74	69.64 70.62	13.85 14.05	69.57	14.16 14.35	69.51 70.49	14.46	71 72
73	71.66	13.93	71.60	14.24	71.53	14.55	71.47	14.87	73
74	72.64	14.12	72.58	14.44	72.51	14.75	72.45	15.07	74
75 76	73.62	14.31 14.50	73.56 74.54	14.63 14.83	73.49 74.47	14.95 15.15	73.43 74.41	15.27 15.48	75 76
77	75.59	14.69	75.52	15.02	75.45	15.35	75.39	15.68	77
78	76.57	14.88	76.50	15.22	76.43	15.55	76.37	15.88	78
79 80	77.55 78.53	15.07 15.26	77,48 78.46	15.41 15.61	77.41 78.39	15.75 15.95	77.34 78.32	16.09 16.29	79 80
81	79.51	15.46	79.44	15.80	79.37	16.15	79.30	16.49	81
82	80.49	15.65	80.42	16.00	80.35	16.35	80.28 81.26	16.70	82 83
83 84	81.48 82.46	15,84 16,03	81.41 82.39	16.19 16.39	81.33 82.31	16.55 16.75	82.24	16.90 17.11	84
85	83.44	16.22	83.37	16.58 16.78	83,29	16.95	83.22	17.31	85
86 87	84.42	16.41	84.35 85.33	16.78 16.97	84.27 85.25	17.15 17.35	84.20 85.18	17.51 17.72	86 87
88	86.38	16.60 16.79	86.31	17.17	86.23	17.54	86.16	17.92	88
89	87.36 88.35	16,98	87.29	17.36	87.21	17.74	87.14	18.12	89
90		17.17	88.27	17.56	88.19	17.94	88.11	18.33	90
91 92	89.33 90.31	17.36 17.55	89.25 90.23	17.75 17.95	89.17 90,15	18.14 18.34	89.09	18.53 18.74	92
93	91.29	17.75	91.21	18.14	91.13	18.54	91.05	18.94	93
94	92.27 93.25	17.94	92.19 93.17	18.34	92.11 93.09	18.74 18.94	92.03 93.01	19.14 19.35	94 95
95 96	94.24	18.13 18.32	94.16	18.53 18.73	94.07	19.14	93.01	19.55	96
97	95.22	18.51	95.14	18.92	95.05	19.34	94.97	19.75	97
98 99	96.20 97.18	18.70 18.89	96.12 97.10	19.12 19.31	96.03 97.01	19.54 19.74	95.95 96.93	19.96 20.16	98 99
100	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	100
nce.	Dep.	Lat.	Dop.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	79 E	eg.	781	Deg.	781	Deg.	781	Deg.	Distance

Distance	12 1	Deg.	12½ l	Deg.	12]	Deg.	12}	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	псе.
1 2 8 4 5 6	0.98 1.96 2.93 8.91 4.89	0.21 0.42 0.62 0.83 1.04	0.98 1.95 3.93 3.91 4.89	0.21 0.42 0.64 0.85 1.06	0.98 1.95 2.93 3.91 4.88	0.22 0.43 0.65 0.87 1.08	0.98 1.95 2.93 3.90 4.88	0.22 0.44 0.66 0.88 1.10	1 2 3 4 5
7 8 9 10	5.87 6.85 7.83 8.80 9.78	1.25 1.46 1.66 1.87 2.08	5.86 6.84 7.82 8.80 9.77	1.27 1.49 1.70 1.91 2.12	5.86 6.83 7.81 8.79 9.76	1.30 1.52 1.73 1.95 2.16	5.85 6.83 7.80 8.78 9.75	1.32 1.54 1.77 1.99 2.21	7 8 9 10
11 12 13 14 15	10.76 11.74 12.72 13.69 14.67	2.29 2.49 2.70 2.91 3.12	10.75 11.73 12.70 13.68 14.66	2.38 2.55 2.76 2.97 3.18	10.74 11.72 12.69 13.67 14.64	2.38 2.60 2.81 3.03 3.25	10.73 11.70 12.68 13.65 14.63	2.43 2.65 2.87 8.09 3.31	11 12 13 14 15
16 17 18 19 20	15.65 16.63 17.61 18.58 19.56	3.33 3.53 3.74 8.95 4.16	15.64 16.61 17.59 18.57 19.54 20.52	3.39 3.61 3.82 4.03 4.24	15.62 16.60 17.57 18.55 19.53	3.46 3.68 3.90 4.11 4.33	15.61 16.58 17.56 18.53 19.51 20.48	3.53 3.75 3.97 4.19 4.41	16 17 18 19 20
21 22 23 24 25 26	20.54 21.52 22.50 23.48 24.45 25.43	4.37 4.57 4.78 4.99 5.20 5.41	20.52 21.50 22.48 23.45 24.43 25.41	4.46 4.67 4.88 5.09 5.30 5.52	20.50 21.48 22.45 23.43 24.41 25.38	4.76 4.98 5.19 5.41 5.63	20.48 21.46 22.43 23.41 24.38 25.36	4.63 4.86 5.08 5.30 5.52 5.74	21 22 23 24 25 26
27 28 29 30 31	26.41 27.39 28.37 29.34 30.32	5.61 5.82 6.03 6.24 6.45	26.39 27.36 28.34 29.32 30.29	5.73 5.94 6.15 6.37 6.58	26.36 27.34 28.31 29.29 30.27	5.84 6.06 6.28 6.49 6.71	26.33 27.31 28.28 29.26 30,24	5.96 6.18 6.40 6.62 6.84	27 28 29 30
32 33 34 35 36	31.30 32.28 33.26 34.24 35.21	6.65 6.86 7.07 7.28 7.48	31.27 32.25 33.23 34.20 35.18	6.79 7.00 7.21 7.43 7.64	31.24 32.22 33.19 34.17 35.15	6.93 7.14 7.36 7.58 7.79	31.21 32.19 33.16 34.14 35.11	7.06 7.28 7.50 7.72 7.95	32 33 34 35 36
37 38 39 40 41	36.19 37.17 38.15 39.13 40.10	7.69 7.90 8.11 8.32 8.52	36.16 37.13 38.11 39.09 40.07	7.85 8.06 8.27 8.49 8.70	36.12 37.10 38.08 39.05 40.03	8.01 8.22 8.44 8.66 8.87	36.09 37.06 38.04 39.01 39.99	8.17 8.39 8.61 8.83 9.05	37 38 39 40
42 43 44 45 46	41.08 42.06 43.04 44.02 44.99	8.73 8.94 9.15 9.36 9.56	41.04 42.02 43.00 43.98 44.95	8.91 9.12 9.34 9.55 9.76	41.00 41.98 42.96 43.93 44.91	9.09 9.31 9.52 9.74 9.96	40.96 41.94 42.92 43.89 44.87	9.27 9.49 9.71 9.93 10.15	42 43 44 45 46
47 48 49 50	45.97 46.95 47.93 48.91	9.77 9.98 10.19 10.40	45.93 46.91 47.88 48.86	9.97 10.18 10.40 10.61	45.89 46.86 47.84 48.81	10.17 10.39 10.61 10.82	45.84 46.82 47.79 48.77	10.37 10.59 10.81 11.03	47 48 49 50
Distance.	78	Lat. Deg.	Dep. 773	Deg.	77½	Lat. Deg.	Dep. 771	Lat.	· Distance.

Dist	12 I	Deg.	124	Deg.	121/2	Deg.	123	Deg.	STATE OF
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ST. ST.
51	49.89	10.60	49.84	10.82	49.79	11.04	49.74	11.26	1
52	50.86	10.81	50.82	11.03	50.77	11.25	50.72 51.69	11.48	1
53	51.84	11.02	51.79	11.25	51.74	11.47		11.70	1
54	52.82	11.23	52.77	11.46	52.72	11.69	52.67	11.92	1
55	53.80	11.44	53.75	11.67	53.70 54.67	11.90	53.64 54.62	12.14	1
56	54.78	11.64	54.72	11.88	55.65	12.12 12.34	55.59	12.58	1
57	55.75	$11.85 \\ 12.06$	55.70	12.09 12.31	56.63	12.55	56.57	12.80	1
59	56.73 57.71	12.27	57.66	12.52	57.60	12.77	57.55	13.02	1
60	58.69	12.47	58.63	12.73	58.58	12:99	58.52	13.24	1
61	59.67	12.68	59.61	12.94	59.55	13.20	59.50	13.46	-
62	60.65	12.89	60.59	13.16	60.53	13.42	60.47	13.68	
63	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90	1
64	62.60	13.31	62.54	13.58	62.48	13.85	62.42	14.12	1
65	63.58	13.51	63.52	13.79	63.46	14.07	63.40	14.35	6
66	64.56	13.72	64.50	14.00	64.44	$14.29 \\ 14.50$	64.37	14.57 14.79	6
67	65.54 66.51	13.93 14.14	65.47	$14.22 \\ 14.43$	65.41 66.39	14.72	66.32	15.01	E
69	67.49	14.35	67.43	14.64	67.36	14.93	67.30	15.23	6
70	68.47	14.55	68.41	14.85	68.34	15.15	68.27	15.45	7
71	69.45	14.76	69.38	15.06	69.32	15.37	69.25	15.67	7
72	70.43	14.97	70.36	15.28	70.29	15.58	70.22	15.89	7
73	71.40	15.18	71.34	15.49	71.27	15.80	71.20	16.11	1/3
74	72.38	15.39	72.32	15.70	72.25	16.02	72.18	16.33	7
75	73.36	15.59	73.29	15.91	73.22	16.23	73.15	$16.55 \\ 16.77$	7
76	74.34	15.80 16.01	74.27 75.25	16.13	74.20 75.17	16.45 16.67	75.10	16.99	7
77	75.32 76.30	16.22	76.22	$16.34 \\ 16.55$	76.15	16.88	76.08	17.21	7
79	77.27	16.43	77.20	16.76	77.13	17.10	77.05	17.44	7
80	78.25	16.43 16.63	77.20 78.18	16.97	78.10	17.10 17.32	78.03	17.66	8
81	79.23	16.84	79.16	17.19	79.08	17.53	79.00	17.88	8
82	80.21	17.05	80.13	17.40	80.06	17.75	79.98	18.10	8
83	81.19	17.26	81.11	17.61	81.03	17.96	80.95	18.32	8
84	82.16	17.46 17.67	82.09	17.82	82.01	18.18 18.40	81.93 82.90	18.54 18.76	8
85	83.14	17.07	83.06	18.04	82.99 83.96	18.61	83.88	18.98	8
86	84.12	17.88 18.09	85.02	18.25 18.46	84.94	18.83	84.85	19.20	8
88	86.08	18.30	86.00	18.67	85.91	19.05	85.83	19.42	8
89	87.06	18.50	86.97	18.88	86.89	19.26	86.81	19.64	8
90	88.03	18.71	87.95	19.10	87.87	19.48	87.78	19.86	9
91	89.01	18.92	88.93	19.31	88.84	19.70	88.76	20.08	9
92	89.99	19.13 19.34	89.91	19.52	89.82	19.91	89.73	20.30	9
93	90.97	19.34	90.88	19.73	90.80	20.13	90.71	20.52 20.75	0
94	91.95	19.54	91.86	19.94	91.77 92.75	20.35 20.56	92.66	20.75	9
95 96	92.92	19.75 19.96	92.84 93.81	20.16 20.37	93.72	20.78	93.63	21.19	9
97	94.88	20.17	94.79	20.58	94.70	20.99	94.61	21.41	0
98	95.86	20.38	95.77	20.79	95.68	21.21	95.58	21.63	1 5
99	96.84	20.58	96.75	21.01	96.65	21.43	96.56	21.85	1 5
100	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	10
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	7.0
Distance.	78	Deg.	774	Deg	771	Deg.	771	Deg.	1

Distance.	13]	Deg.	13 1]	Deg.	13 <u>}</u>]	Deg.	13}	Deg.	Distance.
mce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	6
1 2 3 4 5 6 7	0.97 1.95 2.92 3.90 4.87 5.85	0.23 0.45 0.67 0.90 1.12 1.35	0.97 1.95 2.92 3.89 4.87 5.84	0.23 0.46 0.69 0.92 1.15 1.38	0.97 1.95 2.92 3.89 4.86 5.83	0.23 0.47 0.70 0.93 1.17 1.40	0.97 1.94 2.91 3.89 4.86 5.83	0.24 0.48 0.71 0.95 1.19 1.43	1 2 3 4 5
7 8 9 10	$ \begin{array}{r} 6.82 \\ 7.80 \\ 8.77 \\ \hline 9.74 \\ \hline 10.72 \end{array} $	1.57 1.80 2.02 2.25 2.47	6.81 7.79 8.76 9.73	1.60 1.83 2.06 2.29	6.81 7.78 8.75 9.72	1.63 1.87 2.10 2.33	6.80 7.77 8.74 9.71	1.66 1.90 2.14 2.38 2.61	7 8 9 10 11
12 13 14 15 16	11.69 12.67 13.64 14.62 15.59	2.70 2.92 3.15 3.37 3.60	11.68 12.65 13.63 14.60 15.57	2.75 2.98 3.21 3.44 3.67	11.67 12.64 13.61 14.59 15.56	2.80 3.03 3.27 3.50 3.74	11.66 12.63 13.60 14.57 15.54	2.85 3.09 3.33 3.57 3.80	12 13 14 15 16
17 18 19 20 21	16.57 17.54 18.51 19.49 20.46 21.44	3.82 4.05 4.27 4.50 4.72 4.95	16.55 17.52 18.49 19.47 20.44 21.41	3.90 4.13 4.35 4.58 4.81 5.04	16.53 17.50 18.48 19.45 20.42 21.39	3.97 4.20 4.44 4.67 4.90 5.14	16.51 17.48 18.46 19.43 20.40 21.37	4.04 4.28 4.52 4.75 4.99 5.23	17 18 19 20 21
22 23 24 25 26 27	22.41 23.38 24.36 25.33 26.31	5.17 5.40 5.62 5.85 6.07	22.39 23.36 24.33 25.31 26.28	5.27 5.50 5.73 5.96 6.19	22.36 23.34 24.31 25.28 26.25	5.37 5.60 5.84 6.07 6.30	22.34 23.31 24.28 25.25 26.23	5.23 5.47 5.70 5.94 6.18 6.42	22 23 24 25 26 27
28 29 30 31 32	27.28 28.26 29.23 30.21 31.18	6.30 6.52 6.75 6.97 7.20	27.25 28.23 29.20 30.17 31.15	6.42 6.65 6.88 7.11 7.33	27.23 28.20 29.17 30.14 31.12	6.54 6.77 7.00 7.24 7.47	27.20 28.17 29.14 30.11 31.08	6.66 6.89 7.13 7.37 7.61	28 29 30 31 32
33 34 35 36 37	32.15 33.13 34.10 35.08 36.05	7.42 7.65 7.87 8.10 8.32 8.55	32.12 33.09 34.07 35.04 36.02	7.56 7.79 6.02 8.25 8.48	32.09 33.06 34.03 35.01 35.98	7.70 7.94 8.17 8.40 8.64	32.05 33.03 34.00 34.97 35.94	7.84 8.08 8.32 8.56 8.79	33 34 35 36 37
38 39 40 41 42	37.03 38.00 38.97 39.95 40.92	8.55 8.77 9.00 9.22 9.45	36.99 37.96 38.94 39.91 40.88	8.71 8.94 9.17 9.40 9.63	36.95 37.92 38.89 39.87 40.84	8.87 9.10 9.34 9.57 9.80	36.91 37.88 38.85 39.83 40.80	9.03 9.27 9.51 9.75 9.98	38 39 40 41 42
43 44 45 46 47 48	41.90 42.87 43.85 44.82 45.80 46.77 47.74	9.67 9.90 10.12 10.35 10.57 10.80	41.86 42.83 43.80 44.78 45.75	9.86 19.08 10.31 10.54 10.77 11.00	41.81 42.78 43.76 44.73 45.70 46.67	10.04 10.27 10.51 10.74 10.97 11.21	41.77 42.74 43.71 44.68 45.65 46.62	10.22 10.46 10.70 10.93 11.17 11.41	43 44 45 46 47 48
49 50	47.74 48.72 Dep.	11.02 11.25 Lat.	47.70 48.67 Dep.	11.23 11.46 Lat.	47.65 48.62 Dep.	11.44 11.67 Lat.	47.60 48.57 Dep.	11.65 11.88 Lat.	49 50
Distance	<u> </u>	Deg.		Deg.	<u> </u>	Deg.	<u> </u>	Deg.	Distance.

Distance.	13]	Deg.	131	Deg.	131	Deg.	13}	Deg.	Distan
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
51 52	49.69 50.67	11.47 11.70	49.64 50.62	11.69	49.59 50.56	11.91 12.14	49.54 50.51	12.12 12.36	51 52
53 54	51.64 52.62	11.92 12.15	51.59 52.56	12.15 12.38	51.54 -52.51	12.37 12.61	51.48 52.45	12.60 12.84	53 54
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07	55
56 57	54.56 55.54	12.60 12.82	54.51 55.48 56.46	12.84 13.06	54.45 55.43	13.07 13.31	54.40 55.37	13.31 13.55	56 57
58 59	56.51 57.49	13.05 13.27	56.46 57.43	13.29 13.52	56.40 57.37	13.54 13.77	56.34 57.31	13.79 14.02	58 59
60	58.46	13.50	58.40	13.75	58.34	14.01	58.28	14.26	60
61 62	59.44 60.41	13.72 13.95	59.38 60.35	13.98 14.21	59.31 60.29	14.24 14.47	59.25 60.22	14.50 14.74	61 62
63 64	61.39 62.36	14.17 14.40	61.32	14.44 14.67	61.26 62.23	14.71 14.94	61.19 62.17	14.97 15.21	63 64
65 66	63.33 64.31	14.62 14.85	63.27 64.24	14.90	63.20	15.17	63.14	15.45	65
67	65.28	15.07	65.22	15.13 15.36	64.18 65.15	15.41 15.64	64.11 65.08	15.69 15.93	66 67
68 69	66.26 67.23	15.30 15.52	66.19 67.16 68.14	15.59 15.81	66.12	15.87 16.11	66.05 67.02	16.16 16.40	68 69
70	68.21	15.75		16.04	68.07	16.34	67.99	16.64	70
71 72	69.18 70.15	15.97 16.20	69.11 70.08	16.27 16.50	69.04 70.01	16.57 16.81	68.97 69.94	16.88 17.11	71 72
73 74	71.13 72.10	16.42 16.65	71.06	16.73 16.96	70.98	17.04 17.28	70.91	17.35 17.59	73 74
75 76	73.08 74.05	16.87 17.10	73.00 73.98	17.19 17.42	72.93 73.90	17.50	72.85 73.82	17.83 18.06	75 76
77	75.03	17.32	74.95	17.65	74.87	17.74 17.98	74.79	18.30	77
78 79	76.00 76.98	17.55 17.77 18.00	75.92 76.90	17.88 18.11	75.84 76.82	18.21 18.44	75.76 76.74	18.54 18.78	78 79
80 81	77.95	$\frac{18.00}{18.22}$	$\frac{77.87}{78.84}$	$\frac{18.34}{18.57}$	$\frac{77.79}{78.76}$	$\frac{18.68}{18.91}$	77.71	19.01	80 81
82	79.90	18.45	79.82	18.79	79.73	19.14	79.65	19.49	82
83 84	80.87 81.85	18.67 18.90	80.79 81.76	19.02 19.25	80.71 81.68	19.38 19.61	80.62	19.73. 19.07	83 84
85 86	82.82 83.80	19.12 19.35	82.74 83.71	19.48 19.71	82.65 83.62	19.84 20.08	82.56 83.54	20.20 20.44	85 86
87	84.77	19.57	84.68	19.94	84.60	20.31	84.51	20.68	87 88
88	85.74 86.72	19.80 20.02	85.66 86.63	20.17 20.40	85.57 86.54	20.54 20.78	85.48 86.45	20.92 21.15	89
90 91	87.69 88.67	$\frac{20.25}{20.47}$	87.60 88.58	$\frac{20.63}{20.86}$	87.51	$\frac{21.01}{21.24}$	87.42	$\frac{21.39}{21.63}$	90 91
92	89.64	20.70	89.55	21.09	89.46	21.48	89.36	21.87	92
93 94	90.62 91.59	20.92 21.15	90.52	21.32 21.54	90.43 91.40	21.71 21.94	90.33	22.10 22.34	93 94
95 96	92.57 93.54	21.37 21.60	92.47 93.44	21.77 22.00	92.38 93.35	22.18 22.41	92.28 93.25	22.58 22.82	95 96
97 98	94.51 95.49	21.82 22.05	94.42 95.39	22.23 22.46	94.32 95.29	22.64 22.88	94.22 95.19	23.06 23.29	97 98
99	96.46	22.27	96.36	22.69	96.26	23.11	96.16	23.53	99
100	97.44 Dep.	22.50 Lat.	97.34 Dep.	22.92 Lat.	97.24 Dep.	23.34 Lat.	97,13 Dep.	23,77 Lat.	100
Distance.	Dop.		Дор.	Dat.	Dob.				Distance
Ä	77	Deg.	76 1	Deg.	76 <u>1</u>	Deg.	761	Deg.	Dis
		Deg. 101 Deg.			_				

	Distance	14 I	Deg.	141	Deg.	141	Deg.	14}	Deg.	Distance.
		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	шсе.
I -	1	0.97	0.24	0.97	0.25 0.49	0.97	0.25	0.97	0.25 0.51	
ı	2 3 4 5 6 7	2.91	0.73	2.91	0.74	2.90	0.75	2.90	0.76	2
1	4	3.88 4.85	0.97	3.88 4.85	$0.98 \\ 1.23$	3.87 4.84	1.00	3.87 4.84	1.02	4 5
1	6	5.82	1.45	5.82	1.48	5.81	1.50	5.80	1.53	6
1	8	6.79 7.76	1.69	6.78 7.75	1.72	6.78 7.75	1.75 2.00	6.77 7.74	1.78 2.04	7 8
1	9	8.73	1.94 2.18	8.72	1.97 2.22	8.71	2.25	8.70	2.29	9
	0	9.70	2.42	9.69	2.46	9.68	2.50	9.67	2.55	10
	1 2	10.67	2.66	10.66 11.63	2.71 2.95	10.65 11.62	2.75 3.00	10.64 11.60	2.80 3.06	11 12
	3	12.61	2.90 3.15	12.60	3.20	12.59	3.25	12.57	3.31	13
	5	13.58 14.55	3.39 3.63	13.57	3.45 3.69	13.55 14.52	3.51 3.76	13.54	3.56	14 15
	6	15.52	3.87	14.54 15.51	3.94	15.49	4.01	14.51 15.47	4.07	16
	7	16.50	4.11	16.48	4.18	16.46	4.26	16.44	4.33	17
	8	17.47 18.44	4.35 4.60	17.45 18.42	4.43 4.68	17.43 18.39	4.51	17.41 18.37	4.58	18 19
	<u> 0</u>	19.41	4.84	19.38	4.92	19.36	5.01	19.34	5.09	20
	21	$20.38 \\ 21.35$	5.08 5.32	20.35	5.17	20.33	5.26 5.51	20.31	5.35 5.60	21 22
	23	22.32	5.56	21.32 22.29	5.42 5.66	21.30 22.27	5.76	21.28 22.24	5.86	23
2	24	23.99	5.81	23.26	5.91	23.24	6.01	23.21	6.11	24
	25 26	24.26 25.23	6.05 6.29	24.23 25.20	6.15 6.40	24.20 25.17	6.26	24.18 25.14	6.37	25 26
1 2	27	26.20	6.53	26.17	6.65	26.14	6.76	26.11	6.87	27
	28 29	27.17 28.14	6.77 7.02	27.14 28.11	6.89	27.11 28.08	7.01 7.26	27.08 28.04	7.13	28 29
	30	29.11	7,26	29.08	7.14 7.38	29.04	7.51	29.01	7.64	30
	31	30.08	7.50	30.05	7.63	30.01	7.76	29.98	7.89	31
	32 33	31.05 32.02	7.74	31.02 31.98	7.88 8.12	30.98 31.95	8.01 8.26	30.95 31.91	8.15 8.40	32 33
1 3	34	32.99	8.23 8.47	32.95	8.37	32.92	8.51	32.88	8.66	34
	35 36	33.96 34.93	8.47 8.71	33.92 34.89	8.62 8.86	33.89 34.85	8.76 9.01	33.85 34.81	8.91 9.17	35 36
1 8	37	35.90	8.95	35.86	9.11	35.82	9.26	35.78	9.42	37
	38 39	36.87 37.84	9.19	36.83 37.80	9.35	36.79 37.76	9.51 9.76	36.75	9.67	38 39
	10	38.81	9.68	38.77	9.85	38.73	10.02	37.71 38.68	10.18	40
174	11	39.78	9.92	39.74	10.09	39.69	10.27	39.65	10.44	41
1 2	12 13	40.75 41.72	10.16	40.71 41.68	10.34 10.58	40.66 41.63	10.52 10.77	40.62	10.69 10.95	42 43
	44	42.69	10.64	42.65	10.83	42.60	11.02	42.55	11.20	44
1 5	15 16 17 48	43.66 44.63	10.89	43.62 44.58	11.08	43.57	11.27	43.52	11.46 11.71	45 46
1 3	17	45.60	11.13 11.37	45.55	11.57	44.53 45.50	11.77	44.48 45.45	111.97	40
1	48	46.57	11.61	46.52	11.82	46.47	12.02	46.42		48
	49 50	47.54 48.51	11.85 12.10	47.49 48.46	12.06 12.31	47.44 48.41	12.27 12.52	47.39 48.35		49 50
		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	-
	Distance.	.76	Deg.	75}	Deg.	76 <u>1</u>	Deg.	751	Deg.	Distance.

Dist	14	Deg.	144	Deg.	141	Deg.	143	Deg.	Dist
tance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	49.49	12.34	49.43	12.55	49.38	12.77	49.32	12.98	5
52	50.46	12.58	50.40	12.80	50.34	13.02	50.29	13.24	5
53 54	51.43 52.40	12.82 13.06	51.37 52.34	$13.05 \\ 13.29$	$\begin{bmatrix} 51.31 \\ 52.28 \end{bmatrix}$	$13.27 \\ 13.52$	$51.25 \\ 52.22$	13.49	5 5
55	53.37	13.31	53.31	13.54	53.25	13.77	53.19	$13.75 \\ 14.00$	5
56	54.34	13.55	54.28	13.78	54.22	14.02	54.15	14.26	5
57	55.31	13.79	55.25	14.03	55.18	14.27	55.12	14.51	5
58	56.28	14.03	56.22	14.28	56.15	14.52	56.09	14.77	5
59 60	57.25	14.27	57.18	14.52	57.12	14.77	57.06	15.02	6
61	$\frac{58.22}{59.19}$	$\frac{14.52}{14.76}$	$\frac{58.15}{59.12}$	$\frac{14.77}{15.02}$	$\frac{58.09}{59.06}$	$\frac{15.02}{15.27}$	58.02	15.28	6
62	60.16	15.00	60.09	15.26	60.03	15.52	58.99 59.96	15.53 15.79	6
63	61.13	15.24	61.06	15.51	60.99	15.77	60.92	16.04	6
64	62.10	15.48	62.03	15.75	61.96	16.02	61.89	16.29	6
65	63.07	15.72	63.00	16.00	62.93	16.27	62.86	16.55	6
66	64.04 65.01	15.97	63.97	16.25	$63.90 \\ 64.87$	16.53 16.78	63.83	16.80	6
68	65.98	16.21	64.94	$16.49 \\ 16.74$	65.83	17.03	64.79	17.06	6
69	66.95	16.69	66.88	16.98	66.80	17.28	66.73	17.31 17.57	6
70	67.92	16.93	67.85	17.23	67.77	17.53	67.69	17.82	7
71	68.89	17.18	68.82	17.48	68.74	17.78	68.66	18.08	7
72	69.86	17.42	69.78	17.72	69.71	18.03	69.63	18.33	7
73	70.83	17.66	70.75	17.97	70.67	18.28	70.59	18.59	7
74 75	$71.80 \\ 72.77$	17.90 18.14	$71.72 \\ 72.69$	18.22 18.46	71.64 72.61	18.53 18.78	71.56	18.84	7
76	73.74	18.39	73.66	18.71	73.58	19.03	72.53 73.50	19.10 19.35	7
77	74.71	18.63	74.63	18.95	74.55	19.28	74.46	19.60	7
78	75.68	18.87	75.60	19.20	75.52	19.53	75.43	19.86	7
79	76.65	19.11	76.57	19.45	76.48	19.78	76.40	20.11	7
80	77.62	19.35	77.54	19.69	77.45	20.03	77.36	20.37	8
81	78.59 79.56	19.60	78.51 79.48	19.94	78.42	$20.28 \\ 20.53$	78.33	20.62	8
82 83	80.53	19.84 20.08	80.45	20.18 20.43	79.39 80.36	20.78	80.26	20.88	8
84	81.50	20.32	81.42	20.68	81.32	21.03	81.23	21.39	8
85	82.48	20.56	82.38	20.92	82.29	21,28	82.20	21.64	8
86	83.45	20.81	83.35	21.17	83.26	21.53	83.17	21.90	8
87	84.42 85.39	21.05	84.32	$21.42 \\ 21.66$	84.23 85.20	$21.78 \\ 22.03$	84.13	22.15	8
89	86.36	21.53	86.26	21.91	86.17	22.28	86.07	22.41 22.66	8
90	87.33	21.77	87.23	22.15	87.13	22.53	87.03	22.91	9
91	88.30	22.01	88.20	22.40	88.10	22.78	88.00	23.17	9
92	89.27	22.26	89.17	22.65	89.07	23.04	88.97	23.42	9
93	90.24	22.50	90.14	22.89	90.04	23.29	89.94	23.68	9
94	$91.21 \\ 92.18$	22.74	91.11	23.14	91.01	23.54	90.90	23.93	9
95 96	93.15	22.98 23.22	$92.08 \\ 93.05$	23.38	91.97 92.94	$23.79 \\ 24.04$	91.87	24.19 24.44	9
97	94.12	23.47	94.02	23.88	93.91	24.29	93.80	24.70	9
98	95.09	23.71	94.98	24.12	94.88	24.54	94.77	24.95	9
99	96.06	23 95	95.95	24.37	95.85	24.79	95.74	25.21	9
900	97.03 Dep.	24.19 Lat.	96.92 Dep.	24.62 Lat.	96.81 Dep.	25.04 Lat.	96.70 Dep.	25.46 Lat.	10
stance.	Tollar.	-			-		-		Distance.
Dist	76 I	Deg.	753	Deg.	751	Deg.	754	Deg.	Ö

Dia	15 I	og.	151	Deg.	15 <u>‡</u>	Deg.	15}	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	0.97	0.26	0.96	0.26	0.96	0.27	0.96	0.27	1
2	1.93	0.52	1.93	0.53	1.93	0.53	1.92	0.54	2
8	2.90	0.78	2.89	0.79	2.89	0.80	2.89	0.81	3
2 8 4 5 6 7	3.86 4.83 5.80 6.76	1.04 1.29 1.55 1.81	3.86 4.82 5.79 6.75	1.05 1.32 1.58 1.84	3.85 4.82 5.78 6.75	1.07 1.34 1.60 1.87	3.85 4.81 5.77 6.74	1.09 1.36 1.63 1.90	2 3 4 5 6 7
8	7.73	2.07	7.72	2.10	7.71	2.14	7.70	2.17	8
9	8.69	2.33	8.68	2.37	8.67	2.41	8.66	2.44	9
10	9.66	2.59	9.65	2.63	9.64	2.67	9.62	2.71	10
11	10.63	2.85	10.61	2.89	10.60	2.94	10.59	2.99	11
12	11.59	3.11	11.58	3.16	11.56	3.21	11.55	3.26	12
13	12.56	3.36	12.54	3.42	12.53	3.47	12.51	3.53	13
14	13.52	3.62	13.51	3.68	13.49	3.74	13.47	3.80	14
15	14.49	3.88	14.47	3.95	14.45	4.01	14.44	4.07	15
16	15.45	4.14	15.44	4.21	15.42	4.28	15.40	4.34	16
17	16.42	4.40	16.40	4.47	16.38	4.54	16.36	4.61	17
18	17.39	4.66	17.37	4.73	17.35	4.81	17.32	4.89	18
19	18.35	4.92	18.33	5.00	18.31	5.08	18.29	5.16	19
20	19.32	5.18	19.30	5.26	19.27	5.34	19.25	5.43	20
21	20.28	5.44	20.26	5.52	20,24	5.61	20.21	5.70	21
22	21.25	5.69	21.23	5.79	21,20	5.88	21.17	5.97	22
23	22.22	5.95	22.19	6.05	22,16	6.15	22.14	6.24	23
24	23.18	6.21	23.15	6.31	23,13	6.41	23.19	6.51	24
25 26 27	24.15 25.11 26.08	6.47 6.73 6.99	24.12 25.08 26.05	6.58 6.84 7.10 7.36	24.09 25.05 26.02	6.68 6.95 7.22	24.06 25.02 25.99	6.79 7.06 7.33	25 26 27
28 29 30 31	27.05 28.01 28.98 29.94	$ \begin{array}{r} 7.25 \\ 7.51 \\ 7.76 \\ \hline 8.02 \end{array} $	$ \begin{array}{r} 27.01 \\ 27.98 \\ 28.94 \\ \hline 29.91 \end{array} $	7.36 7.63 7.89 8.15	$ \begin{array}{r} 26.98 \\ 27.95 \\ 28.91 \\ \hline 29.87 \end{array} $	$ \begin{array}{r} 7.48 \\ 7.75 \\ 8.02 \\ \hline 8.28 \end{array} $	$ \begin{array}{r} 26.95 \\ 27.91 \\ 28.87 \\ \hline 29.84 \end{array} $	7.60 7.87 8.14 8.41	28 29 30 31
32	30.91	8.28	30.87	8.42	30.84	8.55	30.80	8.69	32
33	31.88	8.54	31.84	8.68	31.80	8.82	31.76	8.96	33
34	32.84	8.80	32.80	8.94	32.76	9.09	32.72	9.23	34
35	33.81	9.06	33.77	9.21	33.73	9.35	33.69	9.50	35
36	34.77	9.32	34.73	9.47	34.69	9.62	34.65	9.77	36
37	35.74	9.58	35.70	9.73	35.65	9.89	35.61	10.04	37
38	36.71	9.84	36.66	10.00	36.62	10.16	36.57	10.31	38
39	37.67	10.09	37.63	10.26	37.58	10.42	37.54	10.59	39
40	38.64	10.35	38.59	10.52	38.55	10.69	38.50	10.86	40
41	39.60	10.61	39.56	10.78	39.51	10.96	39.46	11.13	41
42	40.57	10.87	40.52	11.05	40.47	11.22	40.42	11.40	42
43	41.53	11.13	41.49	11.31	41.44	11.49	41.39	11.67	43
44	42.50	11.39	42.45	11.57	42.40	11.76	42.35	11.94	44
45	43.47	11.65	43.42	11.84	43.36	12.03	43.31	12.21	45
46	44.43	11.91	44.38	12.10	44.33	12.29	44.27	12.49	46
47	45.40	12.16	45.35	12.36	45.29	12.56	45.24	12.76	47
48	46.36	12.42	46.31	12.63	46.25	12.83	46.20	13.03	48
49	47.33	12.68	47.27	12.89	47.22	13.09	47.16	13.30	49
50	48.30	12.94	48.24	13.15	48.18	13.36	48.12	13.57	50
Distance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Ä	75	Deg.	74}	Deg.	743	Deg.	741	Deg.	ă

Distan	15	Deg.	151	Deg.	151	Deg.	157	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	псе.
51 52	49.26 50.23	13.20 13.46	49.20 50.17	13.41 13.68	49.15 50.11	13.63 13.90	49,09 50.05	13.84 14.11	51 52
53	51.19	13.72	51.13	13.94	51.07	14.16	51.01	14.39	53
54 55	52.16 53.13	13.98 14.24	52.10 53.06	14.20 14.47	52.04 53.00	14.43	51.97 52.94	14.66 14.93	54 55
56	54.09 55.06	14.49 14.75	54.03	14.73	53.96	14.70 14.97	53.90	15.20	56
57 58	56.02	15.01	54.99 55.96	14.99 15.26	54.93 55.89	15.23 15.50	54.86 55.82	15.47 15.74	57· 58
59 60	56.99 57.96	15.27 15.53	56.92 57.89	15.52 15.78	56.85 57.82	15.77 16.03	56.78 57.75	16.01 16.29	59 60
61	58.92	15.79	58.85	16.04	58.78	16.30	58.71	16.56	61
62 63	59.89 60.85	16.05 16.31	59.82 60.78	16.31 16.57	59.75 60.71	16.57 16.84	59.67 60.63	16.83 17.10	62 63
64	61.82	16.56	61.75	16.83	61.67	17.10	61.60	17.37	64
65 66	62.79 63.75	16.82 17.08	62.71 63.68	17.10 17.36	62.64 63.60	17.37 17.64	62.56 63.52	17.64 17.92	65 66
67	64.72 65.68	17.34 17.60	64.64	17.62	64.56	17.90	64.48	18.19	67
68 69	66.65	17.86	65.61 66.57	17.89 18.15	65.53 66.49	18.17 18.44	65.45 66.41	18.46 18.73	68 69
70	67.61	18.12	67.54	18.41	67.45	18.71	67.37	19.00	70
71 72	68.58 69.55	18.38 18.63	68.50 69.46	18.68 18.94	68.42 69.38	18.97 19.24	68.33 69.30	19.27 19.54	71 72
73	70.51	18.89	70.43	19.20	70.35	19.51	70.26	19.82	73
74 75	71.48 72.44	19.15 19.41	71.39 72.36	19.46 19.73	71.31 72.27	19.78 20.04	71.22 72.18	20.09 20.36	74 75
76	73.41	19.67	73.32	19.99	73.24	20.31	73.15	20.63	76
77	74.38 75.34	19.93 20.19	74.29 75.25	20.25	74.20 75.16	20.58 20.84	74.11 75.07	20.90 21.17	77
79	76.31	20.45	76.22	20.78	76.13	21.11	76.03	21.44	79
$\frac{80}{81}$	$\frac{77.27}{78.24}$	$\frac{20.71}{20.96}$	$\frac{77.18}{78.15}$	$\frac{21.04}{21.31}$	77.09	$\frac{21.38}{21.65}$	77.96	$\frac{21.72}{21.99}$	80
82	79 21	21.22	79.11	21.57	79.02	21.91	78.92	22.26	. 82
83 84	80.17 81.14	21.48 21.74	80.08	21.83 22.09	79.98 80.94	22.18 22.45	79.88 80.85	22.53 22.80	83 84
85	82.10	22.00	82.01	22.36	81.91	22.72	81.81	23.07	85
86 87	83.07 84.04	$22.26 \\ 22.52$	82.97 83.94	22.62 22.88	82.87 83.84	22.98 23.25	82.77 83.73	23.34 23.62	86 87
88	85.00	22.78	84.90	23.15	84.80	23.52	84.70	23.89	88
89 90	85.97 86.93	23.03 23.29	85.87	23.41 23.67	85.76 86.73	23.78 24.05	85.66 86.62	24.16 24.43	89 9 0
91	87.90	23.55	87.80	23.94	87.69	24.32	87.58	24.70	91
92 93	88.87	23.81 24.07	88.76	24.20 24.46	88.65 89.62	24.59 24.85	88.55 89.51	24.97 25.24	92 93
94	90.80	24.33	90.69	24.72	90.58	25.12	90.47	25.52	94
95 96	91.76 $ 92.73 $	24.59 24.85	91.65	24.99 25.25	91.54 92.51	25.39 25.65	91.43 92.40	25.79 26.06	95 96
97	93.69	25.11	93.58	25.51	93.47	25.92	93.36	26.33	97
98 99	94.66	25.36 25.62	94.55 95.51	25.78 26.04	94.44 95.40	26.19 26.46	94.32 95.28	26.60 26.87	98
100	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	75	Deg.	743	Deg.	74 <u>1</u>	Deg.	741	Deg.	Dist

Distance.	16	Deg.	16 1]	Dog.	16] 1	Deg.	167	Deg.	Distance.
58	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
3 4 4 5 5 6 7 8 8 9 9 10 11 12 13 13 14 15 16 16 17 18 19 20 23 24 25 26 27 28	0.96 1.92 2.88 3.85 5.77 6.73 8.65 9.61 10.57 11.54 12.50 13.48 16.34 16.34 17.30 18.26 19.23 20.19 20.19 22.11 22.11 23.07 24.03 24.99 25.95 26.92	0.28 0.55 0.83 1.10 1.38 1.65 1.93 2.21 2.48 2.76 3.03 3.31 3.58 3.86 4.13 4.41 4.96 5.24 5.79 6.34 6.89 7.17 7.44 7.72	0.96 1.92 2.88 3.84 5.76 6.768 8.64 9.60 10.56 11.52 12.48 13.44 11.52 12.48 18.24 19.20 12.20 20.16 21.12 22.08 23.04 24.00 24.96 25.92 26.88	0.28 0.56 0.84 1.12 1.68 1.968 2.24 2.52 2.80 3.36 3.36 3.44 4.70 4.48 4.70 5.88 6.16 6.44 6.72 7.28 7.58	0.96 1.92 2.88 3.84 4.79 5.75 6.71 7.67 8.63 9.59 10.55 11.51 12.46 13.42 14.38 16.30 17.26 18.22 19.18 20.14 21.09 22.05 23.97 24.93 25.89 25.85	0.28 0.58 1.14 1.42 1.70 1.99 2.27 2.84 3.12 3.12 3.43 4.54 4.83 5.11 5.68 5.96 6.25 6.25 6.25 7.10 8.27 7.98 7.98 7.98	0.96 1.92 2.67 3.83 4.79 5.75 6.70 7.66 8.62 9.58 10.53 11.49 12.45 13.41 14.36 15.32 16.28 17.24 18.19 19.15 20.11 21.07 22.02 22.98 23.94 24.90 25.85	0.29 0.58 0.86 1.15 1.73 2.02 2.88 3.17 3.46 3.75 4.03 4.90 5.48 5.76 6.05 6.34 6.63 6.92 7.49 7.78 8.07	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 24 22 25 26 27 28 28 28 28 28 28 28 28 28 28 28 28 28
30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50	27. 88 28. 84 29. 80 30. 76 31. 72 32. 64 34. 61 35. 57 36. 53 37. 49 38. 46 39. 41. 33 42. 30 43. 26 44. 22 45. 18 46. 14 47. 10 48. 06	7.99 8.27 8.54 9.10 9.37 10.25 11.03 11.38 11.58 11.85 12.13 12.46 12.95 13.23 13.51 13.78	27. 84 28. 80 29. 76 30. 72 31. 68 32. 64 33. 60 34. 56 35. 52 36. 48 37. 44 39. 36 40. 32 41. 28 42. 24 43. 20 44. 16 45. 12 46. 08 47. 04 48. 00	8.11 8.39 8.67 8.95 9.23 9.51 10.07 10.63 10.91 11.19 11.47 12.03 12.31 12.59 13.14 13.43 13.71 13.99	27.81 28.76 30.68 31.64 32.60 33.56 34.52 35.48 37.39 38.35 39.31 40.27 41.23 42.19 44.11 45.06 46.02 46.98 47.94	8.52 8.80 9.99 9.37 9.66 9.94 10.22 10.51 11.08 11.36 11.22 12.78 13.06 13.35 13.63 13.92 14.20	27.77 28.73 29.68 30.64 31.60 32.56 33.51 34.47 35.43 36.39 37.35 38.30 39.26 41.18 42.13 44.05 45.01 45.96 46.92 47.88	8.36 8.65 8.93 9.22 9.51 9.80 10.09 10.38 10.66 11.24 11.52 12.10 12.39 12.68 13.55 13.83 14.12 14.41	31 32 33 34 35 36 37 38 39 40 41 42 43 44 46 47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat. Deg.	Dep.	Lat.	73 1	Lat. Deg.	Distance.

Dist	16 I	Deg.	161	Deg.	$16\frac{1}{2}$	Deg.	163	Deg.	ופוע
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70	5
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99	5
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27	5
54	51.91	14.88	51.84	15.11 15.39	51.78 52.74	15.34	51.71	15.56	5
55	52.87	15.16	52.80	15.39	52.74	15.62	52.67	15.85	5
56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14	5
57 58	54.79	15.71 15.99	54.72 55.68	$15.95 \\ 16.23$	54.65	16.19 16.47	54.58	16.43 16.72	5
59	55.75 56.71	16.26	56.64	16.23	55.61	16.76	55.54 56.50	17.00	5
60	57.68	16.54	57.60	16.79	56.57	17.04	57.45	17.29	5
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58	6
62	59.60	17.09	59.52	17.35	59.45	17.61	59 37	17.87	6
63	60.56	17.37	60.48	17.35 17.63	60.41	17.89	59.37 60.33	17.87 18.16	6
64	61.52	17.64	61.44	17.91	61.36	18.18	61.28	18.44	6
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	6
66	63.44	18.19	63.36	18.47	63.28	18.74	63.20	19.02	6
67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31	6
68	65.37	18.74	65.28	19.03	65.20	19.31	65.11	19.60	6
69	66.33	19.02	66.24	19.31	66.16	19.60	66.07	19.89	6
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	7
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46	7
72 73	69.21	19.85	69.12	20.15	69.03	20.45	68.95	20.75	7
74	70.17	$\frac{20.12}{20.40}$	$70.08 \\ 71.04$	$20.43 \\ 20.71$	69.99	20.73	69.90	21.04 21.33	7
75	72.09	20.67	72.00	20.99	71.91	21.30	71.82	21.61	7
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	7
77	74.02	21.22	73.92	21.55	73.83	21.87	73.73	22.19	7
78	74.98	21.50	74.88	21.83	74.79	21.87 22.15	73.73 74.69	$\frac{22.48}{22.77}$	7
79	75.94	21.78	75.84	22.11	75.75	22:44	75.65	22.77	7
80	76.90	22.05	76.80	22.39	76.71	22.72	76.61	23.06	8
81	77.86	22.33	77.76	22.67	77.66	23.01	77.56	23.34	8
82	78.82	22.60	78.72 79.68	22.95	78.62	23.29	78.52	23.63	8
83	79.78	22.88	79.68	23.23	79.58	23.57	79.48	23.92	8
84	80.75	23.15 23.43	80.64	23.51	80.54	23.86	80.44	24.21	8
86	$81.71 \\ 82.67$	23 70	81.60	$23.79 \\ 24.07$	81.50 82.46	24.14 24.43	81.39	24.50	8
87	83.63	23.70 23.98	83.52	24.35	83.42	24.71	82.35 83.31	24.78 25.07	8
88	84.59	24.26	84.48	24.62	84.38	24.99	84.27	25.36	8
89	85.55	24.53	85.44	24.90	85 33	25.28	85.22	25.65	8
90	86.51	24.81	85.44 86.40	25.18	86.29	25.28 25.56	86.18	25.94	9
91	87.47	25.08	87.36	25.46	87.25	25.85	87.14	26.23	9
92	88.44	25.36	88.32	25.74	88.21	26.13	88.10	26.51	9
93	89.40	25.63	89.28	26.02	89.17	26.41	89.05	26.80	9
94	$90.36 \\ 91.32$	25.91	90.24	26.30	90.13	26.70	90.01	27.09	9
95 96	92.28	26.19 26.46	91.20 92.16	26.58	91.09 92.05	26.98	91.93	27.38 27.67	9
97	93.24	26.74	93.12	27.14	93.01	27.27	92.88	27.95	9
98	94.20	27.01	94.08	27.14 27.42	93.96	27.83	93.84	28.24	9
99	95.16	27.29	95.04	27.70	94.92	28.12	94.80	28.53	9
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	10
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
ista	77.7	1	703	n	Mai	n	Mol	D.	1
A	141	Deg.	134	Deg.	131	Deg.	- 734	Deg.	1 6

Distance	17	Deg.	171	Deg.	17½	Deg.	172	Deg.	Dist
1 8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4	0.96 1.91 2.87	0.29 0.58 0.88	0.95 1.91 ·2.87	0.30 0.59 0.89	0.95 1.91 2.86	0.30 0.60 0.90	0.95 1.90 2.86	0.30 0.61 0.31	1 2 3
5 6 7	3.83 4.78 5.74	1.17 1.46 1.75	3.82 4.78 5.73	1.19 1.48 1.78	3.81 4.77 5.72	1.20 1.50 1.80	3.81 4.76 5.71	1.22 1.52 1.83	4 5 6
8 9 10	6.69 7.65 8.61 9.56	2.05 2.34 2.63 2.92	6.69 7.64 8.60 9.55	2.08 2.37 2.67 2.97	6.68 7.63 8.58 9.54	2.10 2.41 2.71 3.01	6.67 7.62 8.57 9.52	2.13 2.44 2.74 3.05	7 8 9 10
11 12 13	10.52 11.48 12.43	3.22 3.51 3.80	10.51 11.46 12.42	3.26 3.56 3.85	10.49 11.44 12.40	3.31 3.61 3.91	10.48 11.43 12.38	3.35 3.66 3.96	11 12 13
14 15 16 17	13.39 14.34 15.30 16.26	4.09 4.39 4.68	13.37 14.33 15.28	4.15 4.45 4.74	13.35 14.31 15.26	4.21 4.51 4.81	13.33 14.29 15.24	4.27 4.57 4.88	14 15 16
18 19 20	17.21 18.17 19.13	4.97 5.26 5.56 5.85	16.24 17.19 18.15 19.10	5.04 5.34 5.63 5.93	16.21 17.17 18.12 19.07	5.11 5.41 5.71 6.01	16.19 17.14 18.10 19.05	5.18 5.49 5.79 6.10	17 18 19 20
21 22 23	20.08 21.04 21.99	6.14 6.43 6.72	20.06 21.01 21.97	6.23 6.52 6.82	20.03 20.98 21.94	6.31 6.62 6.92	20.00 20.95 21.91	6.40 6.71 7.01	21 22 23
24 25 26 27	22.95 23.91 24.86	7.02 7.31 7.60	22.92 23.88 24.83	7.12 7.41 7.71 8.01	22.89 23.84 24.80	7.22 7.52 7.82	22.86 23.81 24.76	7.32 7.62 7.93	24 25 26
28 29 30	25.82 26.78 27.73 28.69	7.89 8.19 8.48 8.77	25.79 26.74 27.70 28.65	8.30 8.60 8.30	25.75 26.70 27.66 28.61	8.12 8.42 8.72 9.02	25.71 26.67 27.62 28.57	8.23 8.54 8.84 9.15	27 28 29 30
31 32 33	29.65 30.60 31.56	9.06 9.36 9.65	29.61 30.56 31.52	9.19 9.49 9.79	29.57 30.52 31.47	9.32 9.62 9.92	29.52 30.48 31.43	9.45 9.76 10.06	31 32 33
34 35 36 37	32.51 33.47 34.43	9.94 10.23 10.53	32.47 33.43 34.38	10.08 10.38 10.68	32.43 33.38 34.33	10.22 10.52 10.83	32.38 33.33 34.29	10.37 10.67 10.98	34 35 36
38 39 40	35.38 36.34 37.30 38.25	10.82 11.11 11.40 11.69	35.34 36.29 37.25 38.20	10.97 11.27 11.57 11.86	35.29 36.24 37.19 38.15	11.13 11.43 11.73 12.03	35 24 36.19 37.14 38.10	11.28 11.58 11.89 12.19	37 38 39 40
41 42 43	39.21 40.16 41.12	11.99 12.28 12.57	39.16 40.11 41.07	12.16 12.45 12.75	39.10 40.06 41.01	12.33 12.63 12.93	39.05 40.00 40.95	12.50 12.80 13.11	41 42 43
44 45 46	42.08 43.03 43.99	12.86 13.16 13.45	42.02 42.98 43.93	13.05 13.34 13.64	41.96 42.92 43.87	13.23 13.53 13.83	41.91 42.86 43.81	13.41 13.72 14.02	44 45 46
47 48 49 50	44.95 45.90 46.86 47.82	13.74 14.03 14.33 14.62	44.89 45.84 46.80 47.75	13.94 14.23 14.53 14.83	44.82 45.78 46.73 47.69	14.13 14.43 14.73 15.04	44.76 45.71 46.67 47.62	14.33 14.63 14.94 15.24	47 48 49 50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance	73 1	Deg.	72}	Deg.	72 <u>1</u>	Deg.	721	Deg.	Distance.

Dist	17 I	Deg.	174	Deg.	171	Deg.	173	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	48.77	14.91 15.20	48.71 49.66	15.12 15.42	48.64 49.59	15.34 15.64	48.57	15.55 15.85	51 52
53	49.73 50.68	15.50	50.62	15.72	50.55	15.94	50.48	16.16	53
54	51.64	15.79	51.57	16.01	51.50	16.24	51.43	16.46	54
55	52.60	16.08 16.37	52.53 53.48	16.31 16.61	52.45 53.41	16.54 16.84	52.38 53.33	$16.77 \\ 17.07$	55
57	54.51	16.67	54.44	16.90	54.36	17.14	54.29	17.38	57
58	55.47	16.96	55.39	17.20	55.32	17.44 17.74	55.24	17.68	58
59 60	56.42 57.38	17.25 17.54	56.35 57.30	$17.50 \\ 17.79$	56.27 57.22	18.04	56.10 57.14	17.99 18.29	59
61	58.33	17.83	58.26	18.09	58.18	18.34	58.10	18.60	61
62	59.29	18.13	59.21	18.39	59.13	18.64	59.05	18.90	62
63	60.25	18.42	60.17	18.68	60.08	18.94	60.00	19.21	63
64 65	61.20 62.16	18.71 19.00	61.12 62.08	$18.98 \\ 19.28$	61.04	19.25 19.55	60.95	19.51 19.82	64
66	63.12	19.30	63.03	19.57	62.95	19.85	62.86	20.12	66
67	64.07	19.59	63.99	19.87	63.90	20.15	63.81	20.43	67
68	65.03	19.88	$64.94 \\ 65.90$	$20.16 \\ 20.46$	64.85	20.45	$64.76 \\ 65.72$	20.73 21.04	68
70	66.94	20.47	66.85	20.76	66.76	21.05	66.67	21.34	70
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65	71
72	68.85	21.05	68.76	21.35	68.67	21.65	68.57	21.95	72
73 74	69.81	21.34 21.64	$69.72 \\ 70.67$	21.65	69.62 70.58	21.95 22.25	69.52	22.26 22.56	74
75	71.72	21.93	71.63	22.24	71.53	22.55	71.43	22.86	75
76	72.68	22.22	72.58	22.54	72.48	22.85	72.38	23.17	76
77	73.64 74.59	$22.51 \\ 22.80$	73.54 74.49	22.83 23.13	73.44 74.39	23.46	73.33 74.29	23.78	78
79	75.55	23.10	75.45	23.43	75.34	$23.76 \\ 24.06$	75.24	24.08	79
80	76.50	23.39	76.40	23.72	76.30		76.19	24.39	80
81	77.46	23.68	77.36	$24.02 \\ 24.32$	77.25	$24.36 \\ 24.66$	77.14 78.10	24.69 25.00	81
82 83	78.42	23.97	78.31	24.61	78.20	25.96	79.05	25.30	83
84	79.37	24.56	79.27 80.22	24.91	80.11	25.26	80.00	25.61	84
85 86	81.29	24.85	81.18	25.21 25.50	81.07	25.56 25.86	80.95	25.91 26.22	88
87	82.24 83.20	25.44	82.13 83.09	25.80	82.97	26.16	82.86	26.52	8
88	84.15	25.73	84.04	26.10	83.93	26.46	83.81	26.83	88
89	85.11	26.02 26.31	85.00 85.95	26.39	84.88	26.76 27.06	84.76 85.72	27.13	89
$\frac{90}{91}$	87.02	26.61	86.91		86.79	27.36	86.67	27.74	9
92	87.98	26.90	87.86	26.99 27.28	87.74	27.66	87.62	28.05	95
93	88.94	27.19	88.82	27.58	88.70	27.97	88.57	28.35	9:
94 95	89.89	27.48	89.77 90.73	27.87	89.65	28.27	89.53 90.48	28.66 28.96	9.
96	91.81	27.48 27.78 28.07	91.68	28.47	91.56	28.87	91.43	29.27	9
97	92.76 93.72	28.36	92.64	28.76	92.51	29.17	92.38	29.57	9
98	93.72	28.65 28.94	93.59 94.55	29.06 29.36	93.46 94.42	29.47 29.77	93.33 94.29	29.88	9
100	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	10
-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	904
Distance.	73	Deg.	723	Deg.	721	Deg.	721	Deg.	Distance

Distance	18	Deg.	184	Deg.	181	Deg.	18}	Deg.	Distance.
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	8
23 34 4 5 6 6 7 7 8 9 10 11 12 13 14 16 16 17 8 19 20 22 23 34 36 27 28 33 34 35 36 36 37	1.41. 0.95 1.90 2.85 3.80 4.76 6.66 7.61 8.56 9.51 10.46 11.41 11.2.36 13.31 14.2.3 16.17 17.12 18.07 19.02 19.92 21.87 22.88 24.73 25.66 28.53 27.58 28.53 29.48 30.43 31.38 31.38 31.38 32.56 32.56 33.38 34.24 35.19 36.38 36.38 37.58 38.38 39.48 3	0.31 0.69 0.93 1.24 1.55 2.16 2.47 2.78 3.09 3.40 4.63 4.63 4.94 5.25 5.87 6.18 6.80 7.11 7.42 8.93 8.94 9.27 9.28 9.28 9.28 9.28 9.28 9.28 9.28 9.28	1.44. 0.95 1.90 2.85 3.80 4.75 5.70 6.65 9.50 10.45 11.40 11.2.35 13.30 14.23 15.20 16.14 17.09 18.04 18.99 11.84 22.79 23.74 24.69 25.56 27.54 28.49 29.44 30.39 31.34 29.44 30.39 31.34 34.19 35.11	0.31 0.63 1.25 1.57 1.88 2.19 2.51 3.44 3.74 4.38 4.07 4.38 5.01 5.32 6.26 6.58 7.52 6.26 6.89 7.20 7.52 8.14 8.47 9.39 9.39 9.71 10.02 10.03 10.96 11.25 11.59	Lat. 0.95 1.90 2.84 3.79 4.74 5.69 8.53 9.48 10.43 11.38 12.33 13.28 14.22 15.17 16.12 17.07 18.02 18.97 19.91 20.86 21.81 22.76 23.71 24.66 23.71 24.66 25.60 28.45 27.50 28.45 31.29 30.35 31.29 32.24 33.19 34.14	0.32 0.635 1.27 1.59 1.90 2.22 2.54 3.17 3.49 3.817 4.12 4.44 4.44 4.44 4.5.08 5.39 6.35 6.66 6.98 7.69 8.25 8.57 9.52 9.52 9.52 9.52 10.15 10.79 11.11 11.74	1.31 1.32 1.33 1.34 1.33 1.34 1.31 1.3.26 1.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.26 1.3.31 1.3.	0.32 0.64 0.96 1.29 1.61 1.93 2.25 2.87 3.54 3.54 4.50 4.18 4.50 4.18 6.75 6.11 6.43 6.77 7.39 7.71 8.36 8.68 8.68 8.68 8.68 9.32	1 2 3 4 4 5 6 6 7 8 9 10 11 2 13 14 5 16 17 8 19 20 1 22 23 24 25 26 27 28 29 30 31 32 23 33 4 35 6 36 37
38 39 40 41 42 43 44 45 46 47 48 49 50	36.14 37.09 38.04 38.99 39.94 40.90 41.85 42.80 43.75 44.70 45.65 46.60 47.55 Dep.	11.74 11.74 12.05 12.36 12.67 12.98 13.29 13.60 13.91 14.52 14.52 14.83 15.14 15.45	36.09 37.04 37.99 38.94 39.89 40.84 41.79 42.74 43.69 44.64 45.59 46.54 47.48 Dep.	11.90 11.90 12.21 12.53 12.84 13.15 13.47 13.78 14.09 14.41 14.72 15.03 15.35 15.66	36.04 36.98 37.93 38.88 39.83 40.78 41.73 42.67 43.62 44.57 45.52 46.47 47.42 Dep.	12.06 12.37 12.69 13.01 13.33 13.64 13.96 14.28 14.60 14.91 15.23 15.55 15.87	35.98 36.93 37.88 38.82 39.77 40.72 41.66 42.61 43.56 44.51 45.45 46.40 47.35 Dep.	12.21 12.24 12.86 13.18 13.50 13.82 14.14 14.46 15.11 15.43 15.75 16.07 Lat.	38 39 40 41 42 43 44 45 46 47 48 49 50
Distance	72 I	Deg.	713	Deg.	711/2	Deg.	711	Deg.	Distance.

Dist	18 I	Deg.	184	Deg.	181	Deg.	183	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	48.50	15.76	48.43	15.97	48.36	16.18	48.29	16.39	51
52	49.45	16.07	$\frac{49.38}{50.33}$	16.28	49.31	16.50	49.24	16.71 17.04	52
53	50.41	16.38		16.60	50.26	16.82	50.19	17.04	53
54	51.36	16.69	51.28	16.91	51.21	17.13	51.13	17.36	54
55	52.31	17.00	52.23	17.22 17.54	52.16	17.45	52.08	17.68	55 56
56	53.26	17.30	53.18	17.54	53.11	17.77	53.03	18.00 18.32	57
57	54.21	17.61	54.13 55.08	17.85	54.05 55.00	18.40	53.98 54.92	18.64	58
58 59	55.16 56.11	17.92 18.23	56.03	18.48	55.95	18.72	55.87	18.96	59
60	57.06	18.54	56.98	18.79	56.90	19.04	56.82	19.29	60
61	58.01	18 85	57.93	19.10	57.85	19.36	57.76	19.61	61
62	58.97	19.16	58.88	19.42	58.80	19.67	58.71	19.93	62
63	59.92	19.47	59.83	19.73	59.74	19.99	59.66	20.25	63
64	60.87	19.47 19.78	60.78	20.04	60.69	20.31	60.60	20.57	64
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.89	65
66	62.77	20.40	62.68	20.67	62.59	20.94	62.50	21.22	66
67	63.72	20.70	63.63	20.98	63.54	21.26	63.44	21.54	68
68	64.67	21.01	64.58	21.30	64.49 65.43	21.58 21.89	64.39	21.86 22.18	69
69 70	65.62	21.32 21.63	65.53	$21.61 \\ 21.92$	66.38	22.21	66.29	22.50	70
* 12 2 1 2 m	2000	100	-		-	22.53	67.23	22.82	71
71	67.53	21.94	67.43	22.23 22.55	67.33 68.28	22.85	68.18	23.14	72
72 73	68.48	22.25 22.56	69.33	22.86	69.23	23.16	69.13	23.47	73
74	70.38	22.87	70.28	23.17	70.18	23.48	70.07	23.79	74
75	71.33	23.18	71.23	23.49	71.12	23.80	71.02	24.11	75
76	72.28	23.49	72.18	23.80	72.07	24.12	71.97	24.43	76
77	73.23	23.79	73.13	24.11	73.02	24.43	72.91	24.75	77
78	74.18	24.10	74.08	24.43	73.97	24.75	73.86	25.07	78
79	75.13	24.41	75.03	24.74	74.92	25.07	74.81	25.39 25.72	79 80
80	76.08	24.72	75.98	25.05	75.87	25.38	75.75		81
81	77.04	25.03	76.93	25.37	76.81	25.70 26.02	76.70 77.65	26.04 26.36	82
82 83	77.99 78.94	25.34 25.65	77.88	25.68	77.76 78.71	26.34	78.60	26.68	83
84	79.89	25.96	79.77	25.99 26.31	79.66	26.65	79.54	27.00	84
85	80.84	26.27	80.72	26.62	80.61	26.97	80.49	27.32	85
. 86	81.79	26.58	81.67	26.93	81.56	27.29	81.44	27.64	86
87	82.74	26.88	82.62	27.25	82.50	27.61	82.38	27.97	87
88	83.69	27.19	83.57	27.56	83.45	27.92	83.33	28.29	88
89	84.64	27.50	84.52	27.87	84.40	28.24 28.56	84.28	28.61 28.93	90
90	85.60	27.81	85.47	28.18	85.35		_	-	91
91	86.55	28.12	86.42	28.50	86.30 87.25	28.37 29.19	86.17	29.25 29.57	92
92	87.50	28.43	87.37	28.81 29.12	87.25	29.19	88.06	29.89	93
93 94	88.45	28.74 29.05	89 27	29.12	89.14	29.83	89.01	30.22	94
95	90.35	29.36	90.22	29.75	90.09	30.14	89.96	30.54	95
96	91.30	29.67	91.17	30.06	91.04	30.46	90.91	30.86	96
97	92.25	29.97	92.12	30.38	91.99	30.78	91.85	31.18	97
98	93.20	30.28	93.07	30.69	92.94	31.10	92.80	31.50	98
99	94.15	30.59	94.02	31.00	93.88	31.41 31.73	93.75 94.69	31.82	100
100	95.11 Dep.	30.90 Lat.	94.97 Dep.	31.32 Lat.	94.83 Dep.	Lat.	Dep.	Lat.	
Distance.	Dep.	Lace	- Dop.	1 200					Distance.
18	79	Deg.	713	Deg.	711	Deg.	713	Deg.	0

Distance.	: 19 I	og.	19 1	Deg.	19½	Deg.	19‡	Deg.	Distance.
į.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2 3 4 5 6 7 8 9	0.95 1.89 2.84 3.78 4.73 5.67 6.62 7.56 8.51 9.46	0.33 0.65 0.98 1.30 1.63 1.95 2.28 2.60 2.93	0.94 1.89 2.83 3.78 4.72 5.66 6.61 7.55 8.50 9.44	0.33 0.66 0.99 1.32 1.65 1.98 2.31 2.64 2.97	0.94 1.89 2.83 3.77 4.71 5.66 6.60 7.54 8.48 9.43	0.33 0.67 1.00 1.34 1.67 2.00 2.34 2.67 3.00 3.34	0.94 1.88 2.82 3.76 4.71 5.65 6.59 7.53 8.47 9.41	0.34 0.68 1.01 1.35 1.69 2.03 2.37 2.70 3.04 3.38	1 2 3 4 5 6 7 8 9
11 12 13 14 15 16 17 18 19	10.40 11.35 12.29 13.24 14.18 15.13 16.07 17.02 17.96	3.58 3.91 4.23 4.56 4.88 5.21 5.53 5.86 6.19	10.38 11.33 12.27 13.22 14.16 15.11 16.05 16.99 17.94	3.63 3.96 4.29 4.62 4.95 5.28 5.60 5.93 6.26	10.37 11.31 12.25 13.20 14.14 15.08 16.02 16.97 17.91	3.67 4.01 4.34 4.67 5.01 5.34 5.67 6.01 6.34	10.35 11.29 12.24 13.18 14.12 15.06 16.00 16.94 17.88	3.72 4.06 4.39 4.73 5.07 5.41 5.74 6.08	11 12 13 14 15 16 17 18 19
20 21 22 23 24 25 26 27 28 29	18.91 19.86 20.80 21.75 22.69 23.64 24.58 25.53 26.47 27.42 28.37	6.51 6.84 7.16 7.49 7.81 8.14 8.46 8.79 9.12 9.44 9.77	18.88 19.83 20.77 21.71 22.66 23.60 24.55 25.49 26.43 27.38 28.32	6.59 6.92 7.25 7.58 7.91 8.24 8.57 8.90 9.23 9.56 9.89	18.85 19.80 20.74 21.68 22.62 23.57 24.51 25.45 26.39 27.34 28.28	7.01 7.34 7.68 8.01 8.35 8.68 9.01 9.35 9.68 10.01	18.82 19.76 20.71 21.65 22.59 23.53 24.47 25.41 26.35 27.29 28.24	6.76 7.10 7.43 7.77 8.11 8.45 8.79 9.12 9.46 9.80 10.14	20 21 22 23 24 25 26 27 28 29 30
31 32 33 84 35 36 37 38 39 40	29.31 30.26 31.20 32.15 33.09 34.04 34.98 35.93 36.88 37.82	10.09 10.42 10.74 11.07 11.39 11.72 12.05 12.37 12.70 13.02	29.27 30.21 31.15 32.10 33.04 33.99 34.93 85.88 36.82 37.76	10.22 10.55 10.88 11.21 11.54 11.87 12.20 12.53 12.86 13.19	29.22 30.16 31.11 32.05 32.99 33.94 34.88 35.82 36.76 37.71	10.35 10.68 11.02 11.35 11.68 12.02 12.35 12.68 13.02 13.35	29.18 30.12 31.06 32.00 32.94 33.88 34.82 35.76 36.71 37.65	10.48 10.81 11.15 11.49 11.83 12.17 12.50 12.84 13.18 13.52	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	38.77 39.71 40.66 41.60 42.55 43.49 44.44 45.38 46.33 47.28	13.35 13.67 14.00 14.92 14.65 14.98 15.90 15.63 15.95 16.28	38.71 39.65 40.60 41.54 42.48 43.43 44.37 45.32 46.26 47.20	13.52 13.85 14.18 14.51 14.84 15.17 15.50 15.83 16.15 16.48	38.65 39.59 40.53 41.48 42.42 43.36 44.30 45.25 46.19 47.13	13.69 14.02 14.35 14.69 15.02 15.36 15.69 16.02 16.36 16.69	38.59 39.53 40.47 41.41 42.35 43.29 44.24 45.18 46.12 47.06	13.85 14.19 14.53 14.87 15.21 15.54 15.88 16.22 16.56 16.90	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat. Deg.	Dep. 701	Lat. Deg.	Dep.	Lat.	Dep.	Lat. Deg.	Distance.

Dis	19 D	eg.	191	Deg.	$19\frac{1}{2}$	Deg.	19¾ I	eg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
-	48.22	16.60	48.15	16.81	48.07	17.02	48.00	17.23	51
52	49.17	16.93	49.09	17.14	49.02	17.36 17.69	48.94	17.57 17.91	52
53	50.11 51.06	17.26 17.58	50.04	17.47	49.96	17.69	49.88	17.91	53
54	51.06	17.58	50.98	17.80 18.13	50.90	18.03	50.82	18.25	54
55	52.00	17.91	51.92		51.85	18.36	51.76	18.59 18.92	55 56
56	52.95	18.23	52.87	18.46	52.79	18.69	52.71	19.26	57
57	53.89	18.56	53.81	18.79 19.12	53.73	19.03	53.65 54.59	19.60	58
58	54.84	18.88	54.76 55.70	19.12	54.67 55.62	19.36 19.69	55.53	19.94	59
59	55.79 56.73	19.21 19.53	56.65	19.78	56.56	20.03	56.47	20.27	60
		19.86	57.59	20.11	57.50	20.36	57.41	20,61	61
61	57.68 58.62	20.19	58.53	20.44	58.44	20.30	58.35	20.95	62
62 63	59.57	20.51	59.48	20.77	59.39	20.70 21.03	59.29	21.29	63
64	60.51	20.84	60.42	21.10	60.33	21.36	60.24	21,63	64
65	61.46	21.16	61.37	21 43	61.27	21.70	61.18	21.96	65
66	62.40	21.16 21.49	62.31	21.76	62.21	22.03	62.12	22.30	66
67	63.35	21.81	63.25	22.09	63.16	22.37	63.06	22.64	67
68	64.30	22.14	64.20	22.42	64.10	22.70	64.00	22.98	68
69	65.24	22.46	65.14	22.75	65.04	23.03	64.94	23.32	69
70	66.19	22.79	66.09	23.08	65.98	23.37	65.88	23.65	
71	67.13	23.12	67.03	23.41	66.93	23.70	66.82	23.99 24.33	7
72	68.08	23.44	67.97	23.74	67.87	24.03	67.76	24.67	7:
73	69.02	23.77	68.92	24.07	68.81	24.37	68.71	25.01	7
74	69.97	24.09	69.86	24.40 24.73	69.76	25.04	70.59	25.34	7
75	70.91	24.42	71.75	25.06	71.64	25.37	71.53	25.68	7
77	72.80	24.74 25.07	72.69	25.39	72.58	25.70	72.47	26.02	7
78	73.75	25.39	72.69 73.64	25.72	73.53	26,04	73.41	26.36	78
79	74.70	25.72	74.58	26.05	74.47	26.37	74.35	26.70	7
80	75.64	26.05	75.53	26.38	75.41	26.70	75.29	27.03	8
81	76.59	26.37	76.47	26.70	76.35	27.04	76.24	27,37	8
82	77.53	26.70	77.42	27.03 27.36	77.30	27.37 27.71	77.18	27.71	8
83	78.48	27.02	78.36	27.36	78.24	27.71	78.12	28.05	8
84	79.42 80.37	27.35 27.67	79.30	27.69	79.18	28.04	79.06	28.72	8
85		27.67	80.25 81.19	28.02 28.35	80.12 81.07	28.37 28.71	80.00	29.06	8
86	81.31	28.00	81.19	28.35	81.07	29.04	81.88	29.40	8
87	82.26	28.32 28.65	82.14 83.08	29.01	82.01 92.95		82.82	29.74	8
88	84.15	28.98	84.02	29.34	83.90	29.71	83.76	30.07	8
90	85.10	29.30	84.97	29.67	84.84	30.04	84.71	30.41	9
91	86.04	29.63	85.91	30.00	85.78		85.65	30.75	9
92	86.99	29.95	86.86	30.33	86.72	30.71	86.59	31.09	9
93	87.93	30.28	87.80	30.66	87.67	31.04	87.53	31.43	9
94	88.88	30.60	87.80 88.74	30.99	88.61	31.38	88.47	31.76	9
95	89.82	30.93	89.69	31.32	89.55	31.71	89.41	32.10	9
96	90.77	31.25	90.63	31.65	90.49	32.05	90.35	32.44 32.78	9
97	91.72	31.58	91.58		91.44	32.38	91.29	33.12	9
98	92.66	31.91	92.52		92.38			33.45	9
99	93.61	32.23	93.46						10
100	94.55 Dep.	Lat.	Dep.		Dep.	-	Dep.	Lat.	
Distance.	-	Deg.		Deg.	-	Deg.	701	Deg.	Distance

Distance.	20	Deg.	201	Deg.	201	Deg.	20}	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5	0.94 1.88 2.82 3.76 4.70	0.34 0.68 1.03 1.37 1.71 2.05	0.94 1.88 2.81 3.75 4.69 5.63	0.35 0.69 1.04 1.38 1.73 2.08	0.94 1.87 2.81 3.75 4.68 5.62	0.85 0.70 1.05 1.40 1.75 2.10	0.94 1.87 2.81 3.74 4.68 5.61	0.35 0.71 1.06 1.42 1.77 2.13	1 2 3 4 5
7 8 9 10 11	5.64 6.58 7.52 8.46 9.40	2.39 2.74 3.08 3.42 3.76	6.57 7.51 8.44 9.38	2.42 2.77 3.12 3.46 3.81	6.56 7.49 8.43 9.37	2.45 2.80 3.15 3.50 3.85	6.55 7.48 8.42 9.35	2.48 2.83 3.19 3.54 3.90	7 8 9 10
12 13 14 15 16	11.28 12.22 13.16 14.10 15.04	4.10 4.45 4.79 5.13 5.47	11.26 12.20 13.13 14.07 15.01	4.15 4.50 4.85 5.19 5.54	11.24 12.18 13.11 14.05 14.99	4.20 4.55 4.90 5.25 5.60	11.22 12.16 13.09 14.03 14.96	4.25 4.61 4.96 5.31 5.67	12 13 14 15 16
17 18 19 20 21	15.97 16.91 17.85 18.79	5.81 6.16 6.50 6.84 7.18	15.95 16.89 17.83 18.76	5.88 6.23 6.58 6.92 7.27	15.92 16.86 17.80 18.73	5.95 6.30 6.65 7.00 7.35	15.90 16.83 17.77 18.70	6.02 6.38 6.73 7.09 7.44	17 18 19 20 21
22 23 24 25 26 27	20.67 21.61 22.55 23.49 24.43 25.37	7.52 7.87 8.21 8.55 8.89 9.23	20.64 21.58 22.52 23.45 24.39 25.33	7.61 7.96 8.31 8.65 9.00 9.35	20.61 21.54 22.48 23.42 24.35 25.29	7.70 8.05 8.40 8.76 9.11 9.46	20.57 21.51 22.44 23.38 24.31 25.25	7.79 8.15 8.50 8.86 9.21 9.57	22 23 24 25 26 27
28 29 30 31 32	26.31 27.25 28.19 29.13	9.58 9.92 10.26	26.27 27.21 28,15 29.08 30.02	9.69 10.04 10.38 10.73	26.23 27.16 28.10 29.04	9.81 10.16 10.51 10.86	26.18 27.12 28.05 28.99	$\begin{array}{r} 9.92 \\ 10.27 \\ 10.63 \\ \hline 10.98 \end{array}$	28 29 30 31
33 34 35 36 37	30.07 31.01 31.95 32.89 33.83 34.77	10.94 11.29 11.63 11.97 12.31 12.65	30.02 30.96 31.90 32.84 33.77 34.71	11.08 11.42 11.77 12.11 13.46 12.81	29.97 30.91 31.85 32.78 33.72 34.66	11.21 11.56 11.91 12.26 12.61 12.96	29.92 30.86 31.79 32.73 33.66 34.60	11.34 11.69 12.05 12.40 12.75 13.11	32 33 34 35 36 37
38 39 40 41 42	35.71 36.65 37.59 38.53 39.47	13.00 13.34 13.68 14.02	35.65 36.59 37.53 38.47 39.40	13.15 13.50 13.84 14.19 14.54	35.59 36.53 37.47 38.40 39.34	13.31 13.66 14.01 14.36 14.71	35.54 36.47 37.41 38.34 39.28	13.46 13.82 14.17 14.53 14.88	38 39 40 41 42
43 44 45 46 47 48	40.41 41.35 42.29 43.23 44.17 45.11	14.71 15.05 15.39 15.73 16.07	40.34 41.28 42.22 43.16 44.09 45.03	14.88 15.23 15.58 15.92 16.27	40.28 41.21 42.15 43.09 44.02 44.96	15.06 15.41 15.76 16.11 16.46	40.21 41.15 42.08 43.02 43.95 44.89	15.23 15.59 15.94 16.30 16.65	43 44 45 46 47
Distance. 95	46.04 46.98 Dep.	16.76 17.10 Lat.	45.97 46.91 Dep.	16.61 16.96 17.31 Lat.	45.90 46.83 Dep.	16.81 17.16 17.51 Lat.	45.82 46.76 Dep.	17.36 17.71 Lat.	Distance. 988
Ä	70	Deg.	694	Deg.	69 <u>}</u>	Deg.	691	Deg.	Dist

Dist	20]	Deg	201	Deg.	201	Deg.	201	Deg.	Dist
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance
51 52 53 54 55 56 57 58 59 60	47.92 48.86 49.80 50.74 51.68 52.62 53.56 64.50 55.44 56.38	17.44 17.79 18.13 18.47 18.81 19.15 19.50 19.84 20.18 20.52	47.85 48.79 49.72 50.66 51.60 52.54 53.48 54.42 55.35 56.29	17.65 18.00 18.34 18.69 19.04 19.38 19.73 20.07 20.42 20.77	47.77 48.71 49.64 50.58 51.52 52.45 53.39 54.33 55.26 56.20	17.86 18.21 18.56 18.91 19.26 19.61 19.96 20.31 20.66 21.01 21.36	47.69 48.63 49.56 50.50 51.43 52.37 53.30 54.24 55.17 56.11 57.04	18.07 18.42 18.78 19.13 19.49 19.84 20.19 20.55 20.90 21.26 21.61	51 52 53 54 55 56 57 58 59 60 61
62 63 64 65 66 67 68 69 70	58.26 59.20 60.14 61.08 62.02 62.96 63.90 64.84 65.78	21.21 21.55 21.89 22.23 22.57 22.92 23.26 23.60 23.94	58.17 59.11 60.04 60.98 61.92 62.86 63.80 64.74 65.67	21.46 21.81 22.15 22.50 22.84 23.19 23.54 23.88 24.23	58.07 59.01 59.95 60.88 61.82 62.76 63.69 64.63 65.57	21.71 22.06 22.41 22.76 23.11 23.46 23.81 24.16 24.51	57.98 58.91 59.85 60.78 61.72 62.65 63.59 64.52 65.46	21.97 22.32 22.67 23.03 23.38 23.74 24.09 24.45 24.80	62 63 64 65 66 67 68 69 70
71 72 73 74 75 76 77 78 79 80	66.72 67.66 68.60 69.54 70.48 71.42 72.36 73.30 74.24 75.18	24.28 24.63 24.97 25.31 25.65 25.99 26.34 26.68 27.02	66.61 67.55 68.49 69.43 70.36 71.30 72.24 73.18 74.12	24.57 24.92 25.27 25.61 25.96 26.30 26.65 27.00 27.34	66.50 67.44 68.38 69.31 70.25 71.19 72.12 73.06 74.00	24.86 25.21 25.57 25.92 26.27 26.62 26.97 27.32 27.67	66.39 67.33 68.26 69.20 70.14 71.07 72.01 72.94 73.88	25.15 25.51 25.86 26.22 26.57 26.93 27.28 27.63 27.99	71 72 73 74 75 76 77 78 79
81 82 83 84 85 86 87 88 89	76.12 77.05 77.99 78.93 79.87 80.81 81.75 82.69 83.63 84.57	27.36 27.70 28.05 28.39 28.73 29.07 29.41 29.76 30.10 30.44 30.78	75.06 75.99 76.93 77.87 78.81 79.75 80.68 81.62 82.56 83.50 84.44	27.69 28.04 28.38 28.73 29.07 29.42 29.77 30.11 30.46 30.80 31.15	74.93 75.87 76.81 77.74 78.68 79.62 80.55 81.49 82.43 83.36 84.30	28.02 28.37 28.72 29.07 29.42 29.77 30.12 30.47 30.82 31.17 31.52	74.81 75.75 76.68 77.62 78.55 79.49 80.42 81.36 82.29 83.23 84.16	28.34 28.70 29.05 29.41 29.76 30.11 30.47 30.82 31.18 31.53 31.89	80 81 82 83 84 85 86 87 88 89
91 92 93 94 95 96 97 98 99 100	85.51 86.45 87.39 88.33 89.27 90.21 91.15 92.09 93.03 93.97	31.12 31.47 31.81 32.15 32.49 32.83 33.18 33.52 33.86 34.20	85.38 86.31 87.25 88.19 89.13 90.07 91.00 91.94 92.88 93.82	31.50 31.84 32.19 32.54 32.88 33.23 33.57 33.92 34.27 34.61	85.24 86.17 87.11 88.05 88.98 89.92 90.86 91.79 92.73 93.67	31.87 32.22 32.57 32.92 33.27 33.62 33.97 34.32 34.67 35.02	85.10 86.03 86.97 87.90 88.84 89.77 90.71 91.64 92.58 93.51	32.24 32.59 32.95 33.30 33.66 34.01 34.37 34.72 35.07 35.43	91 92 93 94 95 96 97 98 99 100
Distance.	Dер. 70 I	Lat.	Dep.	Lat. Deg.	Dep. 69½	Lat. Deg.	Dep.	Lat. Deg.	Distance.

Dist	21	Dog.	211	Deg.	21 <u>1</u>	Deg. '	211	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	tance.
1	0.93	0.36	0.93	0.36	0.93	0.37	0.93	0.37	1
2	1.87	0.72	1.86	0.72	1.86	0.73	1.86	0.74	2
3	2.80	1.08	2.80	1.09	2.79	1.10	2.79	1.11	3
4	3.73	1.43	3.73	1.45	3.72	1.47	3.72	1.48	4
5	4.67	1.79	4.66	1.81	4.65	1.83	4.64	1.85	5
6	5.60	2.15	5.59	2.17	5.58	2.20	5.57	2.22	6
7	6.54	2.51	6.52	2.54	6.51	2.57	6.50	2.59	7
8	7.47	2.87	7.46	2.90	7.44	2.93	7.43	2.96	8
9	8.40	3.23	8.39	3.26	8.37	3.30	8.36	3.34	9
10	9.34	3.58	9.32	3.62	9.30	3.67	9.29	3.71	10
12	11.20	4.30	11.18	4.35	11.17	4.40	11.15	4.45	12
13	12.14	4.66	12.12	4.71	12.10	4.76	12.07	4.82	13
14	13.07	5.02	13.05	5.07	13.03	5.13	13.00	5.19	14
15	14.00	5.38	13.98	5.44	13.96	5.50	13.93	5.56	15
16	14.94	5.73	14.91	5.80	14.89	5.86	14.86	5.93	16
17	15.87	6.09	15.84	6.16	15.82	6.23	15.79	6.30	17
18	16.80	6.45	16.78	6.52	16.75	6.60	16.72	6.67	18
19	17.74	6.81	17.71	6.89	17.68	6.96	17.65	7.04	19
20	18.67	7.17	18.64	7.25	18.61	7.33	18.58	7.41	20
21	19.61	7.53	19.57	7.61	19.54	7.70	19.50	7.78	21
22	20.54	7.88	20.50	7.97	20.47	8.06	20.43	8.15	22
23 24 25 26 27 28 29 30	21.47 22.41 23.34 24.27 25.21 26.14 27.07 28.01	8.24 8.60 8.96 9.32 9.68 10.03 10.39 10.75	21.44 22.37 23.30 24.23 25.16 26.10 27.03 27.96 28.89	8.34 8.70 9.06 9.42 9.79 10.15 10.51 10.87	21.40 22.33 23.26 24.19 25.12 26.05 26.98 27.91 28.84	8.43 8.80 9.16 9.53 9.90 10.26 10.63 11.00	21.36 22.29 23.22 24.15 25.08 26.01 26.94 27.86	8.52 8.89 9.26 9.63 10.01 10.38 10.75 11.12	23 24 25 26 27 28 29 30
32	29.87	11.47	29.82	11.60	29.77	11.73	29.72	11.86	32
33	30.81	11.83	30.76	11.96	30.70	12:09	30.65	12.23	33
34	31.74	12.18	31.69	12.32	31.63	12.46	31.58	12.60	34
35	32.68	12.54	32.62	12.69	32.56	12.83	32.51	12.97	35
36	33.61	12.90	33.55	13.05	33.50	13.19	33.44	13.34	36
37	34.54	13.26	34.48	13.41	34.43	13.56	34.37	13.71	37
38	35.48	13.62	35.42	13.77	35.36	13.93	35.29	14.08	38
39	36.41	13.98	36.35	14.14	36.29	14.29	36.22	14.45	39
40	37.34	14.33	37.28	14.50	37.22	14.66	37.15	14.82	40
41	38.28	14.69	38.21	14.86	38.15	15.03	38.08	15.19	41
42	39.21	15.05	39.14	15.22	39.08	15.39	39.01	15.56	42
43	40.14	15.41	40.08	15.58	40.01	15.76	39.94	15.93	43
44	41.08	15.77	41.01	15.95	40.94	16.13	40.87	16.30	44
45	42.01	16.13	41.94	16.31	41.87	16.49	41.80	16.68	45
46	42.94	16.48	42.87	16.67	42.80	16.86	42.73	17.05	46
47	43.88	16.84	43.80	17.03	43.73	17.23	43.65	17.42	47
48	44.81	17.20	44.74	17.40	44.66	17.59	44.58	17.79	48
49	45.75	17.56	45.67	17.76	45.59	17.96	45.51	18.16	49
50	46.68	17.92	46.60	18.12	46.52	18.33	46.44	18.53	50
Distance.	Dep. 69	Lat.	Dep.	Lat. Deg.	Dep. 68½	Lat. Deg.	Dep. 681	Lat. Deg.	Distance.

Distance.	21 I	Deg.	211	Deg.	211	Deg.	213	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince
51	47.61	18.28	47.53	18.48	47.45	18.69	47.37	18.90	51
52	48.55	18.64	48.46	18.85	48.38	19.06	48.30	19.27	52
53 54	49.48 50.41	18.99 19.35	$\frac{49.40}{50.33}$	19.21	49.31 50.24	19.42	49.23	19.64 20.01	53
55	51.35	19.71	51.26	19.93	51.17	20.16	51.08	20.38	55
56	52.28	20.07	52.19	20.30	52.10	20.52	52.01	20.75	56
57	53.21	20.43	53.12	20.66	53.03	20.89	52.94	21.12	57
58	54.15	20.79	54.06	21.02	53,96	21.26	53.87	21.49	58
59 60	55.08 56.01	$21.14 \\ 21.50$	54.99 55.92	21.38 21.75	54.89 55.83	21.62 21.99	54.80 55.73	21.86 22.23	59
61	56.95	21.86	56.85	22.11	56.76	22.36	56.66	22.60	61
62	57.88	22.22	57.78	22.47	57.69	22.72	57.59	22.97	62
63	58.82	22.58	58.72	22.83	58.62	23.09	58.52	23.35	68
64	59.75 60.68	22.94	59.65	23.20	59.55	23.46	59.44	23.72	64
65	61.62	23.29 23.65	$60.58 \\ 61.51$	$23.56 \\ 23.92$	60.48	23.82 24.19	60.37	24.09 24.46	65
67	62.55	24.01	62.44	24.28	62.34	24.56	62.23	24.83	67
68	63.48	24.37	63.38	24.65	63.27	24.92	63.16	25.20	68
69	64.42	24.73	64.31	25.01	64.20	25.29	64.09	25.57	. 69
70	65.35	25.09	65.24	25.37	65.13	25.66	65.02	25.94	70
71	66.28	25.44	66.17	25.73	66.06	26.02	65.95	26.31	71
72 73	67.22 68.15	25.80 26.16	67.10 68.04	26.10 26.46	66.99	26.39 26.75	66.87	26.68 27.05	79
74	69.08	26.52	68.97	26.82	68.85	27.12	68.73	27.42	7
75	70.02	26.88	69.90	27.18	69.78	27.49	69.66	27.79 28.16	7
76	70.95	27.24	70.83	27.55	70.71	27.85	70.59		76
77	71.89 72.82	27.59 27.95	71.76	27.91 28.27	71.64	28.22 28.59	71.52 72.45	28.53 28.90	7
79	73.75	28.31	72.70 73.63	28.63	73.50	28.95	73.38	29.27	78
80	74.69	28.67	74.56	29.00	74.43	29.32	74.30	29.64	80
81	75.62	29.03	75.49	29.36	75.36	29.69	75.23	30.02	8
82	76.55	29.39	76.42	29.72	76.29	30.05	76.16	30.39	8
83 84	77.49 78.42	29.74 30.10	77.36 78.29	$\frac{30.08}{30.44}$	77.22 78.16	$\frac{30.42}{30.79}$	77.09	$30.76 \\ 31.13$	8:
85	79.35	30.46	79.22	30.81	79.09	31.15	78.95	31.50	8
86	80.29	30.82	80.15	31.17	80.02	31.52	79.88	31.87	8
87	81.22	31.18	81.08	31.53	80.95	31.89	80.81	32.24	8
88	82.16 83.09	31.54	82.02 82.95	31.89	81.88	$32.25 \\ 32.62$	81.74	32.61 32.98	8
90	84.02	32.25	83.88	32.62	83.74	32.99	83.59	33.35	9
91	84.96	32.61	84.81	32.98	84.67	33.35	84.52	33.72	9
92	85.89	32.97	85.74	33.34	85.60	33.72	85.45	34.09	9
93	86.82	33.33	86.68	33.71	86.53	34.08	86.38	34.46	9
94 95	87.76 88.69	33.69 34.04	87.61 88.54	34.07	87.46	34.45	87.31 88.24	34.83 35.20	9
96	89.62	34.40	89.47	34.79	89.32	35.18	89.17	35.57	9
97	90.56	34.76	90.40	35.16	90.25	35.55	90.09	35.94	9
98	91.49	35.12	91.34	35.52	91.18	35.92	91.02	36.31	9
100	92.42	35.48	92.27	$35.88 \\ 36.24$	92.11 93.04	36.28	91.95	36.69 37.06	10
-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	-
Distance	69	Deg.	683	Deg.	681	Deg.	681	Deg.	Dietanos

Distance	22	Deg.	224]	221 Deg.		Deg.	22 1	Deg.	Dist
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8	0.93 1.85 2.78 3.71 4.64 5.56 6.49 7.42 8.34	0.37 0.75 1.12 1.50 1.87 2.25 2.62 3.00 3.37	0.93 1.85 2.78 3.70 4.63 5.55 6.48 7.40 8.33	0.38 0.76 1.14 1.51 1.89 2.27 2.65 3.03 3.41	0.92 1.85 2.77 3.70 4.62 5.54 6.47 7.39 8.31	0.38 0.77 1.15 1.53 1.91 2.30 2.68 3.06 3.44	0.92 1.84 2.77 3.69 4.61 5.53 6.46 7.38 8.30	0.39 0.77 1.16 1.55 1.93 2.32 2.71 3.09 3.48	1 2 3 4 5 6 7 8 9
10 11 12 13 14 15 16 17	9.27 10.20 11.13 12.05 12.98 13.91 14.83 15.76	3.75 4.12 4.50 4.87 5.24 5.62 5.99 6.37	9.26 10.18 11.11 12.03 12.96 13.88 14.81 15.73	3.79 4.17 4.54 4.92 5.30 5.68 6.06 6.44	9.24 10.16 11.09 12.01 12.93 13.86 14.78 15.71	3.83 4.21 4.59 4.97 5.36 5.74 6.12 6.51	9.22 10.14 11.07 11.99 12.91 13.83 14.76 15.68	3.87 4.25 4.64 5.03 5.41 5.80 6.19 6.57	10 11 12 13 14 15 16 17
18 19 20 21 22 23 24 25	16.69 17.62 18.54 19.47 20.40 21.33 22.25 23.18	6.74 7.12 7.49 7.87 8.24 8.62 8.99 9.37	16.66 17.59 18.51 19.44 20.36 21.29 22.21 23.14	6.82 7.19 7.57 7.95 8.93 8.71 9.09 9.47	16.63 17.55 18.48 19.40 20.33 21.25 22.17	6.89 7.27 7.65 8.04 8.42 8.80 9.18 9.57	16.60 17.52 18.44 19.37 20.29 21.21 22.13 23.05	6.96 7.35 7.73 8.12 8.51 8.89 9.28	18 19 20 21 22 23 24
25 26 27 28 29 30 31 32	24.11 25.03 25.96 26.89 27.82 28.74 29.67	9.74 10.11 10.49 10.86 11.24 11.61 11.99	23.14 24.06 24.99 25.92 26.84 27.77 28.69 29.62	9.47 9.84 10.22 10.60 10.98 11.36 11.74 12.12	23.10 24.02 24.94 25.87 26.79 27.72 28.64 29.56	9.95 10.33 10.72 11.10 11.48 11.86 12.25	23.05 23.98 24.90 25.82 26.74 27.67 28.59 29.51	9.67 10.05 10.44 10.83 11.21 11.60 11.99 12.37	25 26 27 28 29 30 31 32
33 34 35 36 37 38 39 40	30.60 31.52 32.45 33.38 34.31 35.23 36.16 37.09	12.36 12.74 13.11 13.49 13.86 14.24 14.61 14.98	30.54 31.47 32.39 33.32 34.24 35.17 36.10 37.02	12.50 12.87 13.25 13.63 14.01 14.39 14.77 15.15	30.49 31.41 32.34 33.26 34.18 35.11 36.03 36.96	12.63 13.01 13.39 13.78 14.16 14.54 14.92 15.31	30.43 31.35 32.28 33.20 34.12 35.04 35.97 36.89	12.76 13.15 13.53 13.92 14.31 14.70 15.08 15.47	33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49	38.01 38.94 39.87 40.80 41.72 42.65 43.58 44.50 45.43 46.36	15.36 15.73 16.11 16.48 16.86 17.23 17.61 17.98 18.36	37.95 38.87 39.80 40.72 41.65 42.57 43.50 44.43 45.35	15.52 15.90 16.28 16.66 17.04 17.42 17.80 18.18	37.88 38.80 39.73 40.65 41.57 42.50 43.42 44.35 45.27	15.69 16.07 16.46 16.84 17.22 17.60 17.99 18.37 18.75	37.81 38.73 39.65 40.58 41.50 42.42 43.34 44.27 45.19	15.86 16.24 16.63 17.02 17.40 17.79 18.18 18.56 18.95	41 42 43 44 45 46 47 48 49
Distance. S	Dep.	18.73 Lat. Deg.	46.28 Dep.	Lat. Deg.	46.19 Dep.	19.13 Lat. Deg.	46.11 Dep.	19.34 Lat. Deg.	Distance. S

Distance.	22 l	Deg.	221	Deg.	22 <u>1</u>	Deg.	22]	Deg.	Distance
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
51 52	47.29 48.21	19.10 19.48	47.20 48.13	19.31 19.69	$47.12 \\ 48.04$	19.52 19.90	47.03 47.95	19.72 20.11	51 52
53	49.14	19.85	49.05	20.07	48.97	20.28	48.88	20.59	53
54	50.07	20.23	49.98	20.45	49.89	20.66	49.80	20.88	54
55 56	51.00 51.92	20.60 20.98	50.90 51.83	20.83 21.20	50.81 51.74	21.05 21.43	50.72 51.64	21.27 21.66	55 56
57	52.85	21.35	52.76	21.58	52.66	21.81	52.57	22.04	57
58	53.78	21.73	53.68	21.96	53.59	22.20	53.49	22.43	58
59 6 0	54.70 55.63	22.10 22.48	54.61 55.53	$\frac{22.34}{22.72}$	54.51 55.43	$22.58 \\ 22.96$	54.41	22.82 23.20	59 60
61	56.56	22.85	56.47	23.10	56.36	$\frac{23.34}{23.34}$	56.25	23.59	61
62	57.49	23.23	57.38	23.48	57.28	23.73	57.18	23.98	62
63 64	58.41 59.34	23.60 23.97	58.31 59.23	23.85 24.23	58.20 59.13	24.11 24.49	58.10 59.02	24.36 24.75	63 64
65	60.27	24.35	60.16	24.61	60.05	24.87	59.94	25.14	65
66	61.19	24.72	61.09	24.99	60.98	25.26	60.87	25.52	66
67 68	63.12 63.05	25.10 25.47	62.01 62.94	25.37 25.75	$61.90 \\ 62.82$	25.64 26.02	61.79 62.71	25.91 26.30	67 68
6 9	63.98	25.85	63.86	26.13	63.75	26.41	63.63	26:68	69
70	64.90	26.22	64.79	26.51	64.67	26.79	64.55	27.07	70
71 72	65.83	26.60 26.97	65.71	26.88 27.26	65.60 66.52	27.17 27.55	$65.48 \\ 66.40$	27.46 27.84	71 72
73	67.68	27.35	67.56	27.64	67.44	27.94	67.32	28.23	73
74	68.61	27.35 27.72	68.49	28.02	68.37	28.32	68.24	28.62	74
75 76	69.54	28.10 28.47	69.42 70.34	28.40 28.78	69.29 70.21	28.70	69.17 70.09	29.00 29.39	75 76
77	71.39	28.84	71.27	29.16	71.14	29.47	71.01	29.78	77
78	72.32	29.22	72.19	29.53	72.06	29.85	71.93	30.16	78
79 80	73.25 74.17	29.59 29.97	73.12 74.04	29.91 30.29	72.99 73.91	30.23	72.85 73.78	30.55 30.94	79 80
81	75.10	30.34	74.97	30.67	74.83	31.00	74.70	31.32	81
82	76.03	30.72	75.89	31.05	75.76	31.38	75.62	31.71	82
83 84	76.96	31.09	76.82	31.43	76.68 77.61	31.76	76.54 77.46	$\begin{vmatrix} 32.10 \\ 32.48 \end{vmatrix}$	83 84
85	78.81	31.84	77.75 78.67	32.19	78.53	$\begin{vmatrix} 32.15 \\ 32.53 \end{vmatrix}$	78.39	32.87	85
86	79.74	32.22	79.60	32.56	79.45	32.91	79.31	33.26	86
87 88	80.66	32.59 32.97	80.52 81.45	32.94 33.32	80.38 81.30	33.29 33.68	80.23	33.64	87
89	82.52	33.34	82.37	33.70	82.23	34.06	82.08	34.42	89
90	83.45	33.71	83.30	34.08	83.15	34.44	83.00	34.80	90
91	84.37 85.30	34.09 34.46	84.22 85.15	34.46 34.84	84.07	34.82	83.92 84.84	35.19 35.58	91 92
92 93	86.23	34.40	86.08	35.21	85.00 85.92	35.21	85.76	35.96	93
94	87.16	35.21	87.00	35.59	86.84	35.97	86.69	36.35	94
95 96	88.08	35.59 35.96	87.93 88.85	35.97 36.35	87.77 88.69	36.35	87.61 88.53	36.74	95 96
96	89.94	36.34	89.78	36.73	89.62	36.74 37.12	89.45	37.12 37.51	97
98	90.86	36.71	90.70	37.11	90.54	37.50	90.38	37.90	98
. 99 :100	91.79 92.72	37.09 37.46	91.63 92.55	37.49 37.86	91.46 92.39	37.89 38.27	91.30 92.22	38.28 38.67	99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance	68	Deg.	673	Deg.		Deg.	671	Deg.	Distance.

Distance	23 I	Эeg.	234	231 Deg.		Deg.	23 1	Deg.	Distance
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	inco.
1 2	0.92	0.39 0.78	0.92 1.84	0.39	0.92	0.40	0.92	0.40	1 2
3	2.76	1.17	2.76	1.18	2.75	1.20	1.83 2.75	1.21	3
5	3.68 4.60	1.56 1.95	3.68 4.59	1.58	3.67 4.59	1.59 1.99	3.66 4.58	1.61 2.01	4 5
5 6 7	5.52	2.34	5.51	2.37	5.50 6.42	2.39 2.79	5.49 6.41	2.42 2.82	5 6 7
8	6.44 7.36	3.74 3.13	6.43 7.35	3.76 3.16	7.34	3.19	7.32	3.22	8
10	8.28 9.20	3.52 3.91	8.27 9.19	3.55 3.95	8.25 9.17	3.59 3.99	8.24 9.15	8.62 4.03	9 10
11 12	10.13 11.05	4.30	10.11	4.34	10.09	4.39 4.78	10.07 10.98	4.43	11 12
13	11.97	5.08	11.94	5.13	11.92	5.18	11.90	5.24	13
14 15	12.89 13.81	5.47 5.86	12.86	5.53 5.92	12.84	5.58 5.98	12.81 13.73	5.64 6.04	14 15
16	14.73	6.25	13.78 14.70	6.32	14.67	6.38	14.64	6.44	16
17 18	15.65 16.57	6.64 7.03	15.62 16.54	6.71 7.11	15.59 16.51	6.78 7.18	15.56 16.48	6.85 7.25	17 18
19 20	17.49 18.41	7.42 7.81	17.46 18.38	7.50 7.89	17.42 18.34	7.58 7.97	17.39 18.31	7.65 8.05	19 20
21	19.33	8.21	19.29	8.29	19.26	8.37	19.22	8.46	21
22 23 24	20.25 21.17	8.60 8.99	20.21 21.13	8.68 9.08	20.18	8.77 9.17	20.14	8.86 9.26	22 23
24 25	22.09 23.01	9.38	22.05 22.97	9.47	22.01 22.93	9.57 9.97	21.97	9.67 10.07	24 25
26	23.93	10.16	23.89	10.26	23.84	10.37	22.88 23.80	10.47	26
27 28	24.85 25.77	10.55	24.81 25.73	10.66 11.05	24.76 25.68	10.77	24.71 25.63	10.87 11.28	27 28
29 30	26.69	11.33	26.64	11.45	26.59	11.56	26.54	11.68	29 30
31	27.62 28.54	12.11	27.56 28.48	11.84	$\frac{27.51}{28.43}$	$\frac{11.96}{12.36}$	27.46	$\frac{12.08}{12.49}$	31
32	29.46 30.38	12.50	29.40	12.63	29.35	12.76	29.29	12.89	32
33 84	31.30	12.89 13.28	30.32 31.24	13.03 13.42	30.26 31.18	13.16 13.56	30.21 31.12	13.29 13.69	33 34
35 36	32.22 33.14	13.68	32.16 33.08	13.82 14.21	32.10 33.01	13.96 14.35	32.04 32.95	14.10	35 36
37	34.06	14.46	34.00	14.61	33.93	14.75	33.87	14.90	37
38 39	34.98 35.90	14.85 15.24	34.91 35.83	15.00 15.39	34.85 35.77	15.15	34.78 35.70	15.30 15.71	38 39
40	36.82	15.63	36.75	15.79	36.68	15.95	36.61	16.11	40
41 42	37.74 38.66	16.02 16.41	37.67 38.59	16.18 16.58	37.60 38.52	16.35 16.75	37.53 38.44	16.51	41 42
43	39.58	16.80	39.51	16.97	39.43	17.15	39.36	17.32	43
44 45	40.50	17.19 17.58	40.43 41.35	17.37 17.76	40.35 41.27	17.54 17.94	40.27 41.19	17.72 18.12	44 45
46 47	42.34 43.26	17.97	42.26 43.18	18.16 18.55	42.18 43.10	18.34 18.74	42.10 43.02	18.53 18.93	46 47
48	44.18	18.76	44.10	18.95	44.02	19.14	43.93	19.33	48
49 50	45.10 46.03	19.15 19.54	45.02 45.94	19.34 19.74	44.94 45.85	19.54 19.94	44.85	19.73 20.14	49 50
8	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	mce.
Distance	67	Deg.	66}	Deg.	66-1	Deg.	661	Deg.	Distance

Dis	23 I	Deg.	234	De	g.	$23\frac{1}{2}$	De	g.	233	Deg	•	Distance.
Distance.	Lat.	Dep.	Lat.	D	ep.	Lat.	D	ep.	Lat.	D	ep.	nce.
	100	19.93	46.86	20	. 13	46.77	20	.34	46.68	20		51
51 52	46.95	20.32	47.78	20	.53	47.69	20	.73	47.60	20	.94	52 53
53	48.79	20.71	48.70		.92	48.60	21	.13	48.51 49.43	21	.75	54
54	49.71	21.10	49.61 50.53	21	.32	50.44	21	.93	50.34	22	.15	55
55	50.63	21.49 21.88	51.45	22	2.11	51.36	25	2.33	51.26		.55	56 57
56 57	51.55 52.47	22.27	52.37	22	2.50	51.36 52.27		2.73	52.17		.96	58
58	53.39	22.66	53.29		2.90	53.19 54.11		3.13	53.09 54.00		.76	59
59	54.31	23.05	54.21		3.29	55.02		3.92	54.92		.16	60
60	55.23	23.44	55.13	_	4.08	55.94		4.32	55.83		.57	61
61	56.15	23.83 24.23	56.9		4.47	56.86	2	4.72	56.75		.97	62 63
62 63	57.99	24.62	57.88	3 2	4.87	57.77	2	5.12	57.66 58.58	25	.78	64
64	158.91	25.01	58.8		5.26	58.69 59.61	2	$5.52 \\ 5.92$	59.50		1.18	65
65	59.83	25.40 25.79	59.7	4 2	5.66 6.05	60.53	2	6.32	60.41	26	5.58	66
66	60.75		61.5	6 2	6.45	61.44		6.72	61.33	26	7.39	67 68
68	62.50	26.57	62.4	8 2	6.84	62.36 63.28		7.11	63.16		7.79	69
69	63.51	26.96	63.4	0 2	7.24	64.19		7.91	64.07		3.19	70
70		27.35			8.03	65.11	-	8.31	64.99		8.59	71
71		27.74		5 2	8.42	66.03	1 2	28.71	65.90		9.00	72
72 73		28.5	67.0	7 2	28.82	66.95	1 2	29.11	66.8		$9.40 \\ 9.80$	74
74	68.1	2 28.9	67.9	9 2	29.21	67.86	200	29.51 29.91	68.6		0.21	75
75	69.0				29.61	69.70	13	30.30	69.5	6 3	0.61	76
76					30.40	69.70	1 3	30.70	70.4		1.01 1.41	78
78			3 71.6	37 1 5	30.79	71.5	3 3	$\frac{31.10}{31.50}$			1.82	7
79	72.7	2 30.8	7 72.	8	31.18	72.43		31.90			2.22	8
8	-				$\frac{31:58}{31.97}$	74.28		32.30	74.1	4 3	32.62	8
8					32.37	75.2	0	32.70 33.10	75.0		33.03	8
8				26	$\frac{32.76}{33.16}$	76.1	2				33.43 33.83	8
8			2 77.	18	33.16	77.0	3	33.49 33.89		0	34.23	8
8	5 78.2	4 33.2			$\frac{33.55}{33.95}$	78.8	7	34.2	9 78.7	2 3	34.64	
	6 79.1	6 33.6			34.34	79.7	8	34.6	9 79.6		$35.04 \\ 35.44$	
	8 81.0	00 34.3	8 80.	85	34.74			$35.0 \\ 35.4$			35.84	
8	9 81.9	2 34.7		77	35.13 35.58			35.8			36.25	
	0 82.8				35.92	_	_	36.2	9 83.		36.65	
	1 83.	77 35.5 69 35.9			36.32			36.6	8 84.		37.05	5 9
	2 84.	61 36.5	85.		36.7	85.2		37.0	8 85.		37.46	
	14 86.	53 36.	73 86.	37	37.1	86.2		$\frac{37.4}{37.8}$	8 86.		38.26	
1 5	5 87.	45 37.	12 87.	29	37.50	87.1)4	38.2	8 87.	87	38.66	3 9
	6 88.	37 37. 29 37.	90 89		38.2	9 88.9	95	38.6	8 88.		39.0	
	97 89. 98 90.	21 38.	29 90	.04	38.6	8 89.8	37	39.0			39.4	
	99 91.	13 38.	68 90	.96	39.0			39.4			40.2	
	92. De			.88 ep.	39.4 Lat	-	_	La		ep.	Lat	
1	Tan	. 1	-	-		-	01	Doc		661	Deg.	-
1 ;	5 (37 Deg.		664	Deg.	6	02	Deg.		004	- 6.	1

تق	24	Deg.	241	Deg.	241	Deg.	241	Deg.	Dia
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	0.91 1.83 2.74	0.41 0.81 1.22	0.91 1.82 2.74	0.41 0.82	0.91 1.82 2.73	0.41 0.83 1.24	0.91 1.82 2.72	0.42 0.84 1.26	1 2 3 4
5 6	3.65 4.57 5.48	1.63 2.03 2.44	3.65 4.56 5.47	1.23 1.64 2.05 2.46	3.64 4.55 5.46	1.66 2.07 2.49	3.63 4.54 5.45	1.67 2.09 2.51	4 5 6 7
2 3 4 5 6 7 8	6.39 7.31 8.22	2.85 3.25 3.66	6.38 7.29 8.21	2.87 3.29 3.70	6.37 7.28 8.19	2.90 3.32 3.73	6.36 7.27 8.17	2.93 3.35 3.77	7 8 9
$\begin{array}{c} 10 \\ \hline 11 \\ 12 \end{array}$	$\frac{9.14}{10.05}$	4.07 4.47 4.88	$\frac{9.12}{10.03}$	4.11 4.52 4.93	9.10 10.01 10.92	4.15 4.56 4.98	9.08 9.99 10.90	4.19 4.61 5.02	10 11 12
13 14 15	10.96 11.88 12.79 13.70	5.29 5.69 6.10	10.94 11.85 12.76 13.68	5.34 5.75 6.16	11.83 12.74 13.65	5.39 5.81 6.22	11.81 12.71 13.62	5.44 5.86 6.28	13 14 15
16 17 18	14.62 15.53 16.44	6.51	14.59 15.50 16.41	6.57 6.98 7.39	14.56 15.47 16.38	6.64 7.05 7.46	14.53 15.44 16.35	6.70 7.12 7.54	16 17 18
19 20 21	$\frac{17.36}{18.27}$ $\frac{19.18}{19.18}$	7.32 7.73 8.13 8.54	17.32 18.24 19.15	7.80 8.21 8.63	17.29 18.20 19.11	7.88 8.29 8.71	17.25 18.16 19.07	7.95 8.37 8.79	19 20 21
22 23 24	20.10 21.01 21.93	8.95 9.35 9.76	20.06 20.97 21.88	9.04 9.45 9.86	20.02 20.93 21.84	9.12 9.54 9.95	19.98 20.89 21.80	9.21 9.63 10.05	22 23 24
25 26 27	22.84 23.75 24.67	10.17 10.58 10.98	22.79 23.71 24.62	10.27 10.68 11.09	22.75 23.66 24.57	10.37 10.78 11.20	22.70 23.61 24.52	10.47 10.89 11.30	25 26 27
28 29 30	25.58 26.49 27.41	11.39 11.80 12.20	25.53 26.44 27.35	11.50 11.91 12.32	25.48 26.39 27.30	11.61 12.03 12.44	25.43 26.34 27.24	11.72 12.14 12.56	28 29 30
31 32 33	28.32 29.23 30.15	12.61 13.02 13.42	28.26 29.18 30.09	12.73 13.14 13.55	28.21 29.12 30.03	12.86 13.27 13.68	28.15 29.06 29.97	12.98 13.40 13.82	31 32 33
34 35 36	31.06 31.97 32.89	13.83 14.24 14.64	31.00 31.91 32.82	13.96 14.38 14.79	30.94 31.85 32.76	14.10 14.51 14.93	30.88 31.78 32.69	14.23 14.65 15.07 15.49	34 35 36
37 38 39	33.80 34.71 35.63 36.54	15.05 15.46 15.86	33.74 34.65 35.56	15.20 15.61 16.02	33.67 34.58 35.49	15.34 15.76 16.17	33.60 34.51 35.42	15.91 16.33	37 38 39
40 41 42	$\frac{36.54}{37.46}$ $\frac{38.37}{38.37}$	$\frac{16.27}{16.68}$ 17.08	$\frac{36.47}{37.38}\\38.29$	$\frac{16.43}{16.84}$ 17.25	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{16.59}{17.00}$ 17.42	36.33 37.23 38.14	16.75 17.16 17.58	40 41 42
43 44 45	39.28 40.20 41.11	17.49 17.90 18.30	39.21 40.12 41.03	17.66 18.07 18.48	39.13 40.04 40.95	17.83 18.25 18.66	39.05 39.96 40.87	18.00 18.42 18.84	43 44 45
46 47 48	42.02 42.94 43.85	18.71 19.12 19.52	41.94 42.85 43.76	18.89 19.30 19.71	41.86 42.77 43.68	19.08 19.49 19.91	41.77 42.68 43.59	19.26 19.68 20.10	46 47 48
49 50	44.76 45.68	19.93 20.34	44.68 45.59	20.13 20.54	44.59 45.50	$20.32 \\ 20.73$	44.50 45.41	20.51 20.93	49 50
Distance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dig	6 6 1	Deg.	65}	Deg.	65 ½	Deg.	651	Deg.	Dis

Di	24]	Deg.	241	Deg.	241	Deg.	241	Deg.	Dia
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance
51 52	46.59 47.50	20.74 21.15	46.50	20.95 21.36	46.41 47.32	21.15	46.32 47.22	21.35 21.77	51 52
53 54	48.42 49.33	21.56 21.96	48.32 49.24	21.77 22.18	48.23 49.14	21.98 22.39	48.13 49.04	22.19 22.61	53 54
55 56	50.24 51.16	22.37 22.78	50.15 51.06	22.59 23.00	50.05 50.96	22.81 23.22	49.95 50.86	23.03 23.44	5 5 5 6
57 58	52.07 52.99	23.18 23.59	51.97 52.88	23.41 23.82	51.87 52.78	23.64 24.05	51.76 52.67	23.86 24.28	57 58
59 60	53.90 54.81	24.00 24.40	53.79 54.71	24.23 24.64	53.69 54.60	24.47 24.88	53.58 54.49	24.70 25.12	59 60
61	55.73	24.81	55.62	25.05	55.51	25.30	55.40 56.30	25.54 25.96	61 62
62 63	56.64 57.55	25.22 25.62	56.53 57.44	25.46 25.88	56.42 57.33	$25.71 \\ 26.13$	57.21	26.38	63
64 65	58.47 59.38	26.03 26.44	58.35 59.26	26.29 26.70	58.24 59.15	26.54 26.96	58.12 59.03	26.79 27.21	64 65
66	60.29	26.84	60.18	27.11	60.06	27.37	59.94 60.85	27.63 28.05	66 67
67 68	61.21 62.12	27.25 27.66	61.09	27.52 27.93	60.97	27.78 28.20	61.75	28.47	68
6 9 7 0	63.03 63.95	28.06 28.47	$62.91 \\ 63.82$	28.34 28.75	$62.79 \\ 63.70$	28.61 29.03	62.66	28.89 29.31	69 70
71	64.86	28.88	64.74	29.16	64.61	29.44	64.48	29.72	71
72 73	65.78 66.69	29.28 29.69	65.65	29.57 29.98	65.52	29.86 30.27	65.39	30.14 30.56	72 73
74 75	67.60 68.52	30.10 30.51	67.47 68.38	30.39 30.80	67.34	30.69 31.10	67.20 68.11	30.98 31.40	74 75
76	69.43	30.91	69.29	31.21	68.25 69.16	31.52	69.02	31,82	76
77 78	70.34 71.26	$31.32 \\ 31.73$	70.21	31.63 32.04	70.07	31.93 32.35	69.93 70.84	32.24 32.66	77
79 80	72.17 73.08	32.13 32.54	72.03 72.94	32.45 32.86	71.89	32.76 33.18	71.74 72.65	33.07 33.49	79 80
81	74.00	32.95	73.85	$\frac{32.80}{33.27}$	73.71	$\frac{33.18}{33.59}$	73.56	33.91	81
82 83	74.91 75.82	33.35 33.76	74.76 75.68	33.68 34.09	74.62 75.53	34.00 34.42	74.47 75.38	34.33 34.75	83 83
84	76.74	34.17	76.59	34.50	76.44	34.83	76.28	35.17	84
85 86	77.65 78.56	34.57 34.98	77.50 78.41	34.91 35.32	77.35 78.26	35.25 35.66	77.19 78.10	35.59 36.00	85 86
87 88	79.48 80.39	35.39 35.79	79.32 80.24	35.73 36.14	79.17 80.08	36.08 36.49	79.01 79.92	36.42 36.84	87 88
89	81.31	36.20	81.15	36.55	80.99	36.91	80.82	37.26	89
90	$\frac{82.22}{83.13}$	$\frac{36.61}{37.01}$	$\frac{82.06}{82.97}$	$\frac{36.96}{37.38}$	$\frac{81.90}{82.81}$	$\frac{37.32}{37.74}$	$\frac{81.73}{82.64}$	$\frac{37.68}{38.10}$	90
92	84.05	37.42	83.88	37.79	83.72	38.15	83.55	38.52	92
93 94	84.96 85.87	37.83 38.23	84.79 85.71	38.20 38.61	84.63	38.57 38.98	84.46 85.37	38.94 39.35	93 94
95 96	86.79 87.70	38.64 39.05	86.62 87.53	39.02 39.43	86.45	39.40	86.27	39.77 40.19	95 96
97	88.61	39.45	88.44	39.84	87.36 88.27	39.81 40.23	87.18 88.09	40.61	97
98 99	89.53 90.44	39.86 40.27	89.35 90. 2 6	40.25 40.66	89.18 90.09	40.64	89.00 89.91	41.45	98
100	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Dist	66 I	Dog.	65 ‡ :	Deg.	651	Deg.	651	Deg.	Dist

5	25	Deg.	251	Deg.	251	Deg.	25}	Deg.	Dist
Vietairo.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
	0.91	0.42 0.85	0.90	0.43	0.90	0.43 0.86	0.90	0.43 0.87	1 2 3
	1.81 2.72 1 3.63	1.69	2.71 3.62	1.28	2.71 3.61	1.29	2.70 3.60	1.30	3 4 5
1 1	4.53 5.44	2.11 2.54	4.52 5.43	2.13 2.56	4.51 5.42	2.15 2.58	4.50 5.40	2.17 2.61	6
1	7 6.34 7.25	2.96 3.38	6.33 7.24	2.99 3.41	6.32	3.01 3.44	6.30 7.21	3.04 3.48	8
1	8.16 9.06	3.80 4.23	8.14 9.04	3.84 4.27	8.12 9.03	3.87 4.31	8.11 9.01	3.91 4.34	9 10
1 1:		4.65 5.07	9.95 10.85	4.69 5.12	9.93 10.83	4.74 5.17	9.91 10.81	4.78 5.21	11 12
11	11.78	5.49 5.92	11.76 12.66	5.55 5.97	11.73 12.64	5.60 6.03	11.71 12.61	5.65 6.08	13 14
1	13.59	6.34	13.57 14.47	6.40	13.54 14.44	6.46 6.89	13.51 14.41	6.52 6.95	15 16
Î	7 15.41	7.18	15.38 16.28	7.25 7.68	15.34 16.25	7.32 7.75	15.31 16.21	7.39 7.82	17 18
1 2	17.22	8.03 8.45	17.18 18.09	8.10 8.53	17.15 18.05	8.18 8.61	17.11 18.01	8.25 8.69	19 20
2 2	19.03	8.87 9.30	18.99 19.90	8.96 9.38	18.95 19.86	9.04	18.91 19.82	9.12 9.56	21
2 2	3 20.85	9.72 10.14	20.80 21.71	9.81 10.24	20.76 21.66	9.90 10.33	20.72 21.62	9.99 10.43	22 23 24
2 2	22.66	10.57	22.61	10.66	22.56 23.47	10.76	22.52 23.42	10.86	25
2	24.47	11.41	23.52	11.52	24.37	11.62	24.32	11.73 12.16	26 27
2:	26.28	11.83 12.26	25.32 26.23	11.94	25.27 26.17	12.05 12.48	25.22 26.12	12.60	28 29
3	28.10	$\frac{12.68}{13.10}$	$\frac{27.13}{28.04}$	$\frac{12.80}{13.22}$	$\frac{27.08}{27.98}$	$\frac{12.92}{13.35}$	$\frac{27.02}{27.92}$	$\frac{13.03}{13.47}$	30
33	3 29.91	13.52 13.95	28.94 29.85	13.65 14.08	28.88 29.79	13.78 14.21	28.82 29.72	13.90 14.34	32 33
3	31.72	14.37 14.79	30.75 31.66	14.50 14.93	30.69 31.59	14.64 15.07	30.62 31.52	14.77 15.21	34 35
3	7 33.53	15.21 15.64	32.56 33.46	15.36 15.78	32.49 33.40	15.50 15.93	32.43 33.33	15.64 16.07	36 37
3	35.35	16.06 16.48	34.37 35.27	16.21 16.64	34.30 35.20	16.36 16.79	34.23 35.13	16.51 16.94	38 39
4		$\frac{16.90}{17.33}$	$\frac{36.18}{37.08}$	$\frac{17.06}{17.49}$	$\frac{36.10}{37.01}$	$\frac{17.22}{17.65}$	$\frac{36.03}{36.93}$	17.38	40
4:	8 38.06	17.75 18.17	37.99 38.89	17.92 18.34	37.91 38.81	18.08	37.83 38.73	18.25 18.68	42 43
4	39.88	18.60 19.02	39.80 40.70	18.77	39.71 40.62	18.94	39.68 40.53	19.12	44 45
4	41.69	19.44	41.60 42.51	19.62	41.52	19.80	41.43 42.33	19.98 20.42	46 47
44	43.50	20.29	43.41 44.32	20.48	43.32 44.23	20.66	43.23 44.13	20.85	46 49
50	45.32	21.13	45.22	21.33	45.13	21.53	45.03	21.72	50
rnce	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	- PCG
Distance	65	Deg.	641	Deg.	. 64}	Deg.	641	Deg.	Distance

Dista	25 I	Deg.	25‡	Deg.	25]	Deg.	251	Deg.	Distance.
tance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52	46.22 47.13	21.55 21.98	46.13 47.03	21.75 22.18	46.03 46.93	21.96 22.39	45.94 46.84	22.16 22.59	51 52
53	47.13 48.03	22.40	47.94	22.61	47.84	22.82	47.74	23.03	53.
54 55	48.94	22.82 23.24	48.84	23.03 23.46	48.74 49.64	23.25	48.64	23.46 23.89	54
56	49.85 50.75	23.67	50.65	23.89	50.54	23.68 24.11	49.54 50.44	24.33	55 56
57	51.66	24.09	51.55	24.31	51.45	24.54	51.34	24.76	57
58 59	52.57 53.47	$24.51 \\ 24.93$	52.46 53.36	24.74 25.17	52.35 53.25	24.97 25.40	52.24 53.14	25.20 25.63	58 59
60	54.38	25.36	54.27	25.59	54.16	25.83	54.04	26.07	60
61	55.28	25.78	55.17	26.02	55.06	26.26	54.94	26.50	61
62 63	56.19 57.10	26.20 26.62	56.08 56.98	26.45 26.87	55.96 56.86	26.69 27.12	55.84 56.74	26.94 27.37	62 63
64	58.00	27.05	57.89	27.30	57.77	27.55	57.64	27.80	64
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.24	65
66 67	59.82 60.72	27.89 28.32	59.69 60.60	28.15 28.58	59.57 60.47	28.41 28.84	59.45 60.35	28.67 29.11	66 67
68	61.63	28.74	61.50	29.01	61.38	29.27	61.25	29.54	68
69	62.54	29.16	62.41	29.43	62.28	29.71	62.15	29.98	69
$\frac{70}{71}$	$\frac{63.44}{64.35}$	$\frac{29.58}{30.01}$	$\frac{63.31}{64.22}$	$\frac{29.86}{30.29}$	$\frac{63.18}{64.08}$	$\frac{30.14}{30.57}$	63.95	$\frac{30.41}{30.85}$	$\frac{70}{71}$
72	65.25	30.43	65.12	30.71	64.99	31.00	64.85	31.28	72
73	66.16	30.85	66.03	31.14	65.89	31.43	65.75	31.71	73
74 75	67.07	31.27 31.70	66.93 67.83	31.57 31.99	66.79	31.86	66.65	32.15 32.58	74 75
76	68.88	32.12	68.74	32.42	68.60	$32.29 \ 32.72$	68.45	33.02	76
77	69.79	32.54	69.64	32.85	69.50	33.15	69.35	33.45	77
78 79	70.69 71.60	32.96 33.39	70.55 71.45	$\frac{33.27}{33.70}$	70.40	33.58 34.01	70.25	33.89 34.32	78 79
80	72.50	33.81	72.36	34.13	72.21	34.44	72 06	34.76	80
. 81	73.41	34.23	73.26	34.55	73.11	34.87	72.96	35.19	81
82	74.32 75.22	34.65 35.08	74.17 75.07	34.98	74.01	35.30	73.86 74.76	35.62 36.06	82 83
83 84	76.13	35.50	75.97	35.41 35.83	74.91 75.82	35.73 36.16	75.66	36.49	84
85	77.04	35.92	76.88	36.26	76.72	36.59	76.56	36.93	85
86 87	77.94 78.85	36.35 36.77	77.78	36.68 37.11	77.62 78.52	37.02 37.45	77.46 78.36	37.36 37.80	86
88	79.76	37.19	79.59	37.54	79.43	37.88	79.26	38.23	88
89	80.66	37.61	80.50	37.96	80.33	38.32	80.16	38.67	89
90	81.57	38.04	81.40	38.39	81.23	38.75	81.06	39.10	90
91 92	82.47 83.38	38.46 38.88	82.31 83.21	38.82 39.24	82.14 83.04	39.18 39.61	81.96 82.86	39.53 39.97	91 92
93	84.29	39.30	84.11	39.67	83.94	40.04	83.76	40.40	93
94	85.19	39.73	85.02	40.10	84.84	40.47	84.67	40.84	94
95 96	86.10 87.01	40.15 40.57	85.92	$ 40.52 \\ 40.95 $	85.75	40.90 41.33	85.57 86.47	41.27	95 96
97	87.91	40.99	87.73	41.38	87.55	41.76	87.37	42.14	97
98 99	88.82 89.72	41.42 41.84	88.64	41.80 42.23	88.45 89.36	$42.19 \\ 42.62$	88.27 89.17	42.58 43.01	98
100	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance	65	Deg.	643	Deg.	641	Deg.	641	Deg.	Distance.

Dist	26 1	Deg.	261 I	eg.	26 <u>1</u>	Deg.	261	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	0.90	0.44	0.90	0.44	0.89	0.45	0.89	0.45	1
2	1.80	0.88	1.79	0.88	1.79	0.89	1.79	0.90	2
3	2.70	1.32	2.69	1.33	2.68	1.34	2.68	1.35	3
4	3.60	1.75	3.59	1.77	3.58	1.78	3.57	1.80	4
5	4.49	2.19	4.48	2.21	4.47	2.23	4.46	2.25	5
6	5.39	2.63	5.38	2.65	5.37	2.68	5.36	2.70	6
7	6.29	3.07	6.28	3.10	6.26	3.12	6.25	3.15	7
8	7.19	3.51	7.17	3.54	7.16	3.57	7.14	3.60	8
9	8.09	3.95	8.07	3.98	8.05	4.02	8.04	4.05	9
10	8.99	4.38	8.97	4.42	8.95	4.46	8.93	4.50	10
11	9.89	4.82	9.87	4.87	9.84	4.91	9.82	4.95	11
12	10.79	5.26	10.76	5.31	10.74	5.35	10.72	5.40	12
13	11.68	5.70	11.66	5.75	11.63	5.80	11.61	5.85	13
14	12.58	6.14	12.56	6.19	12.53	6.25	12.50	6.30	14
15	13.48	6.58	13.45	6.63	13.42	6.69	13.39	6.75	15
16	14.38	7.01	14.35	7.08	14.32	7.14	14.29	7.20	16
17	15.28	7.45	15.25	7.52	15.21	7.59	15.18	7.65	17
18 19 20 21	$ \begin{array}{r} 16.18 \\ 17.08 \\ 17.98 \\ \hline 18.87 \end{array} $	7.89 8.33 8.77 9.21	$ \begin{array}{r} 16.14 \\ 17.04 \\ 17.94 \\ \hline 18.83 \end{array} $	$ \begin{array}{r} 7.96 \\ 8.40 \\ \hline 8.85 \\ \hline 9.29 \end{array} $	$ \begin{array}{r} 16.11 \\ 17.00 \\ 17.90 \\ \hline 18.79 \end{array} $	8.03 8.48 8.92 9.37	16.07 16.97 17.86 18.75	8.10 8.55 9.60 9.45	18 19 20 21
22	19.77	9.64	19.73	9.73	19.69	9.82	19.65	9.90	22
23	20.67	10.08	20.63	10.17	20.58	10.26	20.54	10.35	23
24	21.57	10.52	21.52	10.61	21.48	10.71	21.43	10.80	24
25 26 27	22.47 23.37 24.27 25.17	10.96 11.40 11.84	22.42 23.32 24.22	11.06 11.50 11.94	22.37 23.27 24.16	11.15 11.60 12.05	22.32 23.22 24.11	11.25 11.70 12.15	25 26 27
28 29 30 31	26.06 26.96 27.86	12.27 12.71 13.15 13.59	25.11 26.01 26.91 27.80	12.38 12.83 13.27 13.71	25.06 25.95 26.85 27.74	12.49 12.94 13.39 13.83	25.00 25.90 26.79 27.68	12.60 13.05 13.50 13.95	28 29 30 31
32 33 34	28.76 29.66 30.56	14.03 14.47 14.90	28.70 29.60 30.49	14.15 14.60 15.04	28.64 29.53 30.43	14.28 14.72 15.17	28.58 29.47 30.36	14.40 14.85	32 33 34
35	31.46	15.34	31.39	15.48	31.32	15.62	31.25	15.75	35
36	32.36	15.78	32.29	15.92	32.22	16.06	32.15	16.20	36
37	33.26	16.22	33.18	16.36	33.11	16.51	33.04	16.65	37
38	34.15	16.66	34.08	16.81	34.01	16.96	33.93	17.10	38
39	35.05	17.10	34.98	17.25	34.90	17.40	34.83	17.55	39
40	35.95	17.53	35.87	17.69	35.80	17.85	35.72	18.00	40
41	36.85	17.97	36.77	18.13	36.69	18.29	36.61	18.45	41
42	37.75	18.41	37.67	18.58	37.59	18.74	37.51	18.90	42
43	38.65	18.85	38.57	19.02	38.48	19.19	38.40	19.35	43
44	39.55	19.29	39.46	19.46	39.38	19.63	39.29	19.80	44
45	40.45	19.73	40.36	19.90	40.27	20.08	40.18	20.25	45
46	41.34	20.17	41.26	20.35	41.17	20.53	41.08	20.70	46
47	42.24	20.60	42.15	20.79	42.06	20.97	41.97	21.15	47
48	43.14	21.04	43.05	21.23	42.96	21.42	42.86	21.60	48
49	44.04	21.48	43.95	21.67	43.85	21.86	43.76	22.05	49
50	44.94	21.92	44.84	22.11	44.75	22.31		22.50	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
å	64	Deg.	63 1	Deg.	63⅓	Deg.	631	Deg.	ij

Dist	26 1	Deg.	261	Deg.	261	Deg.	263	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52 53 54 55 56 57 58 59 60 61 62 53 64 65 66 67 67 71 72 73 74	45.84 46.74 47.64 48.53 50.33 51.23 52.13 53.03 54.83 55.73 56.62 57.52 59.32 60.22 62.02 62.02 63.81 64.71 65.61 66.51 67.41	22.36 22.80 23.23 24.11 24.55 24.99 25.43 25.86 26.30 26.718 27.18 27.62 28.49 28.49 28.89 30.25 30.69 31.12 32.44 32.88	45.74 46.64 47.53 48.43 49.33 50.22 52.02 52.02 53.81 54.71 55.61 56.50 57.40 58.30 59.19 60.09 61.88 62.78 63.68 64.57 65.47 66.37 67.27	22.56 23.00 23.44 23.88 24.33 24.77 25.21 25.65 26.09 26.54 26.98 27.42 27.86 28.31 30.52 30.96 31.40 32.29 32.73 33.77	45.64 46.54 47.43 48.33 49.22 50.12 51.01 52.80 53.70 54.59 55.49 56.38 57.28 58.17 59.96 60.86 61.75 62.65 63.54 64.44 65.33 66.23 67.12	22.76 23.20 23.65 24.09 24.54 24.99 25.43 26.33 26.77 27.22 27.22 27.22 27.22 27.22 29.90 29.45 29.90 31.23 31.68 32.13 32.57 33.06	45.54 46.43 47.33 48.22 49.11 50.90 51.79 52.69 53.58 54.47 55.36 56.26 57.15 58.04 58.94 59.83 60.72 61.62 62.51 63.40 64.29 65.19 66.97	22.96 23.41 23.86 24.31 24.76 25.21 25.66 27.01 27.46 27.91 28.81 30.16 31.06 31.06 31.51 31.92 32.41 32.86 33.31 33.76	51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 70 71 72 73 74 75
76 77 78 79 80 81 82 83 84	68.31 69.21 70.11 71.00 71.90 72.80 73.70 74.60 75.50	33.32 33.75 34.19 34.63 35.07 35.51 35.95 36.38 36.82	68.16 69.06 69.96 70.85 71.75 72.65 73.54 74.44 75.34	33.61 34.06 34.50 34.94 35.38 35.83 36.27 36.71 37.15	68.01 68.91 69.80 70.70 71.59 72.49 73.38 74.28 75.17	33.91 34.36 34.80 35.25 35.70 36.14 36.59 37.03 37.48	67.87 68.76 69.65 70.55 71.44 72.33 73.22 74.12 75.01	34.21 34.66 35.11 35.56 36.01 36.46 36.91 37.36 37.81	76 77 78 79 80 81 82 83 84
85 86 87 88 89 90 91	76.40 77.30 78.20 79.09 79.99 80.89 81.79	37.26 37.70 38.14 38.58 39.01 39.45 39.89	76.23 77.13 78.03 78.92 79.82 80.72 81.62	37.59 38.04 38.48 38.92 39.36 39.81 40.25	76.07 76.96 77.86 78.75 79.65 80.54	37.93 38.37 38.82 39.27 39.71 40.16 40.60	75.90 76.80 77.69 78.58 79.48 80.37 81.26	38.26 38.71 39.16 39.61 40.06 40.51 40.96	85 86 87 88 89 90
92 93 94 95 96 97 98 99 100	82.69 83.59 84.49 85.39 86.28 87.18 88.08 88.98 89.88	40.33 40.77 41.21 41.65 42.08 42.52 42.96 43.40 43.84	82.51 83.41 84.31 85.20 86.10 87.00 87.89 88.79 89.69	40.69 41.13 41.58 42.02 42.46 42.90 43.34 43.79 44.23	82.33 83.23 84.12 85.02 85.91 86.81 87.70 88.60 89.49	41.05 41.50 41.94 42.39 42.83 43.28 43.73 44.17 44.62	82.15 83.05 83.94 84.83 85.73 86.62 87.51 88.40 89.30	41.41 41.86 42.31 42.76 43.21 43.66 44.11 44.56 45.01	92 93 94 95 96 97 98 99 100
Distance.	Dep. 64 I	Lat.	Dep. 633	Lat.	Dep. 63½	Lat. Deg.	Dep. 631	Lat.	Distance.

Distance.	27]	Deg.	271	Deg.	27½	Deg.	271	Deg.	Distance.
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
1 2 3 4 5 6	0.89 1.78 2.67 3.56	0.45 0.91 1.36 1.82	0.89 1.78 2.67 3.56	0.46 0.92 1.37 1.83	0.89 1.77 2.66 3.55	0.46 0.92 1.39 1.85	0.88 1.77 2.65 3.54	0.47 0.93 1.40 1.86	1 2 3 4
7 8	4.45 5.35 6.24 7.13	2.27 2.72 3.18 3.63	4.45 5.33 6.22 7.11	2.29 2.75 3.21 3.66	4.44 5.32 6.21 7.10	2.31 2.77 3.23 3.69	4.42 5.31 6.19 7.08	2.33 2.79 3.26 3.72	5 6 7 8
10	8.02	4.09	8.89	4.12	7.98 8.87	4.16	7.96 8.85	4.19	10
11 12 13 14 15	9.80 10.69 11.58 12.47 13.37	4.99 5.45 5.90 6.36 6.81	9.78 10.67 11.56 12.45 13.34	5.04 5.49 5.95 6.41 6.87	9.76 10.64 11.53 12.42 13.31	5.08 5.54 6.00 6.46 6.93	9.73 10.62 11.50 12.39 13.27	5.12 5.59 6.05 6.52 6.98	11 12 13 14 15
16 17 18 19 20	14.26 15.15 16.04 16.93 17.82	7.26 7.72 8.17 8.63 9.08	14.22 15.11 16.00 16.89 17.78	7.33 7.78 8.24 8.70 9.16	14.19 15.08 15.97 16.85 17.74	7.39 7.85 8.31 8.77 9.23	14.16 15.04 15.93 16.81 17.70	7.45 7.92 8.38 8.85 9.31	16 17 18 19 20
21 22 23. 24 25	18.71 19.60 20.49 21.38 22.28	9.53 9.99 10.44 10.90 11.35	18.67 19.56 20.45 21.34 22.23	9.62 10.07 10.53 10.99 11.45	18.63 19.51 20.40 21.29 22.18	9.70 10.16 10.62 11.08 11.54	18.58 19.47 20.35 21.24 22.12	9.78 10.24 10.71 11.17 11.64	21 22 23 24 25
26 27 28 29 30	23.17 24.06 24.95 25.84 26.73	11.80 12.26 12.71 13.17 13.62	23.11 24.00 24.89 25.78 26.67	11.90 12.36 12.82 13.28 13.74	23.06 23.95 24.84 25.72 26.61	12.01 12.47 12.93 13.39 13.85	23.01 23.89 24.78 25.66 26.55	12.11 12.57 13.04 13.50 13.97	26 27 28 29 30
31 32 33 34	27.62 28.51 29.40 30.29	14.07 14.53 14.98 15.44	27.56 28.45 29.34 30.23	14.19 14.65 15.11 15.57	27.50 28.38 29.27 30.16	14.31 14.78 15.24 15.70	27.43 28.32 29.20 30.09	14.43 14.90 15.37 15.83	31 32 33 34
35 36 37 38 39	31.19 32.08 32.97 33.86 34.75	15.89 16.34 16.80 17.25 17.71 18.16	31.12 32.00 32.89 33.78 34.67	16.03 16.48 16.94 17.40 17.86	31.05 31.93 32.82 33.71 34.59	16.16 16.62 17.08 17.55 18.01	30.97 31.86 32.74 33.63 34.51	16.30 16.76 17.23 17.69 18.16	35 36 37 38 39
40 41 42 43 44	35.64 36.53 37.42 38.31	18.61 19.07 19.52	35.56 36.45 37.34 38.23	18.31 18.77 19.23 19.69	35.48 36.37 37.25 38.14	18.47 18.93 19.39 19.86	35.40 36.28 37.17 38.05	18.62 19.09 19.56 20.02	40 41 42 43
45 46 47 48	39.20 40.10 40.99 41.88 42.77	19.98 20.43 20.88 21.34 21.79	39.12 40.01 40.89 41.78 42.67	20.15 20.60 21.06 21.52 21.98	39.03 39.92 40.80 41.69 42.58	20.32 20.78 21.24 21.70 22.16	38.94 39.82 40.71 41.59 42.48	20.49 20.95 21.42 21.88 22.35	44 45 46 47 48
49 50	43.66 44.55	22.25 22.70	43.56 44.45	22.44 22.89	43.46 44.35	22.63 23.09	43.36 44.25	22.82 23.28	49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	ance.
Diet	63	Deg.	62}	Deg.	62 <u>1</u>	Deg.	621	Deg.	Distance

Distance.	27	Deg.	271	Deg.	271	Deg.	27}	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
-51	45.44	23.15	45.34	23.35	45.24	23.55	45.13	23.75	51
52 53	46.33	23.61 24.06	46.23 47.12	23.81 24.27	46.12 47.01	24.01 24.47	46.02 46.90	24.21 24.68	52 53
54	48.11	24.52	48.01	24.73	47.90	24.93	47.79	25.14	54
55 56	49.01	24.97 25.42	48.90	25.18	48.79	25.40	48.67	25.61	55
57	49.90 50.79	25.42	49.78 50.67	25.64 26.10	49.67 50.56	25.86 26.32	49.56 50.44	26.07 26.54	56 57
58	51.68	26.33	51.56	26.56	51.45	26.78	51.33	27.01	58
59 60	52.57 53.46	26.79 27.24	52.45 53.34	27.01 27.47	52.33 53.22	27.24 27.70	52.21 53.10	27.47	59 60
61	54.35	27.69	54.23	27.93	54.11	$\frac{27.70}{28.17}$	53.10	28.40	61
62	55.24	28.15	55.12	28.39	54.99	28.63	54.87	28.87	62
63	56.13	28.60	56.01	28.85	55.88	29.09	55.75	29.33	63
64 65	57.02 57.92	29.06 29.51	56.90 57.79	29.30 29.76	56.77 57.66	29.55 30.01	56.64 57.52	29.80 30.26	64 65
66	58.81	29.96	58.68	30.22	58.54	30.48	58.41	30.73	66
67	59.70	30.42	59.56	30.68	59.43 60.32	30.94	59.29	31.20	67
68 69	60.59	31.33	60.45	31.59	61.20	31.40	60.18	31.66 32.13	68 69
70	62.37	31.78	62.23	32.05	62.09	32.32	61.95	32.59	70
71	63.26	32.23	63.12	32.51	62.98	32.78	62.83	33.06	71
72 73	65.04	32.69 33.14	64.01 64.90	32.97 33.42	63.86 64.75	33.25 33.71	63.72	33.52 33.99	72
74	65.93	33.60	65.79	33.88	65.64	34.17	65.49	34.46	74
75	66.83	34.05	66.68	34.34	66.53	34.63	66.37	34.92	75
76 77	67.72	34.50	67.57 68.45	34.80 35.26	67.41 68.30	35.09	67.26 68.14	35.39 35.85	76 77
78	69.50	35.41	69.34	35.71	69.19	35.55 36.02	69.03	36.32	78
79	70.39	35.87	70.23	36.17	70.07	36.48	69.91	36.78	79
80	71.28	36.32	71.12	36.63	70.96	36.94	70.80	37.25	80
81 82	72.17 73.06	36.77 37.23	72.01 72.90	37.09 37.55	71.85 72.73	37.40 37.86	71.68	37.71 38.18	81 82
83	73.95	37.68	73.79	38.00	73.62	38.33	73.45	38.65	83
84	74.84	38.14	74.68	38.46	74.51	38.79	74.34	39.11	84
85 86	75.74	38.59 39.04	75.57 76.46	38.92 39.38	75.40 76.28	39.25 39.71	75.22 76.11	39.58 40.04	85 86
87	77.52	39.50	77.34	39.83	77.17	40.17	76.99	40.51	87
88	78.41	39.95	78.23 79.12	$ 40.29 \\ 40.75$	78.06	40.63	77.88	40.97	88
89 90	79.30	40.41 40.86	80.01	41.21	78.94 79.83	41.10	78.76 79.65	41.91	89 90
91	81.08	41.31	80.90	41.67	80.72	42.02	80.53	42.37	91
92	81.97	41.77	81.79	42.12	81.60	42.48	81.42	42.84	92
93 94	82.86 83.75	42.22 42.68	82.68 83.57	42.58 43.04	82.49 83.38	42.94 43.40	82.30 83.19	43.30 43.77	93 94
95	84.65	43.13	84.46	43.50	84.27	43.40	84.07	44.23	95
96	85.54	43.58	85.35	43.96	85.15	44.33	84.96	44.70	96
. 97 98	86.43 87.32	44.04 44.49	86.23 87.12	44.41 44.87	86.04 86.93	44.79 45.25	85.84 86.73	45.16 45.63	97 98
99	88.21	44.95	88.01	45.33	87.81	45.71	87.61	46.10	99
100	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46,56	100
8	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	n C8
Distance.	63 I	Deg.	621	Deg.	621	Deg.	621	Deg.	Distance

Dia	28 1	De g.	281	Deg.	281	Deg.	28 į	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8 9	0.88 1.77 2.65 3.53 4.41 5.30 6.18 7.06 7.95 8.83	0.47 0.94 1.41 1.88 2.35 2.82 3.29 3.76 4.23 4.69	0.88 1.76 2.64 3.52 4.40 5.29 6.17 7.05 7.93 8.81	0.47 0.95 1.42 1.89 2.37 2.84 3.31 3.79 4.26 4.73	0.88 1.76 2.64 3.52 4.39 5.27 6.15 7.03 7.91 8.79	0.48 0.95 1.43 1.91 2.39 2.86 3.34 3.82 4.29	0.88 1.75 2.63 3.51 4.38 5.26 6.14 -7.01 7.89 8.77	0.48 0.96 1.44 1.92 2.40 2.89 3.37 3.85 4.33 4.81	1 2 3 4 5 6 7 8 9
11	9.71	5.16	9.69	5.21	9.67	5.25	9.64	5.29	11
12	10.60	5.63	10.57	5.68	10.55	5.73	10.52	5.77	12
13	11.48	6.10	11.45	6.15	11.42	6.20	11.40	6.25	13
14	12.36	6.57	12.33	6.63	12.30	6.68	12.27	6.73	14
15	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.21	15
16	14.13	7.51	14.09	7.57	14.06	7.63	14.03	7.70	16
17	15.01	7.98	14.98	8.05	14.94	8.11	14.90	8.18	17
18	15.89	8.45	15.86	8.52	15.82	8.59	15.78	8.66	18
19	16.78	8.92	16.74	8.99	16.70	9.07	16.66	9.14	19
20	17.66	9.39	17.62	9.47	17.58	9.54	17.53	9.62	20
21	18.54	9.86	18.50	9.94	18.46	10.02	18.41	10.10	21
22	19.42	10.33	19.38	10.41	19.33	10.50	19.29	10.58	22
23	20.31	10.80	20.26	10.89	20.21	10.97	20.16	11.06	23
24	21.19	11.27	21.14	11.36	21.09	11.45	21.04	11.54	24
25	22.07	11.74	22.02	11.83	21.97	11.93	21.92	12.02	25
26	22.96	12.21	22.90	12.31	22.85	12.41	22.79	12.51	26
27	23.84	12.68	23.78	12.78	23.73	12.88	23.67	12.99	27
28	24.72	13.15	24.66	13.25	24.61	13.36	24.55	13.47	28
29	25.61	13.61	25.55	13.73	25.49	13.84	25.43	13.95	29
30	26.49	14.08	26.43	14.20	26.36	14.31	26.30	14.43	30
31	27.37	14.55	27.31	14.67	27.24	14.79	27.18	14.91	31
32	28.25	15.02	28.19	15.15	28.12	15.27	28.06	15.39	32
33	29.14	15.49	29.07	15.62	29.00	15.75	28.93	15.87	33
34	30.02	15.96	29.95	16.09	29.88	16.22	29.81	16.35	34
35	30.90	16.43	30.83	16.57	30.76	16.70	30.69	16.83	35
36	31.79	16.90	31.71	17.04	31.64	17.18	31.56	17.32	36
37	32.67	17.37	32.59	17.51	32.52	17.65	32.44	17.80	37
38	33.55	17.84	33.47	17.99	33.39	18.13	33.32	18.28	38
39	34.43	18.31	34.35	18.46	34.27	18.61	34.19	18.76	39
40	35.32	18.78	35.24	18.93	35.15	19.09	35.07	19.24	40
41	36.20	19.25	36.12	19.41	36.03	19.56	35.95	19.72	41
42	37.08	19.72	37.00	19.88	36.91	20.04	36.82	20.20	42
43	37.97	20.19	37.88	20.35	37.79	20.52	37.70	20.68	43
44	38.85	20.66	38.76	20.83	38.67	20.99	38.58	21.16	44
45	39.73	21.13	39.64	21.30	39.55	21.47	39.45	21.64	45
46	40.62	21.60	40.52	21.77	40.43	21.95	40.33	22.13	46
47	41.50	22.07	41.40	22.25	41.30	22.43	41.21	22.61	47
48	42.38	22.53	42.28	22.72	42.18	22.90	42.08	23.09	48
49	43.26	23.00	43.16	23.19	43.06	23.38	42.96	23.57	49
50	44.15	23.47	44.04	23.67	43.94	23.86	43.84	24.05	50
Distance.	Dep. 62 I	Lat. Deg.	Dep.	Lat. Deg.	Dep. 611	Lat. Deg.	Dep. 611]	Lat. Deg.	Distance.

Distance	28 I	eg.	281]	Deg.	281	Deg.	28 1]	Deg.	Distance
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Ince.
51	45.03	23.94	44.93	24.14	44.82	24.34	44.71	24.53	51
52 53	45.91 46.80	24.41 24.88	45,81 46.69	24.61 25.09	45.70 46.58	24.81 25.29	45.59 46.47	25.01 25.49	52 53
54	47.68	25.35	47.57	25.56	47.46	25.77	47.34	25.97	54
55	48.56	25.82	48.45	26.03	48.33	26.24 26.72	48.22 49.10	26.45 26.94	55 56
56 57	49.45 50.33	26.29 26.76	49.33 50,21	26.51 26.98	49.21 50.09	27.20	49.97	27.42	57
58	51.21	27 23	51.09	27.45	50.97	27.68	50.85	27.90	58
59 60	52.09 52.98	27.70 28.17	51.97 52.85	27.93 28.40	51.85 52.73	28.15 28.63	51.73 52.60	28.38 28.86	59 60
61	53.86	28.64	53.73	28.87	53.61	29.11	53.48	29.34	61
62	54.74	29.11	54.62	29.35	54.49	29.58	54.36 55.23	29.82 30.30	62 63
63 64	55.63 56.51	29.58 30.05	55.50 56.38	29.82 30.29	55.37 56.24	30.06	56.11	30.78	64
65	57.39	30.52	57.26	30.77	57.12	31.02	56.99	31.26	65
66 67	58.27 59.16	30,99 31.45	58.14 59.02	31.24	58.00 58.88	31.49	57.86 58.74	31.75 32.23	66 67
68	60.04	31.92	59.90	32.19	59.76	32.45	59.62	32.71	68
69	60.92	32.39	60.78	32.66	60.64	32.92	60.49	33.19	69
$\frac{70}{71}$	$\frac{61.81}{62.69}$	$\frac{32.86}{33.33}$	$\frac{61.66}{62.54}$	$\frac{33.13}{33.61}$	$\frac{61.52}{62.40}$	$\frac{33.40}{33.88}$	$\frac{61.37}{62.25}$	$\frac{33.67}{34.15}$	$\frac{70}{71}$
72	63.57	33.80	63.42	34.08	63.27	34.36	63.12	34.63	72
73	64.46	34.27	64.30	34.55	64.15	34.83	64.00	35.11	73
74 75	65.34	34.74 35.21	65.19 66.07	35.03 35.50	65.03 65.91	35.31	64.88	35.59 36.07	74 75
76	67.10	35.68	66.95	35.97	66.79	36.26	66.63	36.56	76
77	67.99	36.15	67.83	36.45	67.67	36.74	67.51	37.04	77
78 79	68.87	36.62 37.09	68.71 69.59	36.92 37.39	68.55 69.43	37.22 37.70	68.38 69.26	38.00	78 79
80	70.64	37.56	70.47	37.87	70.31	38.17	70.14	38.48	80
81	71.52	38.03	71.35	38.34	71.18	38.65	71.01	38.96	81
82	72.40 73.28	38.50	72.23 73.11	38.81 39.29	72.06 72.94	39.13 39.60	71.89	39.44 39.92	82
84	74.17	39.44	73.99	39.76	73.82	40.08	73.64	40.40	84
85 86	75.05	$\begin{vmatrix} 39.91 \\ 40.37 \end{vmatrix}$	74.88 75.76	40.23	74.70	40.56	74.52 75.40	40.88	85
87	76.82	40.84	76.64	41.18	76.46		76.28	41.85	87
88	76.82 77.70	41.31	77.52	41.65	77.34	41.99	77.15		88
89 90	78.58 79.47	41.78	78.40 79.28	42.13 42.60	78.21 79.09	42.47	78.03 78.91	42.81	89 90
91	80.35	42.72	80.16	43.07	79.97		79.78		91
92	81.23	43.19	81.04	43.55	80.85	43.90	80.66	44.25	92
93 94	82.11	43.66 44.13	81.92 82.80	44.02 44.49	81.73 82.61	44.38 44.85	81.54 82.41	44.73 45.21	93
95	83.88	44.60	83.68	44.97	83.49	45.33	83.29	45.69	95
96	84.76	45.07	84.57	45.44	84.87	45.81	84.17	46.17	96
97 98	85.65	45.54 46.01	85.45 86.33	45.91	85.25		85.04		97
99	87.41	46.48	87.21	46.86	87.00	47.24	86.80	47.62	99
100	88.29	46.95	88.09	47.33	87.88	-	87.67	-	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
Dist	62	Deg.	612	Deg.	61 1	Deg.	611	Deg.	, ig

Dist	29 I	Deg.	291 1	Deg.	291	Deg.	291	Deg.	Distance.
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	in Ce
1 2	0.87 1.75	0.48	0.87	0.49	0.87	0.49	0.87	0.50	1 2
3	2.62	1.45	2.62	1.47	2.61	1.48	2.60	1.49	3
4 5 6	3.50 4.37	1.94 2.42	3.49 4.36	1.95 2.44	3.48 4.35	1.97 2.46	3.47 4.34	1.98 2.48	4 5
6	5.25 6.12	2.91 3.39	5.23 6.11	2.93 3.42	5.22 6.09	2.95 3.45	5.21 6.08	2.98 3.47	67
8	7.00	3.88 4.36	6.98 7.85	3.91 4.40	6.96 7.83	3.94 4.43	6.95 7.81	3.97	8
10	7.87 8.75	4.85	8.72	4.89	8.70	4.92	8.68	4.96	10
11 12	.9.62 10.50	5.33 5.82	9.60 10.47	5.37 5.86	9.57	5.42 5.91	9.55 10.42	5.46 5.95	11 12
13	11.37	6.30	11.34	6.35	11.31	6.40	11.29	6.45	13
14 15	12.24 13.12	7.27	12.21 13.09	6.84 7.33	12.18 13.06	6.89 7.39	12.15 13.02	6.95 7.44	14 15
16 17	13.99 14.87	7.76 8.24	13.96 14.83	7.82 8.31	13.93 14.80	7.88 8.37	13.89 14.76	7.94 8.44	16 17
18	15.74	8.73	15.70	. 8.80	15.67	8.86	15.63	8.93	18
19 20	16.62 17.49	9.21 9.70	16.58 17.45	9.28 9.77	16.54 17.41	9.36 9.85	16.50 17.36	9.43	19 20
21	18.37	10.18	18.32	10.26	18.28	10.34	18.23	10.42	21
22 23	19.24 20.12	10.67	19.19 20.07	10.75 11.24	19.15 20.02	10.83 11.33	19.10 19.97	10.92 11.41	22 23
24 25	20.99 21.87	11.64 12.12	20.94 21.81	11.73	20.89 21.76	11.82 12.31	20.84 21.70	11.91	24 25
26	22.74	12.60	22.68	12.70	22.63	12.80	22.57	12.90	26
27 28	23.61 24.49	13.09 13.57	23.56 24.43	13.19 13.68	23.50 24.37	13.30 13.79	23.44 24.31	13.40 13.89	27 28
29 30	25.36 26.24	14.06 14.54	25.30 26.17	14.17 14.66	25.24 26.11	14.28 14.77	25.18 26.05	14.39	29 30
31	27.11	15.03	27.05	15.15	26.98	15.27	26.91	15.38	31
32 33	27.99 28.86	15.51 16.00	27.92 28.79	15.64	27.85 28.72	15.76 16.25	27.78 28.65	15.88 16.38	32 33
34	29.74 30.61	16.48 16.97	29.66 30.54	16.61	29.59	16.74	29.52 30.39	16.87	34
35 36	31.49	17.45	31.41	17.10 17.59	30.46 31.33	17.23 17.73	31.26	17.37 17.86	35 36
37 38	32.36 33.24	17.94 18.42	32.28 33.15	18.08	32.20 33.07	18.22 18.71	32.12 32.99	18.36 18.86	37 38
39	34.11	18.91	34.03	19.06	33.94	19.20	33.86	19.35	39
$\frac{40}{41}$	34.98 35.86	$\frac{19.39}{19.88}$	$\frac{34.90}{35.77}$	$\frac{19.54}{20.03}$	$\frac{34.81}{35.68}$	$\frac{19.70}{20.19}$	34.73 35.60	19.85	40
42	36.73	20.36 20.85	36.64 37.52	20.52	36.55	20.68	36.46	20.84	42
43 44	37.61 38.48	21.33	38.39	21.50	37.43 38.30	21.17	37.33 38.20	21.84 21.83	43 44
45 46	39.36 40.23	21.82 22.30	39.26 40.13	21.99 22.48	39.17 40.04	22.16 22.65	39.07 39.94	22.33 22.83	45 46
47	41.11	22.79	41.01	22.97	40.91	23.14	40.81	23.32	47
48 49	41.98 42.86	23.27 28.76	42.75	23.45 23.94	41.78 42.65	23.63 24.13	41.67		.48 49
50	43.73	24.24	43.62	24.43	43.52	24.62	43.41	-	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
Ö	61	Deg.	- 603	Deg.	603	Deg.	601	Deg.	Dist

Distance.	29]	Deg.	291	Deg.	291	Deg.	293	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51 52	44.61 45.48	24.73 25.21	44.50 45.37	24.92 25.41	44.39 45.26	25.11 25.61	44.28 45.15	25.31 25.80	51 52
53 54	46.35 47.23	25.69 26.18	46.24 47.11	$25.90 \\ 26.39$	46.13	26.10 26.59	46.01	26.30 26.80	53 54
55 56	48.10	26.66 27.15	47.99	26.87 27.36	47.00 47.87 48.74	27.08 27.58	47.75 48.62	27.29	55 56
57 58	49.85 50.73	27.63 28.12	49.73 50.60	27.85 28.34	49.61 50.48	28.07	49.49	27.79 28.28	57
59 60	51.60 52.48	28.60	51.48	28.83	51.35	29.05	50.36	28.78 29.28	58 59
61	53.35	$\frac{29.09}{29.57}$	$\frac{52.35}{53.22}$	$\frac{29.32}{29.81}$	$\frac{52.22}{53.09}$	$\frac{29.55}{30.04}$	$\frac{52.09}{52.96}$	$\frac{29.77}{30.27}$	60
62 63	54.23 55.10	30.06 30.54	54.09 54.97	$\frac{30.29}{30.78}$	53.96 54.83	$30.53 \\ 31.02$	53.83 54.70	30.77	62 63
64 65	55.98	31.03 31.51	55.84 56.71	$\frac{31.27}{31.76}$	55.70 56.57	31.52 32.01	55.56 56.43	31.76	64 65
66	57.72 58.60	32.00 32.48	57.58 58.46	$32.25 \\ 32.74$	57.44 58.31	32.50 32.99	57.30	32.75	66
68 69	59.47 60.35	32.97 33.45	59.33	33.23	59.18	33.48	58.17 59.04	33.25 33.74	67 68
70	61.22	33.94	$60.20 \\ 61.07$	$\frac{33.71}{34.20}$	$60.05 \\ 60.92$	$\frac{33.98}{34.47}$	59.91	34.24 34.74	69 70
71 72	62.10 62.97	$34.42 \\ 34.91$	$61.95 \\ 62.82$	34.69 35.18	$61.80 \\ 62.67$	34.96 35.45	61.64 62.51	35.23 35.73	71 72
73	63.85 64.72	35.39 35.88	63.69 64.56	35.67	63.54	35.95 36.44	63.38	36.22	73 74
75 76	65.60 66.47	36.36 36.85	65.44 66.31	36.65 37.14	65.28	36.93 37.42	65.11	37.22 37.71	75 76
77 78	67.35 68.22	37.33 37.82	67.18 68.05	37.62 38.11	67.02	37.92	66.85	38.21	77
79 80	69.09	38.30 38.78	68.93	38.60	67.89	38.41	67.72 68.59	38.70 39.20	78 79
81	70.84	39.27	$\frac{69.80}{70.67}$	$\frac{39.09}{39.58}$	$\frac{69.63}{70.50}$	$\frac{39.39}{39.89}$	$\frac{69.46}{70.32}$	$\frac{39.70}{40.19}$	$\frac{80}{81}$
82 83	71.72 72.59	$\frac{39.75}{40.24}$	71.54	40.07	71.37 72.24	$\frac{40.38}{40.87}$	71.19 72.06	40.69	82 83
84 85	73.47	40.72 41.21	73.29 74.16	41.04 41.53	73.11 73.98	41.36 41.86	72.93 73.80	41.68 42.18	84
86 87	75.22 76.09	41.69 42.18	75.03 75.91	42.02 42.51	74.85	42.35 42.84	74.67 75.53	42.67	86
88 89	76.97 77.84	42.66	76.78	43.00	76.59	43.33	76.40	43.67	88
90	78.72	43.63	78.52	43.98	77.46 78.33	44.32	77.27 78.14	44.16 44.66	89
91 92	79.59 80.46	44.12 44.60	79.40 80.27	44.46 44.95	79.20	44.81 45.30	79.01 79.87	45.16 45.65	91 92
93	81.34	$45.09 \\ 45.57$	81.14 82.01	45.44 45.93	80.94	45.80 46.29	80.74	46.15 46.64	93
95 96	83.09 83.96	46.06 46.54	82.89 83.76	46.42 46.91	82.68 83.55	46.78 47.27	82.48 83.35	47.14 47.64	95 96
97 98	84.84 85.71	47.03 47.51	84.63 85.50	47.40 47.88	84.42 85.29	47.77	84.22 85.08	48.13	97 98
99	86.59 87.46	48.00	86.38 87.25	48.37	86.17 87.04	48.75	85.95 86.82	49.13	99
_	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	61 I	Deg.	603	Deg.	601	Deg.	601	Deg.	Distance.

Distance	30 I	Deg.	301	Deg.	301	Deg.	301	Deg.	Distance.
nnce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1	0.87 1.73	0.50	0.86 1.73	0.50	0.86	0.51 1.02	$0.86 \\ 1.72$	0.51 1.02	1 2
2 3 4 5 6 7	2.60	1.50	2.59	1.51	2.58	1.52	2.58	1.53	2 3 4 5 6
4	3.46 4.33	2.00 2.50	3.46 4.32	2.02 2.52	3.45 4.31	2.03 2.54	3.44 4.30	2.05 2.56	4
6	5.20	3.00	5.18	3.02	5.17	3.05	5.16	3.07	8
8	6.06	3.50 4.00	6.05	3.53 4.03	6.03	3.55 4.06	6.02	3.58 4.09	7 8
9	7.79	4.50	7.77	4.53	7.75	4.57	7.73	4.60	9
10	8.66	5.00	8.64	5.04	8.62	5.08	8.59	5-11	10
11 12	9.53 10.39	5.50 6.00	9.50 10.37	5.54 6.05	9.48 10.34	5.58 6.09	9.45 10.31	5.62 6.14	11 12
13	11.26	6.50	11.23	6.55	11.20	6.6	11.17	6.65	13
14 15	12.12 12.99	7.00 7.50	12.09 12.96	7.05 7.56	12.06 12.92	7.11 7.61	12.03 12.89	7.16 7.67	14 15
16	13.86	8.00	13.82	8.06	13.79	8.12	13.75	8.18	16
17	14.72 15.59	8.50 9.00	14.69 15.55	8.56 9.07	14.65 15.51	8.63 9.14	14.61 15.47	8.69 9.20	17 18
19	16.45	9.50	16.41	9.57	16.37	9.64	16.33	9.71	19
$\frac{20}{21}$	$\frac{17.32}{18.19}$	$\frac{10.00}{10.50}$	$\frac{17.28}{18.14}$	$\frac{10.08}{10.58}$	17.23	$\frac{10.15}{10.66}$	$\frac{17.19}{18.05}$	$\frac{10.23}{10.74}$	20 21
22	19.05	11.00	19.00	11.08	18.96	11.17	18.91	11.25	22
23 24	19.92 20.78	11.50 12.00	19.87 20.73	11.59 12.09	19.82 20.68	11.67 12.18	19.77	11.76 12.27	23 24
25	21.65	12.50	21.60	12.59	21.54	12.69	21.49	12.78	25
26 27	22.52 23.38	13.00 13.50	22.46 23.32	13.10 13.60	22.40 23.26	13.20 13.70	22.34 23.20	13.29 13.80	26 27
28	24.25	14.00	24.19	14.11	24.13	14.21	24.06	14.32	28
29 30	25.11 25.98	14.50 15.00	25.05 25.92	14.61 15.11	24.99 25.85	14.72 15.23	24.92 25.78	14.83 15.34	29 30
31	26.85	15.50	26.78	15.62	26.71	15.73	26.64	15.85	31
32 33	27.71 28.58	16.00	27.64	16.12	27.57	16.24	27.50	16.36	32
84	29.44	16.50 17.00	28.51 29.37	16.62 17.13	28.43 29.30	16.75 17.26	28.36 29.22	16.87 17.38	33 34
35 36	30.31	17.50 18.00	30.23	17.63 18.14	30.16	17.76 18.27	30.08	17.90 18.41	35
37	32.04	18.50	31.10	18.64	31.02	18.78	30.94 31.80	18.92	36 37
38 39	32.91 33.77	19.00 19.50	32.83	19.14	32.74	19.29 19.79	32.66	19.43	38
40	34.64	20.00	33.69 34.55	19.65 20.15	33.60 34.47	20.30	33.52 34.38	19.94 20.45	39 40
41	35.51	20.50	35.42	20.65	35.33	20.81	35.24	20.96	41
42	36.37 37.24	21.00 21.50	36.28 37.14	21.16 21.66	36.19 37.05	21.32 21.82	36.10 36.95	21.47	42 43
44	37.24 38.11	22.00	38.01	22.17	37.91	22.33	37.81	22.50	44
45 46	38.97 39.84	22.50 23.00	38.87 39.74	22.67 23.17	38.77 39.63	22.84 23.35	38.67 39.53	23.01	45 46
47	40.70	23.50	40.60	23.68	40.50	23.85	40.39	24.03	47
48 49	41.57	24.00 24.50	41.46	24.18 24.68	41.36	24.36 24.87	41.25 42.11	24.54	48 49
50	43.30	25.00	43.19	25.19	43.08	25.38	42.97	25.56	50
en ce	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Let.	nce.
Dista	60 1	Deg.	59 1	Deg.	59½	Deg.	591	Deg.	Distance.

Dist	30 I	Deg.	301	Deg.	301	Deg.	30}	Deg.	CISC
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	44.17	25.50	44.06	25.69	43.94	25.88	43.83	26.08	5
52	45.03	26.00	44.92	26.20	44.80	26.39	44.69	26.59	5
53	45.90	26.50	45.78	26.70	45.67	26.90	45.55	27.10	5
54	46.77	27.00 27.50	46.65	27.20	46.53	27.41	46.41	27.61	5
55	47.63	27.50	47.51	27.71	47.39	27.91	47.27	28.12	5.
56	48.50	28.00	48.37	28.21	48.25	28.42	48.13	28.63	5
57	49.36	28.50	49.24	28.72	49.11	28.93	48.99	29.14	5
58 59	50.23	29.00	50.10 50.97	29.22 29.72	49.97	29.44	49.85 50.70	29.65	5
60	51.10 51.96	29.50	51.83	30.23	51.70	30.45	51.56	30.68	6
61		-	52.69	30.73	52.56	30.96	52.42	31:19	6
62	52.83 53.69	$\frac{30.50}{31.00}$	53.56	31 93	53.42	31.47	53.28	31.70	6
63	54.56	31.50	54.42	$\frac{31.23}{31.74}$	54.28	31.97	54.14	32.21	6
64	55.43	32.00	55.29	32.24	55.14	32.48	55.00	32.72	6
65	56.29	32.50	56.15	32.75	56.01	32.99	55.86	33.23	6
66	57.16	33.00	57.01	33.25 33.75	56.87	33.50	56.72	33.75	6
67	58.02	33.50	57.88	33.75	57.73	34.01	57.58	34.26	6
68	58.89	34.00	58.74	34.26	58.59	34.51	58.44	34.77	6
69	59.76	34.50	59.60	34.76	59.45	35.02	59.30	35.28	6
70	60.62	35.00	60.47	35.26	60.31	35.53	60.16	35.79	7
71	61.49	35.50	61.33	35.77	61.18	36.04	61.02	36.30	7
72	62.35	36.00	62.20	36.27	62.04	36.54	61.88	36.81	7
73	63.22	36.50	63.06	36.78	$62.90 \\ 63.76$	37.05	62.74	37.32 37.84	7
74 75	$64.09 \\ 64.95$	37.00 37.50	$63.92 \\ 64.79$	37.28 37.78	64.62	38.07	64.46	38.35	7
76	65.82	38.00	65.65	38.29	65.48	38.57	65.31	38.86	7
77	66.68	38.50	66.52	38.79	66.35	39.08	66.17	39.37	7
78	67.55	39.00	67.38	39.29	67.21	39.59	67.03	39.88	7
79	68.42	39.50	68.24	39.80	68.07	40.10	67.89	40.39	7
80	69.28	40.00	69.11	40.30	68.93	40.60	68.75	40.90	8
81	70.15	40.50	69.97	40.81	69.79	41.11	69.61	41.41	8
82	71.01	41.00	70.83	41.31	70.65	41.62	70.47	41.93	8
83	71.88	41.50	71.70	41.81	71.52	42.13	71.33	42.44	8
84	72.75	42.00	72.56	42.32	72.38	42.63 43.14	72.19	$42.95 \\ 43.46$	8
85	73.61	$\frac{42.50}{43.00}$	73.43 74.29	$\frac{42.82}{43.32}$	73.24 74.10	43.65	73.91	43.97	8
86	74.48	43.50	75.15	43.83	74.96	44.16	74.77	44.48	8
88	76.21	44.00	76.02	44.33	75.82	44.66	75.63	44.99	8
89	77.08	44.50	76.88	44.84	76.68	45.17	76.49	45.51	8
90	77.94	45.00	77.75	45.34	77.55	45.68	77.35	46.02	9
91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53	9
92	79.67	46.00	79.47	46.35	79.27	46.69	79.07	47.04	9
93	80.54	46.50	80.34	46.85	80.13	47.20	79.92	47.55	9
94	81.41	47.00	81.20	47.35	80.99	47.71	80.78	48.06	9
95	82.27	47.50	82.06	47.86	81.85	48.22	81.64	48.57	9
96	83.14	48.00	82.93	48.36	82.72 83.58	$48.72 \\ 49.23$	82.50	49.08	9
97	84.00	48.50	83.79	48.87	84.44	49.23	83.36	49.60 50.11	9
98	84.87	49.50	85.52	49.87	85.30	50.25	85.08	50.62	9
100	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	10
-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	904
Distance.	60	Deg.	593	Deg.	591	Deg.	591	Deg.	Distance

Distance	31	Dog.	314]	Deg.	314	Deg.	311	Deg.	Distance.
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
34 455 677 889 910 111 122 133 144 155 166 177 188 199 200 212 223 224 226 227 228 239 300 313 323 333 335 355 365 377	0.86 1.71 2.57 3.43 5.14 6.86 7.71 8.57 9.43 11.14 12.00 13.71 14.57 16.29 17.14 18.00 18.86 19.71 20.57 21.43 22.29 24.86 19.71 20.57 21.43 22.29 24.86 25.71 26.57 27.43 28.29 29.14 30.00 30.86 30.77	0.51 1.03 1.55 2.06 2.58 3.61 4.12 4.64 5.15 5.67 6.18 9.27 10.30 10.82 11.33 11.85 12.88 13.99 13.91 14.94 15.45 15.45 15.97 16.48 17.00 17.51 18.03 18.54 19.03	1.0	0.52 1.04 1.56 2.59 3.11 3.63 4.67 5.19 5.71 6.23 6.74 7.78 8.30 8.32 8.32 9.34 9.36 10.38 11.41 11.93 12.45 12.49 14.01 14.53 15.04 16.08 16.08 17.12 17.64 18.16 18.16 19.19	0.85 1.71 2.56 3.41 4.26 5.12 5.97 6.82 7.67 8.53 9.38 10.23 11.94 12.76 11.96 12.36 11.94 12.76 19.61 20.46 21.32 22.17 23.02 23.87 24.73 25.58 26.43 27.28 28.14 28.99 29.84 30.70	0.52 1.04 1.57 2.09 3.13 3.66 4.18 4.70 5.22 5.75 6.79 7.84 8.36 8.88 8.88 8.99 9.93 10.45 10.45 10.47 11.49 12.02 13.06 13.58 14.11 14.63 15.15 16.72 17.76 18.29 18.81 19.33	0.85 1.70 2.55 3.40 4.25 5.10 6.80 7.65 8.50 9.35 10.20 11.05 11.90 12.76 13.61 14.46 15.31 16.16 17.86 18.71 19.56 20.416 22.11 22.96 22.11 22.96 23.81 24.66 23.81 24.66 25.51 28.06 28.91 29.76 30.616	0.53 1.05 1.05 1.58 2.10 2.63 3.68 4.21 4.74 5.26 5.79 6.31 7.37 7.89 8.42 11.05 11.58 12.10 12.63 13.68 14.21 13.68 14.21 13.68 14.21 13.68 14.21 13.68 14.73 15.26 15.79 16.84 17.37 16.84 17.37 16.84 17.37 16.84 17.37 16.84 17.37 16.84 17.37 18.42 18.94 19.41	12345678910 112314456178920 2122234256728930 31323435637
38 39 40	32.57 33.43 34.29	19.57 20.09 20.60	32.49 33.34 34.20	19.71 20.23 20.75	32.40 33.25 34.11	19.85 20.38 20.90	32.31 33.16 34.01	20.00 20.52 21.05	38 39 4 0
41 42 43 44 45 46 47 48 49 50	35.14 36.00 36.86 37.72 38.57 39.43 40.29 41.14 42.00 42.86	21.12 21.63 22.15 22.66 23.18 23.69 24.21 24.72 25.24 25.75	35.05 35.91 36.76 37.62 38.47 39.33 40.18 41.04 41.89 42.75	21.27 21.79 22.31 22.83 23.34 23.86 24.38 24.90 25.42 25.94	34.96 35.81 36.66 37.52 38.37 39.22 40.07 40.93 41.78 42.63	21.42 21.94 22.47 22.99 23.51 24.03 24.56 25.60 26.12	34.86 35.71 36.57 37.42 38.27 39.12 39.97 40.82 41.67 42.52	21.57 22.10 22.63 23.15 23.68 24.21 24.73 25.26 25.78 26.31	41 42 43 44 45 46 47 48 49 50
Distance.	Dep. 59 1	Lat. Deg.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep. 581	Lat.	Distance.

Diat	- 31	Deg.	311	Deg.	311	Deg.	313	Deg.	Dia
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	tance.
51	43.72	26.27	43.60	26.46	43.48	26.65	43.37	26.84	51
52	44.57	26.78	44.46	26.98	44.34	27.17	44.22	27.36	52
53	45.43	27.30	45.31	27.49	45.19	27.69	45.07	27.89	53
54 55	46.29 47.14	27.81 28.33	46.17	28.01 28.53	46.04	28.21	45.92	28.42 28.94	54 55
56	48.00	28.84	47.88	29.05	47.75	28.74 29.26	47.62	29.47	56
-57	48.86	29.36	48.73	29.57	48.60	29.78	48.47	29.99	57
58	49.72	29.87	49.58	30.09	49.45	30.30	49.32	30.52	58
59	50.57	30.39	50.44	30.61	50.31	30.83	50.17	31.05	59
60	51.43	30.90	51.29	31.13	51.16	31.35	51.02	31.57	60
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10	61
62	53.14	31.93	53.00	32.16	52.86	32.39	52.72	32.63	62
63	54.00	32.45	53.86	32.68	53.72	32.92	53.57	33.15	63 64
64 65	54.86 55.72	32.96 33.48	54.71 55.57	33.20 33.72	54.57 55.42	33.44 33.96	54.42 55.27	33.68 34.20	65
66	55.72 56.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73	66
67	57.43	34.51	57.28	34.76	57.13	35.01	56.98	35,26	67
68	58.29	35.02	58.13	35.28	57.98	85.53	57.82	35.78	68
69	59.14	35.54	58.99	35.80	58.83	36.05	58.67	36.31	69
70	60.00	36.05	59.84	36.31	59,68	36.57	59.52	36.83	70
71	60.86	36.57	60.70	36.83	60.54	37.10	60.37	37.36	71
72	61.72	37.08	61.55	37.35	61.39	37.62	61.23	37.89	72
73	62.57 63.43	37.60 38.11	62.41	37.87 38.39	62.24 63.10	38.14 38.66	62.08 62.93	38.41 38.94	73 74
74 75	64.29	38.63	64.12	38.91	63.95	39.19	63.78	39.47	75
76	65.14	39.14	64.97	39.43	64.80	39.71	64.63	39.99	76
77	66.00	39.66	65.83	39.95	65.65	40.23	65.48	40.52	77
78	66.86	40.17	66.68	40.46	66.51	40.75	66.33	41.04	78
79	67.72	40.69	67.54	40.98	67.36	41.28	67.18	41.57	79
80	68.57	41.20	68.39	41.50	68.21	41.80	58.03	42.10	80
81	69.43	41.72	69.25	42.02	69.06	42.32	68.88	42.62	81
82	70.29	42.23 42.75	70.10	42.54 43.06	69.92 70.77	42.84	69.73	43.15 43.68	82 83
83 84	71.14 72.00	43.26	71.81	43.58	71.62	43.89	71.43	44.20	84
85	72.86	43.78	72.67	44.10	72.47	44.41	72.28	44.73	85
86	73.72	44.29	73.52	44.61	73.33	44.93	73.13	45.25	86
87	74.57	44.81	74.38	45.13	74.18	45.46	73.98	45.78	87
88	75.43	45.32	75.23	45.65	75.03	45.98	74.83	46.31	88
89	76.29	45.84	76.09	46.17	75.88	46.50	75.68 76.53	46.83	89 90
90	77.15	46.35	76.94		76.74	47.02	77.38	47.89	91
91	78.00 78.86	46.87	77.80 78.65	47.21 47.73	77.59 78.44	47.55 48.07	78.23	48.41	91
92 93	79.72	47.38 47.90	79.51	48.25	79.30	48.59	79.08	48.94	93
94	80.57	48.41	80.36	48.76	80.15	49.11	79.93	49.47	94
95	81.43	48.93	81.22	49.28	81.00	49 -64	80.78	49.99	95
96	82.29	49.44	82.07	49.80	81.85	50.16	81.63	50.52	96
97	93.15	49.96	82.93	50.32	82.71	50.68	82.48	51.04 51.57	97
98 99	84.00 84.86	50.47 50.99	83.78	50.84 51.36	83.56 84.41	51.20 51.73	83.33 84.18	52.10	99
100	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	100
					l		l		1
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
ist	50		500	n	503	D	F01	Diam	i
Ä	-59 I	Deg.	58 ‡	Deg.	58 <u>1</u>	Deg.	584	Deg.	a
1	l		H		.		504 Dog.		1

Distance	32]	Dog.	321	Deg.	321	Deg.	351	Deg.	Distance
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	nce.
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0.85 1.70 2.54 3.39 4.24 5.09 6.78 7.63 8.48 9.33 10.18 11.02 11.87	0.53 1.06 1.59 2.12 2.65 3.18 3.71 4.24 4.77 5.30 5.83 6.36 6.89 7.42 7.95	0.85 1.69 2.54 3.38 4.23 5.07 5.92 6.77 7.61 8.46 9.30 10.15 10.99 11.84 12.69	0.53 1.07 1.60 2.13 2.67 3.20 3.74 4.27 4.80 5.34 5.87 6.40 6.94 7.47 8.00	0.84 1.69 2.53 3.37 4.22 5.06 5.90 6.75 7.59 8.43 9.28 10.12 10.96 11.81	0.54 1.07 1.61 2.15 2.69 3.22 3.76 4.30 4.84 5.37 5.91 6.45 6.98 7.52 8.06	0.84 1.68 2.52 3.36 4.21 5.05 5.89 6.73 7.57 8.41 9.25 10.09 10.93 11.77 12.62	0.54 1.08 1.62 2.16 2.70 3.25 3.79 4.33 4.87 5.41 5.95 6.49 7.03 7.57 8.11	. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
16 17 18 19 20 21	13.57 14.42 15.26 16.11 16.96 17.81	8.48 9.01 9.54 10.07 10.60 11.13	13.53 14.38 15.22 16.07 16.91	8.54 9.07 9.61 10.14 10.67	13.49 14.34 15.18 16.02 16.87	8.60 9.13 9.67 10.21 10.75 11.28	13.46 14.30 15.14 15.98 16.82	8.66 9.20 9.74 10.28 10.82	16 17 18 19 20 21
22 23 24 25 26 27 28 29 30	18.66 19.51 20.35 21.20 22.05 22.90 23.75 24.59 25.44	11.66 12.19 12.72 13.25 13.78 14.31 14.84 15.37	18.61 19.45 20.30 21.14 21.99 22.83 23.68 24.53 25.37	11.74 12.27 12.81 13.34 13.87 14.41 14.94 15.47 16.01	18.55 19.40 20.24 21.08 21.93 22.77 23.61 24.46 25.30	11.82 12.36 12.90 13.43 13.97 14.51 15.04 15.58 16.12	18.50 19.34 20.18 21.03 21.87 22.71 23.55 24.39 25.23	11.90 12.44 12.98 13.52 14.07 14.61 15.15 15.69 16.23	22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	26.29 27.14 27.99 28.83 29.68 30.53 31.38 32.23 33.07 33.92	16.43 16.96 17.49 18.02 18.55 19.08 19.61 20.14 20.67 21.20	26.22 27.06 27.91 28.75 29.60 30.45 31.29 32.14 32.98 33.83	16.54 17.08 17.61 18.14 18.68 19.21 19.74 20.28 20.81 21.34	26.15 26.99 27.83 28.68 29.52 30.36 31.21 32.05 32.89 33.74	16.66 17.19 17.73 18.27 18.81 19.34 19.88 20.42 20.95 21.49	26.07 26.91 27.75 28.60 29.44 30.28 31.12 31.96 32.80 33.64	16.77 17.31 17.85 18.39 18.93 19.48 20.02 20.56 21.10 21.64	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	34.77 35.62 36.47 37.31 38.16 39.01 39.86 40.71 41.55 42.40	21.73 22.26 22.79 23.32 23.85 24.38 24.91 25.44 25.97 26.50	34.67 35.52 36.37 37.21 38.06 38.90 39.75 40.59 41.44 42.29	21.88 22.41 22.95 23.48 24.01 24.55 25.08 25.61 26.15 26.68	34.58 35.42 36.27 37.11 37.95 38.80 39.64 40.48 41.33 42.17	22.03 22.57 23.10 23.64 24.18 24.72 25.25 25.79 26.33 26.86	34.48 35.32 36.16 37.01 37.85 38.69 39.53 40.37 41.21 42.05	22.18 22.72 23.26 23.80 24.34 24.88 25.43 25.97 26.51 27.05	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat.	Dep.	Lat. Deg.	Dep,	Lat.	Dep. 571	Lat.	Distance.

Distance.	32 I	Deg.	321	Deg.	. 32 <u>1</u>	Deg.	321	Deg.	Distance
100	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	nce.
51 52	43.25 44.10	27.03 27.56	43.13 43.98	27.21 27.75	43.01 43.86	27.40 27.94	42.89 43.73	27.59 28.13	51 52
53	44.95	28.09	44.82	28.28	44.70	28.48	44.58	28.67	53
54 55	45.79 46.64	28.62 29.15	45.67 46.51	28.82 29.35	45.54	29.01 29.55	45.42 46.26	29.21 29.75	5 <u>4</u> 55
56	47.49	29.68	47.36	29.88	47.23	30.09	47.10	30.29	56
57 58	48.34 49.19	30.21 30.74	48.21 49.05	30,42 30.95	48.07	30.63 31.16	47.94 48.78	30.84 31.38	57 58
59 60	50.03	31.27	49.90	31.48	49.76	31.70	49.62	81.92	59
61	$\frac{50.88}{51.73}$	$\frac{31.80}{32.33}$	$\frac{50.74}{51.59}$	$\frac{32.02}{32.55}$	$\frac{50.60}{51.45}$	$\frac{32.24}{32.78}$	50.46	33.00	60
62	52.58	32.85	52.44	33.08	52.29	33.31	52.14	33.54	62
63 64	53.43 54.28	33.38 33.91	53.28 54.13	33.62 34.15	53.13 53.98	33.85 34.39	52.99 53.83	34.08 34.62	68 64
65 66	55.12	34.44	54.97	34.68	54.82	34.92	54.67	35.16	65 66
67	55.97 56.82	34.97 35.50	55.82 56.66	35.22 35.75	55.66 56.51	35.46 36.00	55.51 56.35	35.70 86.25	67
68 69	57.67 58.52	36.03 36.56	57.51 58.36	36.29 36.82	57.85 58.19	36.54 37.07	57.19 58.03	36.79 37.33	68 69
70	59.36	37.09	59.20	37.35	59.04	37.61	58.87	37.87	70
71 72	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	71
73	61.91	38.15 38.68	60.89	38.42 38.95	60.72	38.69 39.22	60.55	38.95 39.49	72 73
74 75	62.76 63.60	39.21 39.74	62.58 63.43	39.49 40.02	62.41 63.25	39.76 40.30	62.24 63.08	40.03	74 75
76	64.45	40.27	64.28	40.55	64.10	40.83	63.92	41.11	76
77	65.30 66.15	40.80 41.33	65.12 65.97	41.09	64.94	41.37	64.76 65.60	41.65	77 78
79	67.00	41.86	66.81	42.16	66.63	42.45	66.44	42.74	79
80	$\frac{67.84}{68.69}$	$\frac{42.39}{42.92}$	67.66	$\frac{42.69}{43.22}$	67.47	$\frac{42.98}{43.52}$	$\frac{67.28}{68.12}$	43.28	80
82	69.54	43.45	69.35	43.76	68.31 69.16	44.06	68.97	44.36	82
83 84	70.89 71.24	43.98 44.51	70.20 71.04	44.29 44.82	70.00	44.60 45.13	69.81 70.65	44.90 45.44	83 84
85	72.08	45.04	71.89	45.36	71.69	45.67	71.49	45.98	85
86 87	72.93 73.78	45.57 46.10	72.73	45.89	72.53	46.21	72.33 73.17	46.52	86 87
88	74.63	46.63	74.42	46.96	74.22	47.28	74.01	47.61	88
89 90	75.48 76.32	47.16 47.69	75.27 76.12	47.49	75.06 75.91	47.82 48.36	74.85 75.69	48.15	89 90
91	77.17	48.22	76.96	48.56	76.75	48.89	76.53	49.23	91
92 93	78.02	48.75 49.28	77.81	49.09	77.59 78.44	49.43	77.38 78.22	49 .77 50.31	92 93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
95 96	80.56 81.41	50.34 50.87	80.34	50.69	80.12 80.97	51.04	79.90 80.74	51.39 51.93	95 96
97 98	82.26 83.11	51.40 51.93	82.04 82.88	51.76 52.29	81.81	52.12 52.66	81.58 82.42	52.47 53.02	97
99	83.96	52.46	83.73	52.83	82.65 83.50	53.19	83.26	53.56	99
100	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
Dist	58]	Dog.	57}	Deg.	571	Deg.	571	Deg.	Dist

R

Distance	83	Dog.	331	Deg,	331	Deg.	33}	Deg.	Distance
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Б Се.
1 23 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.84 1.68 2.52 3.35 4.19 5.03 5.87 6.71 7.55 8.89 9.23 10.06 10.90 11.74 12.58 13.42 14.26 15.10	0.54 1.09 1.63 2.18 2.72 3.27 3.27 3.81 4.36 4.90 5.45 7.08 7.62 7.62 7.62 7.62 7.62 7.62 7.62 7.63	0.84 1.67 2.51 3.95 4.18 5.02 5.85 6.69 7.53 8.36 9.20 10.04 10.87 11.71 12.54 13.38 14.22 15.05 15.89	0.55 1.10 1.64 2.174 3.29 3.84 4.39 4.93 5.48 6.03 6.58 7.13 7.68 8.22 8.77 9.87 10.42	0.83 1.67 2.50 3.34 4.17 5.00 5.84 9.17 10.01 10.84 11.67 12.51 13.34 14.18 15.01 15.68	0.55 1.10 1.66 2.76 3.31 3.86 4.42 4.97 5.60 7.18 8.83 9.38 9.38 10.49	0.83 1.66 2.49 3.43 4.16 4.99 5.65 7.48 8.31 9.15 9.98 10.81 11.64 12.47 13.80 14.13 14.97 15.80	0.56 1.11 1.67 2.22 2.78 3.33 3.89 4.44 4.44 6.67 7.22 7.78 8.33 8.89 9.44 10.00 10.56	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19
21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36	16.77 17.61 18.45 19.29 20.13 20.97 21.81 22.64 24.32 25.16 26.84 27.68 28.51 29.35 30.19 31.03	10.89 11.44 11.98 12.53 13.07 13.62 14.16 14.71 15.25 15.79 16.34 16.88 17.43 17.97 18.52 19.06 19.61	16.73 17.56 18.40 19.23 20.07 20.91 21.74 22.58 23.42 24.25 25.09 25.92 26.76 28.43 29.27 30.11 30.94	10.97 11.51 12.06 12.61 13.16 13.71 14.26 14.80 15.35 15.90 16.45 17.00 17.55 18.09 18.64 19.19 19.74	16.68 17.51 18.35 19.18 20.01 20.85 21.68 22.51 23.35 24.18 25.02 25.85 26.68 27.52 28.35 29.19 30.02	11.04 11.59 12.14 12.69 13.25 13.80 14.35 14.90 15.45 16.01 16.56 17.11 17.66 18.21 18.77 19.32 19.87 20.42	16:63 17.46 18:29 19:19:96 20:79 21:62 22:45 23:28 24:11 24:94 25:78 26:61 27:44 28:27 29:10 29:93 30:76	11.11 11.67 12.28 12.78 13.33 13.89 14.44 15.00 16.67 17.22 17.78 18.33 18.89 19.44 20.00 20.56	20 22 22 23 24 25 26 27 28 29 31 32 33 34 35 36 37 38 39 39 39 39 39 39 39 39 39 39 39 39 39
37 38 39 40 41 42 43 44 45 46 47 48 49 50	31.87 32.71 33.55 34.39 35.22 36.06 36.90 37.74 38.58 39.42 40.26 41.09 41.93	20.13 20.70 21.24 21.79 22.33 22.87 23.42 23.96 24.51 25.05 25.60 26.14 26.69 27.23	31.78 32.62 33.45 34.29 35.12 35.96 36.80 37.63 38.47 39.31 40.14 40.98 41.81	20.29 20.84 21.38 21.93 22.48 23.03 23.58 24.12 24.67 25.22 25.77 26.32 26.87 27.41	31.69 32.52 33.36 34.19 35.02 35.86 36.69 37.52 38.36 39.19 40.03 40.86 41.69	20.42 20.97 21.53 22.08 22.63 23.18 23.73 24.29 24.84 25.39 25.94 26.49 27.04 27.60	31.60 32.43 33.26 34.09 34.92 35.75 36.58 37.42 38.25 39.08 39.91 40.74 41.57	20.36 21.11 21.67 22.22 22.78 23.33 23.89 24.45 25.56 26.11 26.67 27.22 27.78	37 38 39 40 41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep. 561	Lat. Deg.	Distance.

Distance.	33	Deg.	331	Deg.	331	Deg.	331	Deg.	Dist
ınce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Distance.
51	42.77	27.78	42.65	27.96	42.53	28.15	42.40	28.33	5
52	43.61	28.32	43.49	28.51	43.36	28.70 29.25	43.24	28.89	5
53 54	44.45 45.29	28.87	44.32	29.06	44.20		44.07	29.45	5
55	46.13	29.41 29.96	45.16 46.00	29.61 30.16	45.03 45.86	29.80 30.36	44.90	30.00	5
56	46.97	30.50	46.83	30.70	46.70	30.91	45.73 46.56	$30.56 \\ 31.11$	5
57	47.80	31.04	47.67	31.25	47.53	31.46	47.30	31.67	5
58	48.64	31.59	48.50	31.80	48.37	32.01	48.23	32.22	5
59	49.48	32.13	49.34	32.35	49.20	32.56	49.06	32.78	5
60	50.32	32.68	50.18	32.90	50.03	33.12	49.89	33.33	60
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89	6
62 63	52.00	33.77	51.85	33.99	51.70	34.22	51.55	34.45	65
64	52.84 53.67	34.31 34.86	52.69	34.54 35.09	52.53 53.37	$\frac{34.77}{35.32}$	52.38	35.00	6
65	54.51	35.40	53.52 54.36	35.64	54.20	35.88	53.21 54.05	35.56	64
66	55.35	35.95	55.19	36.19	55.04	36.43	54.88	36.11 36.67	66
67	56.19	36.49	56.03	36.74	55.87	36.98	55.71	37.22	6
68	57.03	$\frac{37.04}{37.58}$	56.87	37.28	56.70	37.53	56.54	37.78	68
69	57.87	37.58	57.70	37.83	57.54	38.08	57.37	38.33	69
70	58.71	38.12	58.54	38.38	58.37	38.64	58.20	38.89	70
71	59.55	38.67	59.38	38.93	59.21	39.19	59.03	39.45	7]
72 73	60.38 61.22	$\frac{39.21}{39.76}$	60.21	39.48	60.04	39.74	59.87	40.00	72
74	62.06	40.30	61.05	40.03	60.87	40.29	60.70	40.56	73
75	62.90	40.85	62.72	41.12	62.54	41.40	$61.53 \\ 62.36$	41.11 41.67	75
76	63.74	41.39	63.56	41.67	63.38	41.95	63.19	42.22	76
77	64.58	41.94	64.39	42.22	64.21	42.50	64.02	42.78	77
78	65.42	42.48	65.23	42.77	65.04	43.05	64.85	43.33	78
79 80	66.25 67.09	43.03	66.07	43.32	65.88	43.60	65.69	43.89	75
-		43.57	66.90	43.86	66.71	44.15	66.52	44.45	80
81 82	67.93 68.77	44.12	67.74	44.41	67.54	44.71	67.35	45.00	81
83	69.61	45 20	68.58	44.96 45.51	68.38 69.21	$\frac{45.26}{45.81}$	68.18 69.01	45.56	83
84	70.45	45.75	70.25	46.06	70.05	46.36	69.84	46.11	84
85	71.29	46.29	71.08	46.60	70.88	46.91	70.67	47.22	8
86	72.13	46.84	71.92	47.15	71.71	47.47	71.51	47.78	86
87	72.96	47.38	72.76	47.70	72.55	48.02	72.34	48.33	87
88 89	73.80 74.64	47.93 48.47	73.59 74.43	48.25	73.38	48.57	73.17	48.89	88
90	75.48	49.02	75.27	$48.80 \\ 49.35$	74.22	$\frac{49.12}{49.67}$	74.00 74.83	$\frac{49.45}{50.00}$	89
91	76.32	49.56	76.10	49.89	75.88	50.23			9
92	77.16	50.11	76.94	50.44	76.72	50.78	75.66 76.50	50.56 51.11	9:
93	77.16 78.00	50.65	77.77	50.99	77.55	51.33	77.33	51.67	93
94	78.83	51.20	78.61	51.54	78.39	51.88	78.16	52.22	94
95	79.67	51.74	79.45	52.09	79.22	52.43	78.99	52.78	9
96	80.51	52.29	80.28	52.64	80.05	52.99	79.82	53.33	90
97 98	81.35 82.19	52.83 53.37	81.12	53.18	80.89	53.54	80.65	53.89	9
99	83.03	53.92	81.96	53.73 54.28	81.72 82.55	54.09 54.64	81.48 82.32	54.45	98
00	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.00 55.56	100
-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	57 I	Deg.	563	Deg.	561	Deg.	561	Deg.	Distance.

D	34 I	og.	341	Deg.	341	Deg.	341	Dog.	Distance
8	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
284567890 10	0.83 1.66 2.49 3.32 4.15 4.97 5.80 6.63 7.46 8.29	0.56 1.12 1.68 2.24 2.80 3.36 3.91 4.47 5.03 5.59	0.83 1.65 2.48 3.31 4.13 4.96 5.79 6.61 7.44 8.27	0.56 1.13 1.69 2.25 2.81 8.38 3.94 4.50 5.07 5.63	0.82 1.65 2.47 3.30 4.12 4.94 5.77 6.59 7.42 8.24	0.57 1.13 1.70 2.27 2.83 3.40 3.96 4.53 5.10 5.66	0.82 1.64 2.46 8.29 4.11 4.93 5.75 6.57 7.39 8.22	0.57 1.14 1.71 2.28 2.85 3.42 3.99 4.56 5.13 5.70	1 2 3 4 5 6 7 8 9 10
11 12 13 14 15 16 17 18 19	9.12 9.95 10.78 11.61 12.44 18.26 14.09 14.92 15.75 16.58	6.15 6.71 7.27 7.83 8.39 8.95 9.51 10.07 10.62	9.09 9.92 10.75 11.57 12.40 13.23 14.05 14.88 15.71	6.19 6.75 7.32 7.88 8.44 9.00 9.57 10.13 10.69 11.26	9.07 9.89 10.71 11.54 12.36 13.19 14.01 14.83 15.66 16.48	6.23 6.80 7.36 7.93 8.50 9.06 9.63 10.20 10.76 11.33	9.04 9.86 10.68 11.50 12.32 13.15 13.97 14.79 15.61 16.43	6.27 6.84 7.41 7.98 8.55 9.12 9.69 10.26 10.83 11.40	11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30	17.41 18.24 19.07 19.90 20.73 21.55 22.38 23.21 24.04 24.87	11.18 11.74 12.30 12.86 13.42 13.98 14.54 15.10 15.66 16.22 16.78	16.53 17.36 18.18 19.01 19.84 20.66 21.49 22.32 23.14 23.97 24.80	11.20 11.82 12.38 12.94 13.51 14.07 14.63 15.20 15.76 16.32 16.88	17.31 18.13 18.95 19.78 20.60 21.43 22.25 23.08 23.90 24.72	11.89 12.46 13.03 13.59 14.16 14.73 15.29 15.86 16.43 16.99	17.25 18.08 18.90 19.72 20.54 21.36 22.18 23.01 23.83 24.65	11.97 12.54 13.11 13.68 14.25 14.82 15.39 15.96 16.53 17.10	21 22 23 24 25 26 27 28 29 30
31 32 33 34 35 36 37 38 39 40	25.70 26.53 27.36 28.19 29.02 29.85 30.67 31.50 32.33 33.16	17.33 17.89 18.45 19.01 19.57 20.13 20.69 21.25 21.81 22.37	25.62 26.45 27.28 28.10 28.93 29.76 30.58 31.41 32.24 33.06	17.45 18.01 18.57 19.14 19.70 20.26 20.82 21.39 21.95 22.51	25.55 26.37 27.20 28.02 28.84 29.67 30.49 31.32 32.14 32.97	17.56 18.12 18.69 19.26 19.82 20.39 20.96 21.52 22.09 22.66	25.47 26.29 27.11 27.94 28.76 29.58 30.40 31.22 32.04 32.87	17.67 18.24 18.81 19.38 19.95 20.52 21.09 21.66 22.23 22.80	31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50	33.99 34.82 35.65 36.48 37.31 38.14 38.96 39.79 40.62 41.45	22.93 23.49 24.05 24.60 25.16 25.72 26.28 26.84 27.40 27.96	33.89 34.72 35.54 36.37 37.20 38.02 38.85 39.68 40.50 41.33	23.07 23.64 24.20 24.76 25.33 25.89 26.45 27.01 27.58 28.14	33.79 34.61 35.44 36.26 37.09 37.91 38.73 39.56 40.38 41.21	23.22 23.79 24.36 24.92 25.49 26.05 26.62 27.19 27.75 28.32	33.69 34.51 35.33 36.15 36.97 37.80 38.62 39.44 40.26 41.08	23.37 23.94 24.51 25.08 25.65 26.22 26.79 27.36 27.93 28.50	41 42 43 44 45 46 47 48 49 50
Distance.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep.	Lat. Deg.	Dep. 554	Lat.	Distance.

Distanc	34	Deg.	341	Deg.	341	Deg.	341	Deg.	Distance.
11 Ce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	HOO.
51	42.28	28.52	42.16	28.70	42.03	28.89	41.90	29.07	51
52 53	43.11 43.94	29.08 29.64	42.98 43.81	29.27 29.83	42.85 43.68	29.45 30.02	42.73 43.55	29.64 30.21	52 53
54	44.77	30.20	44.64	30.39	44.50	30.59	44.37	30.78	54
55	45.60	30.76	45.46	30.95	45.33	31.15	45.19	31.35	55
56 57	46.43 47.26	31.31 31.87	46.29 47.12	$31.52 \\ 32.08$	46.15 46.98	31.72 32.29	46.01 46.83	31.92 32.49	56 57
58	48.08	32.43	47.94	32.64	47.80	32.85	47.66	33.06	58
59	48.91	32.99	48.77	33.21	48.62	33.42	48.48	33.63	59
$\frac{60}{61}$	49.74 50.57	$\frac{33.55}{34.11}$	49.60 50.42	33.77	49.45	33.98	49.30	34.20	60
62	51.40	34.67	51.25	34.89	50.27 51.10	34.55 35.12	50.12 50.94	35.34	62
63	52.23	35.23	52.08	35.46	51.92	35.68	51.76	35.91	63
64 65	53.06 53.89	35.79 36.35	52.90 53.73	36.02 36.58	52.74 53.57	36.25 36.82	52.59 53.41	36.48 37.05	64 65
66	54.72	36.91	54.55	37.15	54.39	37.38	54.23	37.62	66
67	55.55	37.46	55.38	37.71	55.22	37.95	55.05	38.19	67
68 69	56.37 57.20	38.03 38.58	56.21 57.03	38.27 38.83	56.04 56.86	38.52 39.08	55.87 56.69	38.76 39.33	68 69
70	58.03	39.14	57.86	39.40	57.69	39.65	57.52	39.90	70
71	58.86	39.70	58.69	39.96	58.51	40.21	58.34	40.47	71
72	59.69 60.52	40.26	59.51	40.52 41.08	59.34	40.78	59.16	41.04	72 73
73 74	61.35	40.82	60.34 61.17	41.65	60.16 60.99	41.35 41.91	59.98 60.80	41.61 42.18	74
75	62.18	41.94	61.99	42.21	61.81	42.48	61.62	42.75 43.32	75
76	63.01	42.50 43.06	62.82	42.77	62.63	43.05	62.45	43.32 43.89	76 77
77 78	64.66	43.62	63.65 64.47	43.90	63.46 64.28	43.61 44.18	63.27 64.09	44.46	
79	65.49	44.18	65.30	44.46	65.11	44,75	64.91	45.03	78 79
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60	80
81 82	67.15 67.98	45.29 45.85	66.95 67.78	45.59 46.15	66.75 67.58	45.88 46.45	66.55 67.37	46.17 46.74	81
83	68.81	46.41	68.61	46.71	68.40	47.01	68.20	47.31	82 83
84	69.64	46.97	69.43	47.28	69.23	47.58	69.02	47.88	84
85 86	70.47 71.30	47.53 48.09	70.26	47.84 48.40	70.05 70.87	48.14 48.71	69.84 70.66	48.45 49.02	85 86
87	72.13	48.65	71.91	48.96	71.70	49.28	71.48	49.59	87
88	72.96	49.21 49.77	72.74	49.53 50.09	72.52 73.35	49.84	72.30	50.16 50.78	88 89
89 90	74.61	50.33	74.39	50.65	74.17	50.41 50.98	73.95	51.30	90
91	75.44	50.89	75.22	51.22	75.00	51.54	74.77	51.87	91
92	76.27	51.45	76.05	51.78	75.82	52.11	75.59	52.44	92
93 94	77.10	52.00 52.56	76.87 77.70	52.34 52.90	76.64	52.68 53.24	76.41 77.23	53.01 53.58	93 94
95	78.76	53.12	78.53	53.47	78.29	53.81	78.06	54.15	95
96	79.59 80.42	53.68 54.24	79.35	54.03	79.12	54.37	78.88 79.70	54.72 55.29	96 97
97 98	81.25	54.80	80.18	54.59 55.15	79.94 80.76	54.94 55.51	80.52	55.86	98
99	82.07	55.36	81.83	55.72	81.59	56.07	81.34	56.43	99
100	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	100
ğ	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	ance
Distance	56	Deg.	551	Deg.	55]	Deg.	55 1	Deg.	Distance.

Distance	35	Deg.	351	Deg.	351	Deg.	35}	Deg.	Dist
Ş	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5 6 7 8 9	0.82 1.64 2.46 3.28 4.10 4.91 5.73 6.55 7.37 8.19	0.57 1.15 1.72 2.29 2.87 3.44 4.01 4.59 5.16 5.74	0.82 1.63 2.45 3.27 4.08 4.90 5.72 6.53 7.35 8.17	0.58 1.15 1.73 2.31 2.89 3.46 4.04 4.62 5.19 5.77	0.81 1.63 2.44 3.26 4.07 4.88 5.70 6.51 7.33 8.14	0.58 1.16 1.74 2.32 2.90 3.48 4.06 4.65 5.23 5.81	0.81 1.62 2.43 3.25 4.06 4.87 5.68 6.49 7.30 8.12	0.58 1.17 1.75 2.34 2.92 3.51 4.09 4.67 5.26 5.84	1 2 3 4 5 6 7 8 9
111 112 113 114 115 116 117 118 119 20 21 22 22 22 22 22 22 23 23 33 34 36 36 37 38 38 39 40 41 41 42 42 42 42 42 43 44 44 44 44 44 44 44 44 44 44 44 44	9.01 9.83 10.65 11.47 13.29 13.11 13.93 14.74 15.56 16.38 17.20 18.02 18.02 18.02 18.02 19.66 20.48 21.30 22.12 22.94 23.76 24.57 25.39 26.21 27.03 27.85 28.67 29.49 30.31 31.13 31.93 31.93 31.93 31.93 31.93 32.73 33.59 34.40 35.22 35.22 36.22 36.23 37.20 37.20 38.23 39.31 31.13 31.9	6.31 6.88 7.46 8.03 8.60 9.18 9.75 10.32 11.47 12.05 11.49 11.43 14.34 14.31 15.49 16.66 16.63 17.78 18.35 19.50 20.08 20.08 21.22 21.80 22.37 22.37 22.39 24.09	8.98 9.80 10.62 11.43 12.25 13.07 13.88 14.70 15.52 16.33 17.15 17.97 18.78 19.60 20.42 21.23 22.05 22.05 22.87 23.68 24.50 25.32 26.13 26.95 27.77 28.58 29.40 30.22 31.03 31.85 32.67 33.48 34.30 35.12	6.35 6.93 7.508 8.66 9.23 10.39 10.39 11.54 12.12 12.70 13.27 14.43 15.01 15.58 16.16 16.73 17.89 18.47 19.05 20.20 20.20 20.78 21.35 21.93 22.51 23.09 23.66 24.24 24.24	8.96 9.77 10.58 11.40 12.21 13.03 13.84 14.65 15.47 16.28 17.10 17.91 18.72 19.54 20.35 21.17 21.98 22.80 23.61 24.42 25.24 26.05 28.49 29.31 30.94 30.94 31.75 32.56 33.38 34.19 35.01	6.39 6.97 7.55 8.13 8.71 9.29 9.87 10.45 11.63 11.63 11.63 11.63 11.63 11.63 11.64 12.19 12.78 13.36 16.26 16.26 16.26 17.42 18.58 19.16 19.74 20.32 22.07 22.07 22.07 22.265 23.23 23.81 24.97	8.93 9.74 10.55 11.36 12.17 12.99 13.80 14.61 15.42 16.23 17.04 17.85 18.67 19.48 20.29 21.10 21.91 22.72 23.54 25.16 25.97 26.78 27.59 28.41 29.22 30.03 30.84 31.64 31.27 34.09 34.90	6.43 7.01 7.60 8.18 8.76 9.35 10.52 11.68 12.27 12.85 13.40 14.61 15.77 16.36 19.28 19.86 20.45 21.03 21.62 22.29 23.37 23.95 24.54	112 134 145 166 197 188 190 20 21 222 232 242 256 267 287 338 339 40 412 443
44 45 46 47 48 49 50	36.04 36.86 37.68 38.50 39.32 40.14 40.96	25.24 25.81 26.38 26.96 27.53 28.11 28.68	35.93 36.75 37.57 38.38 39.20 40.02 40.83	25.39 25.97 26.55 27.13 27.70 28.28 28.86	35.82 36.64 37.45 38.26 39.08 39.89 40.71	25.55 26.13 26.71 27.29 27.87 28.45 29.04	35.71 36.52 37.33 38.14 38.96 39.77 40.58	25.71 26.29 26.88 27.46 28.04 28.63 29.21	44 45 46 47 48 49 50
Distance.	Dep. 55 l	Lat. Deg.	Dep. 541	Lat. Deg.	Dep. 541	Lat. Deg.	Dep. 541	Lat. Deg.	Distance.

Dist	35 I	Deg.	351	Deg.	351	Deg.	351	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	41.78	29.25	41.65	29.43	41.52	29.62	41.39	29.80	51
52	42.60	29.83	42.47	30.01	42.33	30.20	42.20	30.38	52
53	43.42	30.40	43.28	30.59	43.15	30.78	43.01	30.97	53
54	44.23	30.97	44.10	31.17	43.96	31.36	43.82	$31.55 \\ 32.13$	54
55 56	45.05	31.55 32.12	44.92 45.73	$\frac{31.74}{32.32}$	44.78 45.59	$\frac{31.94}{32.52}$	44.64	32.72	56
57	46.69	32.69	46.55	32.90	46.40	33.10	46.26	33.30	57
58	47.51	33.27	47.37	33.47	47.22	33.68	47.07	33.89	58
59	48.33	33.84	48.18	34.05	48.03	34.26	47.88	34.47	59
60	49.15	34.41	49.00	34.63	48.85	34.84	48.69	35.05	60
61	49.97	34.99	49.82	35,21	49.66	35.42	49.51	35.64	61
62	50.79	35.56	50.63	35.78	50.48	36.00	50.32	$36.22 \\ 36.81$	62
63 64	51.61 52.43	36.14 36.71	$51.45 \\ 52.27$	$36.36 \\ 36.94$	$51.29 \\ 52.10$	36.58	51.13 51.94	37.39	63
65	53.24	37.28	53.08	37.51	52.92	37.75	52.75	37.98	65
66	54.06	37.86	53.90	38.09	53.73	38.33	53.56	38.56	66
67	54.88	38.43	54.71	38.67	54.55	38.91	54.38	39.14	67
68	55.70	39.00	55.53	39.25	55.36	39.49	55.19	39.73	68
69	56.52 57.34	$\frac{39.58}{40.15}$	56.35 57.16	$\frac{39.82}{40.40}$	56.17 56.99	$\frac{40.07}{40.65}$	56.00 56.81	40.31 40.90	69
71			57.98	40.98	57.80	41.23	57.62	41.48	71
72	58.16 58.98	40.72	58.80	41.55	58.62	41.81	58.43	42.07	75
73	59.80	41.87	59.61	42.13	59.43	42.39	59.24	42.65	75
74	60.62	42.44	60.43	42.71	60.24	42.97	60.06	43.23	74
75	61.44	43.02	61.25	43.29	61.06	43.55	60.87	43.82	7:
76	62.26	43.59	62.06	$\frac{43.86}{44.44}$	62.69	44.13	61.68	44.40	77
78	63.89	44.17	62.88	45.02	63.50	45.29	63.30	45.57	78
79	64.71	45.31	64.51	45.59	64.32	45.88	64.11	46.16	75
80	65.53	45.89	65.33	46.17	65.13	46.46	64.93	46.74	80
81	66.35	46.46	66.15	46.75	65.94	47.04	65.74	47.32	81
82	67.17	47.03	66.96	47.33	66.76	47.62	66.55	47.91 48.49	82
83	67.99	47.61	67.78	47.90	67.57	48.20	67.36	49.08	83
84 85	68.81	48.18	68.60	48.48	68.39 69.20	48.78	68.98	49.66	8
86	70.45	49.33	70.23	49.63	70.01	49.94	69.80	50.25	86
87	71.27	49.90	71.05	50.21	70.83	50.52	70.61	50.83	8
88	72.09	50.47	71.86	50.79	71.64	51.10	71.42	51.41 52.00	88
89 90	72.90	51.05	72.68	51.37 51.94	72.46	51.68 52.26	72.23 73.04	52.58	89
_	Charles and the second		74.31	52.52	$\frac{73.27}{74.08}$	52.84	73.85	53.17	9
91 92	74.54	52.20	75.13	53.10	74.90	53.42	74.66	53.75	95
93	75.36 76.18	52.77 53.34	75.95	53.67	75.71	54.01	75.48	54.34	9:
. 94	77.00	53.92	76.76	54.25	76.53	54.59	76.29	54.92	94
95	77.82	54.49	77.58	54.83	77.34	55.17	77.10	55.50	9.
96	78.64	55.06	78.40	55.41	78.16 78.97	55.75	77.91 78.72	56.09 56.67	9
97	79.46 80.28	55.64	79.21 80.03	55.98	79.78	56.91	79.53	57.26	98
99	81.10	56.21 56.78	80.85	57.14	80.60	57.49	80.35	57.84	9
100	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	55	Deg.	543	Deg.	541	Deg.	541	Deg.	Distance

<u> </u>	i		T :	<u></u>	i		¥		
Di	36	Deg.	361	Deg.	36 <u>1</u>	Deg.	361	Deg.	Distance.
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	mce.
-1	0.81	0.59	0.81	0.59	0.80	0.59	0.80	0.60	1
3	1.62 2.43	1.18	1.61 2.42	1.18	1.61 2.41	1.19	1.60 2.40	1.79	2 3 4
4	3.24	2.35	3.23	2.37	3.22	2.38	3.20	2.39	
5	4.05	2.94	4.03	2.96	4.02	2.97 3.57	4.01 4.81	3.59	5 6 7
6 7	4.85 5.66	3.53 4.11	4.84 5.65	3.55 4.14	4.82 5.63	4.16	5.61	4.19	7
8	6.47	4.70	6.45	4.73	6.43	4.76	6.41	4.79	8
9 10	7.28	5.29 5.88	7.26 8.06	5.32 5.91	7.23 8.04	5.35 5.95	7.21 8.01	5.38 5.98	10
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81	6.58	11
12 13	9.71	7.05 7.64	9.68 10.48	7.10	9.65 10.45	7.14	9.61 10.42	7.18	12 13
14	11.33	8.23	11.29	8.28	11.25	8.33	11.22	8.38	14
15	12.14	8.82	12.10	8.87	12.06	8.92	12.02	8.97	15
16 17	12.94 13.75	9.40	12.90 13.71	9.46	12.86 13.67	9.52	12.82 13.62	9.57	16 17
is	14.56	10.58	14.52	10.64	14.47	10.71	14.42	10.77	18
19	15.37	11.17	15.32	11.23	15.27	11.30	15.32	11.37	19
20 21	16.18	$\frac{11.76}{12.34}$	$\frac{16.13}{16.94}$	$\frac{11.83}{12.42}$	$\frac{16.08}{16.88}$	$\frac{11.90}{12.49}$	$\frac{16.03}{16.83}$	$\frac{11.97}{12.56}$	20 21
22	17.80	12.93	17.74	13.01	17.68	13.09	17.63	13.16	22
23	18.61	13.52	18.55	13.60	18.49	13.68	18.43	13.76	23
24 25	19.42 20.23	14.11	19.35 20.16	14.19 14.78	19.29 20.10	14.28 14.87	19.23 20.03	14.36	24 25
26	21.03	15.28	20.97	15.37	20.90	15.47	20.83	15.56	26
27	21.84	15.87	21.77	15.97	21.70	16.06	21.63	16.15	27
28 29	22.65 23.46	16.46 17.05	22.58 23.39	16.56 17.15	22.51 23.31	16.65 17.25	22.44 23.24	16.75 17.35	28 29
30	24.27	17.63	24.19	17.74	24.12	17.84	24.04	17.95	30
31	25.08	18.22	25.00	18.33	24.92	18.44	24.84	18.55	31
32 33	25.89 26.70	18.81 19.40	25.81 26.61	18.92 19.51	25.72 26.53	19.03 19.63	25.64 26.44	19.15 19.74	32 33
34	27.51	19.98	27.42	20.10	27.33	20.22	27.24	20.34	34
35 36	28.32	20.57 21.16	28.23 29.03	20.70 21.29	28.13 28.94	20.82 21.41	28.04 28.85	20.94 21.54	35 36
37	29.93	21.75	29.84	21.88	29.74	22.01	29.65	22.14	37
38	30.74	22.34	30.64	22.47	30.55	22.60	30.45	22.74	38
39 40	31.55 32.36	22.92 23.51	31.45 32.26	23.06 23.65	31.35 32.15	23.20 23.79	31.25 32.05	23.38 23.93	3 9 4 0
41	33.17	24.10	33.06	24.24	32.96	24.39	32.85	24.53	41
42	33.98	24.69	33.87	24.83	33.76	24.98	33.65	25.18	42
43	34.79 35.60	25.27 25.86	34.68 35.48	25.43 26.02	34.57 35.37	25.58 26.17	34.45 35.26	25.78 26.33	43 · 44
45	36.41	26.45	36.29	26.61	36.17	26-77	36.06	26.92	45
46 47	37.21 38.02	27.04 27.63	37.10 37.90	27.20 27.79	36.98 37.78	27.36 27.96	36.86 37.66	27.52 28.12	46 47
48	38.83	28.21	38.71	28.38	38.59	28.55	38.46	28.72	48
49 50	39.64 40.45	28.80	39.52 40.32	28.97	39.39 40.19	29.15	39.26 40.06	29.32	49
_	Dep.	29.39 Lat.	Dep.	29.57 Lat.	Dep.	29.74 Lat.	Dep.	29.92 Lat.	<u>50</u>
Distance.	54 I	Deg.	531	Deg.	531	Deg.	584	Deg.	Distance
ا						1		1	

Distance.	36	Deg.	361	Deg.	361	Deg.	361	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
51 52	41.26	29.98	41.13	30.16	41.00	30.34	40.86	30.51 31.11	51 52
53	42.07 42.88	30.56	41.94	30.75 31.34	41.80 42.60	30.93	42.47	31.71	53
54	43.69	31.74	43.55	31.93	43.41	32.12	43.27	32.31	54
55 56	44.50 45.30	32.33 32.92	44.35 45.16	32.52 33.11	44.21 45.02	32.72 33.31	44.07	32.91 33.51	55 56
57	46.11	33.50	45.97	33.70	45.82	33.90	45.67	84.10	57
58 59	46.92	34.09	46.77	34.30 34.89	46.62	34.50 35 09	46.47	34.70 35.30	58 59
60	48.54	35.27	48.39	35.48	48.23	35.69	48.08	35.90	60
61	49.35	35.85	49.19	36.07	49.04	36.28	48.88	36.50	61
62 63	50.16	36.44	50.00	36.66 37.25	49.84	36.88 37.47	49.68 50.48	37.10 37.69	62
64	50.97	37.03 37.62	50.81 51.61	37.84	50.64 51.45	38.07	51.28	38.29	64
65	52.59	38.21	52.42	38.44	52.25	38.66	52.08	38.89	65
66 67	53.40 54.20	38.79 39.38	53.23 54.03	39.03 39.62	53.05 53.86	39.26 39.85	52.88 53.68	39.49 40.09	66 67
.68	55.01	39.97	54.84	40.21	54.66	40.45	54.49	40.69	68
69	55.82	40.56	55.64	40.80	55.47	41.04	55.29	41.28	69
$\frac{70}{71}$	57.44	$\frac{41.14}{41.73}$	56.45	$\frac{41.39}{41.98}$	$\frac{56.27}{57.07}$	$\frac{41.64}{42.23}$	56.89	41.88	$\left \frac{70}{71} \right $
72	58.25	42.32	58.06	42.57	57.88	42.83	57.69	43.08	72
78	59.06	42.91	58.87	43.17	58.68	43.42	58.49	43.68	78
74 75	59.87 60.68	43.50 44.08	59.68 60.48	43.76 44.35	59.49 60.29	44.02 44.61	59.29 60.09	44.28 44.87	74 75
76	61.49	44.67	61.29	44.94	61.09	45.21	60.90	45.47	76
77	62.29	45.26	62.10	45.53	61.90	45.80	61.70	46.07	77
78 79	63.10 63.91	45.85 46.43	62.90 63.71	46.12 46.71	62.70 63.50	46.40 46.99	62.50 63.30	46.67 47.27	78 79
80	64.72	47.02	64.52	47.30	64.31	47.59	64.10	47.87	80
81	65.53	47.61	65.32	47.90	65.11	48.18	64.90	48.46	81
82 83	66.34	48.20 48.79	66.13	48.49 49.08	65.92 66.72	48.78 49.37	65.70 66.50	49.06 49.66	82 83
84	67.15 67.96	49.37	66.93 67.74	49.67	67.52	49.97	67.31	50.26	84
85	68.77	49.96	68.55	50.26	68.33	50.56	68.11	50.86	85
86 87	69.58 70.38	50.55 51.14	69.35 70.16	50.85 51.44	69.13 69.94	51.15 51.75	68.91 69.71	51.46 52.05	86 87
88	71.19	51.73	70.97	52.04	70.74	52.34	70.51	52.65	88
89	72.00	52.31	71.77	52.63	71.54	52.94	71.31	53.25	89
90	72.81	52.90	72.58	53.22	72.35	53.53	$\frac{72.11}{72.91}$	$\frac{53.85}{54.45}$	90
91 92	73.62 74.43	53.49 54.08	73.39 74.19	53.81 54.40	73.15 73.95	54.13 54.72	73.72	55.05	92
93	75.24	54.66	75.00	54.99	74.76	55.32	74.52	55.64	98
94	76.05	55.25	75.81	55.58	75.56 76.37	55.91	75.32 76.12	56.24 56.84	94 95
95 96	76.86 77.67	55.84 56.43	76.61 77.42	56.17 56.77	77.17	56.51 57.10	76.92	57.44	96
97	78.47	57.02	78.23	57.36	77.97	57.70	77.72	58.04	97
98 99	79.28 80.09	57.60 58.19	79.03 79.84	57.95 58.54	78.78 79.58	58.29 58.89	78.52 79.32	58.64 59.23	98 99
100	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	1906.
Distance.	54 I	Deg.	534	Deg.	53½]	Deg.	534	Deg.	Distance.

Dist	87	Deg.	371	Deg.	371	Deg.	371	Dog.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3	0.80 1.60 2.40	0.60 1.20 1.81	0.80 1.59 2.39	0.61 1.21 1.82	0.79 1.59 2.38	0.61 1.22 1.83	0.79 1.58 2.37	0.61 1.22 1.84	1 2 3
4 5	3.19 3.99	2.41 3.01	3.18 3.98	2.42 3.03	3.17	2.43 3.04	3.16 3.95	2.45 3.06	4 5
6	4.79 5.59	3.61 4.21	4.78 5.57	3.63 4.24	4.76 5.55	3.65 4.26	4.74 5.53	3.67 4.29	6
8	6.39	4.81 5.42	6.37 7.16	4.84 5.45	6.35 7.14	4.87 5.48	6.33	4.90 5.51	8
$\frac{10}{11}$	7.99 8.78	$\frac{6.02}{6.62}$	7.96 8.76	6.05	7.93 8.73	6.09	7.91 8.70	$\frac{6.12}{6.73}$	10
12 13	9.58	7.22 7.82	9.55 10.35	7.26 7.87	9.52 10.31	7.31 7.91	9.49 10.28	7.35 7.96	12 13
14 15	11.18	8.43 9.03	11.14	8.47 9.08	11.11	8.52 9.13	11.07	8.57 9.18	14
16 17	12.78 13.58	9.63 10.23	12.74 13.53	9.68 10.29	12.69	9.74 10.35	12.65 13.44	9.80 10.41	16 17
18 19	14.38 15.17	10.83 11.43	14.33 15.12	10.90	14.28 15.07	10.96	14.23 15.02	11.02	18 19
20 21	$\frac{15.97}{16.77}$	12.04 12.64	$\frac{15.92}{16.72}$	$\frac{12.11}{12.71}$	15.87	12.18	15.81	$\frac{12.24}{12.86}$	20
22 23	17.57 18.37	13.24	17.51 18.31	13.32 13.92	17.45 18.25	13.39 14.00	17.40 18.19	13.47 14.08	22 23
24 25	19.17	14.44 15.05	19.10	14.53 15.13	19.04 19.83	14.61 15.22	18.98 19.77	14.69 15.31	24 25
26 27	20.76 21.56	15.65 16.25	20.70	15.74 16.34	20.63 21.42	15.83 16.44	20.56 21.35	15.92 16.53	26 27
28 29	22.36 23.16	16.85	22.29 23.08	16.95 17.55	22.21 23.01	17.05 17.65	22.14 22.93	17.14 17.75	28 29
30	23.96 24.76	17.45 18.05 18.66	$\frac{23.88}{24.68}$	18.16	23.80 24.59	18.26	$\frac{23.72}{24.51}$	18.37	$\frac{30}{31}$
92 33	25.56 26.35	19.26 19.86	25.47 26.27	19.37 19.97	25.39 26.18	19.48	25.30 26.09	19.59 20.20	32
34 35	27.15 27.95	20.46 21.06	27.06 27.86	20.58 21.19	26.97 27.77	20.70	26.88 27.67	20.82 21.43	34 35
36 37	28.75 29.55	21.67 22.27	28.66 29.45	21.79 22.40	28.56 29.35	21.92 22.52	28.46 29.26	22.04 22.65	36 37
38 39	30.35 31.15	22.87 23.47	30.25 31.04	23.00 23.61	30.15	23.13 23.74	30.05 30.84	23.26 23.88	38 39
40	31.95	24.07	31.84	24.21 24.82	$\frac{31.73}{32.53}$	24.35	31.63	24.49 25.10	40
42 43	33.54 34.34	25.28 25.88	33.43 34.23	25.42 26.03	33.32 34.11	25.57 26.18	33.21 34.00	25.71 25.33	41 42 43
44 45	35.14 35.94	26.48 27.08	35.02 35.82	26.63 27.24	34.91 35.70	26.79 27.39	34.79 35.58	26.94 27.55	44 45
46 47	36.74 37.54	27.68 28.29	36.62 37.41	27.84 28.45	36.49 37.29	28.00 28.61	36.37 37.16	28.16 28.77	46 47
48 49	38.33 39.13	28.89 29.49	38.21 39.00	29.05 29.66	38.08	29.22 29.83	37.95 38.74	29.39 30.00	48 49
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61	50
Distance,	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
Dist	53]	Deg.	5 2 }	Deg.	52 <u>}</u>	Deg.	521	Deg.	Diet

Distance.	37	Deg.	371	Deg.	371	Deg.	371	Deg.	Dist
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	istance.
51 52	40.73 41.53	30.69 31.29	40.60	30.87 31.48	40.46	31.05 31.66	40.33 41.12	31.22 31.84	51 52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54 55	43.13 43.92	32.50 33.10	42.98 43.78	32.69 33.29	42.84 43.63	32.87 33.48	42.70	33.06 33.67	54 55
56 57	44.72 45.52	33.70 34.30	44.58	33.90 34.50	44.43	34.09 34.70	44.28	34.28	56
58	46.32	34.91	45.37 46.17	35.11	45.22 46.01	35.31	45.07 45.86	34.90 35.51	57 58
5 9	47.12 47.92	35.51 36.11	46.96 47.76	35.71 36.32	46.81 47.60	35.92 36.53	46.65 47.44	36.12 36.73	59 60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62 63	49.52 50.31	37.31 37.91	49.35 50.15	37.53 38.13	49.19 49.98	37.74 38.35	49.02 49.81	37.96 38.57	62 63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65 66	$51.91 \\ 52.71$	39.12 39.72	51.74 52.54	39.34 39.95	51.57 52.36	39.57 40.18	51.39 52.19	39.79 40.41	65 66
67	53.51 54.31	40.32 40.92	53.33 54.13	40.55	53.15	40.79 41.40	52.98	41.02	67
68 69	55.11	41.53	54.92	41.16	53.95 54.74	42.00	53.77 54.56	41.63 42.24	68 69
$\frac{70}{71}$	$\frac{55.90}{56.70}$	$\frac{42.13}{42.73}$	55.72	42.37	55.53	42.61	55.35	42.86	70
72	57.50 58.30	43.33	56.52 57.31	42.98 43.58	56.33 57.12	43.22 43.83	56.14 56.93	43.47 44.08	71 72
73 74	58.30 59.10	43.93 44.53	58.11 58.90	44.19 44.79	57.91 58.71	44.44 45.05	57.72 58.51	44.69 45.30	73 74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76 77	60.70 61.49	45.74 46.34	60.50	46.00 46.61	60.29 61.09	46.27 46,87	60.09	46.53 47.14	76 77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47,75	.78
79 80	63.09 63.89	47.54 48.15	62.88 63.68	47.82 48.42	62.67 63.47	48.09 48.70	62.46 63.26	48.37 48.98	79 80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82 83	65.49 66.29	49.35 49.95	65.27	49.63 50.24	65.05 65.85	49.92 50.53	64.84 65.63	50.20 50.81	82 83
84 85	67.09 67.88	50.55 51.15	66.86	50.84 51.45	66.64 67.43	51.14	66.42 67.21	51.43 52.04	84 85
86	68.68	51.76	68.46	52.06	68.23	51.74 52.35	68.00	52.65	86
87 88	69.48 70.28	52.36 52.96	69.25 70.05	52.66 53.27	69.02 69.82	52.96 53.57	68.79 69.58	53.26 53.88	87 88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	$\frac{71.88}{72.68}$	$\frac{54.16}{54.77}$	$\frac{71.64}{72.44}$	54.48	$\frac{71.40}{72.20}$	$\frac{54.79}{55.40}$	71.16	55.71	90
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93 94	74.27 75.07	55.97 56.57	74.03 74.82	56.29 56.90	73.78 74.58	56.61 57.22	73.53 74.32	56.94 57.55	93 94
95 96	75.87 76.67	57.17 57.77	75.62	57.50	75.37 76.16	57.83	75.12	58.16	95
97	77.47	58.38	76.42 77.21	58.11 58.71	76.96	58.44 59.05	75.91 76.70	58.77 59.39	96 97
98 99	78.27 79.06	58.98 59.58	78.01 78.80	59.32 59.92	77.75 78.54	59.66 60.27	77.49	60.00	98 99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	nce.
Distance.	53 I	Deg.	52 1	Deg.	521	Deg.	521	Deg.	Distance

Distance	38 1	Deg.	38 <u>‡</u> I	Deg.	381	Deg.	38}	Deg.	Dist
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1 2 3 4 5	0.79 1.58 2.36 3.15 3.94	0.62 1.23 1.85 2.46 3.08	0.79 1.57 2.36 3.14 3.93	0.62 1.24 1.86 2.48 3.10	0.78 1.57 2.35 3.13 3.91	0.62 1.24 1.87 2.49 3.11	0.78 1.56 2.34 3.12 3.90	0.63 1.25 1.88 2.50 3.13	1 2 3 4 5
5 6 7 8 9	4.73 5.52 6.30 7.09 7.88	3.69 4.31 4.93 5.54 6.16	4.71 5.50 6.28 7.07 7.85	3.71 4.33 4.95 5.57 6.19	4.70 5.48 6.26 7.04 7.83	3.74 4.36 4.98 5.60 6.23	4.68 5.46 6.24 7.02 7.80	3.76 4.38 5.01 5.63 6.26	6 7 8 9
11 12 13 14 15	8.67 9.46 10.24 11.03 11.82	6.77 7.39 8.00 8.62 9.23	8.64 9.42 10.21 10.99 11.78	6.81 7.43 8.05 8.67 9.29	8.61 9.39 10.17 10.96 11.74	6.85 7.47 8.09 8.72 9.34	8.58 9.36 10.14 10.92 11.70	6.89 7.51 8.14 8.76 9.39	11 12 13 14 15
16 17 18 19 20	12.61 13.40 14.18 14.97 15.76	9.85 10.47 11.08 11.70 12.31	12.57 13.35 14.14 14.92 15.71	9.91 10.52 11.14 11.76 12.38	12.52 13.30 14.09 14.87 15.65	9.96 10.58 11.21 11.83 12.45	12.48 13.26 14.04 14.82 15.60	10.01 10.64 11.27 11.89 12.52	16 17 18 19 20
21 22 23 24 25	16.55 17.34 18.12 18.91 19.70	12.93 13.54 14.16 14.78 15.39	16.49 17.28 18.06 18.85 19.63	13.00 13.62 14.24 14.86 15.48	16.43 17.22 18.00 18.78 19.57	13.07 13.70 14.32 14.94 15.56	16.38 17.16 17.94 18.72 19.50	13.14 13.77 14.40 15.02 15.65	21 22 23 24 25
26 27 28 29 30	20.49 21.28 22.06 22.85 23.64 24.43	16.01 16.62 17.24 17.85 18.47	20.42 21.20 21.99 22.77 23.56	16.10 16.72 17.33 17.95 18.57	20.35 21.13 21.91 22.70 23.48	16.19 16.81 17.43 18.05 18.68	20.28 21.06 21.84 22.62 23.40	16.27 16.90 17.53 18.15 18.78	26 27 28 29 30
31 32 33 34 35 36	25.22 26.00 26.79 27.58 28.37	19.09 19.70 20.32 20.93 21.55 22.16	24.34 25.13 25.92 26.70 27.49 28.27	19.19 19.81 20.43 21.05 21.67 22.29	24.26 25.04 25.83 26.61 27.39 28.17	19.92 20.54 21.17 21.79 22.41	24.18 24.96 25.74 26.52 27.30 28.08	19.40 20.03 20.66 21.28 21.91 22.53	31 32 33 34 35 36
37 38 39 40 41	29.16 29.94 30.73 31.52 32.31	22.78 23.40 24.01 24.63 25.24	29.06 29.84 30.63 31.41 32.20	22.91 23.53 24.14 24.76 25.38	28.96 29.74 30.52 31.30 32.09	23.03 23.66 24.28 24.90 25.52	28.86 29.64 30.42 31.20	23.16 23.79 24.41 25.04 25.66	37 38 39 40 41
42 43 44 45 46	33.10 33.88 34.67 35.46 36.25	25.86 26.47 27.09 27.70 28.32	32.98 33.77 34.55 35.34 36.12	26.00 26.62 27.24 27.86 28.48	32.87 33.65 34.43 35.22 36.00	26.15 26.77 27.39 28.01 28.64	32.76 33.53 34.31 35.09 35.87	26.29 26.91 27.54 28.17 28.79	42 43 44 45 46
47 48 49 50	37.04 37.82 38.61 39.40	28.94 29.55 30.17 30.78	36.91 37.70 38.48 39.27	29.10 29.72 30.34 30.95	36.78 37.57 38.35 39.13	29.26 29.88 30.50 31.13	36.65 37.43 38.21 38.99	29.42 30.04 30.67 31.30	47 48 49 50
· Distance.	Dep. 52 1	Lat.	Dep. 513	Lat. Deg.	Dep. 51½	Lat. Deg.	Dep. 511	Lat. Deg.	Distance.

_	+		-						_
Distance.	38	Deg.	38 1	Deg.	381	Deg.	381	Deg.	Distance.
Ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Ince.
51	40.19	31.40	40.05	31.57	39.91	31.75	39.77	31.92	51
52	40.98	32.01	40.84	32.19	40.70	32.37	40.55	32.55	52
53 54	41.76	32.63 33.25	41.62 42.41	32.81 33.43	41.48	32.99 33.62	41.33	$\begin{vmatrix} 33.17 \\ 33.80 \end{vmatrix}$	53 54
55	43.34	33.86	43.19	34.05	43.04	34.24	42.89	34.43	55
56	44.13	34.48	43.98	34.67	43.83		43.67	35.05	56
57	44.92	35.09	44.76	35.29	44.61	35.48	44.45	35.68	57
58 59	45.70 46.49	35.71 36.32	45.55 46.33	35.91 36.53	45.39 46.17	36.11 36.73	45.23 46.01	36.30 36.93	58 59
60	47.28	36.94	47.12	37.15	46.96	37.35	46.79	37.56	60
61	48.07	37.56	47.90	37.76	47.74	37.97	47.57	38.18	61
-62	48.86	38.17	48.69	38.38	48.52	38.60	48.35	38.81	62
63 64	49.64	38.79	49.47 50.26	39.00 39.62	49.30 50.09	39.22 39.84	49.13	39.43 40.06	63 64
65	50.43	39.40 40.02	51.05	40.24	50.87	40.46	49.91 50.69	40.68	65
66	52.01	40.63	51.83	40.86	51.65	41.09	51.47	41.31	66
67	52.80	41.25	52.62	41.48	52.43	41.71	52.25	41.94	67
68 69	53.58 54.37	41.86	53.40 54.19	42.10 42.72	53.22 54.00	42.33 42.95	53.03 53.81	42.56 43.19	68 69
70	55.16	43.10	54.97	43.34	54.78	43.58	54.59	43.81	70
71	55.95	43,71	55.76	43.96	55.57	44.20	55.37	44.44	71
72	56.74	44.33	56.54	44.57	56.35	44.82	56.15	45.07	72
73 74	57.52	44.94	57.33 58.11	45.19	57.13	45.44	56.93	45.69	73 74
75	58.31 59.10	45.56 46.17	58.90	45.81 46.43	57.91 58.70	46.69	57.71 58.49	46.32	75
76	59.89	46.79	59.68	47.05	59.48	47.31	59.27	47.57	76
77	60.68	47.41	60.47	47.67	60.26	47.93	60.05	48.20	77
78 79	61.46	48.02 48.64	61.25 62.04	48.29 48.91	61.04	48.56	60.83	48.82 49.45	78 79
80	63.04	49.25	62.83	49.53	62.61	49.80	62.39	50.07	80
81	63.83	49.87	63.61	50.15	63.39	50.42	63.17	50.70	81
82	64.62	50.48	64.40	50.77	64.17	51.05	63.95	51.33	82
83 84	65.40	51.10 51.72	65.18 65.97	51.38 52.00	64.96 65.74	51.67 52.29	64.78 65.51	51.95 52.58	83 84
85	66.98	52.33	66.75	52.62	66.52	52.91	66.29	53.20	85
86	67.77	52.95	67.54	53.24	67.30 68.09	53.54	67.07	53.83	86
87	68.56	53.56	68.32	53.86		54.16	67.85	54.46	87
88 89	69.34	54.18 54.79	69.11 69.89	54.48 55.10	68.87 69.65	54.78 55.40	68.63 69.41	55.08	88 89
90	70.92	55.41	70.68	55.72	70.43	56.03	70.19	55.71 56.33	90
91	71.71	56.03	71.46	56.34	71.22	56.65	70.97	56.96	91
92	72.50	56.64	72.25	56.96	72.00	57.27	71.75	57.58	92
93 94	73.28 74.07	57.26 57.87	73.03 73.82	57.58 58.19	72.78 73.57	57.89 58.52	72.53 73.31	58.21 58.84	93 94
95	74.86	58.49	74.61	58.81	74.35	59.14	74.09	59.46	95
96	75.65	59.10	75.39	75.39 59.43		59.76	74.87	60.09	96
97 98	76.44	59.72 60.33	76.18 60.05		75.91 76.70	60.38 61.01	75.65 76.43	60.71 61.34	97 98
99	77.22 78.01	60.95	77.75	61.29	77.48	61.63	77.21	61.97	99
100	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	100
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	100
Distance.	5 2 I	Deg.	51}	Deg.	513	Deg.	511	Deg.	Distance.

Dist	39]	Deg.	391	Deg.	391	Deg.	391	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
1	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64 1.28	ī
3	1.55 2.33	1.26 1.89	1.55 2.32	1.27	1.54 2.31	1.27	1.54 2.31	1.92	3
4	3.11	2.52	3.10	2.53	3.09	2.54	3.08	2.56	4
5	3.89	3.15	3.87	3.16	3.86	3.18 3.82	3.84 4.61	3.20 3.84	5 6
5 6 7	4.66 5.44	3.78 4.41	4.65 5.42	3.80 4.43	4.63 5.40	4.45	5.38	4.48	7
8	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12	8
9 10	6.99 7.77	5.66 6.29	6.97 7.74	5.69 6.33	6.94 7.72	5.72 6.36	6.92 7.69	5.75 6.39	9 10
11	8.55	6.92	8.52	6.96	8.49	7.00	8.46	7.03	11
12 13	9.33	7.55 8.18	9.29	7.59 8.23	9.26 10.03	7.63 8.27	9.23	7.67 8.31	12 13
14	10.10	8.81	10.07	8.86	10.80	8.91	10.76	8.95	14
15	11.66	9.44	11.62	9.49	11.57	9.54	11.53	9.59	15
16 17	12.43 13.21	10.07	12.39 13.16	10.12 10.76	12.35 13.12	10.18 10.81	12.30	10.23 10.87	16 17
. is	13.99	11.33	13.94	11.39	13.89	11.45	13.84	11.51	18
19	14.77	11.96	14.71	12.02	14.66	12.09	14.61	12.15	19 2 0
3 0 3 1	$\begin{array}{ c c } \hline 15.54 \\ \hline 16.32 \\ \hline \end{array}$	$\frac{12.59}{13.22}$	$\frac{15.49}{16.26}$	$\frac{12.65}{13.29}$	$\frac{15.43}{16.20}$	$\frac{12.72}{13.36}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		21
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07	22
23	17.87	14.47	17.81	14.55	17.75	14.63	17.68 14.71		23
24 25	18.65 19.43	15.10 15.73	18.59 19.36	15.18 15.82	18.52 19.29	15.27 15.90	18.45	15.35 15.99	24 25
26	20.21	16.36	20.13	16.45	20.06	16.54	19.99	16.63	26
27	20.98	16.99	20.91	17.08	20.83	17.17	20.76	17.26	27
28 29	21.76 22.54	17.62 18.25	21.68 22.46	17.72 18.35	21.61 22.38	17.81 18.45	21.53 22.30	17.90 18.54	28 29
30	23.31	18.88	23.23	18.98	23.15	19.08	23.07	19.18	30
31	24.09	19.51	24.01	19.61 20.25	23.92 24.69	19.72 20.35	23.83 24.60	19.82 20.46	31 32
32 33	24.87 25.65	20.14 20.77	24.78 25.55	20.88	25.46	20.99	25.37	21.10	33
34	26.42	21.40	26.33	21.51	26.24	21.63	26.14	21.74	34
35 36	27.20 27.98	22.03 22.66	27.10 27.88	22.14 22.78	27.01 27.78	22.26 22.90	26.91 27.68	22.38 23.02	35 36
37	28.75	23.28	28.65	23.41	28.55	23.53	28.45	23.66	37
38	29.53	23.91	29.43	24.04	29.32	24.17	29.22	24.30	38
39 40	30.31	24.54 25.17	30.20 30.98	24.68 25.31	30.09 30.86	24.81 25.44	29.98 30.75	24.94 25.58	39 40
41	31.86	25.80	31.75	25.94	31.64	26.08	31.52	26.22	41
42 43	32.64	26.43	32.52	26.57	32.41	26.72	32.29	26.86	42 43
43 44	33.42 34.19	27.06 27.69	33.30 34.07	27.21 27.84	33.18 33.95	27.35 27.99	33.83	33.06 27.50	
45	34.97	28.32	34.85	28.47	34.72	28.62	34.60 28.77		44 45
46 47	35.75 36.53	28.95 29.58	35.62 36.40	29.10 29.74	35.49 36.27	29.26 29.90	35.37 29.41		46 47
48	37.30	30.21	37.17	30.37	37.04	30.53	36.14 30.05 36.90 30.69		48
49	38.08	30.84	37.95	31.00	37.81	31.17	37.67	31.33	49
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97	50
Dustance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
뒿			503	D	503	D	501	Dog	ig.
A	51.1	Deg.	50∄	Deg.	501	Deg.	503	Deg.	
	·		<u> </u>		1		I		

Dist	39 1	Deg.	394	Deg.	391	Deg.	393	Deg.	Dist
tance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	39.63	32.10	39.49	32.27	39.35	32.44	39.21	32.61	51
52	40.41	32.72	40.27	32.90	40.12	33.08	39.98	33.25	55
53	41.19	33.35	41.04	33.53	40.90	33.71	40.75	33.89	58
54	41.97	33.98	41.82	34.17	41.67	34.35	41.52	34.53	54
50	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17	5
56	43.52	35.24	43.37	35.43	43.21	35.62	43.06	35.81	5
57	44.30	35.87	44.14	36.06	43.98	36.26	43.82	36.45	5
58	45.07	36.50	44.91	36.70	44.75	36.89	44.59 45.36	37.09	5
59 60	45.85 46.63	37.13 37.76	45.69	37.33 37.96	45.53	37.53	46.13	38.37	6
1	AND A SECTION		46.46		46.30		46.90	39.01	6
61 62	47.41	$\frac{38.39}{39.02}$	47.24 48.01	$\frac{38.60}{39.23}$	47.07	38.80	47.67	39.65	6
63	48.18	39.65	48.79	39.86	47.84 48.61	40.07	48.44	40.28	6
64	49.74	40.28	49.56	40.49	49.38	40.71	49.21	40.92	6
65	50.51	40.91	50.34	41.13	50.16	41.35	49.97	41.56	6
66	51.29	41.54	51.11	41.76	50.93	41.98	50.74	42.20	6
67	52.07	42.16	51.88	42.39	51.70	42.62	51.51	42.84	6
68	52.85	42.79	52.66	43.02	52.47	43.25	52.28	43.48	6
69	53.52	43.42	53.43	43.66	53.24	43.89	53.05	44.12	6
70	54.40	44.05	54.21	44.29	54.01	44.53	53.82	44.76	7
71	55.18	44.68	54.98	44.92	54.79	45.16	54.59	45.40	7
72	55.95	45.31	55.76	45.55	55.56	45.80	55.36	46.04	7
73	56.73	45.94	56.53	46.19	56.33	46.43	56.13	46.68	7
74	57.51	46.57	57.31	46.82	57.10	47.07	56.89	47.32	7
75	58.29	47.20	58.08	47.45	57.87	47.71	57.66	47.96	7
76	59.06	47.83	58.85	48.09	58.64	48.34	58.43	49.24	7
77	59.84	48.46	59.63	48.72	59.42	48.98	59.20 59.97	49.88	7
78	60.62	49.09	60.40	$\frac{49.35}{49.98}$	60.19	49.61 50.25	60.74	50.52	7
80	$61.39 \\ 62.17$	50.35	61.95	50.62	61.73	50.89	61.51	51.16	8
81	62.95	50.97	62.73	51.25	62.50	51.52	62.28	51.79	8
82	63.73	51.60	63.50	51.88	63.27	52.16	63.04	52.43	8
83	64.50	52.23	64.27	52.51	64.04	52.79	63.81	53.07	8
84	65.28	52.86	65.05	53.15	64.82	53.43	64.58	53.71	8
85	66.06	53.49	65.82	53.78	65.59	54.07	65.35	54.35	8
86	66.83	54.12	66.60	54.41	66.36	54.70	66.12	54.99	8
87	67.61	54.75	67.37	55.05	67.13	55.34	66.89	55.63	8
88	68.39	55.38	68.15	55.68	67.90	55.97	67.66	56.27	8
89	69.17	56.01	68.92	56.32	68.67	56.61	68.43	56.91	8
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20	57.55	-
91	70.72	57.27	70.47	57.58	70.22	57.88	69.96	58.19	0
92	71.50	57.90	71.24	58.21	70.99	58.52	70.73	58.83	6
93	$72.27 \\ 73.05$	58.53	72.02	58.84	71.76	59.16 59.79	71.50	60.11	0
94	73.05	59.16 59.79	72.79	59.47	73.30	60.43	73.04	60.75	Š
95 96	74.61	60.41	74.34	60.74	74.08	61.06	73.81	61.39	g
97	75.38	61.04	75.12	61.37	74.85	61.70	74.58	62.03	9
98	76.16	61.67	75.89	62.01	75.62	62.34	75.35	62.66	9
99	76.94	62.30	76.66	62.64	76.39	62.97	76.12	63.30	5
100	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	10
nce.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Town state
Distance.	E1 1	Deg.	503	Deg.	501	Deg.	501	Deg.	1

Distance.	40,1	Deg.	40 <u>1</u>	Deg.	401	Deg.	401	Deg.	Dist
ince.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	tance.
1 2 3	0.77 1.53 2.30	0.64 1.29 1.93	0.76 1.53 2.29	0.65 1.29 1.94	0.76 1.52 2.28	0.65 1.30 1.95	0.76 1.52 2.27	0.65 1.31 1.96	1 2 8
4 5 6	3.06 3.83 4.60	2.57 3.21 3.86	3.05 3.82 4.58	2.58 3.23 3.88	3.04 3.80 4.56	2.60 3.25 3.90	3.03 3.79 4.55	2.61 3.26 3.92	4 5 6
7 8 9	5.36 6.13 6.89	4.50 5.14 5.79	5.34 6.11 6.87	4.52 5.17	5.32 6.08 6.84	4.55 5.20 5.84	5.30 6.06 6.82	4.57 5.22 5.87	8
10	7.66	7.07	7.63	5.82 6.46 7.11	7.60	7.14	7.58	7.18	10
12 13 14	9.19 9.96 10.72	7.71 8.36 9.00	9.16 9.92 10.69	7.75 8.40 9.05	9.12 9.89 10.65	7.79 8.44 9.09	9.09 9.85 10.61	7.83 8.49 9.14	12 13 14
15 16 17	11.49 12.26 13.02	9.64 10.28 10.93	11.45 12.21 12.97	9.69 10.34 10.98	11.41 12.17 12.93	9.74 10.39 11.04	11.36 12.12 12.88	9.79 10.44 11.10	15 16 17
18 19 20	13.79 14.55 15.32	11.57 12.21 12.86	13.74 14.50 15.26	11.63 12.28 12.92	13.69 14.45 15.21	11.69 12.34 12.99	13.64 14.39	11.75 12.40 13.06	18 19 20
21 22	16.09 16.85	13.50 14.14	16.03 16.79	13.57 14.21	15.97 16.73	13.64 14.29	15.15 15.91 16.67	13.71 14.36	21 22
23 24 25	17.62 18.39 19.15	14.78 15.43 16.07	17.55 18.32 19.08	14.86 15.51 16.15	17.49 18.25 19.01	14.94 15.59 16.24	17.42 18.18 18.94	15.01 15.67 16.32	23 24 25
26 27 28	19.92 20.68 21.45	16.71 17.36 18.00	19.84 20.61 21.37	16.80 17.45 18.09	19.77 20.53 21.29	16.89 17.54 18.18	19.70 20.45 21.21	16.97 17.62 18.28	26 27 28
29 30 81	22.22 22.98 23.75	18.64 19.28 19.93	22.13 22.90 23.66	18.74 19.38 20.03	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{18.83}{19.48}$ 20.13	$\frac{21.97}{22.73}$ $\overline{23.48}$	$\frac{18.93}{19.58}$ 20.24	29 30
32 33	24.51 25.28 26.05	20.57 21.21 21.85	24.42 25.19 25.95	20.68 21.32 21.97	24.33 25.09	20.78 21.43	24.24 25.00	20.89 21.54	31 32 33
34 35 36	26.81 27.58	22.50 23.14	26.71 27.48	22.61 23.26	25.85 26.61 27.37	22.08 22.73 23.38	25.76 26.51 27.27	22.19 22.85 23.50	34 35 36
37 38 39	28.34 29.11 29.88	23.78 24.43 25.07	28.24 29.00 29.77	23.91 24.55 25.20	28.13 28.90 29.66	24.03 24.68 25.33	28.03 28.79 29.54	24.15 24.80 25.46	37 38 39
40 41 42	30.64 31.41 32.17	25.71 26.35 27.00	30.53 31.29 32.06	25.84 26.49 27.14	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	25.98 26.63 27.28	$\frac{30.30}{31.06}$	$\frac{26.11}{26.76}$ 27.42	40 41 42
43 44 45	32.94 33.71 34.47	27.64 28.28 28.93	32.82 33.58 34.35	27.78 28.43 29.08	32.70 33.46 34.22	27.93 28.58 29.23	32.58 33.33 34.09	28.07 28.72 29.37	43 44 45
46 47 48	35.24 36.00 36.77	29.57 30.21 30.85	35.11 35.87 36.64	29.72 30.37 31.01	34.98 35.74 36.50	29.87 30.52 31.17	34.85 35.61 36.36	30.03 30.68 31.33	46 47
49 50	37.54 38.30	31.50 32.14	37.40 38.16	31.66 32.31	37.26 38.02	31.17 31.82 32.47	37.12 37.88	31.99 32.64	48 49 50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
å	50	Deg.	491	Deg.	491	Deg.	491	Deg.	Dist

Dist	40]	Deg.	40}	Deg.	401	Deg.	40}	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
51 52	39.07 39.83	32.78 33.42	38.92 39.69	32.95 33.60	38.78 39.54	33.12 33.77	38.64 39.39	33.29 33.94	51 52
53 54	40.60 41.37	34.07 34.71	40.45	34.24 34.89	40.30	34.42 35.07	40.15	34.60 35.25	53 54
55 56	42.13 42.90	35.35 36.00	41.98	35.54 36.18	41.82 42.58	35.72 36.37	41.67	35.90 36.55	55 56
57 · 58	43.66	36.64	43.50 44.27	36.83	43.34 44.10	37.02	43.18 43.94	37.21 37.86	57 58
59	44.43 45.20	37.28 37.92	45.03	37.48 38.12	44.86	37.67	44.70	38.51	59
$\frac{60}{61}$	$\frac{45.96}{46.73}$	$\frac{38.57}{39.21}$	$\frac{45.79}{46.56}$	$\frac{38.77}{39.41}$	$\frac{45.62}{46.38}$	$\frac{38.97}{39.62}$	$\frac{45.45}{46.21}$	39.17	60
62 63	47.49 48.26	39.85 40.50	47.32 48.08	40.06	47.15 47.91	40.27 40.92	46.97 47.73	40.47	62 63
64 65	49.03 49.79	41.14	48.85 49.61	41.35 42.00	48.67 49.43	41.56 42.21	48.48 49.24	41.78 42.43	64 65
66 67	50.56 51.32	42.42 43.07	50.37 51.14	42.64 43.29	50.19 50.95	42.86 43.51	50.00 50.76	43.08 43.73	66 67
68 69	52.09 52.86	43.71 44.35	51.90 52.66	43.94 44.58	51.71 52.47	44.16 44.81	51.51 52.27	44.39 45.04	68 69
70	53.62	45.00	53.43	45.23	53.23	45.46	53.03	45.69	70
71 72	54.39 55.16	45.64 46.28	54.19 54.95	45.87 46.52	53.99 54.75	46.11 46.76	53.79 54.54	46.35 47.00	71 72
73 74	55.92 56.69	46.92 47.57	55.72 56.48	47.17 47.81	55.51 56.27	47.41 48.06	55.30 56.06	47.65 48.30	73 74
75 76	57.45 58.22	48.21 48.85	57.24 58.01	48.46 49.11	57.03 57.79	48.71 49.36	56.82 57.57	48.96	75 76
77	58.99 59.75	49.49 50.14	58.77 59.53	49.75 50.40	58.55 59.31	50.01 50.66	58.33 59.09	50.26 50.92	77
79 80	60.52 61.28	50.78 51.42	60.30	51.04 51.69	60.07	51.31 51.96	59.85 60.61	51.57 52.22	79 80
81	62.05	52.07	61.82	52.34	61.59	52.61	61.36	52.87	81
82 83	62.82 63.58	52.71 53.35	62.59 63.35	52.98 53.63	62.35 63.11	53.25 53.90	62.12 62.88	53.53 54.18	82 83
84 85	64.35 65.11	53.99 54.64	64.11 64.87	54.27 54.92	63.87 64.63	54.55 55.20	63.64	54.83 55.48	84 85
86 87	65.88 66.65	55.28 55.92	65.64 66.40	55.57 56.21	65.39 66.16	55.85 56.50	65.15 65.91	56.14 56.79	86 87
88 89	67.41 68.18	56.57 57.21	67.16 67.93	56.86 57.50	66.92 67.68	57.15 57.80	66.67 67.42	57.44 58.10	88 89
90	68.94	57.85 58.49	68.69	58.15	68.44	58.45	68.18	58.75	90
91 92	69.71 70.48	59.14	69.45 70.22	58.80 59.44	69.20 69.96	59.10 59.75	68.94 69.70	59.40 60.05	91 92
93 94	71.24 72.01	59.78 60.42	70.98 71.74	60.09	70.72 71.48	60.40 61.05	70.45 71.21	60.71	93 94
95 96	72.77 73.54	61.06 61.71	72.51 73.27	61.38 62.03	$72.24 \\ 73.00$	61.70 62.35	71.97 72.73	62.01 62.66	95 96
97 98	74.31 75.07	62.35 62.99	74.03 74.80	62.67 63.32	73.76 74.52	63.00 63.65	73.48 74.24	63.3 2 63.97	97 98
99 100	75.84 76.60	63.64 64.28	75.56 76.32	63.97 64.61	75.28 76.04	64.30 64.94	75.00 75.76	64.62 65.28	99 100
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep. Lat.		
Distance	50]	Deg.	493	Deg.	49½	Deg.	491	Deg.	Distance
<u> </u>		· · · · · · · · · · · · · · · · · · ·		T		-, !	<u>'</u>		

Dist	41	Deg.	411	Deg.	41½	Deg.	41‡	Deg.	Distance
8	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
	0.75	0.66	0.75	0.66	0.75	0.66	0.75	0.67	1
2 3	1.51 2.26	1.31	1.50 2.26	1.32	1.50 2.25	1.33	1.49 2.24	1.33	2 3 4
4	3.02	2.62	3.01	2.64	3.00	2.65	2.98	2.66	4
5 6	3.77 4.53	3.28 3.94	3.76 4.51	3.30 3.96	3.74 4.49	3.31 3.98	3.73 4.48	3.33 4.00	5 6
7	5.28	4.59	5.26	4.62	5.24	4.64	5.22	4.66	7
8	6.04	5.25	6.01	5.27	5.99	5.30	5.97	5.33	8 9
9 10	6.79 7.55	5.90 6.56	6.77 7.52	5.93 6.59	6.74 7.49	5.96 6.63	6.71 7.46	5.99 6.66	10
11	8.30	7.22	8.27	7.25	8.24	7.29	8.21	7.32	Ti
12	9.06	7.87	9.02	7.91	8.99	7.95	8.95	7.99	12
13 14	9.81 10.57	8.53 9.18	9.77 10.53	8.57 9.23	9.74 10.49	8.61 9.28	9.70 10.44	8.66 9.32	13 14
15	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99	15
16 17	12.08	10.50	12.03	10.55	11.98	10.60	11.94	10.65	16
18	12.83 13.58	11.15	12.78 13.53	$11.21 \\ 11.87$	12.73 13.48	$\begin{array}{c} 11.26 \\ 11.93 \end{array}$	12.68 13.43	11.32 11.99	17 18
19	14.34	12.47	14.28	12.53	14.23	12.59	14.18	12.65	19
20	15.09	13.12	15.04	13.19	14.98	13.25	14.92	13.32	_20
21 22	15.85 16.60	13.78 14.43	15.79 16.54	13.85 14.51	15.73 16.48	13.91 14.58	15.67 16.41	13.98 14.65	21
23	17.36	15.09	17.29	15.16	17.23	15.24	17.16	15.32	22 23
24	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98	24
25 26	18.87 19.62	16.40 17.06	18.80 19.55	16.48 17.14	18.72 19.47	16.57 17.23	18.65 19.40	16.65	25 26
27	20.38	17.71	20.30	17.80	20.22	17.89	20.14	17.31 17.98	27
28	21.13	18.37	21.05	18.46	20.97	18.55	20.89	18.64	28
29	21.89 22.64	19.03 19.68	21.80 22.56	19.12 19.78	21.72 22.47	19.22 19.88	21.64 22.38	19.31 19.98	29 30
31	23.40	20.34	23.31	20.44	23.22	20.54	23.13	20.64	31
32	24.15	20.99	24.06	21.10	23.97	21.20.	23.87	21.31	32
33 34	24.91 25.66	21.65 22.31	24.81 25.56	21.76 22.42	24.72 25.46	21.87 22.53	24.62 25.37	21.97 22.64	33 34
85	26.41	22.96	26.31	23.08	26.21	23.19	26.11	23.31	35
36	27.17	23.62	27.07	23.74	26.96	23.85	26.86	23.97	36
37 38	27.92 28.68	24.27 24.93	27.82 28.57	24.40 25.06	27.71 28.46	24.52 25.18	27.60 28.35	24.64 25.30	37 38
39	29.43	25.59	29.32	25.71	29.21	25.84	29.10	25.97	39
40	30.19	26.24	30.07	26.37	29.96	26.50	29.84	26.64	40
41 42	30.94 31.70	26.90 27.55	30.83 31.58	27.03 27.69	30.71 31.46	27.17 27.83	30.59	27.30 27.97	41
43	32.45	28.21	32.33	28.35	32.21	28.49	31.33 32.08	28.63	42 43
44	33.21	28.87	33.08	29.01	32.95	29.16	32.83	29.30	44
45 46	33.96 34.72	29.52 30.18	33.83 34.58	$\begin{array}{c} 29.67 \\ 30.33 \end{array}$	33.70 34.45	29.82 30.48	$33.57 \\ 34.32$	29.97 30.63	45 46
47	35.47	30.83	35.34	30.99	35.20	31.14	35.06	31.30	40
48 49	36.23 36.98	31.49	36.09	31.65	35.95	31.81	35.81	31.96	48
50	37.74	32.15 32.80	36.84 37.59	32.31 32.97	36.70 37.45	$ 32.47 \\ 33.13 $	36.56 37.30	32.63 33.29	49 50
	Dep.	Lat.	37.59 32.97 Dep. Lat.		Dep.	Lat.	Dep.	Lat.	
Distance.	49 I	Deg.	48} Deg.		481	Deg.	481 Deg.		Distance,

Distance.	41]	Deg.	411	Deg.	413	Deg.	413	Deg.	Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51 52	38.49 39.24	33.46 34.12	38.34 39.10	33.63 34.29	38.20 38.95	33.79 34.46	38.05 38.79	33.96 34.63	51 52
53	40.00	34.77	39.85	34.95	39.69	35.12	39.54	35.29	53
54 55	40.75	35.43 36.08	40.60 41.35	35.60 36.26	40.44 $ 41.19 $	35.78 36.44	40.29	35.96 36.62	54 55
56	42.26	36.74	42.10	36.92	41.94	37.11	41.78	37.29	56
57 58	43.02 43.77	37.40 38.05	42.85 43.61	$37.58 \\ 38.24$	42.69 43.44	37.77 38.43	42.53 43.27	37.96 38.62	57 58
59	44.53	38.71	44.36	38.90	44.19	39.09	44.02	39.29	59
60	45.28	39.36	45.11	39.56	44.94	$\frac{39.76}{40.42}$	44.76	39.95	60
61 62	46.79	40.02	45.86 46.61	40.22	45.69 46.44	41.08	45.51 46.26	40.62	61 62
63	47.55 48.30	41.33	47.37	41.54	47.18	41.75	47.00	41.95	63
64 65	49.06	41.99 42.64	48.12 48.87	$ \begin{array}{c} 42.20 \\ 42.86 \end{array} $	47.93 48.68	$42.41 \\ 43.07$	47.75 48.49	42.62 43.28	64 65
66	49.81	43.30	49.62	43.52	49.43	43.73	49.24	43.95	66
67 68	50.57	43.96 44.61	50.37	44.18 44.84	50.18 50.93	44.40 45.06	49.99 50.73	44.61 45.28	68
69	52.07	45.27	51.88	45.49	51.68	45.72	51.48	45.95	69
70	52.83	45.92	$\frac{52.63}{52.29}$	46.15	52.43	46.38	52.22	46.61	70
71 72	53.58 54.34	46.58	53.38 54.13	46.81 47.47	53.18 53.92	47.05 47.71	$52.97 \\ 53.72$	47.28 47.94	71 72
73	55.09	47.89	54.88	48.13	54.67	48.37	54.46	48.61	73
74 75	55.85 56.60	48.55	55.64 56.39	48.79 49.45	55.42 56.17	49.03 49.70	55.21 55.95	49.28 49.94	74 75
76	57.36	49.86	57.14	50.11	56.92	50.36	56.70	50.61	76
77 78	58.11 58.87	50.52 51.17	57.89 58.64	50.77 51.43	57.67 58.42	51.02 51.68	57.45 58.19	51.27 51.94	77
79	59.62	51.83	59.40	52.09	59.17	52.35	58.94	52.60	79
80	60.38	52.48	60.15	52.75	59.92	53.01	59.68	53.27	80
81 82	61.13	53.14 53.80	60.90	53.41 54.07	60.67	53.67 54.33	$60.43 \\ 61.18$	53.94 54.60	81 82
83	62.64	54.45	62.40	54.73	62.16	55.00	61.92	55.27	83
84 85	63.40 64.15	55.11 55.76	63.15	55.38 56.04	62.91	55.66 56.32	62.67 63.41	55.93 56.60	84
86	64.90	56.42	64.66	56.70	64.41	56.99	64.16	57.27	86
87	65.66	57.08	65.41	57.36	65.16	57.65	64.91	57.93	87
88 89	$ 66.41 \\ 67.17$	57.73 58.39	66.16	58.02 58.68	65.91 66.66	58.31 58.97	65.65 66.40	58.60 59.26	88
90	67.92	59.05	67.67	59.34	67.41	59.64	67.15	59.93	90
91	68.68 69.43	59.70 60.36	$68.42 \\ 69.17$	60.00	68.15 68.90	60.30	67.89 68.64	60.60	91
92 93	70.19	61.01	69.92	61.32	69.65	61.62	69.38	61.26	92
94	70.94	61.67	70.67	61.98	70.40	62.29	70.13	62.59	94
95 96	71.70	62.33 $ 62.98 $	71.43	$62.64 \\ 63.30$	71.15	62.95	70.88	63.26 63.92	95 96
97	73.21	63.64	72.93	63.96	72.65	64.27	72.37	64.59	97
98 99	73.96	64.29 64.95	73.68 74.43	64.62	73.40	64.94	73.11 73.86	65.26 65.92	98
100	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	100
nce.	Dep.	Lat.	Dep. Lat.		Dep. Lat.		Dep. Lat.		nce.
Distance.	49]	Deg.	483	Deg.	481	Deg.	481	Deg.	Distance

į.	42 I	og.	421	Deg.	421	Dog.	494	Deg.	Distance
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	псе.
1 2 3 4 5 5 6 7 8 8 9 10 11 12 2 13 3 14 15 6 16 17 18 19 19 19 20 21 22 23 24 25 6 27 28 29 30 31 32 33 34 4 35 6 6	0.74 1.49 2.23 2.97 4.46 5.20 5.20 7.43 8.92 9.66 9.66 11.15 11.89 12.63 13.38 14.12 16.35 17.84 18.58 19.78 20.06 20.81 22.22 23.78 24.75 24.75 25.27 26.77	7.36 8.03 8.03 8.03 8.03 8.03 8.03 8.03 8.03	0.74 1.48 2.22 2.96 5.92 6.66 7.40 8.88 9.62 10.36 10.36 11.84 12.58 13.32 14.06 16.28 17.77 18.51 19.99 20.73 21.47 19.99 20.73 21.47 22.21 22.95 23.66 24.43 25.17 25.61	0.67 1.34 2.02 2.69 4.03 4.71 5.38 6.05 6.72 7.40 8.07 8.74 10.09 10.76 8.74 11.43 12.10 11.43 12.10 11.47 11.47 11.47 11.48 11.48 11.49 1	0.74 1.47 2.21 2.95 5.169 4.42 5.190 6.64 7.37 7.37 18.85 9.58 11.06 11.85 11.06 11.25 11.25 11.25 11.25 11.25 11.25 11.25 11.25 11.25 12.	0.68 1.35 2.03 2.79 3.38 4.05 4.75 6.08 6.76 6.76 10.13 10.13 10.13 11.48 12.16 12.84 12.84 12.84 16.21 14.86 15.51 14.86 15.51 14.92 17.57 20.27 20.27 20.94 21.62 22.29 22.29 22.36 24.32	0.73 1.47 2.20 2.94 4.41 5.14 7.34 8.08 8.81 9.55 10.28 11.01 11.74 13.22 13.95 16.16 19.59 16.16 19.83 20.56 21.30 22.03 22.76 23.56 24.23 24.23 24.23 24.23 24.23 24.23 24.23	0.68 2.04 2.73 4.07 4.75 4.75 6.11 6.79 7.47 8.15 8.82 10.18 10.18 11.54 12.22 12.90 16.97 16.93 16.91 17.65 18.33 19.01 16.93 19.01 20.36 21.72 22.40 23.08 23.74 24.44	1 2 3 4 4 5 5 6 7 8 9 10 11 12 13 14 15 6 17 18 19 20 21 22 32 24 25 6 27 28 29 30 31 32 33 34 35 36
37 38 39 40 41 42 43	27.50 28.24 28.98 29.73 30.47 31.21 31.96	24.76 25.43 26.10 26.77 27.43 28.10 28.77	27.39 28.13 28.87 29.61 30.35 31.09 31.83	24.88 25.55 26.22 26.89 27.57 28.24 28.91	27.28 28.02 28.75 29.49 30.23 30.97 31.70	25.00 25.67 26.35 27.02 27.70 28.37 29.05	27.17 27.90 28.64 29.37 30.11 30.84 31.58	25.12 25.79 26.47 27.15 27.83 28.51 29.19	37 38 39 40 41 42 43
44 45 46 47 48 49 50	32.70 33.44 34.18 34.93 35.67 36.41 37.16	29.44 30.11 30.78 31.45 32.12 32.79 33.46	32.57 33.31 34.05 34.79 35.53 36.27 37.01	29.58 30.26 30.93 31.60 32.27 32.95 33.62	32.44 33.18 33.91 34.65 35.39 36.13 36.86	29.73 30.40 31.08 31.75 32.43 33.10 33.78	32.31 33.04 33.78 34.51 35.25 35.98 36.72	29.87 30.55 31.22 31.90 32.58 33.26 33.94	44 45 46 47 48 49 50
Distance.	Dep.	Lat. Deg.	Dep. 471	Lat. Deg.	Dep. 47½	Lat. Deg.	Dep. 471	Lat. Deg.	Distance.

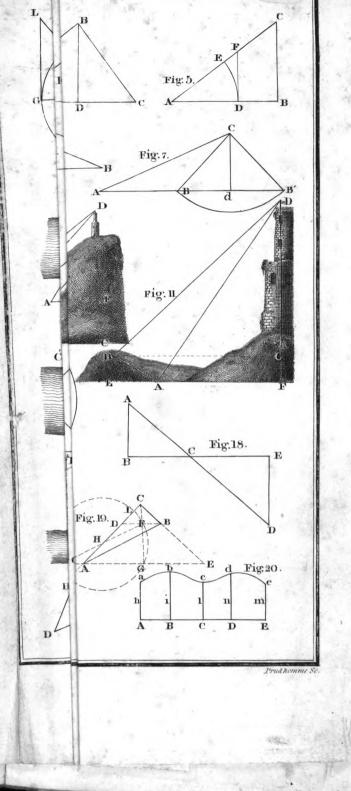
Dist	42 I	Deg.	421]	Deg.	421	Deg.	423 I	Deg.	Dist
Distance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Distance.
51	37.90	34.13	37.75	34.29	37.60	34.46	37.45	34.62	51
52	38.64	34.79	38.49	34.96	38.34	35,13	38.18	35.30	52
53	39.39	35.46	39.23	35.64	39.08	35.81	38.92	35.98	53
54	40.13	36.13	39.97	36,31	39.81	36.48	39.65	36.66	54
55	40.87	36.80	40.71	36.98	40.55	37.16	40.39	38.01	56
56	41,62	37.47	41.45	37.65	41.29 42.02	37,83	41.12 41.86	38.69	57
57 58	42.36	38.14	$\frac{42.19}{42.93}$	$\frac{38.32}{39.00}$	42.76	39.18	42.59	39.37	58
59	$\frac{43.10}{43.85}$	39.48	43.67	39.67	43.50	39.86	43.32	40.05	59
60	44.59	40.15	44.41	40.34	44.24	40.54	44.06	40.73	60
61	45.33	40,82	45.15	41.01	44.97	41.21	44.79	41.41	6
62	46.07	41.49	45.89	41.69	45.71	41.89	45.53	42.09	6:
63	46.82	42.16	46.63	42.36	46.45	42.56	46.26	42.76	68
64	$\frac{46.82}{47.56}$	42.82	47.37	43.03	47.19	43.24	47.00	43.44	6
65	48.30	43.49	48.11	43.70	47.92	43.91	47.73	44.12	6
66	49.05	44,16	48.85	44.38	48.66	44.59	48.47	45.48	6
67 68	49.79 50.53	44.83 45.50	49.59 50.33	$\frac{45.05}{45.72}$	49.40 50.13	45.94	49.93	46.16	6
69	51.28	46.17	51.07	46.39	50.87	46.62	50.67	46.84	6
70	52.02	46.84	51.82	47.07	51.61	47.29	51.40	47.52	7
71	52.76	47.51	52.56	47.74	52.35	47.97	52.14	48.19	7
72	53.51	48.18	53.30	48.41	53.08	48.64	52.87	48.87	7
73	54.25	48.85	54.04	49.08	53.82	49.32	53.61	49.55	7
74	54.99	49.52	54.78	49.76	54.56	49.99	54.34	50.23	7
75	55.74	50.18	55.52	50.43	55.30	50.67	55.07	50.91	7
76	56.48	50.85	56.26 57.00	51.10	56.03	$\begin{bmatrix} 51.34 \\ 52.02 \end{bmatrix}$	55.81 56.54	52.27	7
78	57.22 57.97	51.52	57.74	51.77	57.51	52.70	57.28	52.95	7
79	58.71	52.86	58.48	53.12	58.24	53.37	58.01	53.63	7
80	59.45	53.53	59.22	53.79	58.98		58.75		8
81	60.19	54.20	59.96	54.46	59.72		59.48		8
82	60.94	54.87	60.70	55.13	60.46	55.40	60.21	55.66	80 00
83	61.68	55.54	61.44	55.81	61.19		60.95		8
84	62.42	56.21	62.18	56.48	61.98		61.68		8
86	63.17 63.91	56.88 57.55	62.92	57.15	62.67		63.15		8
87	64.65	58.21	64.40	58.50	64.14		63.89	59.06	8
88	65.40	58.88	65.14	59.17	64.88	59.45	64.62	59.73	8
89	66.14	59.55	65.88	59.84	65.62	60.13		60.41	8
.90	66.88	60.22	66.62	60.51	66.35		-		9
91	67.63	60.89	67.36	61.19			66.82	61.77	9
92	68.37	61.56	68.10	61.86					9
93	69.11	62.23	68.84	62.53			68.29		g
94	69.86	63.57	70.32	63.20					9
96		64.24	71.06	64.55			70.49	65.16	9
97	72.08	64.91	71.80	65.22		65.53	71.23	65.84	9
98	72.83	65.57	72.54	65.89	72.25	66.21	71.96	66.52	. 9
99		66.24	73.28					67.20	10
100 e	74.31 Dep.	66.91 Lat.	74.02 Dep.	67.24 Lat.	73.78 Dep.	67.56	73.43 Dep.	67.88 Lat.	1
Distance.		1. 1943.	-P.	1	- Dop.	1	-	A velages.	
ist	40	Dom	172	Dan	1 471	Don	471	Deg.	1
0	48	Deg.	4.4	Deg.	1 4/2	Deg.	412	Dog.	1 2

Distance.	43	Deg.	431	Deg.	43 <u>}</u>	Deg.	431	Deg.	Distance
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ince.
1 2 3 4	0.73 1.46 2.19	0.68 1.36 2.05	0.73 1.46 2.19	0.69 1.37 2.06	0.73 1.45 2.18	0.69 1.38 2.07	0.72 1.44 2.17	0.69 1.38 2.07	1 2 3
5	2.93 3.66	2.73 3.41	2.91 3.64	2.74 3.43	2.90 3.63	2.75 3.44	2.89 3.61	2.77 3.46	4 5 6
6 7 8	4.39 5.12 5.85	4.09 4.77 5.46	4.37 5.10 5.83	4.11 4.80 5.48	4.35 5.08 5.80	4.13 4.82 5.51	4.33 5.06 5.78	4.15 4.84 5.53	6 7 8
9 10	6.58	6.14	6.56 7.28	6.17	6.53 7.25	6.20	6.50 7.22	6.22 6 92	9 10
11 12	8.04 8.78	7.50 8.18	8.01 8.74	7.54 8.22	7.98 8.70	7.57 8.26	7.95 8.67	7.61 8.30	11 12
13 14 15	9.51 10.24 10.97	8.87 9.55 10.23	9.47 10.20 10.93	8.91 9.59 10.28	9.43 10.16 10.88	8.95 9.64 10.33	9.39 10.11 10.84	8.99 9.68 10.37	13 14 15
16 17	11.70 12.43	10.91 11.59	11.65 12.38	10.96 11.65	11.61 12.33	11.01	11.56 12.28	11.06 11.76	16 17
18 19 20	13.16 13.90 14.63	12.28 12.96 13.64	13.11 12.33 11.70 13.06 12.39 13.08 13.08 14.57 13.70 14.51 13.77		13.00 13.72 14.45	12.45 13.14 13.83	18 19 20		
21 22	15.36 16.09	14.32 15.00	15.30 16.02	14.39 15.07	15.23 15.96	14.46 15.14	15.17 15.89	14.52 15.21	21 22
23 24 25	16.82 17.55 18.28	15.69 16.37 17.05	16.75 17.48 18.21	15.76 16.44 17.13	16.68 17.41 18.13	15.83 16.52	16.61 17.34 18.06	15.90 16.60 17.29	23 24 25
26 27	19.02	17.73 18.41	18.94 19.67	17.81 18 50	18.86 19.59	17.21 17.90 18.59	18.78 19.50	17.98 18.67	26 27
28 29 30	20.48 21.21 21.94	19.10 19.78 20.46	20.39 21.12 21.85	19.19 19.87 20.56	20.31 21.04 21.76	19.27 19.96 20.65	20.23 20.95 21.67	19.36 20.05 20.75	28 29 30
31 32	22.67 23.40	21.14 21.82	22.58 23.31	21.24 21.93	22.49 23.21	21.34 22.03	22.39 23.12	21.44 22.13	31 32
33 34 35	24.13 24.87 25.60	22.51 23.19 23.87	24.04 24.76 25.49	22.61 23.30 23.98	23.94 24.66 25.39	22.72 23.40 24.09	23.84 24.56 25.28	22.82 23.51 24.20	33 34 35
36 37	26.33 27.06	24.55 25.23	26.22 26.95	24.67 25.35	26.11 26.84	24.78 24.78 25.47	26.01 26.73	24.89 25.59	36 37
38 39	27.79 28.52 29.25	25.92 26.60 27.28	27.68 28.41	26.04 26.72	27.56 28.29	26.16 26.85	27.45 28.17	26.28 26.97 27.66	38 39 40
$\begin{array}{r} 40 \\ \hline 41 \\ 42 \end{array}$	29.25 29.99 30.72	27.96 28.64	29.13 29.86 30.59	$\frac{27.41}{28.09}$	29.01 29.74 30.47	$\frac{27.53}{28.22}$	$ \begin{array}{r} 28.89 \\ \hline 29.62 \\ 30.34 \end{array} $	28.35 29.04	41 42
43 44	31.45 32.18	29.33 30.01	30.59 28.78 30.47 28.91 31.32 29.46 31.19 29.60 32.05 30.15 31.92 30.29		31.06 31.78	29.74 30.43	43 44		
45 46 47	32.91 33.64	30.69 31.37 32.05	32.78 33.51 34.23	32.78 30.83 33.51 31.52		30.98 31.66	32.51 33.23 33.95	31.12 31.81 32.50	45 46 47
47 48 49	34.37 35.10 35.84	32.74 32.42	34.23 34.96 35.69	32.20 32.89 33.57	34.09 34.82 35.54	32.35 33.04 33.73	34.67 35.40	33.19 33.88	48 49
50 8	36.57 Dep.	34.10 Lat.	36.42 Dep.	36.42 34.26		34.42 Lat.	36.12 Dep.	34.58 Lat.	50 8
Distance		Deg.	46}	<u>'</u>	Dep. 46½	Deg.	461	Ь	Distance.

51 37.30 34.78 37.15 34.94 36.99 35.11 36.84 35.96 52 38.03 35.46 37.88 35.63 37.72 35.79 37.66 35.96 54 39.49 36.83 39.33 37.06 39.90 37.86 39.33 37.07 39.90 37.86 39.73 38.03 44.1.50 44.55	Distance.	43	Deg.	431	Deg.	43 <u>1</u>	Deg.	431	Deg.	Distance
52 38.03 35.46 37.88 36.63 37.72 35.70 37.56 85.06 53 38.76 36.15 38.60 38.31 38.44 36.48 38.29 36.65 54 39.49 36.83 39.33 37.00 39.90 37.86 39.73 38.03 56 40.96 38.87 41.52 39.06 40.62 38.55 40.45 38.87 57 41.69 38.87 41.52 39.06 41.35 39.24 41.17 39.42 60 43.88 40.92 42.27 40.43 42.80 40.61 42.22 40.80 63 46.08 42.28 45.16 42.48 44.97 42.86 44.97 42.88 43.57 64 46.81 43.65 46.62 43.85 46.74 44.97 42.87 45.51 43.57 64 46.81 43.65 46.62 43.85 46.42 44.97 42.88 47.94	nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ance.
54 39.49 36.83 39.33 37.00 39.17 37.17 39.01 37.34 55 40.96 38.19 40.79 38.37 40.62 38.55 40.45 38.72 57 41.69 38.87 41.52 39.06 41.35 39.24 41.17 39.42 59 43.15 40.24 42.97 40.43 42.80 40.61 42.62 40.80 60 43.88 40.92 43.70 41.11 43.52 41.30 43.34 41.49 61 44.61 41.60 44.43 41.80 44.25 41.99 44.06 42.48 63 46.08 42.97 45.89 43.17 45.70 43.37 46.79 42.87 63 46.08 42.97 45.89 43.17 45.70 43.37 46.51 43.57 64 45.14 48.07 45.91 48.07 46.81 43.65 46.62 43.85 46.42 44.05	52	38.03	35.46	37.88	35 63	37.72	35.79	37.56	35.96	51 52
56 40.96 38.19 40.79 38.37 40.62 38.55 40.45 38.72 57 41.69 38.87 41.52 39.06 41.35 39.24 41.17 39.42 59 43.15 40.24 42.97 40.43 42.80 40.61 42.62 40.80 60 43.88 40.92 43.70 41.11 43.52 41.30 43.34 41.49 61 44.61 41.60 44.43 41.80 44.25 41.99 44.06 42.18 62 45.34 42.28 45.16 42.48 44.97 42.68 44.79 42.87 64 46.81 43.65 46.62 43.85 46.24 44.06 42.18 44.26 44.06 42.18 44.76 44.65 44.54 47.15 44.74 46.93 44.96 44.86 44.96 44.96 44.96 44.96 44.96 44.96 44.96 44.96 44.96 44.96 44.96 <t< td=""><td>54</td><td>39.49</td><td>36.83</td><td>39.33</td><td>37.00</td><td>39.17</td><td>37.17</td><td>39.01</td><td>37.34</td><td>53 54</td></t<>	54	39.49	36.83	39.33	37.00	39.17	37.17	39.01	37.34	53 54
57 41.69 38.87 41.52 39.06 41.35 39.24 41.19 40.11 58 42.42 39.56 42.25 39.74 42.07 39.92 41.90 40.11 60 43.88 40.92 43.70 41.11 43.52 41.99 44.06 42.48 61 44.61 41.60 44.43 41.80 44.25 41.99 44.06 42.18 63 46.08 42.97 45.89 43.17 45.70 43.37 45.51 43.57 64 46.81 43.65 46.62 43.85 46.42 44.05 44.79 42.87 66 47.54 44.33 47.34 44.54 47.15 44.76 45.23 47.86 44.95 46.23 44.95 67 49.00 45.69 48.00 45.91 48.60 46.12 44.40 49.43 68 50.46 47.06 50.99 47.96 50.76 48.87 51.19	56	40.96	38.19	40.79	38.37		37.86 38.55	40.45	38.72	55 56
60 43.88 40.92 43.70 41.11 43.52 41.30 43.34 41.49 61 44.61 41.60 44.43 41.80 44.25 41.99 44.06 42.18 62 45.34 42.28 45.16 42.48 44.97 42.68 44.79 42.87 64 46.81 43.65 46.62 43.85 46.42 44.05 46.53 44.26 65 47.54 41.30 47.34 47.34 47.34 47.34 47.44 44.95 44.95 66 48.27 45.01 48.80 45.91 48.60 46.12 48.40 46.33 68 49.73 46.88 49.53 46.59 49.33 46.81 49.12 47.02 69 50.46 47.06 50.26 47.28 50.05 47.50 49.84 47.71 70 51.19 47.46 50.92 47.96 50.78 48.18 50.57 48.41	58	42.42	39.56	42.25	39.74	42.07	39.24 39.92	41.90	40.11	57 58
62 45.34 42.28 45.16 42.48 44.97 42.68 44.79 42.87 63 46.08 42.97 45.89 43.17 45.70 43.37 45.51 43.57 64 46.81 43.35 46.62 43.85 46.42 44.05 46.23 44.26 66 47.50 44.34 47.15 44.74 46.95 44.95 67 49.00 45.69 48.80 45.91 46.60 46.12 48.40 46.33 68 49.73 46.38 49.53 46.59 49.33 46.81 49.12 47.02 69 50.46 47.06 50.26 47.28 50.05 47.50 49.84 47.71 70 51.19 47.74 50.99 47.96 50.78 48.18 50.57 48.41 71 51.93 49.79 53.17 50.02 52.95 50.25 52.73 50.48 72 52.66 49.10										59 60
63					41.80					61 62
66 47.54 44.33 47.34 44.54 47.15 44.74 46.95 44.95 66 48.27 45.01 48.07 45.22 47.87 45.43 47.68 44.95 68 49.73 46.38 49.53 46.59 49.33 46.81 49.12 47.02 69 50.46 47.06 50.26 47.28 50.05 47.50 49.84 47.71 70 51.19 47.74 50.99 47.96 50.78 48.18 50.57 48.41 71 51.93 49.79 53.17 50.02 52.95 50.25 52.01 49.79 73 53.39 49.79 53.17 50.02 52.95 50.25 53.45 51.19 74 54.12 50.47 53.90 50.70 53.68 50.94 53.45 51.17 75 54.85 51.83 55.36 52.07 55.13 52.31 54.90 52.55 76	63	46.08	42.97	45.89	43.17	45.70	43.37	45.51	43.57	63 64
68 49.73 46.38 49.53 46.59 49.33 46.81 49.12 47.02 69.50.46 47.06 50.26 47.28 50.05 47.50 49.84 77.71 70 51.19 47.74 50.99 47.96 50.78 48.18 50.57 48.41 72.24 67.72 52.66 49.10 52.44 49.33 52.23 49.56 52.01 49.79 73 53.39 49.79 53.17 50.02 52.95 50.25 52.73 50.48 74 54.12 50.47 53.90 50.70 53.68 50.94 53.45 51.17 75 54.85 51.85 55.86 52.07 55.58 51.83 55.36 52.07 55.13 52.31 54.90 52.55 77 55.31 52.51 56.08 52.76 55.85 53.00 55.62 53.25 77 56.31 52.51 56.08 52.76 55.85 53.00 55.62 53.25 77 55.92 59.73 56.18 59.46 55.58 53.69 56.34 53.94 79 57.78 57.78 57.55 59.2 59.78 57.48 13 57.30 54.38 57.07 54.63 58.27 54.81 59.24 55.24 59.00 55.50 58.76 55.76 58.36 50.94 53.45 59.97 55.92 59.73 56.18 59.48 56.45 59.27 55.32 56.26 69.27 55.76 58.65 57.60 58.62 59.97 55.92 59.73 56.18 59.48 56.45 59.23 56.70 83 60.70 56.61 60.45 56.87 60.21 57.13 59.96 57.40 88 62.90 58.65 62.64 58.93 62.28 59.97 55.92 59.33 63.37 56.18 59.48 56.45 59.23 56.70 88 62.90 58.65 62.64 58.93 62.28 59.29 58.65 62.64 58.93 62.28 59.29 58.65 62.64 58.93 62.38 59.20 62.12 59.47 89 65.82 63.43 67.74 63.72 67.82 60.88 63.57 60.85 89 65.09 60.70 64.82 60.98 64.56 61.95 62.85 60.16 63.11 59.49 66.75 70.90 60.70 64.82 60.98 64.56 61.95 60.58 61.50 60.80 58.29 67.40 64.82 60.98 64.56 61.95 60.16 63.11 67.90 60.16 60.40 56.09 60.70 64.82 60.98 64.56 61.95 65.01 62.24 99 68.75 64.11 68.47 63.72 67.46 64.02 67.18 64.31 99 67.28 62.74 67.01 63.04 66.73 63.33 66.46 63.62 99 67.28 62.74 67.04 63.04 66.73 63.33 66.46 63.62 99 67.28 62.74 67.04 63.04 66.75 60.98 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 66.88 60.99 60.70 60.80 60.99 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 60.80 60.90 60.70 6	65	47.54	44.33	47.34	44.54	47.15	44.74	46.95	44.95	65 66
669 50.46 47.08 50.26 47.28 50.05 47.50 49.84 47.71 70 51.19 47.74 50.99 47.96 50.78 48.18 50.57 48.41 72 52.66 49.10 52.44 49.33 52.23 49.56 52.01 49.79 73 53.39 49.79 53.17 50.02 52.95 50.25 52.73 50.48 74 54.12 50.47 53.90 50.70 53.68 50.94 53.45 51.17 75 54.85 51.83 56.36 52.07 53.68 50.94 53.45 51.17 75 56.31 52.51 56.08 52.76 55.35 53.09 54.90 52.66 77 56.31 52.51 56.08 52.76 55.35 53.09 55.62 53.25 78 57.05 53.20 56.81 53.44 56.58 53.69 56.34 53.94 79	67	49.00	45.69	48.80	45.91	48.60	46.12	48.40	46.33	67 68
71 51.93 48.42 51.71 48.65 51.50 48.87 51.29 49.10 72 52.66 49.10 52.44 49.33 52.23 49.56 52.01 49.79 73 53.39 49.79 53.17 50.02 52.95 50.25 52.73 50.48 77 55 54.85 51.15 54.63 51.39 54.40 51.63 54.18 51.16 65.58 51.35 55.36 52.07 55.13 52.31 54.90 52.55 78 57.05 53.20 56.81 53.44 56.58 53.00 55.62 53.25 56.34 53.25 58.35 57.05 56.81 53.44 56.58 53.00 55.62 53.25 56.34 53.25 57.76 55.32 54.90 52.55 78 57.05 53.20 56.81 53.44 56.58 53.09 57.07 54.63 89.27 54.13 57.30 54.38 57.07 55.32 58.07 57.79 56.12 5	69	50.46	47.06	50.26	47.28	50.05	47.50	49.84	47.71	69 70
73 53.39 49.79 53.17 50.02 52.95 50.25 52.73 50.48 74 54.12 50.47 53.90 50.70 53.68 50.94 53.45 51.17 55.485 51.15 54.63 51.39 54.40 51.63 54.41 51.63 54.40 51.63 54.40 51.63 54.40 51.63 54.40 55.58 53.00 55.56 58.27 55.13 52.31 54.90 52.55 56.22 55.25 55.85 53.00 56.34 53.45 79.77 57.78 57.78 55.24 59.00 55.50 55.85 53.00 56.34 53.94 79.77 57.79 55.24 59.00 55.50 58.76 55.77 57.79 55.32 58.27 54.81 58.03 55.70 57.79 55.32 58.27 54.81 58.03 55.07 57.79 55.32 58.27 54.81 58.03 55.76 58.51 56.01 56.01 58.62 59.26 58.27 54.8		51.93	48.42	51.71	48.65	51.50	48.87	51.29	49.10	71 72
76 54.85 51.15 54.63 51.39 54.40 51.63 54.18 51.86 76 55.58 51.83 55.36 52.07 55.13 52.31 54.90 52.55 78 57.05 53.20 56.81 53.44 56.58 53.09 56.34 59.94 79 57.78 53.88 57.54 57.30 54.38 57.07 54.63 80 58.51 54.56 58.27 54.81 57.30 64.38 57.77 56.31 55.24 81 59.24 55.24 59.00 55.50 58.76 55.76 58.51 56.01 56.01 82 69.97 55.92 59.73 56.18 59.48 56.45 59.23 56.70 84 61.43 57.29 61.18 57.56 60.21 57.13 59.96 57.40 86 62.17 57.97 61.91 58.24 61.66 58.51 61.40 58.78	73	53.39	49.79	53.17	50.02	52.95	50.25	52.73	50.48	73 74
77 56.31 52.51 56.08 52.76 55.85 53.00 55.62 53.25 78 57.05 53.20 56.81 53.44 56.58 53.69 56.34 53.24 80 58.51 54.56 58.27 54.81 57.30 54.38 57.07 55.32 58.69 56.34 58.27 54.81 58.03 55.07 57.79 55.32 58.61 58.76 55.76 55.76 55.76 55.76 56.51 56.01 56.01 56.68 59.97 55.92 59.73 56.18 59.48 56.45 59.23 56.70 56.70 58.60 60.93 57.82 60.68 58.70 60.70 56.70 60.91 57.13 59.96 57.40 60.84 56.45 59.23 56.70 56.70 60.88 59.23 56.70 56.70 60.88 57.92 60.68 58.93 60.21 57.13 59.96 57.40 60.68 58.09 60.88 62.99 58.65	75	54.85	51.15	54.63	51.39	54.40	51.63	54.18	51.86	75
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	77	56.31	52.51	56.08	52.76	55.85	53.00	55.62	53.25	76 77
81 59.24 55.24 59.00 55.50 58.76 55.76 58.51 56.01 82 59.97 55.92 59.73 56.18 59.48 56.45 59.23 56.70 83 60.70 56.61 60.45 56.87 60.21 57.13 59.96 57.40 84 61.43 57.29 61.18 57.56 60.93 57.82 60.68 58.09 85.62 62.17 57.97 61.91 58.24 61.66 58.51 61.40 58.78 86 62.90 58.65 62.64 58.93 62.38 59.20 62.12 59.47 88 64.36 60.02 64.10 60.30 63.83 60.58 63.57 60.16 88 64.36 60.02 64.10 60.30 63.83 60.58 63.57 60.85 64.28 60.98 64.56 61.26 64.29 61.54 65.28 61.95 65.01 62.24 65.01 62.24 65.01 62.24 65.01 62.24 65.01 <	79	57.78	53.88	57.54	54.13	57.30	54.38	57.07	54.63	78 79 80
83 60.70 56.61 60.45 56.87 60.21 57.13 59.96 57.40 84 61.43 57.29 61.18 57.56 60.93 57.82 60.68 58.09 68.62 62.17 57.97 61.91 58.24 61.66 58.51 61.40 58.78 86.28 62.90 58.65 62.64 58.93 62.38 59.20 62.12 59.47 88.64.36 60.02 64.10 60.30 63.83 60.58 63.57 60.85 60.58 60.58 61.56 60.58 61.36 65.55 61.67 65.28 61.56 62.06 66.28 62.35 66.01 62.85 65.01 62.24 99 65.82 61.38 65.55 61.67 66.28 61.95 65.01 62.24 66.24 62.35 66.01 62.24 65.01 62.24 99 67.28 62.34 67.74 63.72 67.46 64.02 67.18 64.31 94 68.75 64.11 68.47 64.41	81	59.24	55.24	59.00	55.50	58.76	55.76	58.51	56.01	81
85 62.17 57.97 61.91 58.24 61.60 58.51 61.40 58.78 68.78 86 62.90 58.65 62.64 58.93 62.38 59.20 62.12 59.47 68.63 59.33 63.37 59.61 63.11 59.89 62.85 60.16 68.86 64.36 60.02 64.10 60.30 63.83 60.58 63.57 60.85 69.20 61.54 65.28 61.95 65.01 62.24 66.71 65.24 66.72 65.28 61.95 65.01 62.24 66.71 66.72 66.73 63.33 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.74 63.72 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.46 63.62 63.93 66.43 64.71 <td>83</td> <td>60.70</td> <td>56.61</td> <td>60.45</td> <td>56.87</td> <td>60.21</td> <td>57.13</td> <td>59.96</td> <td>57.40</td> <td>82 83</td>	83	60.70	56.61	60.45	56.87	60.21	57.13	59.96	57.40	82 83
87 63.63 59.33 63.37 59.61 63.11 59.89 62.85 60.16 68.86 60.26 60.16 63.83 60.58 63.57 60.85 69.60 60.86 63.63 60.58 63.57 60.85 60.86 63.63 60.58 63.57 60.85 60.98 65.55 61.67 65.28 61.26 64.29 61.54 65.24 65.74 62.24 65.24 65.74 62.24 65.28 66.01 62.64 65.74 62.93 66.46 66.73 63.33 66.46 63.62 63.62 93 68.02 63.43 67.74 63.72 67.46 64.02 67.18 64.31 64.91 67.18 64.31 65.94 65.94 65.94 65.94 65.94 65.94 65.94 65.95 69.64 66.08 69.35 66.39 66.39 66.77 70.07 67.08 66.39 66.77 70.07 67.08 66.39 66.77 70.07 67.08 77.77 67.77	85	62.17	57.97	61.91	58.24	61.66	58.51	61,40	58.78	84 85
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	87	63.63	59.33	63.37	59.61	62.38 63.11		62.85	60.16	86 87
91 66.55 62.06 66.28 62.35 66.01 62.64 65.74 62.93 92 67.28 62.74 67.01 63.04 66.73 63.33 66.46 63.62 93 68.02 63.43 67.74 63.72 67.46 64.02 67.18 64.31 94 68.75 64.11 68.47 64.41 68.19 64.71 67.90 60.00 96 70.21 65.47 69.92 65.78 69.64 60.08 69.35 66.39 97 70.94 66.15 70.65 66.46 70.36 66.77 70.07 67.08 98 71.67 66.84 71.37 67.15 71.09 67.46 70.79 67.77 99 72.40 67.52 72.11 67.83 71.81 68.15 70.56 68.46 100 73.14 68.20 72.84 68.52 72.54 68.84 72.24 68.15 100 73.14 68.20 72.84 68.52 72.54 68.84 72.24 68.15 10	89	65.09	60.70	64.82	60.98	64.56	61.26	64.29	61.54	88 89
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		66,55			62.35				62.93	90
94 68.75 64.11 68.47 64.41 68.19 64.71 67.90 65.00 95 69.48 64.79 69.20 65.09 68.91 65.39 68.62 65.69 96 70.21 65.47 69.92 65.78 69.64 66.08 69.35 66.39 97 70.94 66.15 70.65 66.46 70.36 66.77 70.07 67.08 98 71.67 66.84 71.37 67.15 71.09 67.46 70.79 67.77 99 72.40 67.52 72.11 67.83 71.81 68.15 71.51 68.46 100 73.14 68.20 72.84 68.52 72.54 68.84 72.24 69.15 10		67.28 68.02		67.01	63.04	66.73	63.33	66.46	63.62	92 93
96 70.21 65.47 69.92 65.78 69.64 66.08 69.35 66.39 97 70.94 66.15 70.65 66.46 70.36 66.77 70.07 67.08 98 71.67 66.84 71.37 67.15 71.09 67.46 70.79 67.77 99 72.40 67.52 72.11 67.83 71.81 68.15 71.51 68.46 100 73.14 68.20 72.84 68.52 72.54 68.84 72.24 69.15 10		68.75 69.48	64.11	68.47	64.41	68.19	64.71	67.90	65.00	94 95
98 71.67 66.84 71.37 67.15 71.09 67.46 70.79 67.77 99 72.40 67.52 72.11 67.83 71.81 68.15 71.51 68.46 91.00 73.14 68.20 72.84 68.52 72.54 68.84 72.24 69.15 100 73.64 72.84		70.21		69.92	65.78 66.46	69.64	66.08	69.35	66.39 67.08	96 97
100 73.14 68.20 72.84 68.52 72.54 68.84 72.24 69.15 10	99	72.40	66.84	71.37	67.15 67.83	71.09	67.46	70.79	67.77 68.46	98 99
Dep. Lat. Dep. Dep. Lat. Dep. De			68.20	72.84 68.52		72.54	68.84	72.24	69.15	100
	tanc	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
దే 47 Deg. 461 Deg. 461 Deg. 2	D.	47 I	Deg.	461	Deg.	461	Deg.	461	Deg.	Dis

Distance.	44 Deg.		44} Deg.		44½ Deg.		441 Deg.		45 Deg.		Distance.
nce.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	mce.
1 2	0.72	0.69 1.39	$0.72 \\ 1.43$	0.70 1.40	0.71 1.43	0.70 1.40	0.71	$0.71 \\ 1.41$	$0.71 \\ 1.41$	0.71	1 2
2 3 4	2.16 2.88	2.08 2.78	2.15 2.87	2.09 2.79	2.14 2.85	2.10 2.80	2.13 2.84	$2.11 \\ 2.82$	2.12 2.83	2.12 2.83	2 3 4
5 6	3.60 4.32	3.47 4.17	3.58 4.30	3.49 4.19	3.57 4.28	3.50 4.21	3.55 4.26	$\frac{3.52}{4.22}$	3.54 4.24	3.54 4.24	5 6
7	5.04 5.75	4.86 5.56	5.01 5.73	4.88 5.58	4.99 5.71	4.91 5.61	4.97 5.68	4.93 5.63	4.95 5.66	4.95 5.66	7 8
9 10	6.47 7.19	6.25 6.95	6.45 7.16	6.28 6.98	6.42 7.13	6.31 7.01	6.39 7.10	6.34 7.04	6.36	6.36	9 10
11	7.91	7.64	7.88	7.68	7.85	7.71	7.81	7.74	$\frac{7.07}{7.78}$	$\frac{7.07}{7.78}$	$\overline{11}$
12 13	8.63 9.35	8.34 9.03	8.60 9.31	8.37 9.07	8.56 9.27	8.41 9.11	8.52 9.23	8.45 9.15	8.49 9.19	8.49 9.19	12 13
14 15	$10.07 \\ 10.79$	$9.73 \\ 10.42$	10.03 10.74	$9.77 \\ 10.47$	9.99 10.70	9.81 10.51	9.94 10.65	9.86 10.56	9.90	9.90 10.61	14 15
16 17	$11.51 \\ 12.23$	11.11	11.46	$\frac{11.16}{11.86}$	11.41 12.13	$\substack{11.21\\11.92}$	$11.36 \\ 12.07$	11.26 11.97	$11.31 \\ 12.02$	11.31 12.02	16 17
18 19	12.95 13.67	12.50 13.20	12.89 13.61	12.56 13.26	12.84 13.55	$\frac{12.62}{13.32}$	$12.78 \\ 13.49$	$12.67 \\ 13.38$	12.73	12.73 13.43	18 19
20	14.39	13.89	14.33	13.96	14.26	14.02	14.20	14.08	14.14	14.14	20
21 22	15.11 15.83	14.59 15.28	15.04 15.76	14.65 15.35	14.98 15.69	$14.72 \\ 15.42$	$14.91 \\ 15.62$	$14.78 \\ 15.49$	14.85 15.56		21 22
24	$16.54 \\ 17.26$	15.98 16.67	16.47 17.19	16.05 16.75	17.12	$16.12 \\ 16.82$		16.19 16.90	$16.26 \\ 16.97$	16.26 16.97	23 24
25 26	17.98 18.70	17.37 18.06	17.91 18.62	17.44 18.14	17.83 18.54	$17.52 \\ 18.22$	17.75 18.46	17.60 18.30	17.68 18.38	17.68 18.38	25 26
	19.42 20.14	18.76 19.45		18.84	19.26 19.97	$18.92 \\ 19.63$	19.17	19.01 19.71		19.09 19.80	27 28
29	20.86	20.15 20.84	$20.77 \\ 21.49$	20.24 20.93	20.68 21.40	$\frac{20.33}{21.03}$	$\frac{20.60}{21.31}$	20.42 21.12	20.51	20.51 21.21	29 30
31	22.30	21.53	22.21	21.63	22.11	21.73	$\overline{22.02}$	21.82	21.92	$\overline{21.92}$	31
33	23.74	22.23 22.92	22.92 23.64	22.33 23.03	$22.82 \\ 23.54$	$22.43 \\ 23.13$	22.73 23.44	22.53 23.23	$\begin{array}{c} 22.63 \\ 23.33 \end{array}$	$22.63 \\ 23.33$	32 33
34	24.46	23.62 24.31	24.35 25.07	$23.72 \\ 24.42$	24.25 24.96	23.83 24.53	$24.15 \\ 24.86$		24.04 24.75		34 35
		25.01 25.70	$25.79 \\ 26.50$	25.12 25.82	25.68 26.39	$25.23 \\ 25.93$	$25.57 \\ 26.28$	25.34 26.05	25.46 26.16	25.46 26.16	36 37
38	27.33 28.05		27.22 27.94	$26.52 \\ 27.21$	27.10 27.82	26.63 27.34	26.99	$26.75 \\ 27.46$		26.87 27.58	38 39
40	28.77	27.79	28.65	27.91	28.53	28.04	28.41	28.16	28.28	28.28	40
42	29.49 30.21	28.48 29.18	$\begin{array}{c} 29.37 \\ 30.08 \end{array}$	28.61 29.31	29.24 29.96	28.74 29.44		28.86 29.57		$28.99 \\ 29.70$	41 42
	30.93 31.65	29.87 30.56	$30.80 \\ 31.52$	30.00 30.70	$\frac{30.67}{31.38}$	30.14 30.84	31.25	$30.27 \\ 30.98$	31.11	30.41 31.11	43 44
45	32.37	31.26 31.95	$32.23 \\ 32.95$	$\frac{31.40}{32.10}$	$32.10 \\ 32.81$	$31.54 \\ 32.24$	31.96 32.67		31.82		45 46
47	33.81 34.53	32.65 33.34	33.67 34.38	32.80	$33.52 \\ 34.24$	32.94		33.09		33.23	47 48
49		34.04	35.10 35.82	34.19	34.95 35.66	34.34 35.05	34.80 35.51		34.65	34.65 35.36	49
	Dep.	Lat.	Dep.		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Distance.	46 Deg.		45-1 Deg.		45½ Deg.		451 Deg.		45 Deg.		Distance.

Dista	44 Deg.		441 Deg.		44½ Deg.		44‡ Deg.		45 Deg.		Distan
ance.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	ınce.
51 52	36.69 3 37.41 3		$\frac{36.53}{37.25}$	35.59 36.29	$\frac{36.38}{37.09}$		$\frac{36.22}{36.93}$	35.90	36.06 36.77		51 52
53	38.12 3	86.82	37.96	36.98	37.80	37.15	37.64	37.31	37.48	37.48	53 54
55	$\begin{vmatrix} 38.84 & 3 \\ 39.56 & 3 \end{vmatrix}$	88.21			39.23	38.55	$\begin{array}{c} 38.35 \\ 39.06 \end{array}$	38.72	$\frac{38.18}{38.89}$	38.89	55
	40.28 3 $ 41.00 3$		$\frac{40.11}{40.83}$	$39.08 \\ 39.77$	$\frac{39.94}{40.66}$	39.25 39.95	$\frac{39.77}{40.48}$	$\frac{39.42}{40.13}$	$39.60 \\ 40.31$		56 57
58	$\frac{41.724}{42.444}$	0.29	$\frac{41.55}{42.26}$	40.47	$\frac{41.37}{42.08}$	40.65	$\frac{41.19}{41.90}$	40.83	$\frac{41.01}{41.72}$		58 59
	43.16 4	1.68	42.98	41.87	42.79	42.05	42.61	42.24	42.43	42.43	60
61 62	$43.884 \\ 44.604$		43.69 44.41	42.57 43.26	$43.51 \\ 44.22$	42.76 43.46	$\frac{43.32}{44.03}$		43.13 43.84	43.13 43.84	61 62
63	45.32 4	3.76	45.13	43.96	44.93	44.16	44.74	44.35	44.55	44.55	63
	$46.044 \\ 46.764$		45.84 46.56	45.36	46.36		45.45 46.16	45.06 45.76	$45.25 \\ 45.96$		64 65
66 67	47.48 4 48.20 4	5.85	$47.28 \\ 47.99$	46.05 46.75	47.07 47.79		46.87 47.58		46.67 47.38		66 67
68	48.92 4	17.24	48.71	47.45	48.50	47.66	48.29	47.87	48.08	48.08	68 69
69 70	$\frac{49.63}{50.35}$		$\frac{49.42}{50.14}$	$\frac{48.15}{48.85}$	$49.21 \\ 49.93$	$\substack{\textbf{48.36}\\\textbf{49.06}}$	$\frac{49.00}{49.71}$		$\frac{48.79}{49.50}$		70
71 72			50.86 51.57	49.54 50.24		49.76 50.47	$\frac{50.42}{51.13}$		50.20		71 72
73	52.51 5	50.71	52.29	50.94	52.07	51.17	51.84	51.39	$50.91 \\ 51.62$	51.62	73
	$\begin{bmatrix} 53.23 \\ 53.95 \\ 5 \end{bmatrix}$		53.01 53.72	$51.64 \\ 52.33$	52.78 53.49	51.87 52.57		52.10 52.80		52.33 53.03	74 75
76 77	54.67 5	2.79	54.44	53.03 53.73	54.21 54.92	$53.27 \\ 53.97$	$53.97 \\ 54.68$	53.51	53.74		76 77
78	56.11 5	4.18	55.87	54.43	55.63	54.67	55.39	54.91	55.15	55.15	78
79 80	56.83 5 57.55 5		56.59 57.30	$\begin{array}{c} 55.13 \\ 55.82 \end{array}$	56.35 57.06	$\begin{array}{c} 55.37 \\ 56.07 \end{array}$		$\begin{array}{c} 55.62 \\ 56.32 \end{array}$		55.86 56.57	79 80
	58.27 5		58.02	56.52	57.77	56.77	57.52		57.28	57.28 57.98	81 82
83	58.99 5 59.71 5	57.66	58.74 59.45	$\begin{array}{c} 57.22 \\ 57.92 \end{array}$	58.49 59.20	57.47 58.18	58.95		58.69	58.69	83
	$60.425 \\ 61.145$		$60.17 \\ 60.89$	58.61 59.31	59.91 60.63	58.88 59.58		59.14 59.84		59.40 60.10	84 85
86	61.86 5 62.58 6	59.74	$61.60 \\ 62.32$	60.01	61.34 62.05		61.08	$60.55 \\ 61.25$	60.81	$60.81 \\ 61.52$	86 87
88	63.30	31.13	63.03	61.41	62.77	61.68	62.50	61.95	62.23	62.23	88
90	$64.026 \\ 64.746$		$63.75 \\ 64.47$	62.10 62.80	63.48 64.19	$62.38 \\ 63.08$	$63.21 \\ 63.92$			$62.93 \\ 63.64$	89 90
91			65.18	63.50	64.91	63.78	64.63		64.35		91
93	66.18 6 66.90 6	4.60	66.62	$64.20 \\ 64.89$	65.62	64.48 65.18	66.05	$64.77 \\ 65.47$	65.76	65.05 65.76	92 93
94 95	67.62 6 68.34 6		$67.33 \\ 68.05$	65.59 66.29	67.05	$65.89 \\ 66.59$	$66.76 \\ 67.47$			66.47 67.18	94 95
96	69.06 6 69.78 6	66.69		66.99 67.69	68.47 69.19	67.29 67.99		67.59	67.88	67.88	96 97
98	70.50 6	8.08	70.20	68.38	69.90	68.69	69.60	68.99	68.59 69.30	69.30	98
99 100	71.21 6			$\begin{array}{c} 69.08 \\ 69.78 \end{array}$	70.61	$69.39 \\ 70.09$	70.31 71.02		70.00 70.71		99 100
nce.	Dep. Lat.		Dep. Lat.		Dep. Lat.		Dep. Lat.		Dep. Lat.		Distance.
Distance.	46 Deg.		451	45 } Deg.		45½ Deg.		451 Deg.		45 Deg.	



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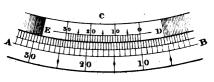
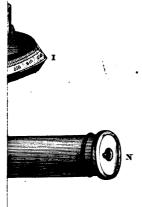


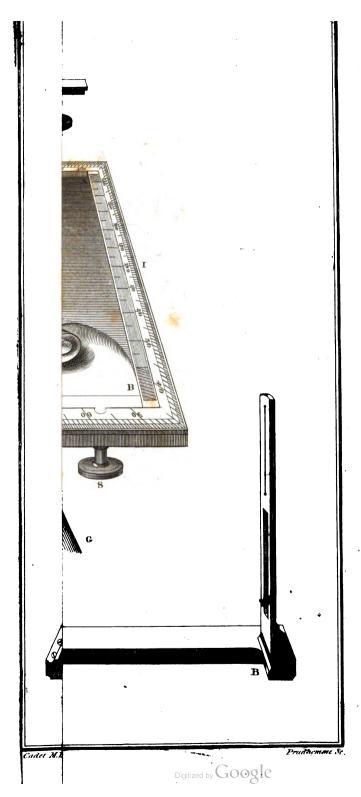
Fig.2.

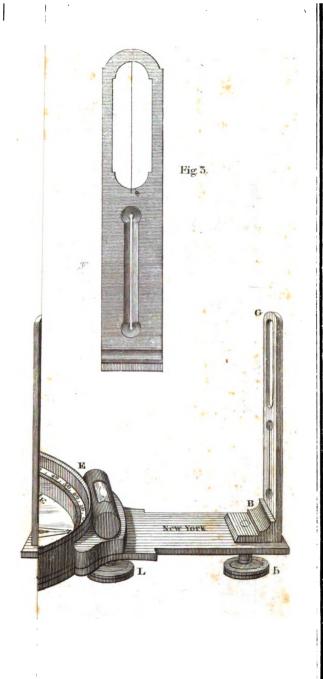


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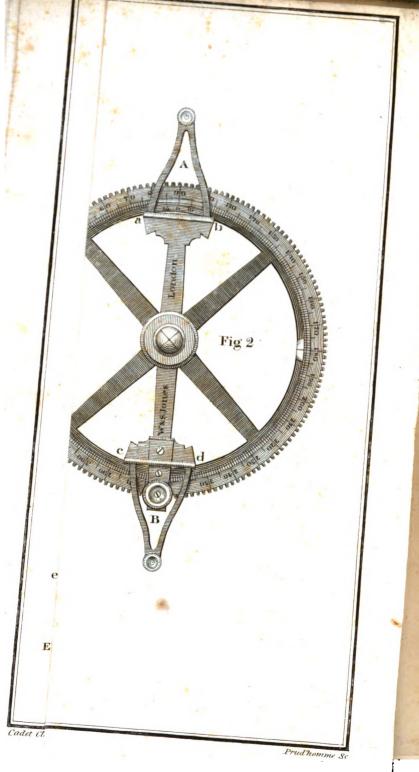
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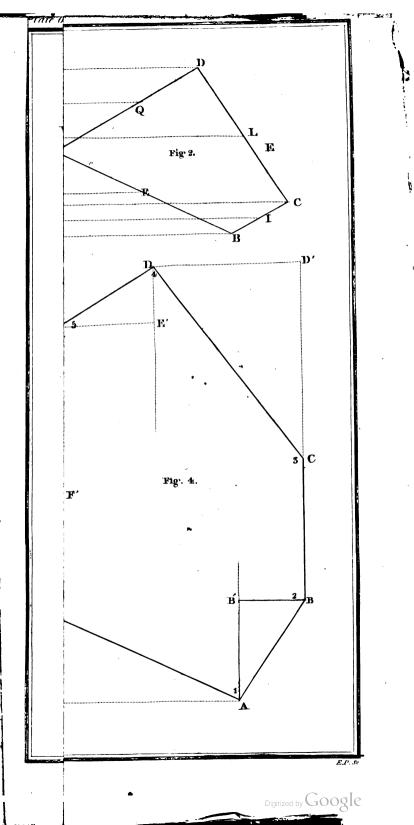


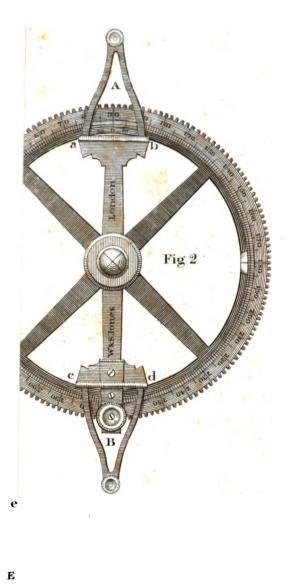


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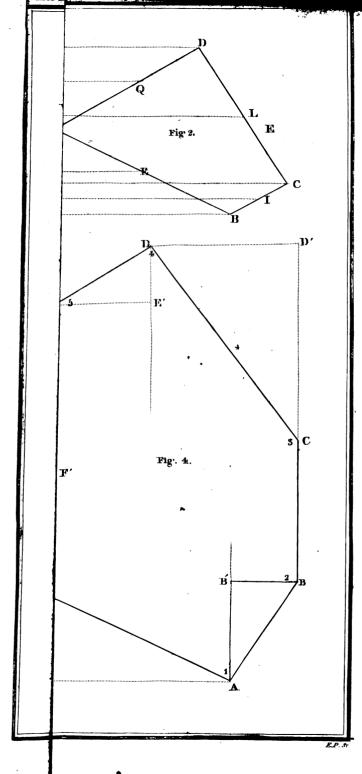


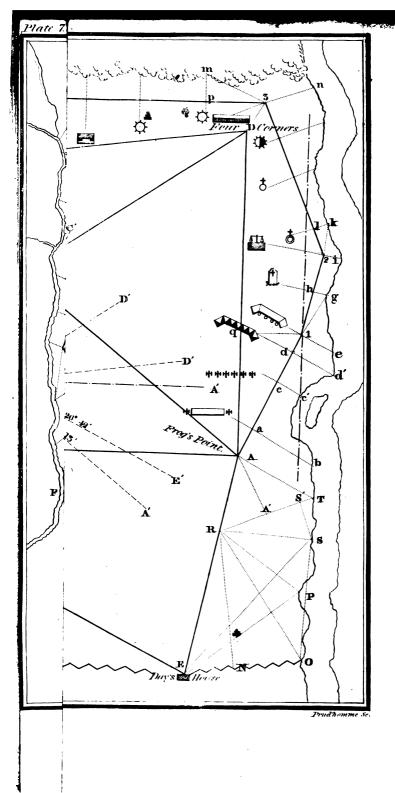


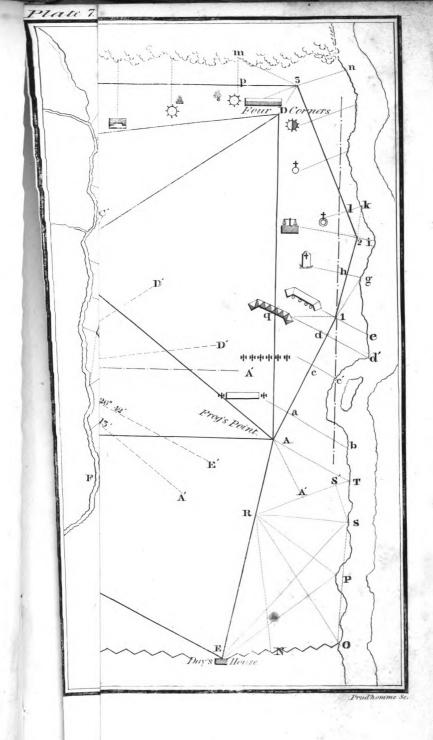


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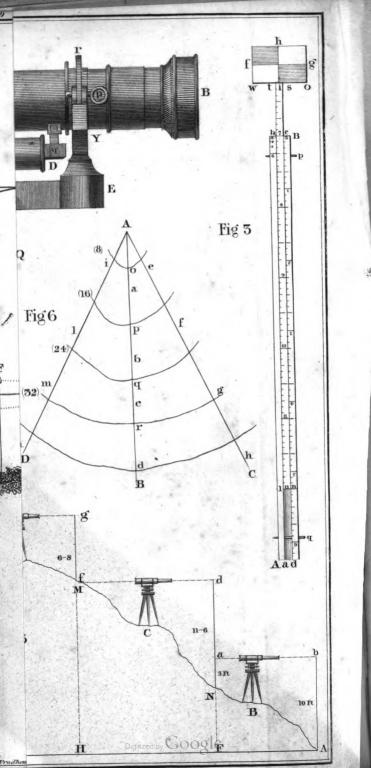
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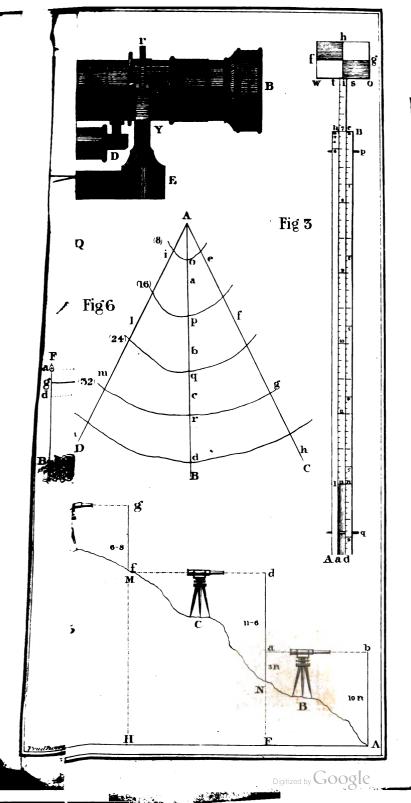


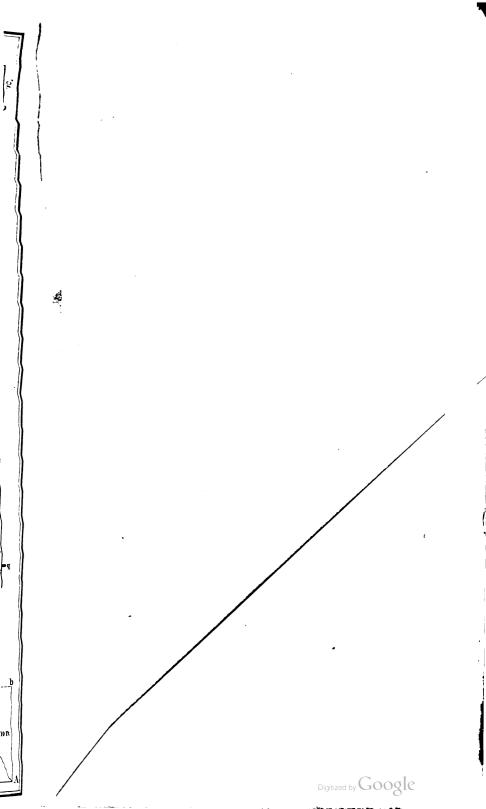












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