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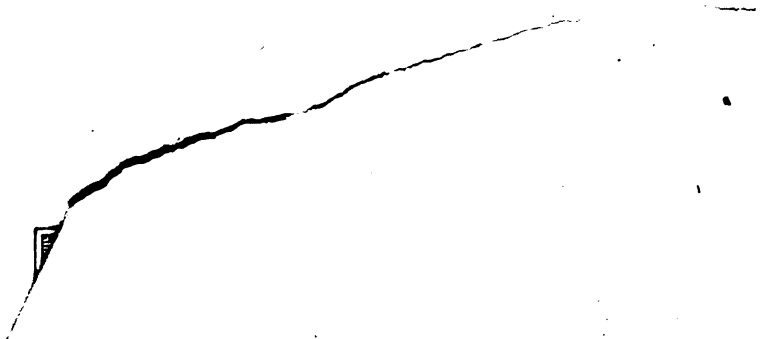
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ELEMENTS  
OF  
SURVEYING,  
AND  
NAVIGATION;

WITH A DESCRIPTION OF THE INSTRUMENTS AND  
THE NECESSARY TABLES.

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BY CHARLES DAVIES, LL.D.

AUTHOR OF FIRST LESSONS IN ARITHMETIC, FIRST LESSONS IN ALGEBRA, PRACTICAL  
GEOMETRY, ELEMENTS OF SURVEYING, ELEMENTS OF DESCRIPTIVE  
GEOMETRY, SHADES SHADOWS AND PERSPECTIVE, ANA-  
LYTICAL GEOMETRY, DIFFERENTIAL AND  
INTEGRAL CALCULUS.

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58 GOLD STREET, NEW YORK.

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The method was originated by Col. Jared Mansfield, whose great acquirements in science introduced him to the notice of President Jefferson, by whom he was appointed surveyor-general of the North-Western Territory.

May it be permitted to one of his pupils, and a graduate of the Military Academy, further to add, that at the organization of the institution in 1812, he was appointed Professor of Natural and Experimental Philosophy. This situation he filled for sixteen years, when he withdrew from the academy to spend the evening of his life in retirement and study. His pupils, who had listened to his instructions with delight, who honored his learning and wisdom, and had been brought near to him by his kind and simple manners, have placed his portrait in the public library, that the institution might possess an enduring memorial of one of its brightest ornaments and distinguished benefactors.

At the solicitation of several distinguished teachers here is added, in the present edition, an article on Plane Sailing, most of which has been taken, by permission of the author, from an excellent work on Trigonometry and its applications by Professor Charles Hackley.

HARTFORD,

*March, 1841.*

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# INTRODUCTION.

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## CHAPTER I.

### *Of Logarithms.*

1. The nature and properties of the logarithms in common use, will be readily understood, by considering attentively the different powers of the number 10. They are,

$$10^0 = 1$$

$$10^1 = 10$$

$$10^2 = 100$$

$$10^3 = 1000$$

$$10^4 = 10000$$

$$10^5 = 100000$$

$$\&c. \quad \&c.$$

It is plain, that the *indices* or *exponents* 0, 1, 2, 3, 4, 5, &c. form an arithmetical series of which the common difference is 1; and that the numbers 1, 10, 100, 1000, 10000, 100000, &c. form a geometrical series of which the common ratio is 10. The number 10, is called the *base* of the system of logarithms; and the *indices*, 0, 1, 2, 3, 4, 5, &c., are the logarithms of the numbers which are produced by raising 10 to the powers denoted by those indices.

2. Let  $a$  denote the base of the system of logarithms,  $m$  any exponent, and  $\mathcal{M}$  the corresponding number: we shall then have,

$$a^m = \mathcal{M}$$

in which  $m$  is the logarithm of  $\mathcal{M}$ .

If we take a second exponent  $n$ , and let  $\mathcal{N}$  denote the corresponding number, we shall have,

$$a^n = \mathcal{N}$$

in which  $n$  is the logarithm of  $\mathcal{N}$ .

If now, we multiply the first of these equations by the second, member by member, we have

$$a^m \times a^n = a^{m+n} = \mathcal{M} \times \mathcal{N};$$

but since  $a$  is the base of the system,  $m+n$  is the logarithm  $\mathcal{M} \times \mathcal{N}$ ; hence,

*The sum of the logarithms of any two numbers is equal to the logarithm of their product.*

Therefore, *the addition of logarithms corresponds to the multiplication of their numbers.*

3. If we divide the equations by each other, member by member, we have,

$$\frac{a^m}{a^n} = a^{m-n} = \frac{\mathcal{M}}{\mathcal{N}};$$

but since  $a$  is the base of the system,  $m-n$  is the logarithm of  $\frac{\mathcal{M}}{\mathcal{N}}$  hence:

*If one number be divided by another, the logarithm of the quotient will be equal to the logarithm of the dividend diminished by that of the divisor.*

Therefore, *the subtraction of logarithms corresponds to the division of their numbers.*

4. Let us examine further the equations

$$\begin{aligned} 10^0 &= 1 \\ 10^1 &= 10 \\ 10^2 &= 100 \\ 10^3 &= 1000 \\ &\&c. \quad \&c. \end{aligned}$$

It is plain that the logarithm of 1 is 0, and that the logarithms of all the numbers between 1 and 10, are greater than 0 and less than 1. They are generally expressed by decimal fractions: thus,

$$\log 2 = 0.301030. \quad \checkmark$$

The logarithms of all numbers greater than 10 and less than 100, are greater than 1 and less than 2, and are generally expressed by 1 and a decimal fraction: thus,

$$\log 50 = 1.698970.$$

The logarithms of numbers greater than 100 and less than 1000, are greater than 2 and less than 3, and are generally expressed by uniting 2 with a decimal fraction; thus,

$$\log 126 = 2.100371.$$

The part of the logarithm which stands on the left of the decimal point, is called the *characteristic* of the logarithm.

The characteristic is always *one less than the places of integer figures in the number whose logarithm is taken.*

Thus, in the first case, for numbers between 1 and 10, there is but one place of figures, and the characteristic is 0. For numbers between 10 and 100, there are two places of figures, and the characteristic is 1; and similarly for other numbers.

## TABLE OF LOGARITHMS.

5. A table of logarithms, is a table in which are written the logarithms of all numbers between 1 and some other given number. The logarithms of all numbers between 1 and 10,000 are written in the annexed table.

6. The first column on the left of each page of the table, is the column of numbers, and is designated by the letter  $\mathcal{N}$ ; the logarithms of these numbers are placed directly opposite them, and on the same horizontal line.

*To find, from the table, the logarithm of any number.*

7. If the number is less than 100, look on the first page of the table, along the column of numbers under  $\mathcal{N}$ , until the number is found: the number directly opposite, in the column designated log, is the logarithm sought. Thus,

$$\log 9 = 0.954243.$$

*When the number is greater than 100, and less than 10,000.*

8. Since the characteristic of every logarithm is less by unity than the places of integer figures in its corresponding number (Art. 4), its value is known by a simple inspection of the number whose logarithm is sought. Hence, it has not been deemed necessary to write the characteristics in the table.

To obtain the decimal part of the logarithm, find, in the column of numbers, the first three figures of the given number. Then, pass across the page, along a horizontal line, into the columns marked 0, 1, 2, 3, 4, 5, &c., until you come to the column which is designated by the fourth figure of the given number: at this place there are four figures of the required logarithm. To the four figures so found, two figures taken from the column marked 0, are to be prefixed. If the four figures thus found, stand opposite to a row of six figures in the column marked 0, the two figures from this column, which are to be prefixed, are the first two on the left hand: but if



the four figures found are opposite a line of only four figures, you are then to ascend the column till you come to the line of six figures; the two figures, at the left hand, are to be prefixed, and then the decimal part of the logarithm is obtained; to which prefix the characteristic, and you have the entire logarithm sought. For example,

$$\log 1122 = 3.049993$$

$$\log 8979 = 3.953228$$

In several of the columns, designated 0, 1, 2, 3, 4, &c., small dots are found. When the logarithm falls at such places, a cipher must be written for each of the dots, and the two figures, from the column 0, which are to be prefixed, are then found in the horizontal line directly below.

Thus, . . . .  $\log 2188 = 3.340047$

the two dots being changed into two ciphers, and the 34 to be taken from the column 0, is found in the horizontal line directly below.

The two figures from the column 0, must also be taken from the horizontal line below, *if any dots shall have been passed over*, in passing along the horizontal line: thus,

$$\log 3098 = 3.491081$$

the 49 from the column 0, being taken from the line 310.

*When the number exceeds 10,000, or is expressed by five or more figures.*

9. Consider all the figures, after the fourth from the left hand, as ciphers. Find from the table the logarithm of the first four figures, and to it prefix a characteristic less by unity than all the places of figures in the given number. Take from the last column on the right of the page, marked *D*, the number on the same horizontal line with the logarithm, and multiply this number by the figures that have been considered as ciphers: then cut off from the right hand as many places for decimals as there are figures in the multiplier, and add the product so obtained to the first logarithm, and the sum will be the logarithm sought.

Let it be required, for example, to find the logarithm of 672887.

$$\log 672800 = 5.827886$$

the characteristic being 5, since there are six places of figures. The corresponding number, in the column *D* is 65, which

being multiplied by 87, the figures regarded as ciphers, gives for a product 5655 ; then pointing off two decimal places, we obtain 56.55 for the number to be added.

$$\begin{array}{r} \text{Hence} \quad . \quad . \quad \log 672800 = 5.827886 \\ \text{Adding} \quad . \quad . \quad . \quad . \quad . \quad + 56.55 \\ \text{gives} \quad . \quad \log 672887 = 5.827943. \end{array}$$

In adding the proportional number, we omit the decimal part ; but when the decimal part exceeds 5 tenths, as in the case above, its value is nearer unity than 0 ; in which case, we augment by one, the figure on the left of the decimal point.

10. This method of finding the logarithms of numbers which exceed four places of figures, does not give the exact logarithm ; for, it supposes that the logarithms are proportional to their corresponding numbers, which is not rigorously true.

To explain the reason of the above method, let us take the logarithm of 672900, a number greater than 672800 by 100. We then have,

$$\begin{array}{r} \log 672900 = 5.827951 \\ \log 672800 = 5.827886 \end{array}$$

Difference of numbers      100                  65 = difference of logarithms.

Then,                                  100 : 65 :: 87 : 56.55

In this proportion the first term 100 is the difference between two numbers, one of which is greater and the other less than the given number ; and the second term 65 is the difference of their logarithms, or tabular difference.

The third term 87 is the difference between the given number and the less number 672800 ; and hence the fourth term 56.55 is the difference of their logarithms. This difference therefore, added to the logarithm of the less number, will give that of the greater, nearly.

Had there been three figures of the given number treated as ciphers, the first term would have been 1000 ; had there been four, it would have been 10000, &c. Therefore, the reason of the rule, for the use of the column of differences, is manifest.

*To find the logarithm of a decimal number.*

11. If the given number is composed of a whole number

and a decimal, such as 36.78, it may be put under the form  $\frac{3678}{100}$ . But since a fraction is equal to the quotient obtained by dividing the numerator by the denominator, its logarithm will be equal to the logarithm of the numerator minus the logarithm of the denominator. Therefore,

$$\log \frac{3678}{100} = \log 3678 - \log 100 = 3.565612 - 2 = 1.565612$$

from which we see, that a mixed number may be treated as though it were entire, except in fixing the value of the characteristic, which is always *one less than the number of the integer figures*.

12. The logarithm of a decimal fraction is also readily found. For,

$$\log 0.8 = \log \frac{8}{10} = \log 8 - 1 = -1 + \log 8. \quad \text{But,}$$

$$\log 8 = 0.903090$$

which is positive and less than 1. Therefore,

$$\log 0.8 = -1 + 0.903090 = -1.903090$$

in which, however, *the minus sign belongs only to the characteristic*. Hence it appears, that the logarithm of tenths is the same as the logarithm of the corresponding whole number, excepting, that the characteristic instead of being 0, is  $-1$ .

If the fraction were of the form 0.06 it might be written  $\frac{06}{100}$ ; taking the logarithms, we have,

$$\log \frac{06}{100} = \log 06 - 2 = -2 + \log 06 = -2.778151$$

in which the minus sign, as before, belongs only to the characteristic. If the decimal were 0.006 its logarithm would be the same as before, excepting the characteristic, which would be  $-3$ . It is, indeed, evident, that the negative characteristic will always be one greater than the number of ciphers between the decimal point and the first significant figure. Therefore, the logarithm of a decimal fraction is found, *by considering it as a whole number, and then prefixing to the decimal part of its logarithm a negative characteristic greater by unity than the number of ciphers between the decimal point and the first significant figure*.

That we may not, for a moment, suppose the negative sign to belong to the whole logarithm, when in fact it belongs only to the characteristic, we place the sign above the characteristic, thus,

$$\log 0.8 = \bar{1}.903090, \text{ and } \log 0.06 = \bar{2}.778151.$$

## EXAMPLES.

log 2756	.	.	.	is	.	.	.	3.440279
log 3270	.	.	.	is	.	.	.	3.514548
log 287.965	.	.	.	is	.	.	.	2.459340
log 1.004	.	.	.	is	.	.	.	0.001734
log 0.002	.	.	.	is	.	.	.	$\bar{3}$ .301030
log 0.000678	.	.	.	is	.	.	.	$\bar{4}$ .831230

*To find in the table, the number answering to a given logarithm.*

13. Search in the columns of logarithms for the decimal part of the given logarithm, and if it can be exactly found, set down the corresponding number. Then, if the characteristic of the given logarithm is positive, point off from the left of the number found, one more place for whole numbers than there are units in the characteristic of the given logarithm, and treat the figures to the right as decimals.

If the characteristic of the given logarithm is 0, there will be one place of whole numbers; if it is  $-1$ , the number will be entirely decimal; if it is  $-2$ , there will be one cipher between the decimal point and the first significant figure; if it is  $-3$ , there will be two, &c

The number whose logarithm is 1.492481, is found at page 5, and is 31.08.

But when the decimal part of the logarithm cannot be exactly found in the table, take the number answering to the nearest less logarithm; take also from the table the corresponding difference in the column *D*. Then, subtract this less logarithm from the given logarithm, and having annexed any number of ciphers to the remainder, divide it by the difference taken from the column *D*, and annex the quotient to the number answering to the less logarithm: this gives the required number, nearly. This rule, like that for finding the logarithm of a number when the places of figures exceed four, supposes the numbers to be proportional to their corresponding logarithms.

1. Find the number answering to the logarithm 1.532708.

Given logarithm is . . . 1.532708

Next less tabular logarithm is 1.532627

Their difference is . . . 81

2

The number corresponding to the tabular logarithm is 34.09  
 And the tabular difference is . . . . 128 :  
 and, 128)81.00(63

The 63 being annexed to the tabular number 34.09 gives  
 34.0963 for the number answering to the logarithm 1.532708.

2. Required the number answering to the logarithm  
 3.233568.

The given logarithm is	. . . . .	3.233568
Next less tabular logarithm of 1712 is	. . . . .	<u>3.233504</u>
Their difference is	. . . . .	<u>64</u>
Tabular difference	. 253)64.00(25	

Hence the number sought, is 1712.25, marking four places  
 for integers since the characteristic is 3.

#### MULTIPLICATION BY LOGARITHMS.

14. When it is required to multiply numbers by means of  
 their logarithms, we first find from the table the logarithms  
 of the numbers to be multiplied; we next add these loga-  
 rithms together, and their sum is the logarithm of the pro-  
 duct of the numbers (Art. 2).

The term *sum* is to be understood in its algebraic sense;  
 therefore, if any of the logarithms have negative charac-  
 teristics, the difference between their sum and that of the  
 positive characteristics, is to be taken, and the sign of the  
 greater prefixed.

#### EXAMPLES.

1. Multiply 23.14 by 5.062.

$\log 23.14 = 1.364363$
$\log 5.062 = 0.704322.$
Product 117.1347 . . . . . <u>2.068685</u>

2. Multiply 3.902, 597.16 and 0.0314728 together.

$\log 3.902 = 0.591287$
$\log 597.16 = 2.776091$
$\log 0.0314728 = \bar{2}.497936$
Product 73.3354 . . . . . <u>1.865314</u>

Here the  $\bar{2}$  cancels the  $+2$ , and the 1 carried from the  
 decimal part is set down.

3. Multiply 3.586, 2.1046, 0.8372, and 0.0294, together.

$$\log 3.586 = 0.554610$$

$$\log 2.1046 = 0.323170$$

$$\log 0.8372 = \bar{1}.922829$$

$$\log 0.0294 = \bar{2}.468347$$

$$\text{Product } 0.1857615 \quad . \quad . \quad \underline{\underline{1.268956.}}$$

In this example the 2, carried from the decimal part, cancels  $\bar{2}$ , and there remains  $\bar{1}$  to be set down.

#### DIVISION OF NUMBERS BY LOGARITHMS.

15. When it is required to divide numbers by means of their logarithms, we have only to recollect, that the subtraction of logarithms corresponds to the division of their numbers (Art. 3). Hence, if we find the logarithm of the dividend, and from it subtract the logarithm of the divisor, the remainder will be the logarithm of the quotient.

This additional caution may be added. The difference of the logarithms, as here used, means the *algebraic difference*; so that, if the logarithm of the divisor have a negative characteristic its sign must be changed to positive, after diminishing it by the unit, if any, carried in the subtraction from the decimal part of the logarithm. Or, if the characteristic of the logarithm of the dividend is negative, it must be treated as a negative number.

#### EXAMPLES.

1. To divide 24163 by 4567.

$$\log 24163 = 4.383151$$

$$\log 4567 = 3.659631$$

$$\text{Quotient } 5.29078 \quad . \quad . \quad \underline{\underline{0.723520.}}$$

2. To divide 0.6314 by .007241

$$\log 0.6314 = \bar{2}.800305$$

$$\log 0.007241 = \bar{3}.859799$$

$$\text{Quotient } . \quad . \quad 8.7198 \quad . \quad . \quad \underline{\underline{0.940506}}$$

Here, 1 carried from the decimal part to the  $\bar{3}$  changes it to  $\bar{2}$ , which being taken from  $\bar{2}$ , leaves 0 for the characteristic.

3. To divide 37.149 by 523.76

$$\log 37.149 = 1.569947$$

$$\log 523.76 = 2.719133$$

$$\text{Quotient } . \quad 0.0709274 \quad . \quad . \quad \underline{\underline{2.850814}}$$

4. To divide 0.7438 by 12.9476

$$\log 0.7438 = \bar{1}.871456$$

$$\log 12.9476 = 1.112189$$

$$\text{Quotient } 0.057447 \quad . \quad . \quad \underline{2.759267}$$

Here, the 1 taken from  $\bar{1}$ , gives  $\bar{2}$  for a result, as set down.

#### ARITHMETICAL COMPLEMENT.

16. The *Arithmetical complement* of a logarithm is the number which remains after subtracting this logarithm from 10.

$$\text{Thus} \quad . \quad . \quad 10 - 9.274687 = 0.725313.$$

Hence, 0.725313 is the arithmetical complement of 9.274687.

17 We will now show that, *the difference between two logarithms is truly found, by adding to the first logarithm the arithmetical complement of the logarithm to be subtracted, and then diminishing the sum by 10.*

Let  $a$  = the first logarithm

$b$  = the logarithm to be subtracted

and  $c = 10 - b$  = the arithmetical complement of  $b$ .

Now the difference between the two logarithms will be expressed by  $a - b$ .

But, from the equation  $c = 10 - b$ , we have

$$c - 10 = -b$$

hence, if we place for  $-b$  its value, we shall have

$$a - b = a + c - 10$$

which agrees with the enunciation.

When we wish the arithmetical complement of a logarithm, we may write it directly from the table, *by subtracting the left hand figure from 9, then proceeding to the right, subtract each figure from 9 till we reach the last significant figure, which must be taken from 10: this will be the same as taking the logarithm from 10.*

#### EXAMPLES.

1. From 3.274107 take 2.104729.

*By common method.*

$$3.274107$$

$$2.104729$$

$$\text{Diff. } \underline{1.169378}$$

subtracting 10

*By arith. comp.*

$$3.274107$$

$$7.895271$$

$$\text{Sum } \underline{1.169378} \text{ after}$$

Hence, to perform division by means of the arithmetical complement we have the following

## RULE.

*To the logarithm of the dividend add the arithmetical complement of the logarithm of the divisor : the sum, after subtracting 10, will be the logarithm of the quotient.*

## EXAMPLES.

1. Divide 327.5 by 22.07.

log 327.5	. . .	2.515211
log 22.07	ar. comp.	8.656198
Quotient . . .	14.839 . . .	1.171409

2. Divide 0.7438 by 12.9476.

log 0.7438	. . .	1.871456
log 12.9476	ar. comp.	8.887811
Quotient . . .	0.057447 . . .	2.759267

In this example, the sum of the characteristics is 8, from which, taking 10, the remainder is 2.

3. Divide 37.149 by 523.76

log 37.149	. . .	1.569947
log 523.76	ar. comp.	7.280867
Quotient . . .	0.0709273 . . .	2.850814

## CHAPTER II.

*Definitions.*

1. **GEOMETRY** is the science which has for its object the measurement of extension.

Extension has three dimensions, length, breadth, height, or thickness.

2 A *line* is length without breadth, or thickness.

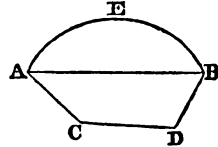
The extremities of a line are called *points* : a point, therefore, has neither length, breadth, nor thickness, but position only.



3. A *straight line* is the shortest distance from one point to another.

4. Every line which is not straight, or composed of straight lines, is a *curved line*.

Thus,  $AB$  is a straight line;  $ACDB$  is a *broken* line, or one composed of straight lines; and  $AEB$  is a curved line.



The word *line*, when used alone, will designate a straight line; and the word *curve*, a curved line.

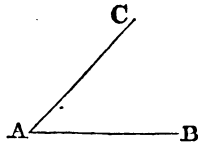
5. A *surface* is that which has length and breadth, without height or thickness.

6. A *plane* is a surface, in which, if two points be assumed at pleasure, and connected by a straight line, that line will lie wholly in the surface.

7. Every surface, which is not a plane surface, or composed of plane surfaces, is a *curved surface*.

8. A *solid* or *body* is that which has length, breadth, and thickness; and therefore combines the three dimensions of extension.

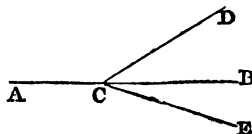
9. When two straight lines,  $AB, AC$ , meet each other, their inclination or opening is called an *angle*, which is greater or less as the lines are more or less inclined or opened. The point of intersection  $A$  is the vertex of the angle, and the lines  $AB, AC$ , are its sides.



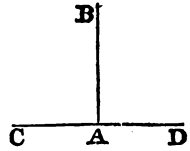
The angle is sometimes designed simply by the letter at the vertex  $A$ ; sometimes by the three letters  $BAC$ , or  $CAB$ , the letter at the vertex being always placed in the middle.

Angles, like all other quantities, are susceptible of addition, subtraction, multiplication, and division.

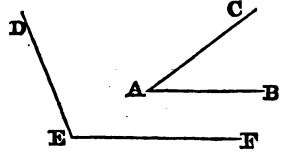
Thus the angle  $DCE$  is the sum of the two angles  $DCB, BCE$ ; and the angle  $DCB$  is the difference of the two angles  $DCE, BCE$ .



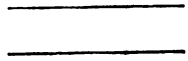
10. When a straight line AB meets another straight line CD, so as to make the adjacent angles BAC, BAD, equal to each other, each of these angles is called a *right angle*; and the line AB is said to be *perpendicular* to CD.



11. Every angle BAC, less than a right angle, is an *acute angle*; and every angle DEF, greater than a right angle, is an *obtuse angle*.

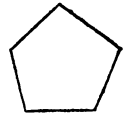


12. Two lines are said to be *parallel*, when being situated in the same plane, they cannot meet, how far soever, either way, both of them be produced



13. A *plane figure* is a plane terminated on all sides by lines, either straight or curved.

If the lines are straight, the space they enclose is called a *rectilineal figure*, or *polygon*, and the lines themselves, taken together, form the contour, or *perimeter* of the polygon.

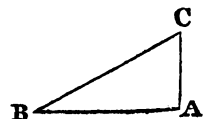


14. The polygon of three sides, the simplest of all, is called a *triangle*; that of four sides, a *quadrilateral*; that of five, a *pentagon*; that of six, a *hexagon*; that of seven, a *heptagon*; that of eight, an *octagon*; that of nine a *nonagon*; that of ten, a *decagon*; that of twelve, a *dodecagon*.



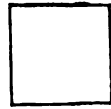
15. An *equilateral* triangle is one which has its three sides equal; an *isosceles* triangle, one which has two of its sides equal; a *scalene* triangle, one which has its three sides unequal.

16. A right-angled triangle is one which has a right angle. The side opposite the right angle is called the *hypotenuse*. Thus, in the triangle ABC, right-angled at A, the side BC is the hypotenuse.



17. Among the quadrilaterals, we distinguish :

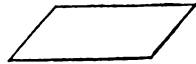
The *square*, which has its sides equal, and its angles right angles.



The *rectangle*, which has its angles right angles, without having its sides equal.



The *parallelogram*, or *rhomboid*, which has its opposite sides parallel.



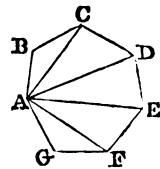
The *rhombus*, or *lozenge*, which has its sides equal, without having its angles right angles.



And lastly, the *trapezoid*, only two of whose sides are parallel.



18. A *diagonal* is a line which joins the vertices of two angles not adjacent to each other. Thus, AF, AE, AD, AC, are diagonals.



19. An *axiom* is a self-evident proposition.

20. A *theorem* is a truth, which becomes evident by means of a train of reasoning called a *demonstration*.

21. A *problem* is a question proposed, which requires a *solution*.

22. A *lemma* is a subsidiary truth, employed for the demonstration of a theorem, or the solution of a problem.

23. The common name, *proposition*, is applied indifferently, to theorems, problems, and lemmas.

24. A *corollary* is an obvious consequence, deduced from one or several propositions.

25. A *scholium* is a remark on one or several preceding propositions, which tends to point out their connexion, their use, their restriction, or their extension.

26. A *hypothesis* is a supposition, made either in the enunciation of a proposition, or in the course of a demonstration.

*Axioms.*

1. Things which are equal to the same thing, are equal to each other.

2. If equals be added to equals, the wholes will be equal.

3. If equals be taken from equals, the remainders will be equal.

4. If equals be added to unequals, the wholes will be unequal.

5. If equals be taken from unequals, the remainders will be unequal.

6. Things which are double of the same thing, are equal to each other.

7. Things which are halves of the same thing, are equal to each other.

8. The whole is greater than any of its parts.

9. The whole is equal to the sum of all its parts.

10. All right angles are equal to each other.

11. From one point to another, only one straight line can be drawn.

12. Through the same point, only one straight line can be drawn which shall be parallel to a given line.

13. Magnitudes, which being applied to each other, coincide throughout their whole extent, are equal.

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### CHAPTER III.

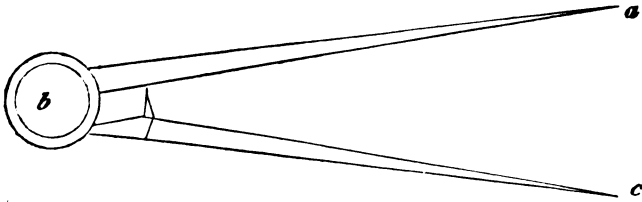
*Description of the Instruments used for Delineating or Drawing Lines and Angles on paper. Construction of Problems.*

18. Drawings, or delineations on paper, are the copies of things which they are intended to represent.

In order that these copies may be exact, their different parts must bear the same proportion to each other that exists between the corresponding parts of the things themselves.

To enable us to delineate lines and angles correctly, upon paper, certain instruments are necessary; these we will now describe.

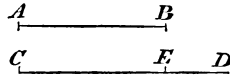
## DIVIDERS.



19. The dividers is the most simple and useful of the instruments used for drawing. It consists of two legs  $ba$ ,  $bc$ , which may be easily turned around a joint at  $b$ .

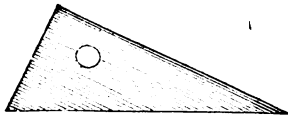
One of the principal uses of this instrument is to lay off on a line, a distance equal to a given line.

For example, to lay off on  $CD$  a distance equal to  $AB$ .



For this purpose, place the forefinger  $C$  on the joint of the dividers, and set one foot at  $A$ : then extend, with the thumb and other fingers, the other leg of the dividers, until its foot reaches the point  $B$ . Then raise the dividers, place one foot at  $C$ , and mark with the other the distance  $CE$ : this will evidently be equal to  $AB$ .

## RULER AND TRIANGLE.



20. A Ruler of a convenient size, is about twenty inches in length, two inches wide, and a fifth of an inch in thickness. It should be made of a hard material, perfectly straight and smooth.

The hypotenuse of the right-angled triangle, which is used in connexion with it, should be about ten inches in

length, and it is most convenient to have one of the sides considerably longer than the other. We can solve, with the ruler and triangle, the two following problems.

**I. To draw through a given point a line which shall be parallel to a given line.**

Let  $C$  be the given point, and  $AB$  the given line.

Place the hypotenuse of the triangle against the edge of the ruler, and then place the ruler and triangle on the paper, so that one of the sides of the triangle shall coincide exactly with  $AB$ : the triangle being below the line.

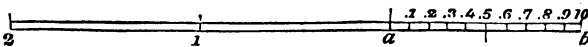
Then placing the thumb and fingers of the left hand firmly on the ruler, slide the triangle with the other hand along the ruler until the side which coincided with  $AB$  reaches the point  $C$ . Leaving the thumb of the left hand on the ruler, extend the fingers upon the triangle and hold it firmly, and with the right hand, mark with a pen or pencil, a line through  $C$ : this line will be parallel to  $AB$ .

**II. To draw through a given point a line which shall be perpendicular to a given line.**

Let  $AB$  be the given line, and  $D$  the given point.

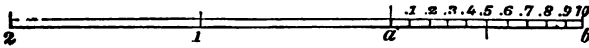
Place the hypotenuse of the triangle against the edge of the ruler, as before. Then place the ruler and triangle so that one of the sides of the triangle shall coincide exactly with the line  $AB$ . Then slide the triangle along the ruler until the other side reaches the point  $D$ : draw through  $D$  a right line, and it will be perpendicular to  $AB$ .

#### SCALE OF EQUAL PARTS.



**21.** A scale of equal parts is formed by dividing a line of a given length into equal portions.

If, for example, the line  $ab$  of a given length, say one inch, be divided into any number of equal parts, as 10, the scale thus formed, is called a scale of ten parts to the inch. The line

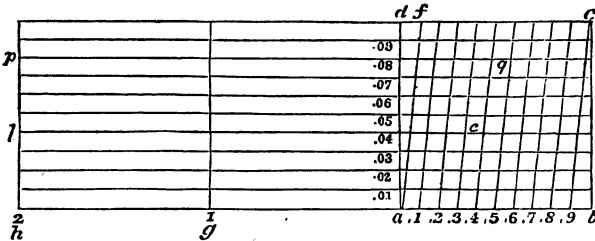


$ab$ , which is divided, is called the *unit of the scale*. This unit is laid off several times on the left of the divided line, and the points marked, 1, 2, 3, &c.

The unit of scales of equal parts, is, in general, either an inch, or an exact part of an inch. If, for example,  $ab$  the unit of the scale, were half an inch, the scale would be one of 10 parts to half an inch, or of 20 parts to the inch.

If it were required to take from the scale a line equal to two inches and six-tenths, place one foot of the dividers at 2 on the left, and extend the other to .6, which marks the sixth of the small divisions: the dividers will then embrace the required distance.

DIAGONAL SCALE OF EQUAL PARTS.



22. This scale is thus constructed. Take  $ab$  for the unit of the scale, which may be one inch,  $\frac{1}{2}$ ,  $\frac{1}{4}$  or  $\frac{3}{4}$  of an inch, in length. On  $ab$  describe the square  $abcd$ . Divide the sides  $ab$  and  $dc$  each into ten equal parts. Draw  $af$  and the other nine parallels as in the figure.

Produce  $ba$  to the left, and lay off the unit of the scale any convenient number of times, and mark the point 1, 2, 3, &c. Then, divide the line  $ad$  into ten equal parts, and through the points of division draw parallels to  $ab$  as in the figure.

Now, the small divisions of the line  $ab$  are each one-tenth (.1) of  $ab$ ; they are therefore .1 of  $ad$ , or .1 of  $ag$  or  $gh$ .

If we consider the triangle  $adf$ , the base  $df$  is one-tenth of  $ad$  the unit of the scale. Since the distance from  $a$  to the first horizontal line above  $ab$ , is one-tenth of the distance  $ad$ , it follows that the distance measured on that line between  $ad$

and  $af$  is one-tenth of  $df$ : but since one-tenth of a tenth is a hundredth, it follows that this distance is one hundredth (.01) of the unit of the scale. A like distance measured on the second line will be two hundredths (.02) of the unit of the scale; on the third, .03; on the fourth, .04, &c.

If it were required to take, in the dividers, the unit of the scale, and any number of tenths, place one foot of the dividers at 1, and extend the other to that figure between  $a$  and  $b$  which designates the tenths. If two or more units are required, the dividers must be placed on a point of division farther to the left.

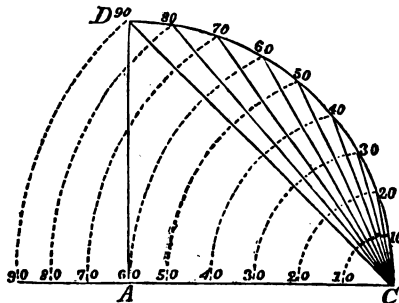
When units, tenths, and hundredths, are required, place one foot of the dividers where the vertical line through the point which designates the units, intersects the line which designates the hundredths: then, extend the dividers to that line between  $ad$  and  $bc$  which designates the tenths: the distance so determined will be the one required.

For example, to take off the distance 2.34, we place one foot of the dividers at  $l$ , and extend the other to  $e$ : and to take off the distance 2.58, we place one foot of the dividers at  $p$  and extend the other to  $q$ .

REMARK I. If a line is so long that the whole of it cannot be taken from the scale, it must be divided, and the parts of it taken from the scale in succession.

REMARK II. If a line be given upon the paper, its length can be found by taking it in the dividers and applying it to the scale.

## SCALE OF CHORDS.



23. If, with any radius, as  $AC$ , we describe the quadrant  $CD$ , and then divide it into 90 equal parts, each part is called a degree.



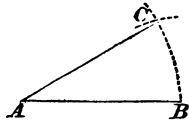
Through  $C$ , and each point of division, let a chord be drawn, and let the lengths of these chords be accurately laid off on a scale: such a scale is called a *scale of chords*. In the figure, the chords are drawn for every ten degrees.

The scale of chords being once constructed, the radius of the circle from which the chords were obtained, is known; for, the chord marked 60 is always equal to the radius of the circle. A scale of chords is generally laid down on the scales which belong to cases of mathematical instruments, and is marked CHO.

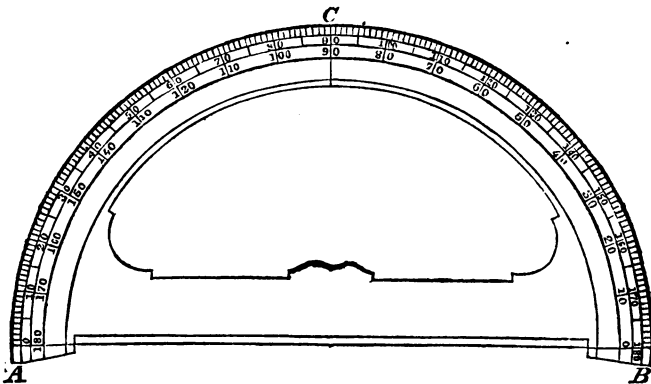
*To lay off, at a given point of a line, with the scale of chords, an angle equal to a given angle.*

Let  $AB$  be the line, and  $A$  the given point.

Take from the scale the chord of 60 degrees, and with this radius and the point  $A$  as a centre, describe the arc  $BC$ . Then take from the scale the chord of the given angle, say 30 degrees, and with this line as a radius, and  $B$  as a centre, describe an arc cutting  $BC$  in  $C$ . Through  $A$  and  $C$  draw the line  $AC$ , and  $BAC$  will be the required angle.



#### SEMICIRCULAR PROTRACTOR.



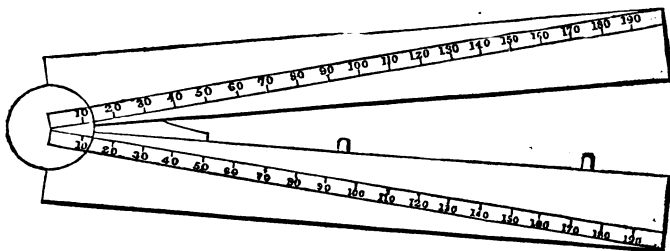
24. This instrument is used to lay down, or protract angles. It may also be used to measure angles included between lines already drawn upon paper.

It consists of a brass semicircle  $ABC$  divided to half degrees. The degrees are numbered from 0 to 180, both ways; that is, from  $A$  to  $B$  and from  $B$  to  $A$ . The divisions, in the figure, are only made to degrees. There is a small notch at the middle of the diameter  $AB$ , which indicates the centre of the protractor.

*To lay off an angle with a Protractor.*

Place the diameter  $AB$  on the line, so that the centre shall fall on the angular point. Then count the degrees contained in the given angle from  $A$  towards  $B$ , or from  $B$  towards  $A$  and mark the extremity of the arc with a pin. Remove the protractor, and draw a line through the point so marked and the angular point: this line will make with the given line the required angle.

**SECTORAL SCALE OF EQUAL PARTS.**



25. The sector is an instrument generally made of ivory or brass. It consists of two arms, or sides, which open by turning round a joint at their common extremity.

There are several scales laid down on the sector: those, however, which are chiefly used in drawing lines and angles, are, the scale of chords already described, and the scale of equal parts now to be explained.

On each arm of the sector, there is a diagonal line that passes through the point about which the arms turn: these diagonal lines are divided into equal parts.

On the sectors which belong to the cases of English instruments, the diagonal lines are designated by the letter  $L$ , and numbered from the centre of the sector, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, to the two extremities. On the sectors which belong

to cases of French instruments, they are designated, "**Les parties egales,**" and numbered, 10, 20, 30, 40, &c. to 200. On the English sectors there are 20 equal divisions between either two of the lines numbered 1, 2, 3, &c., so that, there are 200 equal parts on the scale.

The advantage of the sectoral scale of equal parts, is this—

When it is proposed to draw a line upon paper, on such a scale that any number of parts of the line, 40 for example, shall be represented by one inch on the paper, or by any part of an inch, take the inch, or part of the inch from the scale of inches on the sector: then, placing one foot of the dividers at 40 on one arm of the sector, open the sector until the other foot reaches to the corresponding number on the other arm: then lay the sector on the table without varying the angle.

Now, if we regard the lines on the sector as the sides of a triangle, of which the line 40 measured across, is the base, it is plain, that if any other line be likewise measured across the angle of the sector, the bases of the triangles, so formed, will be proportional to their sides. Therefore, if we extend the dividers from 50 to 50, this distance will represent a line of 50, to the given scale: and similarly for other lines.

Let it now be required to lay down a line of sixty-seven feet, to a scale of twenty feet to the inch.

Take one inch from the scale of inches: then place one foot of the dividers at the twentieth division, and open the sector until the dividers will just reach the twentieth division on the other arm: the sector is then set to the proper angle; after which the required distance to be laid down on the paper, is found, by extending the dividers from the sixty-seventh division on one arm, to the sixty-seventh division on the other.

#### GUNTERS' SCALE.

26. This is a scale of two feet in length, on the faces of which a variety of scales are marked. The face on which the divisions of inches are made, contains, however, all the scales necessary for laying down lines and angles. These are, the scale of equal parts, the diagonal scale of equal parts, and the scale of chords, all of which have been described.

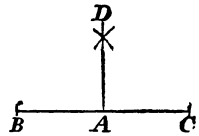
SOLUTION OF PROBLEMS REQUIRING THE USE OF THE INSTRUMENTS THAT HAVE BEEN DESCRIBED.

PROBLEM I.

*At a given point in a given straight line, to erect a perpendicular to the line.*

27. Let  $A$  be the given point, and  $BC$  the given line.

From  $A$  lay off any two distances  $AB$  and  $AC$  equal to each other. Then, from the points  $B$  and  $C$ , as centres, with a radius greater than  $BA$ , describe two arcs intersecting each other in  $D$ : draw  $AD$ , and it will be the perpendicular required.

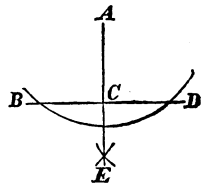


PROBLEM II.

*From a given point without a straight line, to let fall a perpendicular on the line.*

28. Let  $A$  be the given point and  $BD$  the given line.

From the point  $A$  as a centre, with a radius sufficiently great, describe an arc cutting the line  $BD$  in the two points  $B$  and  $D$ : then mark a point  $E$ , equally distant from the points  $B$  and  $D$ , and draw  $AE$ :  $AE$  will be the perpendicular required.

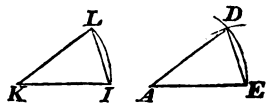


PROBLEM III.

*At a point, in a given line, to make an angle equal to a given angle.*

29. Let  $A$  be the given point,  $AE$  the given line, and  $IKL$  the given angle.

From the vertex  $K$ , as a centre, with any radius, describe the arc  $IL$ , terminating in the two sides of the angle. From the point  $A$  as a centre, with a distance  $AE$  equal to  $KI$ , describe the arc  $ED$ ; then take the chord  $LI$ , with which, from the point  $E$  as a centre, describe an arc cutting the indefinite arc  $DE$ , in  $D$ ; draw  $AD$ , and the angle  $EAD$  will be equal to the given angle  $K$ .

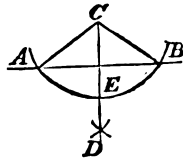


## PROBLEM IV.

*To divide a given angle, or a given arc, into two equal parts.*

30. Let  $C$  be the given angle, and  $AEB$  the arc which measures it.

From the points  $A$  and  $B$  as centres, describe with the same radius two arcs cutting each other in  $D$ : through  $D$  and the centre  $C$  draw  $CD$ : the angle  $ACE$  will be equal to the angle  $ECB$ , and the arc  $AE$  to the arc  $EB$ .

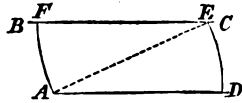


## PROBLEM V.

*Through a given point to draw a parallel to a given line.*

31. Let  $A$  be the given point, and  $BC$  the given line.

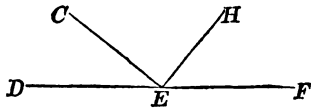
From  $A$  as a centre, with a radius greater than the shortest distance from  $A$  to  $BC$ , describe the indefinite arc  $ED$ : from the point  $E$  as a centre, with the same radius, describe the arc  $AF$ ; make  $ED=AF$ , and draw  $AD$ : then will  $AD$  be the parallel required.



## PROBLEM VI.

*Two angles of a triangle being given, to find the third.*

32. Draw the indefinite line  $DEF$ . At the point  $E$ , make the angle  $DEC$  equal to one of the given angles, and the angle  $CEH$  equal to the other: the remaining angle  $HEF$  will be the third angle required.



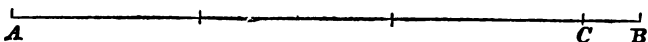
## PROBLEM VII.

*To lay down, on paper, a line of a given length, so that any number of its parts shall correspond to the unit of the scale.*

33. Suppose that the given line were 75 feet in length, and it were required to draw it on paper, on a scale of 25 feet to the inch.

The length of the line 75 feet, being divided by 25, will give 3, the number of inches which will represent the line on paper

Therefore, draw the indefinite line  $AB$ , on which lay off a



distance  $AC$  equal to 3 inches:  $AC$  will represent the given line of 75 feet drawn to the required scale.

REMARK I. This problem explains the manner of laying down a line upon paper, in such a manner that a given number of parts shall correspond to the unit of the scale, whether that unit be an inch or any part of an inch.

When the length of the line to be laid down is given, and it has been determined how many parts of it are to be represented on the paper by a distance equal to the unit of the scale, we find the length which is to be taken from the scale by the following

#### RULE.

*Divide the length of the line by the number of parts which is to be represented by the unit of the scale: the quotient will show the number of parts which is to be taken from the scale.*

#### EXAMPLES.

1. If a line of 640 feet in length is to be laid down on paper, on a scale of 40 feet to the inch; what length must be taken from the scale?

40)640(16 inches.

2. If a line of 357 feet is to be laid down on a scale of 68 feet to the unit of the scale, (which we will suppose half an inch), how many parts are to be taken?

*Ans.*  $\left\{ \begin{array}{l} 5.25, \text{ parts, or} \\ 2.625 \text{ inches.} \end{array} \right.$

REMARK II. When the length of a line is given on the paper, and it is required to find the true length of the line which it represents, take the line in the dividers and apply it to the scale, and note the number of units, and parts of an

unit to which it is equal. Then multiply this number by the number of parts which the unit of the scale represents, and the product will be the length of the line.

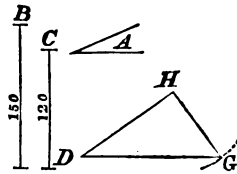
For example, suppose the length of a line drawn on the paper was found to be 3.56 inches, the scale being 40 feet to the inch : then,

$$3.55 \times 40 = 142 \text{ feet, the length of the line.}$$

**PROBLEM VIII.**

*Having given two sides and the included angle of a triangle, to describe the triangle.*

34. Let the line  $B=150$  feet, and  $C=120$  feet, be the given sides ; and  $A=30$  degrees, the given angle : to describe the triangle on a scale of 200 feet to the inch.

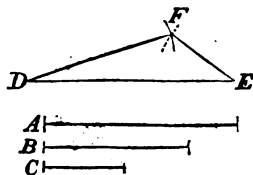


Draw the indefinite line  $DG$ , and at the point  $D$ , make the angle  $GDH$  equal to 30 degrees ; then lay off  $DG$  equal to 150, equal to three quarters of an inch, and  $DH$  equal to 120, equal to six tenths of an inch, and draw  $GH$  :  $DGH$  will be the required triangle.

**PROBLEM IX.**

*The three sides of a triangle being given, to describe the triangle.*

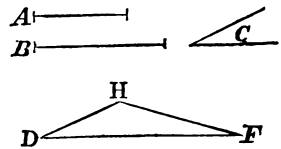
35. Let  $A, B$  and  $C$ , be the sides. Draw  $DE$  equal to the side  $A$ . From the point  $D$  as a centre, with a radius equal to the second side  $B$ , describe an arc : from  $E$  as a centre, with a radius equal to the third side  $C$ , describe another arc intersecting the former in  $F$  ; draw  $DF$  and  $EF$ , and  $DEF$  will be the triangle required.



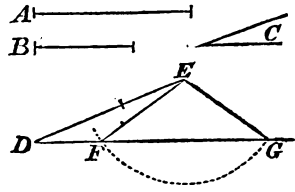
PROBLEM X.

*Having given two sides of a triangle and an angle opposite one of them, to describe the triangle.*

36. Let  $A$  and  $B$  be the given sides, and  $C$  the given angle which we will suppose is opposite the side  $B$ . Draw the indefinite line  $DF$  and make the angle  $FDH$  equal to the angle  $C$ : take  $DH=A$ , from the point  $H$ , as a centre, with a radius equal to the other given side  $B$ , describe an arc cutting  $DF$  in  $F$ ; draw  $HF$ : then will  $DHF$  be the required triangle.



If the angle  $C$  is acute, and the side  $B$  less than  $A$ , then the arc described from the centre  $E$  with the radius  $EF = B$  will cut the side  $DF$  in two points,  $F$  and  $G$ , lying on the same side of  $D$ : hence there will be two triangles,  $DEF$ , and  $DEG$ , either of which will satisfy all the conditions of the problem.

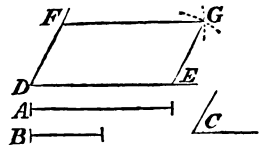


PROBLEM XI.

*The adjacent sides of a parallelogram, with the angle which they contain, being given, to describe the parallelogram.*

37. Let  $A$  and  $B$  be the given sides, and  $C$  the given angle.

Draw the line  $DE=A$ ; at the point  $D$ , make the angle  $EDF=C$ ; take  $DF=B$ : describe two arcs, the one from  $F$ , as a centre, with a radius  $FG=DE$ , the other from  $E$ , as a centre, with a radius  $EG=DF$ ; through the point  $G$ , where these arcs intersect each other, draw  $FG$ ,  $EG$ ;  $DEGF$  will be the parallelogram required.

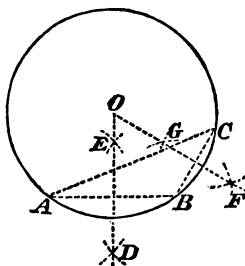




## PROBLEM XII.

*To find the centre of a given circle or arc.*

38. Take three points,  $A$ ,  $B$ ,  $C$ , any where in the circumference, or in the arc : draw  $AB$ ,  $BC$  ; bisect these two lines by the perpendiculars,  $DE$ ,  $FG$  : the point  $O$  where these perpendiculars meet will be the centre sought.



The same construction serves for making a circumference pass through three given points  $A$ ,  $B$ ,  $C$ , and also for describing a circumference, about a given triangle.

## CHAPTER III.

*Plane Trigonometry.*

39. In every plane triangle there are six parts : three sides and three angles. These parts are so related to each other, that if a certain number of them are known or given, the remaining ones can be determined.

40. *Plane Trigonometry* explains the methods of finding, by calculation, the unknown parts of a triangle when a sufficient number of the six parts is given.

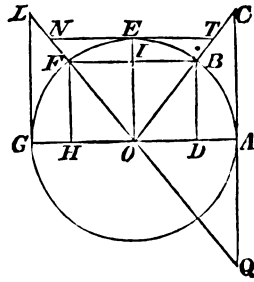
It has already been shown, in the problems, that triangles may be constructed when three parts are known. But these constructions, which are called *graphic methods*, though perfectly correct in theory, would give only a moderate approximation in practice, on account of the imperfection of the instruments required in constructing them.

Trigonometrical methods, on the contrary, being independent of mechanical operations, give solutions with the utmost accuracy.

41. For the purposes of trigonometrical calculations, the circumference of the circle is divided into 360 equal parts, called degrees ; each degree into 60 equal parts, called minutes ; and each minute into 60 equal parts, called seconds.



$\sin AB$  for  $BD$   
 $\cos AB$  for  $OD$   
 $\tan AB$  for  $AC$   
 $\sec AB$  for  $OC$ .



49. If  $ABE$  be equal to a quadrant, or  $90^\circ$ , then  $EB$  will be the complement of  $AB$ . Let the lines  $ET$  and  $IB$  be drawn perpendicular to  $OE$ . Then,

$ET$ , the tangent of  $EB$ , is called the cotangent of  $AB$ ;  
 $IB$ , the sine of  $EB$ , is equal to the cosine of  $AB$ ;  
 $OT$ , the secant of  $EB$ , is called the cosecant of  $AB$ .

In general, if  $A$  is any arc or angle, we have,

$$\begin{aligned}\cos A &= \sin (90^\circ - A) \\ \cot A &= \tan (90^\circ - A) \\ \operatorname{cosec} A &= \sec (90^\circ - A)\end{aligned}$$

50. If we take an arc  $ABEF$ , greater than  $90^\circ$ , its sine will be  $FH$ ;  $OH$  will be its cosine;  $AQ$  its tangent, and  $OQ$  its secant. But  $FH$  is the sine of the arc  $GF$ , which is the supplement of  $AF$ , and  $OH$  is its cosine: hence, *the sine of an arc is equal to the sine of its supplement; and the cosine of an arc is equal to the cosine of its supplement.\**

Furthermore,  $AQ$  is the tangent of the arc  $AF$ , and  $OQ$  is its secant:  $GL$  is the tangent, and  $OL$  the secant, of the supplemental arc  $GF$ . But since  $AQ$  is equal to  $GL$ , and  $OQ$  to  $OL$ , it follows that, *the tangent of an arc is equal to the tangent of its supplement; and the secant of an arc is equal to the secant of its supplement.\**

Let us suppose, that in a circle of a given radius, the lengths of the sine, cosine, tangent, and cotangent, have been calculated for every minute or second of the quadrant, and arranged in a table; such a table is called a table of sines and tangents. If the radius of the circle is 1, the table is called a table of natural sines. A table of natural sines, therefore, shows the

\* These relations are between the *values* of the trigonometrical lines; the algebraic signs, which they have in the different quadrants, are not considered.

values of the sines, cosines, tangents and cotangents of all the arcs of a quadrant, divided to minutes or seconds.

If the sines, cosines, tangents and secants are known for arcs less than  $90^\circ$ , those for arcs which are greater can be found from them. For if an arc is less than  $90^\circ$ , its supplement will be greater than  $90^\circ$ , and the values of these lines are the same for an arc and its supplement. Thus, if we know the sine of  $20^\circ$ , we also know the sine of its supplement  $160^\circ$ ; for the two are equal to each other.

## TABLE OF LOGARITHMIC SINES.

51. In this table are arranged the logarithms of the numerical values of the sines, cosines, tangents and cotangents of all the arcs of a quadrant, calculated to a radius of 10,000,000,000. The logarithm of this radius is 10. In the first and last horizontal lines of each page, are written the degrees whose sines, cosines, &c. are expressed on the page. The vertical columns on the left and right, are columns of minutes.

## CASE I.

*To find, in the table, the logarithmic sine, cosine, tangent, or cotangent of any given arc or angle.*

52. If the angle is less than  $45^\circ$ , look for the degrees in the first horizontal line of the different pages: then descend along the column of minutes, on the left of the page, till you reach the number showing the minutes: then pass along the horizontal line till you come into the column designated, sine, cosine, tangent, or cotangent, as the case may be: the number so indicated is the logarithm sought. Thus, on page 37, for  $19^\circ 55'$  we find,

$\sin 19^\circ 55'$	.	.	9.532312
$\cos 19^\circ 55'$	.	.	9.973215
$\tan 19^\circ 55'$	.	.	9.559097
$\cot 19^\circ 55'$	.	.	10.440903

53. If the angle is greater than  $45^\circ$ , search for the degrees along the bottom line of the different pages: then, ascend along the column of minutes on the right hand side of the page, till you reach the number expressing the minutes: then pass along the horizontal line into the columns designated

tang, cot, sine, or cosine, as the case may be; the number so pointed out is the logarithm required.

54. The column designated sine, at the top of the page, is designated cosine at the bottom; the one designated tang, by cotang, and the one designated cotang, by tang.

The angle found by taking the degrees at the top of the page and the minutes from the first vertical column on the left, is the complement of the angle found by taking the corresponding degrees at the bottom of the page, and the minutes traced up in the right hand column to the same horizontal line. Therefore, sine, at the top of the page, should correspond with cosine, at the bottom; cosine with sine, tang with cotang, and cotang with tang, as in the tables (Art. 49).

If the angle is greater than  $90^\circ$ , we have only to subtract it from  $180^\circ$ , and take the sine, cosine, tangent or cotangent of the remainder.

The column of the table next to the column of sines, and on the right of it, is designated by the letter *D*. This column is calculated in the following manner.

Opening the table at any page, as 42, the sine of  $24^\circ$  is found to be 9.609313; that of  $24^\circ 01'$ , 9.609597: their difference is 284; this being divided by 60, the number of seconds in a minute, gives 4.73, which is entered in the column *D*, omitting the decimal point.

Now, supposing the increase of the logarithmic sine to be proportional to the increase of the arc, and it is nearly so for  $60''$ , it follows, that 473 (the last two places being regarded as decimals), is the increase of the sine for  $1''$ . Similarly, if the arc were  $24^\circ 20'$  the increase of the sine for  $1''$ , would be 465, the last two places being decimals.

The same remarks are equally applicable in respect of the column *D*, after the column cosine, and of the column *D*, between the tangents and cotangents. The column *D*, between the columns tangents and cotangents, answers to both of these columns.

Now, if it were required to find the logarithmic sine of an arc expressed in degrees, minutes, and seconds, we have only to find the degrees and minutes as before; then, multiply the corresponding tabular number by the seconds, cut off two places to the right hand for decimals, and then add the product to the number first found, for the sine of the given arc.

Thus, if we wish the sine of  $40^{\circ} 26' 28''$ .

The sine $40^{\circ} 26'$	9.811952	
Tabular difference . 247		
Number of seconds . 28		
Product . . 69 16 to be added		69.16
Gives for the sine of $40^{\circ} 26' 28''$		9.812021.

The decimal figures at the right are generally omitted in the last result ; but when they exceed five-tenths, the figure on the left of the decimal point is increased by 1 ; this gives the result to the nearest unit.

The tangent of an arc, in which there are seconds, is found in a manner entirely similar. In regard to the cosine and cotangent, it must be remembered, that they increase while the arcs decrease, and decrease as the arcs are increased ; consequently, the proportional numbers found for the seconds, must be subtracted, not added.

EXAMPLES.

1. To find the cosine of  $3^{\circ} 40' 40''$

The cosine of $3^{\circ} 40'$	9.999110	
Tabular difference . 13		
Number of seconds . 40		
Product . . 5.20 to be subtracted		5.20
Gives for the cosine of $3^{\circ} 40' 40''$		9.999105

2. Find the tangent of  $37^{\circ} 28' 31''$

*Ans.* 9.884592.

3. Find the cotangent of  $87^{\circ} 57' 59''$

*Ans.* 8.550356.

CASE II.

*To find the degrees, minutes and seconds, answering to any given logarithmic sine, cosine, tangent or cotangent.*

56. Search in the table, and in the proper column, until the number is found : the degrees will be shown either at the top or bottom of the page, and the minutes in the side columns, either at the left or right.

But, if the number cannot be exactly found in the table, take from the table the degrees and minutes answering to the nearest less logarithm, the logarithm itself, and also the corresponding tabular difference. Subtract the logarithm taken

from the table from the given logarithm, annex two ciphers to the remainder, and then divide the remainder by the tabular difference: the quotient will be seconds, and is to be connected with the degrees and minutes before found; to be added for the sine and tangent, and subtracted for the cosine and cotangent.

## EXAMPLES.

1. Find the arc answering to the sine	9.880054
Sine $49^{\circ} 20'$ , next less in the table	9.879963
Tabular difference . . .	<u>181)9100(50''</u>

Hence, the arc  $49^{\circ} 20' 50''$  corresponds to the given sine 9.880054.

2. Find the arc whose cotangent is .	10.008688
cot $44^{\circ} 26'$ , next less in the table . .	10.008591
Tabular difference . . .	<u>421)9700(23''</u>

Hence,  $44^{\circ} 26' - 23'' = 44^{\circ} 25' 37''$  is the arc answering to the given cotangent 10.008688.

3. Find the arc answering to tangent	9.979110
	<i>Ans.</i> $43^{\circ} 37' 21''$ .

4. Find the arc answering to cosine	9.944599
	<i>Ans.</i> $28^{\circ} 19' 45''$ .

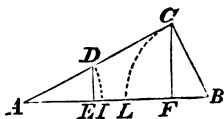
We shall now demonstrate the principal theorems of Plane Trigonometry.

## THEOREM I.

*The sides of a plane triangle are proportional to the sines of their opposite angles.*

57. Let  $ABC$  be a triangle; then will  
 $CB : CA :: \sin A : \sin B$ .

For, with  $A$  as a centre, and  $AD$  equal to the less side  $BC$ , as a radius, describe the arc  $DI$ : and with  $B$  as a centre and the equal radius  $BC$ , describe the arc  $CL$ : now  $DE$  is the sine of the angle  $A$ , and  $CF$  is the sine of  $B$ , to the same radius  $AD$  or  $BC$ . But by similar triangles,  
 $AD : DE :: AC : CF$ .



But  $AD$  being equal to  $BC$ , we have

$$BC : \sin A :: AC : \sin B, \text{ or}$$

$$BC : AC :: \sin A : \sin B.$$

By comparing the sides  $AB, AC$ , in a similar manner, we should find,  $AB : AC :: \sin C : \sin B$ .

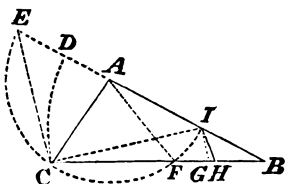
**THEOREM II.**

*In any triangle, the sum of the two sides containing either angle, is to their difference, as the tangent of half the sum of the two other angles, to the tangent of half their difference.*

58. Let  $ACB$  be a triangle: then will

$$AB+AC : AB-AC :: \tan \frac{1}{2}(C+B) : \tan \frac{1}{2}(C-B).$$

With  $A$  as a centre, and a radius  $AC$  the less of the two given sides, let the semicircle  $IFCE$  be described, meeting  $AB$  in  $I$ , and  $BA$  produced, in  $E$ . Then,  $BE$  will be the sum of the sides, and  $BI$  their difference. Draw  $CI$  and  $AF$ .



Since  $CAE$  is an outward angle of the triangle  $ACB$ , it is equal to the sum of the inward angles  $C$  and  $B$  (Bk. I, Prop. XXV, Cor. 6). But the angle  $CIE$  being at the circumference, is half the angle  $CAE$  at the centre (Bk. III, Prop. XVIII); that is, half the sum of the angles  $C$  and  $B$ , or equal to  $\frac{1}{2}(C+B)$ .

The angle  $AFC = ACB$ , is also equal to  $ABC + BAF$ ; therefore,  $BAF = ACB - ABC$ .

But,  $ICF = \frac{1}{2}(BAF) = \frac{1}{2}(ACB - ABC)$ , or  $\frac{1}{2}(C - B)$ .

With  $I$  and  $C$  as centres, and the common radius  $IC$ , let the arcs  $CD$  and  $IG$  be described, and draw the lines  $CE$  and  $IH$  perpendicular to  $IC$ . The perpendicular  $CE$  will pass through  $E$ , the extremity of the diameter  $IE$ , since the right angle  $ICE$  must be inscribed in a semicircle.

But  $CE$  is the tangent of  $CIE = \frac{1}{2}(C+B)$ ; and  $IH$  is the tangent of  $ICB = \frac{1}{2}(C-B)$ , to the common radius  $CI$ .

But since the lines  $CE$  and  $IH$  are parallel, the triangles  $BHI$  and  $BCE$  are similar, and give the proportion,

$$BE : BI :: CE : IH, \text{ or}$$

by placing for  $BE$  and  $BI$ ,  $CE$  and  $IH$ , their values, we have

$$AB+AC : AB-AC :: \tan \frac{1}{2}(C+B) \cdot \tan \frac{1}{2}(C-B).$$

4\*



## THEOREM III.

*In any plane triangle, if a line be drawn from the vertical angle perpendicular to the base, dividing it into two segments : then, the whole base, or sum of the segments, is to the sum of the other two sides, as the difference of those sides to the difference of the segments.*

59. Let  $BAC$  be a triangle, and  $AD$  perpendicular to the base ; then will

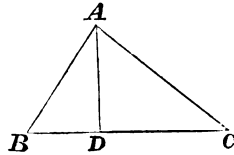
$$BC : CA + AB :: CA - AB : CD - DB$$

For,  $AB^2 = BD^2 + AD^2$

(Bk. IV, Prop. XI) ;

and  $AC^2 = DC^2 + AD^2$

by subtraction  $AC^2 - AB^2 = CD^2 - BD^2$ .



But since the difference of the squares of two lines is equal to the rectangle contained by their sum and difference (Bk. IV, Prop. X), we have,

$$AC^2 - AB^2 = (AC + AB) \cdot (AC - AB)$$

and  $CD^2 - DB^2 = (CD + DB) \cdot (CD - DB)$

therefore,  $(CD + DB) \cdot (CD - DB) = (AC + AB) \cdot (AC - AB)$

hence,  $CD + DB : AC + AB :: AC - AB : CD - DB$ .

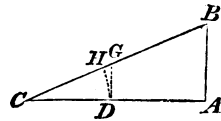
## THEOREM IV.

*In any right-angled plane triangle, radius is to the tangent of either of the acute angles, as the side adjacent to the side opposite.*

60. Let  $CAB$  be the proposed triangle, and denote the radius by  $R$  : then will

$$R : \tan C : AC : AB.$$

For, with any radius as  $CD$  describe the arc  $DH$ , and draw the tangent  $DG$ .



From the similar triangles  $CDG$  and  $CAB$  we shall have,

$$CD : DG :: CA : AB ; \text{ hence,}$$

$$R : \tan C :: CA : AB.$$

By describing an arc with  $B$  as a centre, we could show in the same manner that,

$$R : \tan B :: AB : AC.$$

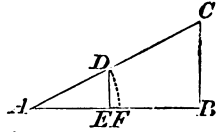
## THEOREM V.

*In every right-angled plane triangle, radius is to the cosine of either of the acute angles, as the hypotenuse to the side adjacent.*

61. Let  $ABC$  be a triangle, right angled at  $B$  then will

$$R : \cos A : AC : AB.$$

For, from the point  $A$  as a centre, and any radius as  $AD$ , describe the arc  $DF$ , which will measure the angle  $A$ , and draw  $DE$  perpendicular to  $AB$ : then will  $AE$  be the cosine of  $A$ .



The triangles  $ADE$  and  $ACB$ , being similar, we have

$$AD : AE :: AC : AB : \text{that is,}$$

$$R : \cos A :: AC : AB.$$

62. REMARK. The relations between the sides and angles of plane triangles, demonstrated in these five theorems, are sufficient to solve all the cases of Plane Trigonometry. Of the six parts which make up a plane triangle, at least three must be given, and one of these a side, before the others can be determined.

If the three angles are given, it is plain, that an indefinite number of similar triangles may be constructed, the angles of which shall be respectively equal to the angles that are given, and therefore, the sides could not be determined.

Assuming, with this restriction, any three parts of a triangle as given, one of the three following cases will always be presented.

- I. When two angles and a side are given.
- II. When two sides and an opposite angle are given.
- III. When two sides and the included angle are given.
- IV. When the three sides are given.

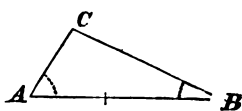
## CASE I.

When two angles and a side are given.

63. Add the given angles together and subtract their sum from 180 degrees. The remaining parts of the triangle can then be found by Theorem I.

## EXAMPLES.

1. In a plane triangle  $ABC$ , there are given the angle  $A=58^{\circ} 07'$ , the angle  $B=22^{\circ} 37'$ , and the side  $AB=408$  yards. Required the other parts.



## INSTRUMENTALLY.

Draw an indefinite straight line  $AB$ , and from the scale of equal parts lay off  $AB$  equal to 408. Then at  $A$  lay off an angle equal to  $58^{\circ} 07'$ , and at  $B$  an angle equal to  $22^{\circ} 37'$ , and draw the lines  $AC$  and  $BC$ : then will  $ABC$  be the triangle required.

The angle  $C$  may be measured either with the protractor or the scale of chords (Arts. 23 and 24), and will be found equal to  $99^{\circ} 16'$ . The sides  $AC$  and  $BC$  may be measured by referring them to the scale of equal parts (Art. 22). We shall find  $AC=158.9$  and  $BC=251$  yards.

## BY LOGARITHMS.

To the angle . . .	$A=58^{\circ} 07'$	
Add the angle . . .	$B=22^{\circ} 37'$	
Their sum . . .	$=80^{\circ} 44'$	
taken from . . .	$180^{\circ} 00'$	
leaves $C$ . . .	$99^{\circ} 16'$	which, exceeding $90^{\circ}$
we use its supplement	$80^{\circ} 44'$	

To find the side  $BC$ .

As $\sin C$ . . .	$99^{\circ} 16'$	. . .	ar. comp. . .	0.005705
: $\sin A$ . . .	$58^{\circ} 07'$	. . .	. . .	9.928972
:: $AB$ . . .	408	. . .	. . .	<u>2.610660</u>
: $BC$ . . .	351.024	(after rejecting 10)	. . .	<u>2.545337</u>

REMARK. The logarithm of the fourth term of a proportion is obtained by adding the logarithm of the second term to that of the third, and subtracting from their sum the logarithm of the first term. But to subtract the first term is the same as to add its arithmetical complement and reject 10 from the sum (Art. 17): hence, the arithmetical complement of the first term added to the logarithms of the second and third terms, will give the logarithm of the fourth term.

To find side  $AC$ .

As $\sin C$	. 99° 16'	ar. comp.	. . .	0.005705
: $\sin B$	. 22° 37'	. . .	. . .	9.584968
: : $AB$	. 408	. . .	. . .	2.610660
: $AC$	. 158.976	. . .	. . .	<u>2.201333</u>

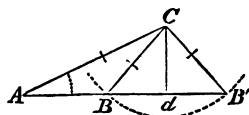
2. In a triangle  $ABC$ , there are given  $A=38^\circ 25'$ ,  $B=57^\circ 42'$ , and  $AB=400$ : required the remaining parts.

*Ans.*  $C=83^\circ 53'$ ,  $BC=249.974$ ,  $AC=340.04$ .

CASE II.

When two sides and an opposite angle are given

64. In a plane triangle  $ABC$ , there are given  $AC=216$ ,  $CB=117$ , the angle  $A=22^\circ 37'$ , to find the other parts.



INSTRUMENTALLY.

Draw an indefinite right line  $ABB'$ : from any point as  $A$ , draw  $AC$  making  $BAC=22^\circ 37'$ , and make  $AC=216$ . With  $C$  as a centre, and a radius equal to 117, the other given side, describe the arc  $B'B$ ; draw  $B'C$  and  $BC$ : then will either of the triangles  $ABC$  or  $AB'C$ , answer all the conditions of the question.

BY LOGARITHMS.

To find the angle  $B$ .

As $BC$	. 117	. ar. comp.	. . .	7.931814
: $AC$	. 216	. . .	. . .	2.334454
: : $\sin A$	. 22° 37'	. . .	. . .	9.584968
: $\sin B'$	45° 13' 55'', or $ABC$ 134° 46' 05''	. . .	. . .	<u>9.851236</u>

The ambiguity in this, and similar examples, arises in consequence of the first proportion being true for either of the angles  $ABC$ , or  $AB'C$ , which are supplements of each other, and therefore have the same sine (Art. 43). As long as the two triangles exist, the ambiguity will continue. But if the side  $CB$ , opposite the given angle, is greater than  $AC$ , the arc  $BB'$  will cut the line  $ABB'$ , on the same side of the point  $A$ , in but one

point, and then there will be only one triangle answering the conditions.

If the side  $CB$  is equal to the perpendicular  $Cd$ , the arc  $BB'$  will be tangent to  $ABB'$ , and in this case also there will be but one triangle. When  $CB$  is less than the perpendicular  $Cd$ , the arc  $BB'$  will not intersect the base  $ABB'$ , and in that case, no triangle can be formed, or it will be impossible to fulfil the conditions of the problem.

2. Given two sides of a triangle 50 and 40 respectively, and the angle opposite the latter equal to  $32^\circ$ : required the remaining parts of the triangle.

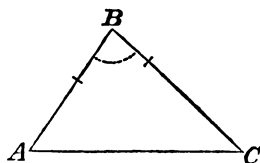
*Ans.* If the angle opposite the side 50 is acute, it is equal to  $41^\circ 28' 59''$ ; the third angle is then equal to  $106^\circ 31' 01''$ , and the third side to 72.368. If the angle opposite the side 50 is obtuse, it is equal to  $138^\circ 31' 01''$ , the third angle to  $9^\circ 28' 59''$ , and the remaining side to 12.436.

### CASE III.

When the two sides and their included angle are given.

65. Let  $ABC$  be a triangle;  $AB$ ,  $BC$ , the given sides, and  $B$  the given angle.

Since  $B$  is known, we can find the sum of the two other angles: for



$$\begin{aligned} A + C &= 180^\circ - B \quad \text{and} \\ \frac{1}{2}(A + C) &= \frac{1}{2}(180^\circ - B) \end{aligned}$$

We next find half the difference of the angles  $A$  and  $C$  by Theorem II. Viz.

$BC + BA : BC - BA :: \tan \frac{1}{2}(A + C) : \tan \frac{1}{2}(A - C)$ .  
in which we consider  $BC$  greater than  $BA$ , and therefore  $A$  is greater than  $C$ ; since the greater angle must be opposite the greater side.

Having found half the difference of  $A$  and  $C$ , by adding it to the half sum  $\frac{1}{2}(A + C)$ , we obtain the greater angle, and by subtracting it from half the sum, we obtain the less. That is

$$\begin{aligned} \frac{1}{2}(A + C) + \frac{1}{2}(A - C) &= A, \quad \text{and} \\ \frac{1}{2}(A + C) - \frac{1}{2}(A - C) &= C. \end{aligned}$$

Having found the angles  $A$  and  $C$ , the third side  $AC$  may be found by the proportion.

$$\sin A : \sin B :: BC : AC.$$

EXAMPLES.

1. In the triangle  $ABC$ , let  $BC=540$ ,  $AB=450$ , and the included angle  $B=80^\circ$ : required the remaining parts.

INSTRUMENTALLY.

Draw an indefinite right line  $BC$  and from any point, as  $B$ , lay off a distance  $BC=540$ . At  $B$  make the angle  $CBA=80^\circ$ : draw  $BA$  and make the distance  $BA=450$ ; draw  $AC$ ; then will  $ABC$  be the required triangle.

BY LOGARITHMS.

$$BC+BA=540+450=990; \text{ and } BC-BA=540-450=90.$$

$$A+C=180^\circ-B=180^\circ-80^\circ=100^\circ, \text{ and therefore,}$$

$$\frac{1}{2}(A+C)=\frac{1}{2}(100^\circ)=50^\circ$$

To find  $\frac{1}{2}(A-C)$ .

As $BC+BA$	. 990	. ar. comp.	. 7.004365
: $BC-BA$	. 90	. . . . .	. 1.954243
:: $\tan \frac{1}{2}(A+C)$	. $50^\circ$	. . . . .	. 10.076187
: $\tan \frac{1}{2}(A-C)$	. $6^\circ 11'$	. . . . .	. 9.034795

Hence,  $50^\circ+6^\circ 11'=56^\circ 11'=A$ ; and  $50^\circ-6^\circ 11'=43^\circ 49'=C$ .

To find the third side  $AC$ .

As $\sin C$	. $43^\circ 49'$	. ar. comp.	. 0.159672
: $\sin B$	. $80^\circ$	. . . . .	. 9.993351
:: $AB$	. 450	. . . . .	. 2.653213
: $AC$	. 640.082	. . . . .	. 2.806236

2. Given two sides of a plane triangle, 1686 and 960, and their included angle  $128^\circ 04'$ : required the other parts.

*Ans.* Angles,  $33^\circ 34' 39''$ ;  $18^\circ 21' 21''$ ; side 2400.

CASE IV.

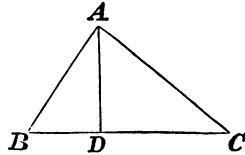
Having given the three sides of a plane triangle, to find the angles.

66. Let fall a perpendicular from the angle opposite the

greater side, dividing the given triangle into two right-angled triangles: then find the difference of the segments of the base by Theorem III. Half this difference being added to half the base, gives the greater segment; and, being subtracted from half the base, gives the less segment. Then, since, the greater segment belongs to the right-angled triangle having the greatest hypotenuse, we have the sides and right angle of two right-angled triangles, to find the acute angles.

## EXAMPLES.

1. The sides of a plane triangle being given; viz.  $BC=40$ ,  $AC=34$  and  $AB=25$ : required the angles.



## INSTRUMENTALLY.

With the three given lines as sides construct a triangle as in Problem IX. Then measure the angles of the triangle, either with the protractor or scale of chords.

## BY LOGARITHMS.

$$\text{As } BC : AC + AB :: AC - AB : CD - BD$$

$$\text{That is, } 40 : 59 :: 9 : \frac{59 \times 9}{40} = 13.275$$

$$\text{Then, } \frac{40 + 13.275}{2} = 26.6375 = CD$$

$$\text{And } \frac{40 - 13.275}{2} = 13.3625 = BD.$$

In the triangle  $DAC$ , to find the angle  $DAC$ .

As	$AC$	34	.	.	ar. comp.	.	8.468521
:	$DC$	26.6375	.	.	.	.	1.425493
::	$\sin D$	$90^\circ$	.	.	.	.	10.000000
·	$\sin DAC$	$51^\circ 34' 40''$	.	.	.	.	<u>9.894014</u>

In the triangle  $BAD$ , to find the angle  $BAD$ .

As	$AB$	. . . 25 . . .	ar. comp.	. . . . .	8.602060
:	$BD$	. . . 13.3625 . . .			1.125887
::	$\sin D$	. . . $90^\circ$ . . .			10.000000
:	$\sin BAD$	. . . $32^\circ 18' 35''$ . . .			9.727947

Hence  $90^\circ - DAC = 90^\circ - 51^\circ 34' 40'' = 38^\circ 25' 20'' = C$

and  $90^\circ - BAD = 90^\circ - 32^\circ 18' 35'' = 57^\circ 41' 25'' = B$

and  $BAD + DAC = 51^\circ 34' 40'' + 32^\circ 18' 35'' = 83^\circ 53' 15'' = A$ .

2. In a triangle, in which the sides are 4, 5 and 6, what are the angles. ?

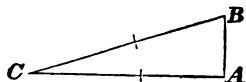
*Ans.*  $41^\circ 24' 35''$ ;  $55^\circ 46' 16''$ ; and  $82^\circ 49' 09''$ .

SOLUTION OF RIGHT-ANGLED TRIANGLES.

67. The unknown parts of a right-angled triangle may be found by either of the four last cases: or, if two of the sides are given, by means of the property that the square of the hypotenuse is equal to the sum of the squares of the other two sides. Or the parts may be found by Theorem V.

EXAMPLES.

1. In a right-angled triangle  $BAC$ , there are given the hypotenuse  $BC = 250$ , and the base  $AC = 240$ : re-



quired the other parts.

To find the angle  $B$ .

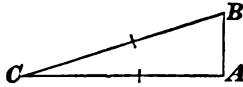
As	$BC$	. . . 250 . . .	ar. comp.	. . . . .	7.602060
:	$AC$	. . . 240 . . .			2.380211
::	$\sin A$	. . . $90^\circ$ . . .			10.000000
:	$\sin B$	. . . $73^\circ 44' 23''$ . . .			9.982271

But  $C = 90^\circ - B = 90^\circ - 73^\circ 44' 23'' = 16^\circ 15' 37''$ ;

Or  $C$  might be found from the proportion.

As	$CB$	. . . 250 . . .	ar. comp.	. . . . .	7.602060
:	$AC$	. . . 240 . . .			9.380211
::	$R$	. . . . .			10.000000
:	$\cos C$	. . . $16^\circ 15' 37''$ . . .			9.982271





To find side  $AB$  by Theorem IV.

As $\sin A$	.	$90^\circ$	ar. comp.	.		0.000000
: $\tan C$	.	$16^\circ 15' 37''$	.	.	.	9.464889
:: $AC$	.	240	.	.	.	<u>2.380211</u>
: $AB$	.	70.0003	.	.	.	<u>1.845100</u>

2. In a right-angled triangle  $BAC$ , there are given  $AC = 384$ , and  $B = 53^\circ 08'$ : required the remaining parts.

*Ans.*  $AB = 287.96$ ;  $BC = 479.979$ ;  $C = 36^\circ 52'$ .

# ELEMENTS OF SURVEYING.

## CHAPTER I

### *Definitions and Introductory Remarks.*

68. Surveying, in its most extensive signification, comprises all the operations necessary for finding,

1st. The area or content of any portion of the surface of the earth ;

2d. The lengths and directions of the bounding lines ; and

3d. The accurate delineation of the whole on paper.

69. The earth being spherical, its surface is curved, and every line traced on its surface is also curved.

If large portions of the surface are to be measured, such as states and territories, the curvature must be taken into account ; and very material errors will arise if it be neglected. When the curvature is considered, the method of measurement and computation is called *Geodesic Surveying*.

The radius of the earth, however, being large, the curvature of its surface is small, and when the measurement is limited to small portions of the surface, the error becomes insensible, if we consider the surface a plane. This method of measurement and computation, is called *Plane Surveying*, and is the only kind that will be treated of in these Elements.

70. If at any point of the surface of the earth, a plane be drawn perpendicular to the radius passing through this point, such plane is tangent to the surface, and is called a *horizontal plane*. All planes parallel to such a plane, are also called *horizontal planes*.

71. A plane which is perpendicular to a horizontal plane is called a *vertical plane*.

72. All lines of a horizontal plane, and all lines which are parallel to it, are called *horizontal lines*.

73. Lines which are perpendicular to a horizontal plane, are called *vertical lines*; and all lines which are inclined to it, are called *oblique lines*.

Thus,  $AB$  and  $DC$  are horizontal lines;  $BC$  and  $AD$  are vertical lines; and  $AC$  and  $BD$  are oblique lines.



74. The horizontal distance between two points, is the horizontal line intercepted between the two vertical lines passing through those points. Thus,  $DC$  or  $AB$  is the horizontal distance between the two points  $A$  and  $C$ , or the points  $B$  and  $D$ .

75. A *horizontal angle* is one whose sides are horizontal; its plane is also horizontal.

A horizontal angle may also be defined to be, the angle included between two vertical planes passing through the angular point, and the two objects which subtend the angle.

76. A vertical angle is one, the plane of whose sides is vertical.

77. An angle of *elevation*, is a vertical angle having one of its sides horizontal, and the inclined side above the horizontal side.

Thus, in the last figure,  $BAC$  is the angle of elevation from  $A$  to  $C$ .

78. An angle of *depression*, is a vertical angle having one of its sides horizontal, and the inclined side under the horizontal side. Thus,  $DCA$  is the angle of depression from  $C$  to  $A$ .

79. An *oblique angle* is one, the plane of whose sides is oblique to the horizontal plane.

80. All lines, which can be the object of measurement, must belong to one of the classes above named, viz.:

- 1st. Horizontal lines:
- 2d. Vertical lines:
- 3d. Oblique lines.

All the angles may also be divided into three classes, viz.:

- 1st. Horizontal angles:

- 2d. Vertical angles ; which may be again divided into angles of elevation and angles of depression : and
- 3d. Oblique angles.

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## CHAPTER II.

### *Of the measurement and calculation of Lines and Angles.*

81. It has been shown (Art. 62), that at least one side and two of the other parts of a plane triangle must be given or known, before the remaining parts can be found by calculation.

When, therefore, distances are to be found, by trigonometrical calculations, two things are necessary.

1st. To measure certain lines on the ground ; and also, as many angles as may be necessary to render at least three parts of every triangle known : and

2d. To calculate, by trigonometry, the other sides and angles that may be required. Our attention, then, is directed,

1st. To the measurement of lines ;

2d. To the measurement of angles ; and

3d. To the calculations for the unknown and required parts.

82. Any tape, rod, or chain, on which equal parts are marked, may be used as a measure ; and one of the equal parts into which the measure is divided, is called the *unit* of the measure. The unit of a measure may be a foot, a yard, a rod, or any other ascertained distance.

83. The measure in general use, is a chain of four rods or sixty-six feet in length ; it is called Gunter's chain, from the name of the inventor. This chain is composed of 100 links. Every tenth link from either end, is marked by a small attached brass plate, which is notched, to designate its number from the end. The division of the chain into 100 equal parts, is a very convenient one, since the divisions or links, are decimals of the whole chain, and in the calculations may be treated as such.

## TABLE.

1 chain = 4 rods = 66 feet = 792 inches = 100 links

Hence, 1 link is equal to 7.92 inches.

80 chains = 320 rods = 1 mile.

40 chains =  $\frac{1}{2}$  mile.

20 chains =  $\frac{1}{4}$  mile.

84. Besides the chain, there are wanted for measuring, ten marking pins, which should be of iron, about ten inches in length and an eighth of an inch in thickness. These pins should be strung upon an iron ring, and this ring should be attached to a belt, to be passed over the right shoulder, suspending the pins at the left side. Two staves are also required. They should be about six feet in length, and have a spike in the lower end to aid in holding them firmly, and a horizontal strip of iron to prevent the chain from slipping off; these staves are to be passed through the rings at the ends of the chain.

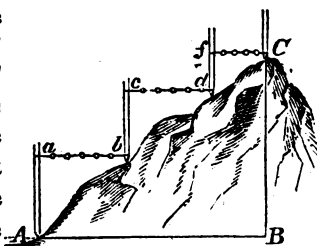
## TO MEASURE A HORIZONTAL LINE.

85. At the point where the measurement is to be begun, place in a vertical position, a signal staff, having a small flag attached to its upper extremity; and place another at the point where the measurement is to be terminated. These two points are generally called *stations*.

Having passed the staves through the rings of the chain, let the ten marking pins and one end of the chain be taken by the person who is to go forward, and who is called the leader, and let him plant the staff as nearly as possible in the direction of the stations. Then, taking the staff in his right hand, let him stand off at arm's length, so that the person at the other end of the chain can align it exactly with the stations: when the alignment is made, let the chain be stretched and a marking pin placed; then measure a second chain in the same manner, and so on, until all the marking pins shall have been placed. When the marking pins are exhausted, a note should be made, that ten chains have been measured; after which, the marking pins are to be returned to the leader, and the measurement continued as before, until the whole distance is passed over.

Great care must be taken to keep the chain horizontal, and if the acclivity or declivity of the ground be too great to admit of measuring a whole chain at a time, a part of a chain only should be measured: the sum of all the horizontal lines so measured, is evidently the horizontal distance between the stations.

For example, in measuring the horizontal distance between  $A$  and  $C$ , we first place a staff at  $A$  and another at  $b$ , in the direction towards  $C$ . Then slide up the chain on the staff at  $A$  until it becomes horizontal, and note the distance  $ab$ . Then remove the



staves and place them at  $b$  and  $d$ : make the chain horizontal, and note the distance  $cd$ . Measure in the same manner the line  $fC$ ; and the sum of the horizontal lines  $ab$ ,  $cd$  and  $fC$ , will be equal to  $AB$ , the horizontal distance between  $A$  and  $C$ .

86. We come now to the measurement of angles, and for this purpose several instruments are used. The one, however, which affords the most accurate results, and which indeed can alone be relied on for nice or extensive operations, is called a Theodolite. This instrument only will be described at present; others will be subsequently explained.

## OF THE THEODOLITE.

Pl. 1. The theodolite is an instrument used to measure horizontal and vertical angles. It is usually placed on a tripod  $ABC$ , which enters by means of a screw the lower horizontal plate  $DE$ , and becomes firmly attached to the body of the instrument. Through the horizontal plate  $DE$ , four small hollow cylinders are inserted, which receive four screws with milled heads, that work against a second horizontal plate,  $FG$ . The upper side of the plate  $DE$  terminates in a curved surface, which encompasses a ball, that is nearly a semi-sphere, with the plane of its base horizontal. This ball, which is hollow, is firmly connected with the smaller base of a hollow conic frustrum, that passes through the curved part

of the plate *DE*, and screws firmly into the curved part of the second horizontal plate *FG*.

A hollow conic spindle passes through the middle of the ball, and the hollow frustrum with which it is connected. To this spindle, a third horizontal and circular plate *HI*, called *the limb of the instrument*, is permanently attached. Within this spindle, and concentric with it, there is a second spindle, called the inner, or solid spindle. To this latter, is united a thin circular plate, called the *vernier plate*, which rests on the limb of the instrument, and supports the upper frame-work. The two spindles terminate at the base of the spherical ball, where a small screw enters the inner one, and presses a washer against the other, and the base of the ball. On the upper surface of the plate *FG*, rests a clamp which goes round the outer spindle, and which being compressed by the clamp-screw *K*, is made fast to it. This clamp is thus connected with the plate *FG*. A small cylinder *a*, is fastened to the plate *FG*: through this cylinder a thumb-screw *L* passes, and works into a small cylinder *b*, connected with the clamp. The cylinders *b* and *a*, admit of a motion round their axes, to relieve the screw *L* of the pressure which would otherwise be occasioned by working it.

Directly above the clamp, is the lower telescope *MN*. This telescope is connected with a hollow cylinder, which is worked freely round the outer spindle, by the thumb-screw *P* having a pinion working into a concealed cog-wheel, that is permanently fastened to the limb of the instrument. By means of a clamp-screw *Q*, the telescope is made fast to the limb, when it will have a common motion with the limb and outer spindle.

The circular edge of the limb is chamfered, and is generally made of silver, and on this circle the graduation for horizontal angles is made. In the instrument described, the circle is cut into degrees and half degrees; the degrees are numbered from 0 to 360.

On the circular edge of the vernier plate, is a small space of silver, called a *vernier*; this space is divided into 30 equal parts, and numbered from the line marked 0 to the left.

There are two levels attached to the vernier plate, at right angles to each other, by small adjusting screws; one of them is seen in the figure. The vernier plate turns freely around

with the inner spindle. It is made fast to the limb of the instrument by the clamp-screw *S*; after which the smaller motions are made by the tangent-screw *T*.

There is a compass on the vernier plate, that is concentric with it, the use of which will be explained under the head compass.

The frame-work which supports the horizontal axis of the vertical semicircle *UV* and the upper telescope, with its attached level, rests on the vernier plate, to which it is made fast by three adjusting screws, placed at the angular points of an equilateral triangle. The vertical semicircle *UV*, is called the *vertical limb*; its motions are governed by the thumb-screw *Z*, which has a pinion, that works with the teeth of the vertical limb. On the face of the vertical limb, opposite the thumb-screw *Z*, the limb is divided into degrees and half degrees: the degrees are numbered both ways from the line marked 0. There is a small plate resting against the graduated face of the vertical limb, called the vernier; it is divided into 30 equal parts, and the middle line is designated by 0.

On the other face of the vertical limb, are two ranges of divisions, commencing at the 0 point, and extending each way 45°. The one shows the vertical distance of any object to which the upper telescope is directed, above or below the place of the instrument, in 100th parts of the horizontal distance: the other, the difference between the hypotenusal and base lines: the hypotenuse being supposed to be divided into one hundred equal parts: therefore, by mere inspection, we can ascertain the number of links, which must be subtracted from every chain of an oblique line, to reduce it to a true horizontal distance.

The supports of the upper telescope are called the wyes, and designated *Y*'s. Two loops, turning on hinges, pass over the telescope, and are made fast by the pins *c* and *d*; these loops confine the telescope in the *Y*'s. By withdrawing the pins, and turning the loops on their hinges, the telescope may be removed for the purpose of being reversed in position; and in both situations, the telescope can be revolved in the *Y*'s about its axis.

In the telescopes attached to the theodolite, are two principal lenses, one at each end. The one at the end where



the eye is placed, is called the eyeglass, the other the object glass.

In order that the axis of the telescope may be directed to an object with precision, two spider's lines, or small hairs, are fixed at right angles to each other, and placed within the barrel of the telescope, and at the focus of the eyeglass. The vertical hair is moved by two small horizontal screws, one of which, *f*, is seen in the figure; and the horizontal hair, by two vertical screws, *g* and *h*.

Before using the theodolite, it must be properly adjusted. The adjustment consists in bringing the different parts to their proper places.

The line of *collimation*, is the axis of the telescope. With this axis, the line drawn through the centre of the eyeglass, and the intersection of the spider's lines, ought to coincide.

**FIRST ADJUSTMENT.** The first adjustment regards the line of collimation: it is, to fix the intersection of the spider's lines in the axis of the telescope.

Having screwed the tripod to the instrument, extend the legs, and place them firmly. Then loosen the clamp-screw *S* of the vernier plate, and direct the telescope to a small, well-defined, and distant object. By means of a small pin *i*, on the under side of the telescope, slide the eyeglass till the spider's lines are seen distinctly; then with the thumb-screw *X*, which forces out and draws in, the object glass, adjust this glass to its proper focus, when the object, as well as the spider's lines, will be distinctly seen: after which, by the tangent-screw *T* and the thumb-screw *Z*, bring the intersection of the spider's lines exactly upon a well-defined point of the object.

Having done this, revolve the telescope in the *Y*'s, half round, when the attached level *mn*, will come to the upper side. See, in this position, if the horizontal hair appears above or below the point, and in either case, loosen one, and tighten the other, of the two screws that work the horizontal hair, till the horizontal hair has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again the intersection of the spider's lines, to the point, and repeat the operation till the horizontal hair neither ascends nor descends, while the tele-

scope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted.

**SECOND ADJUSTMENT.**—*To make the axis of the attached level of the upper telescope, parallel to the line of collimation.*

Turn the vernier plate, till the telescope comes directly over two of the levelling screws, between the plates *DE* and *FG*. Turn these screws contrary ways, keeping them firm against the plate *FG*, till the bubble of the level *mn*, stands at the middle of the tube. Then, open the loops, and reverse the telescope. If the bubble still stands in the middle of the tube, the axis of the tube is horizontal; but if not, it is inclined, the bubble being at the elevated end. In that case, by means of the small vertical screws *m* and *n*, at the ends of the level, raise the depressed end, or depress the elevated one, half the inclination; and then, with the levelling screws, bring the level into a horizontal position. Reverse the telescope in the *Y*'s, and make the same correction again; and so on, until the bubble stands in the middle of the tube, in both positions of the telescope: the axis of the level is then horizontal. Let the telescope be now revolved in the *Y*'s. If the bubble continue in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recede from its centre, the axis of the level is inclined to the line of collimation, and must be made parallel to it by means of two small screws, (one of which is seen at *p*,) which work horizontally. By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation, and then, if the telescope be revolved in the *Y*'s, the bubble will continue in the middle of the tube.

It is difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation; for, if the level were truly horizontal in one position of the telescope, when the telescope is reversed, the bubble would not stand in the middle of the tube, except in one position of the level. This suggests the necessity of making the first part of the adjustment with tolerable accuracy; then, having made the second with care, let the first be again examined, and proceed thus till the adjustment is completed.

**THIRD ADJUSTMENT.**—*To make the limb of the instrument horizontal, or, to make the common axis of the limb and vernier plate truly vertical.*

This adjustment is effected, partly by the levelling screws, and partly by the thumb-screw *Z*. Turn the vernier plate, until the upper telescope comes directly over two of the levelling screws, then turn them contrary ways, till the upper telescope is horizontal; after which, turn the vernier plate  $180^\circ$ , and if the bubble of the level remains in the middle of the tube, one line of the limb is horizontal. But if the bubble recede from the centre of the level, raise the lower, or depress the upper end, one-half by the levelling screws, the other by the thumb-screw *Z*, till it is brought into a horizontal position. Turn the vernier plate again  $180^\circ$ , and if the level be not then horizontal, make it so, by dividing the error as before, and repeat the operation until the line of the limb is truly horizontal. Then turn the vernier plate  $90^\circ$ , and level as before. The limb ought now to be truly horizontal; but lest the first horizontal line may have been changed, in obtaining the second, it is well to bring the telescope and level two or three times over the levelling screws, until an entire revolution can be made without displacing the bubble from the middle of the tube. As this can only be the case when the level revolves around a vertical line, it follows that the limb will then be horizontal, and the axis of the instrument vertical.

This adjustment being completed, the levels of the vernier plate are readily made parallel with it, by means of the small screws at their extremities. The three levels being then horizontal, and perpendicular in direction to the axis of the theodolite, the bubbles will retain the middle places in the tubes, during an entire revolution of the vernier plate, or of the limb and vernier plate together.

But the levels of the vernier plate may be made parallel with the limb, and the limb made truly horizontal, without the aid of the upper level.

Let the upper telescope be placed directly over two of the levelling screws. One of the levels of the vernier plate will then be parallel to the line of these two screws, and the other level will be at right angles to this line, or parallel to the line of the other two levelling screws. In this situation, let the

levels be made horizontal, by means of the levelling screws. Then turn the vernier plate  $180^\circ$ , and if they both continue horizontal, the limb is truly level. But if both, or either of them, be changed from a horizontal position, let the error be divided between the level and the limb; and repeat the operation until the levels will continue horizontal during an entire revolution: the limb is then horizontal, and the axis of the instrument truly vertical.

**FOURTH ADJUSTMENT.**—*To make the axis of the vertical limb truly horizontal, or perpendicular to the axis of the instrument.*

Bring the intersection of the spider's lines of the upper telescope upon a plumb line, or any well-defined vertical object, and move the telescope with the thumb-screw *Z*: if the intersection of the spider's lines continue on the vertical line, the axis is horizontal.

Or, the adjustment may be effected thus: Direct the intersection of the spider's lines to a well-defined point that is considerably elevated: then turn the vertical limb, until the axis of the telescope rests on some other well-defined point, upon or near the ground: reverse the telescope, and turn the vernier plate  $180^\circ$ ; now, if in elevating and depressing the telescope, the line of collimation passes through the two points before noted, the axis is horizontal. If it be found, by either of the above methods, that the axis is not horizontal, it must be made so by the screws which fasten the frame-work to the vernier plate.

There are two important lines of the theodolite, the positions of which are determined with great care by the maker, and fixed permanently. First, the axis of the instrument is placed exactly at right angles with the limb and vernier plate; and unless it have this position, the vernier plate will not revolve at right angles to the axis, as explained in the third adjustment. Secondly, the line of collimation of the upper telescope, is fixed at right angles to the horizontal axis of the vertical limb. We can ascertain whether these last lines are truly at right angles, by directing the intersection of the spider's lines to a well-defined point; then removing the caps which confine the horizontal axis in its supports, and reversing the axis: if the intersection of the spider's lines can be made to

cover exactly the same point, without moving the vernier plate, the line of collimation is at right angles to the axis.

If the theodolite be so constructed that either of the  $Y$ 's admits of being moved laterally, so as to vary the angle between the horizontal axis and the line of collimation, these lines may be adjusted at right angles to each other, if they have not been so placed by the maker.

The lower telescope being used merely as a guard, requires no adjustment, although it is better to make the axis, about which its vertical motions are performed, horizontal, or perpendicular to the axis of the instrument; and this is easily effected by means of the two small screws  $k$  and  $l$ , which work into the slide  $A'$ , that is connected with the horizontal axis.

The theodolite being properly adjusted, the particular uses of its several parts, and the manner of measuring angles, are now to be explained.

There are two verniers on the vernier plate, and the points of them marked 0, are at the opposite extremities of a diameter; which diameter is the intersection of a vertical plane passed through the line of collimation, with the vernier plate. It is important to ascertain the exact arc intercepted on the limb, between its 0 point, (this being the point from which the degrees are numbered), and this diameter, for any position which it may assume. The limb being divided to half degrees, if we had only the line marked 0 on the vernier, to guide us, the place of the extremity of the diameter could only be ascertained with certainty to half degrees, as there would be no means of determining its exact position, when it falls between the lines of division on the limb. But the vernier affords results much more accurate. As most instruments for the measurement of angles have verniers, it will perhaps be best to explain their use generally.

*First.*—Count carefully the number of spaces into which the vernier is divided: this number is one less than the number of lines which limit them.

*Secondly.*—Turn the vernier till the line at one extremity coincides with a line of the graduated limb, when the line at the other extremity will also coincide with a line of the graduated limb; for the sum of the spaces on the vernier is

always exactly equal to a given number of spaces on the limb; then count the number of spaces on the limb which the vernier covers.

*Thirdly.*—Examine the limb of the instrument, and ascertain into what parts of a degree it is divided, and express one of those equal parts in minutes.

Let  $x$  represent the value of one of the equal spaces of the vernier, and  $n$  their number; then  $nx$  will be equal to the space covered by the vernier. Let  $a$  represent the smallest equal space into which the limb is divided, and  $m$  the number of such spaces covered by the vernier; then  $ma$  will be equal to the space on the limb covered by the vernier, which is also equal to  $nx$ .

The equation  $nx=ma$  is called the *equation of the instrument*. In this equation,

$$x = \frac{ma}{n};$$

$m$ ,  $a$ , and  $n$ , being known,  $x$  can be found, as also the difference between  $a$  and  $x$ , which we shall show presently, to be the smallest *certain count* of the instrument.

In the theodolite,  $m=29$ ,  $a=30'$  and  $n=30$  hence;

$$x = \frac{29 \times 30'}{30} = 29';$$

$$\text{and } a - x = 30' - 29' = 1',$$

the excess of a space on the limb over a space on the vernier.

Fig. 2. Let  $AB$  be a portion of the limb of the instrument, and  $CED$  the vernier in one of its positions, its 0 point coinciding with the line marked 10 on the limb. Now, since each space of the vernier is less by  $1'$  than each space of the limb, the first line on the left of 0, will be  $1'$  to the right of the first line on the left of the 10 on the limb; and if the vernier plate be moved  $1'$  towards the left, these lines will coincide, and the second line from 0 will then be  $1'$  to the right of the second line from 10; if the vernier be moved another minute, these last lines will coincide. The vernier would then show  $10^{\circ} 2'$ .

If the vernier plate be turned still farther, till the third, fourth, fifth, &c. lines coincide, it is plain, that the 0 point of the vernier will have passed the line 10 on the limb, by as many minutes as there are lines of the vernier which shall have coincided with lines of the limb. When the last line

of the vernier coincides with a line of the limb, the vernier will have been moved  $30'$ , or half a degree; and the 0 point will at the same time coincide with a line of the limb, and show  $10^{\circ} 30'$ .

The general rule for reading the angle for any position of the vernier may now be stated.

When the 0 line of the vernier coincides with a line of the limb, the arc is easily read from the limb; but when it falls between two lines, note the degrees and half degrees up to the line on the right; then pass along the vernier till a line is found coinciding with a line of the limb: the *number* of this line from the 0 point, indicates the minutes which are to be added to the degrees and half degrees, for the entire angle.

*To measure a horizontal angle with the theodolite.*

Place the axis of the instrument directly over the point at which the angle is to be measured. This is effected by means of a plumb, suspended from the plate which forms the upper end of the tripod.

Having made the limb truly level, place the 0 of the vernier at 0 or  $360^{\circ}$  of the limb, and fasten the clamp-screw *S* of the vernier plate. Then, facing in the direction between the lines which subtend the angle to be measured, turn the limb with the outer spindle, until the telescope points to the object on the left, very nearly. Clamp the limb with the clamp-screw *K*, and by means of the tangent screws *L* and *Z*, bring the intersection of the spider's lines to coincide exactly with the object.

Having loosened the clamp-screw *Q* of the lower telescope *MN*, direct it with the thumb-screw *P* to the same object at which the upper telescope is directed; then tighten the clamp-screw *Q*. This being done, loosen the clamp-screw *S* of the vernier plate, and direct the telescope to the other object: the arc passed over by the 0 point of the vernier, is the measure of the angle sought.

The lower telescope having been made fast to the limb, will indicate any change of its position, should any have taken place; and, as the accuracy of the measurements depends on the fixedness of the limb, the lower telescope ought to be often examined, and if its position has been altered, the limb must be brought back to its place by the tangent-screw *L*.

It is not necessary to place the 0 point of the vernier at the 0 point of the limb, previously to commencing the measurement of the angle, but convenient merely; for, whatever be the position of this point on the limb, it is evident that the arc which it passes over is the true measure of the horizontal angle. If, therefore, its place be carefully noted for the first direction, and also for the second, the difference of these two readings will be the true angle, unless the vernier shall have passed the 0 point of the limb, in which case the greater reading must be subtracted from 360°, and the remainder added to the less.

*To measure a vertical angle.*

In Fig. 3, *AB* represents a view of the vertical limb opposite the thumb-screw *Z*, and *ED* is the vernier. The 0 point of this vernier is at the middle division line, and fifteen spaces lie on each side of it. The relation which exists between the spaces on the limb and those of the vernier, is the same as that between the divisions of the horizontal limb and its vernier, and the degrees and half degrees are read in the same manner: the angles of elevation being read from the 0 of the limb towards the right, and those of depression in the contrary direction. For the minutes, we pass along the vernier in the direction in which the degrees are counted, and if we reach the extreme line, which is the fifteenth, without finding a coincidence, we must then pass to the other extremity of the vernier, and look along towards the 0 point till two lines are found to coincide: the number of the line on the vernier will show the minutes. The lines of the vernier are numbered both ways from the 0 point, and marked 5, 10, 15, to one extremity, and correspondingly from the other extremity 15, 20 and 25, to the 0 point again. The upper range shows the minutes for angles of elevation, and the lower range for those of depression. The vernier in Fig. 3 stands at 2° 15' of depression. Had the 15th line at the left, passed the short line with which it now coincides, we should pass to the line 15, on the lower range to the right, and then count towards the 0 to the left.

The first thing to be done, is to ascertain the point of the vertical limb at which the 0 point of the vernier stands, when the line of collimation of the upper telescope, together with



its attached level, is truly horizontal. This is called the true 0 of the limb.

If the instrument be accurately constructed, and the parts have not been disarranged, this point is the 0 point of the limb. This, however, is easily ascertained by turning the limb till the 0's correspond, and then examining if the upper level be truly horizontal. If not, direct the telescope to a distant and elevated object, and read the degrees on the vertical limb. Turn the vernier plate  $180^\circ$ , reverse the telescope, direct it a second time to the same point, and read the arc on the vertical limb. The half difference of these two readings, counted from the 0 point of the limb, in the direction of the greater arc read, gives the true 0 point of the vertical limb; that is, the point at which the 0 of the vernier stands when the line of collimation is horizontal.

Suppose for example, that we had directed the telescope to a point and found the 0 of the vernier to stand at  $10^\circ$  of elevation. If we now reverse the telescope, it ought to incline at an equal angle of depression. If then we turn the whole  $180^\circ$ , and then raise the depressed end of the telescope with the thumb-screw *Z*, until it is directed to the same point as before, the 0 ought to stand at  $10^\circ$ . If it shows a less arc, the true 0 is between the 0 of the limb and the first arc read; if a greater, it is on the other side, and the difference divided by two will indicate the exact 0 point. The half difference thus found is called the *correction*. When the true 0 falls between the marked 0 and the eyeglass, the correction is to be subtracted from the arc read, for angles of elevation, and added, for angles of depression; and the reverse when it falls on the other side. The eyeglass is supposed to be over the thumb-screw *Z*, as in the plate.

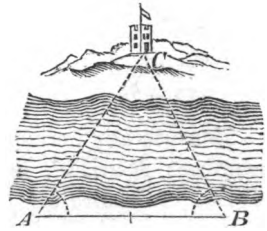
These preparatory steps being taken, let the axis of the telescope be directed to any point either above or below the plane of the limb, and read the arc indicated by the 0 of the vernier. To the arc so read apply the proper correction, if any, and the result will be the true angle of elevation or depression.

87. Having explained the preliminary principles, it only remains to apply them to the measurement of Heights and Distances.

PROBLEM I.

To determine the horizontal distance to a point which is inaccessible by reason of an intervening river.

88. Let  $C$  be the point. Measure along the bank of the river a horizontal base line  $AB$ , and select the stations  $A$  and  $B$ , in such a manner that each can be seen from the other, and the point  $C$  from both of them. Then measure the horizontal angles  $CAB$  and  $CBA$ .



Let us suppose that we have found  $AB=600$  yards,  $CAB=57^\circ 35'$  and  $CBA=64^\circ 51'$ .

$$\text{The angle } C = 180^\circ - (A+B) = 57^\circ 34'.$$

To find the distance  $BC$ .

As	$\sin C$	.	$57^\circ 34'$	.	ar. comp.	.	.	$0.073649$
:	$\sin A$	.	$57^\circ 35'$	.	.	.	.	$9.926431$
::	$AB$	.	$600$	.	.	.	.	$2.778151$
:	$BC$	.	$600.11$ yards.	.	.	.	.	$2.778231$

To find the distance  $AC$ .

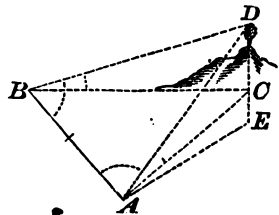
As	$\sin C$	.	$57^\circ 34'$	.	ar. comp.	.	.	$0.073649$
:	$\sin B$	.	$64^\circ 51'$	.	.	.	.	$9.956744$
::	$AB$	.	$600$	.	.	.	.	$2.778151$
:	$AC$	.	$643.94$ yards	.	.	.	.	$2.808544$

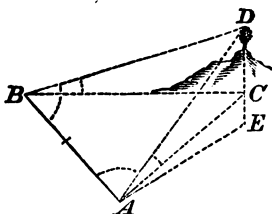
PROBLEM II.

To determine the altitude of an inaccessible object above a given horizontal plane.

FIRST METHOD.

89. Suppose  $D$  to be the inaccessible object, and  $BC$  the horizontal plane from which the altitude is to be estimated: then, if we suppose  $DC$  to be a vertical line, it will represent the required distance.





Measure any horizontal base line, as  $BA$ ; and at the extremities  $B$  and  $A$ , measure the horizontal angles  $CBA$  and  $CAB$ . Measure also, the angle of elevation  $DBC$ .

Then in the triangle  $CBA$  there will be known, two angles and the side  $AB$ ; the side  $BC$  can therefore be determined. Having found  $BC$ , we shall have, in the right-angled triangle  $DBC$ , the base  $BC$  and the angle at the base, to find the perpendicular  $DC$ , which measures the altitude of the point  $D$  above the horizontal plane  $BC$ .

Let us suppose that we have found

$BA=780$  yards, the horizontal angle  $CBA=41^{\circ} 24'$ ,  
the horizontal angle  $CAB=96^{\circ} 28'$ , and the angle of elevation  
 $DBC=10^{\circ} 43'$ .

In the triangle  $BAC$ , to find the horizontal distance  $BC$ .

The angle  $BCA=180^{\circ}-(41^{\circ} 24'+96^{\circ} 28')=42^{\circ} 08'=C$ .

As $\sin C$	. . .	$42^{\circ} 08'$	ar. comp.	. . .	. . .	0.173369
: $\sin A$	. . .	$96^{\circ} 28'$	. . .	. . .	. . .	9.997228
:: $AB$	. . .	780	. . .	. . .	. . .	<u>2.892095</u>
: $BC$	. . .	1155.29	. . .	. . .	. . .	<u>3.062692</u>

In the right-angled triangle  $DBC$ , to find  $DC$ .

As $R$	. . .	. . .	ar. comp.	. . .	. . .	0.000000
: $\tan DBC$	. . .	$10^{\circ} 43'$	. . .	. . .	. . .	9.277043
:: $BC$	. . .	1155.29	. . .	. . .	. . .	<u>3.062692</u>
: $DC$	. . .	218.64	. . .	. . .	. . .	<u>2.339735</u>

REMARK I. It might, at first, appear that the solution which we have given, requires that the points  $B$  and  $A$  should be in the same horizontal plane, but it is entirely independent of such a supposition. •

For, the horizontal distance, which is represented by  $BA$ , is the same, whether the station  $A$  is on the same level with  $B$ , above it, or below it (Art. 74). The horizontal angles  $CAB$  and  $CBA$  are also the same, so long as the point  $C$  is in the vertical line  $DC$  (Art. 75). Therefore, if the horizontal line through  $A$  should cut the vertical line  $DC$ , at any point as  $E$ , above or below  $C$ ,  $AB$  would still be the horizontal distance between  $B$  and  $A$ , and  $AE$  which is equal to  $AC$ , would be the horizontal distance between  $A$  and  $C$ .

If at  $A$ , we measure the angle of elevation of the point  $D$ , we shall know in the right angled  $DAE$ , the base  $AE$ , and the angle at the base ; from which the perpendicular  $DE$  can be determined.

Let us suppose that we had measured the angle of elevation  $DAE$ , and found it equal to  $20^{\circ} 15'$ .

First: In the triangle  $BAC$ , to find  $AC$  or its equal  $AE$ .

As $\sin C$	. . .	$42^{\circ} 08'$	ar. comp.	. . .	$0.173369$
: $\sin B$	. . .	$41^{\circ} 24'$	. . .	. . .	$9.820406$
:: $AB$	. . .	$780$	. . .	. . .	$2.892095$
: $AC$	. . .	$768.9$	. . .	. . .	<u><math>2.885870</math></u>

In the right-angled triangle  $DAE$ , to find  $DE$ .

As $R$	. . .		ar. comp.	. . .	$0.000000$
: $\tan A$	. . .	$20^{\circ} 15'$	. . .	. . .	$9.566932$
:: $AE$	. . .	$768.9$	. . .	. . .	$2.885870$
: $DE$	. . .	$283.66$	. . .	. . .	<u><math>2.452802</math></u>

Now, since  $DC$  is less than  $DE$ , it follows that the station  $B$  is above the station  $A$ . That is,

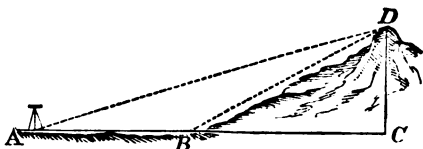
$$DE - DC = 283.66 - 218.64 = 65.02 = EC,$$

which expresses the vertical distance that the station  $B$  is above the station  $A$ .

**REMARK II.** It should be remembered, that the vertical distance which is obtained by the calculation, is estimated from a horizontal line passing through the eye at the time of observation. Hence, the height of the instrument is to be added, in order to obtain the true result.

## SECOND METHOD.

90. When the nature of the ground will admit of it, measure a base line  $AB$  in the direction of the object  $D$ . To do this, it will be well to place the theodolite at  $A$ , and range the chain staves by means of the upper telescope. Having measured the base, measure with the instrument the angles of elevation at  $A$  and  $B$ .



Then, since the outward angle  $DBC$  is equal to the sum of the angles  $A$  and  $ADB$ , it follows, that the angle  $ADB$  is equal to the difference of the angles of elevation at  $A$  and  $B$ . Hence, we can find all the parts of the triangle  $ADB$ . Having found  $DB$ , and knowing the angle  $DBC$ , we can find the altitude  $DC$ .

This method supposes that the stations  $A$  and  $B$  are on the same horizontal plane; and therefore can only be used when the line  $AB$  is nearly horizontal.

Let us suppose that we have measured the base line, and the two angles of elevation, and

$$\text{found } \begin{cases} AB = 975 \text{ yards} \\ A = 15^\circ 36' \\ DBC = 27^\circ 29'; \end{cases}$$

required the altitude  $DC$ .

$$\text{First: } ADB = DBC - A = 27^\circ 29' - 15^\circ 36' = 11^\circ 53'.$$

In the triangle  $ADB$ , to find  $BD$ .

As	$\sin D$	$11^\circ 53'$	ar. comp.		0.686302
:	$\sin A$	$15^\circ 36'$			9.429623
::	$AB$	975			2.989005
:	$DB$	1273.3			<u>3.104930</u>

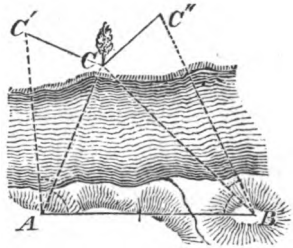
In the triangle  $DBC$ , to find  $DC$ .

As	$R$		ar. comp.		0.000000
:	$\sin B$	$27^\circ 29'$			9.664163
::	$DB$	1273.3			3.104930
:	$DC$	587.61			<u>2.769093</u>

PROBLEM III.

To determine the perpendicular distance of an object below a given horizontal plane.

91. Suppose  $C$  to be directly over the given object, and  $A$  the point through which the horizontal plane is supposed to pass.



Measure a horizontal base line  $AB$ , and at the stations  $A$  and  $B$  conceive the two horizontal lines  $AC, BC$ , to be drawn. The oblique lines from  $A$  and  $B$  to the object will be the hypotenuses of two right-angled triangles, of which  $AC, BC$ , are the bases. The perpendiculars of these triangles will be the distances from the horizontal lines  $AC, BC$ , to the object. If we turn the triangles about their bases  $AC, BC$ , until they become horizontal, the object, in the first case, will fall at  $C'$ , and in the second at  $C''$ .

Measure the horizontal angles  $CAB, CBA$ , and also the angles of depression  $C'AC, C''BC$ .

Let us suppose that we have

$$\text{found } \begin{cases} AB = 672 \text{ yards} \\ \angle BAC = 72^\circ 29' \\ \angle ABC = 39^\circ 20' \\ \angle C'AC = 27^\circ 49' \\ \angle C''BC = 19^\circ 10' \end{cases}$$

First: In the triangle  $ABC$ , the horizontal angle  $\angle ACB = 180^\circ - (\angle A + \angle B) = 180^\circ - 111^\circ 49' = 68^\circ 11'$ .

To find the horizontal distance  $AC$ .

As	$\sin C$	. $68^\circ 11'$	. ar. comp.	. . .	0.032275
:	$\sin B$	. $39^\circ 20'$	. . . . .	. . .	9.801973
::	$AB$	. 672	. . . . .	. . .	2.827369
:	$AC$	. 458.79	. . . . .	. . .	<u>2.661617</u>

To find the horizontal distance  $BC$ .

As	$\sin C$	. $68^\circ 11'$	. ar. comp.	. . .	0.032275
:	$\sin A$	. $72^\circ 29'$	. . . . .	. . .	9.979380
::	$AB$	. 672	. . . . .	. . .	2.827369
.	$BC$	. 690.28	. . . . .	. . .	<u>2.839024</u>

In the triangle  $CAC'$ , to find  $CC'$ .

As	$R$	.	.	ar. comp.	.	0.000000
:	$\tan C'AC$	.	$27^\circ 49'$	.	.	9.722315
::	$AC$	.	458.79	.	.	<u>2.661617</u>
:	$CC'$	.	242.06	.	.	<u>2.383932</u>

In the triangle  $CBC''$ , to find  $CC''$ .

As	$R$	.	.	ar. comp.	.	0.000000
:	$\tan C''BC$	.	$19^\circ 10'$	.	.	9.541061
::	$BC$	.	690.28	.	.	<u>2.839024</u>
:	$CC''$	.	239.93	.	.	<u>2.380085</u>

Hence also,  $CC' - CC'' = 242.06 - 239.93 = 2.13$  yards; which is the height of the station  $A$  above station  $B$ .

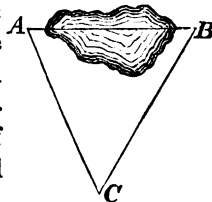
REMARK. In measuring a base line, if great accuracy is required, the theodolite should be placed at one extremity, and the telescope directed to the other, and the alignment of the staves made by means of the intersection of the spider's lines. If the highest degree of accuracy is necessary, the base line should be measured with rods, which admit of being adjusted to a horizontal position by means of a spirit level.

APPLICATIONS.

1. Wanting to know the distance between two inaccessible objects, which lie in a direct line from the bottom of a tower of 120 feet in height, the angles of depression are measured, and are found to be, of the nearest  $57^\circ$ , of the most remote  $25^\circ 30'$ : required the distance between them.

*Ans.* 173.656 feet.

2. In order to find the distance between two trees  $A$  and  $B$ , which could not be directly measured because of a pool which occupied the intermediate space, the distances of a third point  $C$  from each of them were measured, and also the included angle  $ACB$ : it was found that



$$CB = 672 \text{ yards}$$

$$CA = 588 \text{ yards}$$

$$\angle ACB = 55^\circ 40';$$

required the distance  $AB$ .

*Ans.* 592.967 yards.

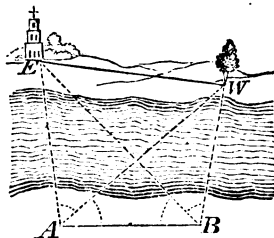
3. Being on a horizontal plane, and wanting to ascertain the height of a tower, standing on the top of an inaccessible hill, there were measured, the angle of elevation of the top of the hill  $40^\circ$ , and of the top of the tower  $51^\circ$ ; then measuring in a direct line 180 feet farther from the hill, the angle of elevation of the top of the tower was  $33^\circ 45'$ ; required the height of the tower.

*Ans.* 83.998 feet.

4. Wanting to know the horizontal distance between two inaccessible objects  $E$  and  $W$ , the following measurements were made,

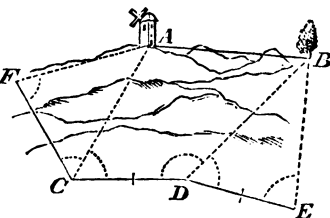
$$\text{viz. } \begin{cases} AB = 536 \text{ yards} \\ BAW = 40^\circ 16' \\ WAE = 57^\circ 40' \\ ABE = 42^\circ 22' \\ EBW = 71^\circ 07' \end{cases}$$

required the distance  $EW$ .



*Ans.* 939.527 yards.

5. Wanting to know the horizontal distance between two inaccessible objects  $A$  and  $B$ , and not finding any station from which both of them could be seen, two points  $C$  and  $D$ , were chosen, at a distance from each other, equal to 200 yards; from the former of these points  $A$  could be seen, and from the latter  $B$ , and at each of the points  $C$  and  $D$  a staff was set up. From  $C$  a distance  $CF$  was measured, not in the direction  $DC$ , equal to 200 yards, and from  $D$  a distance  $DE$  equal to 200 yards, and the following angles taken,



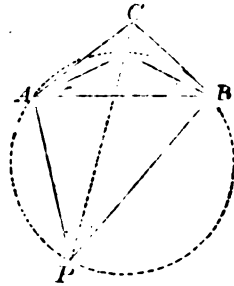
$$\text{viz. } \begin{cases} AFC = 83^\circ 00' & BDE = 54^\circ 30' \\ ACD = 53^\circ 30' & BDC = 156^\circ 25' \\ ACF = 54^\circ 31' & BED = 88^\circ 30' \end{cases}$$

*Ans.*  $AB = 345.467$  yards.



6. From a station  $P$  there can be seen three objects  $A$ ,  $B$  and  $C$ , whose distances from each other are known: viz.  $AB=800$ ,  $AC=600$ , and  $BC=400$  yards. Now, there are measured the horizontal angles

$APC=33^{\circ} 45'$  and  $BPC=22^{\circ} 30'$ : it is required to find the three distances  $PA$ ,  $PC$ , and  $PB$ .



$$\text{Ans. } \begin{cases} PA=710.193 \text{ yards.} \\ PC=1042.522 \\ PB=934.291 \end{cases}$$

#### OF MEASUREMENTS WITH THE TAPE OR CHAIN ONLY.

92. It often happens that instruments for the measurement of angles cannot be easily obtained; we must then rely entirely on the tape or chain.

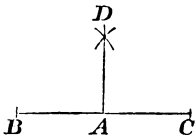
We now propose to explain the best methods of determining distances, without the aid of instruments for the measurement of horizontal or vertical angles.

#### PROBLEM I.

*To trace, on the ground, the direction of a right line, that shall be perpendicular at a given point, to a given right line.*

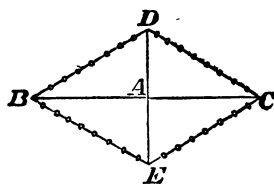
#### FIRST METHOD.

93. Let  $BC$  be the given right line, and  $A$  the given point. Measure from  $A$ , on the line  $BC$ , two equal distances  $AB$ ,  $AC$ , one on each side of the point  $A$ . Take a portion of the chain or tape, greater than  $AB$ , and place one extremity at  $B$ , and with the other trace the arc of a circle on the ground. Then remove the end which was at  $B$ , to  $C$ , and trace a second arc intersecting the former at  $D$ . The straight line drawn through  $D$  and  $A$  will be perpendicular to  $BC$  at  $A$ .



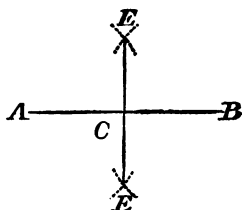
SECOND METHOD.

94. Having made  $AB=AC$ , take any portion of the tape or chain, considerably greater than the distance between  $B$  and  $C$ . Mark the middle point of it, and fasten its two extremities, the one at  $B$  and the other at  $C$ . Then, taking the chain by the middle point, stretch it tightly on either side of  $BC$ , and place a staff at  $D$  or  $E$ : then will  $DAE$  be the perpendicular required.



THIRD METHOD.

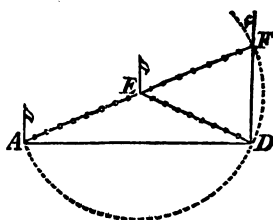
95. Let  $AB$  be the given line, and  $C$  the point at which the perpendicular is to be drawn. From the point  $C$  measure a distance  $CA$  equal to 8. With  $C$  as a centre, and a radius equal to 6, describe an arc on either side of  $AB$ : then, with  $A$  as a centre, and a radius equal to 10, describe a second arc intersecting the one before described at  $E$ : then draw the line  $EC$ , and it will be perpendicular to  $AB$  at  $C$ .



REMARK. Any three lines, having the ratio of 6, 8 and 10, form a right-angled triangle, of which the side corresponding to 10 is the hypotenuse

FOURTH METHOD.

96. Let  $AD$  be the given right line, and  $D$  the point at which the perpendicular is to be drawn. Take any distance on the tape or chain, and place one extremity at  $D$ , and fasten the other at some point as  $E$ , between the two lines which are to form the right angle. Place a staff at  $E$ . Then, having stationed a person at  $D$ , remove the extremity of the chain and carry it round until it ranges on the line  $DA$  at  $A$ . Place a staff at  $A$ : then remove the end of the



chain at  $A$ , and carry it round until it falls on the line  $AE$  at  $F$ . Then place a staff at  $F$ , and  $ADF$  will be a right angle, being an angle in a semi-circle.

97. There is a very simple instrument, used exclusively in laying off right angles on the ground, which is called the

#### SURVEYING CROSS.

Pl. 2. Fig. 1. This instrument consists of two bars,  $AB$  and  $CD$ , permanently fixed at right angles to each other, and firmly attached at  $E$  to a pointed staff, which serves as a support. Four sights are screwed firmly to the bars, by means of the screws  $a$ ,  $b$ ,  $c$ , and  $d$ .

As the only use of this instrument is to lay off right angles, it is of the first importance that the lines of sight be truly at right angles. To ascertain if they are so, let the bar  $AB$  be turned until its sights mark some distinct object; then look through the other sights and place a staff on the line which they indicate: let the cross be then turned until the sights of the bar  $AB$  come to the same line: if the other sights are directed to the first object, the lines of sight are exactly at right angles.

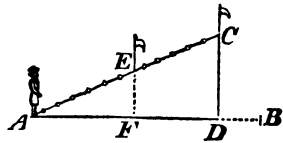
The sights being at right angles, if one of them be turned in the direction of a given line, the other will mark the direction of a line perpendicular to it, at the point where the instrument is placed.

#### PROBLEM II.

*From a given point without a straight line, to let fall a perpendicular on the line.*

98. Let  $C$  be the given point, and  $AB$  the given line.

From  $C$  measure a line, as  $CA$ , to any point of the line  $AB$ . From  $A$ , measure on  $AB$  any distance as  $AF$ , and at  $F$  erect  $FE$  perpendicular to  $AB$ .



Having stationed a person at  $A$ , measure along the perpendicular  $FE$  until the forward staff is aligned on the line  $AC$ : then measure the distance  $AE$ . Now, by similar triangles, we have

$$AE : AF :: AC : AD$$

in which all the terms are known except  $AD$ , which may, therefore, be considered as found. The distance  $AD$  being laid off from  $A$ , the point  $D$ , at which the perpendicular  $CD$  meets  $AB$ , becomes known. If we wish the length of the perpendicular, we use the proportion

$$AE : EF :: AC : CD,$$

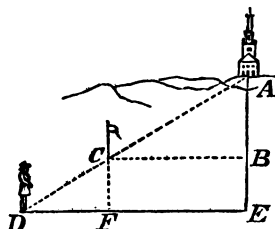
in which all the terms are known, excepting  $CD$ : therefore,  $CD$  is determined.

PROBLEM III.

To determine the horizontal distance from a given point to an inaccessible object.

99. Let  $A$  be an inaccessible object, and  $E$  the point from which the distance is to be measured.

At  $E$  lay off the right angle  $AED$ , and measure in the direction  $ED$ , any convenient distance to  $D$ , and place a staff at  $D$ . Then measure from  $E$ , directly towards the object



$A$ , a distance  $EB$  of a convenient length, and at  $B$  lay off a line  $BC$  perpendicular to  $EA$ . Measure along the line  $BC$ , until a person at  $D$  shall range the forward staff on the line  $DA$ . Now,  $DF$  is known, being equal to the difference between the two measured lines  $DE$  and  $CB$ . Hence, by similar triangles,

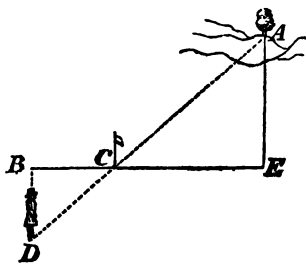
$$DF : FC :: DE : EA,$$

in which proportion all the terms are known, except the fourth, which may, therefore, be regarded as found: hence,  $EA$  is determined.

SECOND METHOD.

100. At the point  $E$  lay off  $EB$  perpendicular to the line  $EA$ , and measure along it any convenient distance, as  $EB$ .

At  $B$  lay off the right angle  $EBD$ , and measure any distance in the direction  $BD$ . Let a person at  $D$  align a staff on  $DA$ ,



while a second person at  $B$  aligns it on  $BE$ : the staff will thus be fixed at  $C$ . Then measure the distance  $BC$ .

The two triangles  $BCD$  and  $CAE$  being similar, we have,

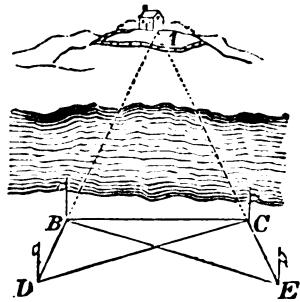
$$BC : BD :: CE : EA,$$

in which all the terms are known, except the fourth, which may, therefore, be regarded as found.

### THIRD METHOD.

101. Let  $B$  be the given point, and  $A$  the inaccessible object, it is required to find  $BA$ .

Measure any horizontal base line, as  $BC$ . Then, having placed staves at  $B$  and  $C$ , measure any convenient distances  $BD$  and  $CE$ , such that the points  $D, B$  and  $A$ , shall be in the same right line, as also, the points  $E, C$  and  $A$ ; then measure the diagonal lines  $DC$  and  $EB$ .



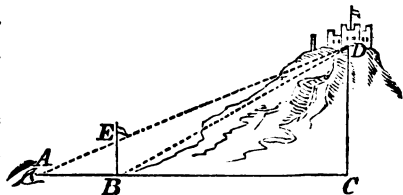
Now, in the triangle  $BEC$ , the three sides are known, therefore, the angle  $ECB$  can be found. In the triangle  $CDB$ , the three sides are also known, therefore the angle  $CBD$  can be determined. These angles being respectively subtracted from  $180^\circ$ , the two angles  $ACB$  and  $ABC$  become known; and hence, in the triangle  $ABC$ , we have two angles and the included side, to find the side  $BA$ .

### PROBLEM IV.

To find the altitude of an object, when the distance to the vertical line passing through the top of it is known.

102. Let  $CD$  be the altitude required, and  $AC$  the known distance.

From  $A$ , measure on the line  $AC$ , any convenient distance  $AB$ , and place a staff vertically at  $B$ . Then placing the eye at  $A$ , sight to



the object  $D$ , and let the point, at which the line  $AD$  cuts the staff  $BE$ , be marked. Measure the distance  $BE$  on the staff; then say,

$$\text{As } AB : BE :: AC : CD,$$

then,  $CD$  becomes known.

If the line  $AC$  cannot be measured, on account of intervening objects, it may be determined by calculation, as in the last problem, and then, having found the horizontal distance, the vertical line is readily determined, as before.

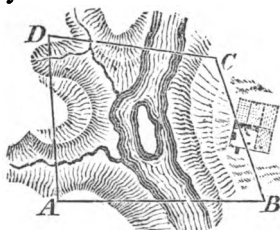
### CHAPTER III.

#### *Of the area or content of ground.—Of laying out and dividing land.*

103. We come next to the determination of the area or content of ground.

The surface of the ground being, in general, broken and uneven, it is impossible, without great trouble and expense, to ascertain its exact area or content. To avoid this inconvenience, it has been agreed to refer every surface to a horizontal plane: that is, to regard all its bounding lines as horizontal, and its area as measured by that portion of the horizontal plane which the boundary lines enclose.

For example, if  $ABCD$  were a piece of ground having an uneven surface, we should refer the whole to a horizontal plane, and take for the measure of the area that part of the plane which is included between the bounding lines  $AB$ ,  $BC$ ,  $CD$ ,  $DA$ .



In estimating land in this manner, the sum of the areas of all the parts into which a tract may be divided, is equal to the area estimating it as an entire piece: but this would not be the case if the areas of the parts had reference to the actual surface, and the area of the whole were calculated from its bounding lines

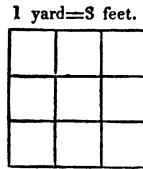
104. The *unit* of a quantity is one of the equal parts of which the quantity is composed (*Arith. In. VI*). Thus, a line of three feet in length is made up of three single feet, and of this line, 1 foot is the unit. The unit of a line may be 1 foot, 1 yard, 1 rod, 1 chain, or any other known distance.

If, on the unit of length, a square be described, it will form the unit for computing areas.

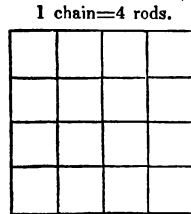
Thus, is 1 square foot, . . . .



1 square yard, or 9 square feet, .



1 square chain, or 16 square rods. .



Thus it is seen that there are two kinds of quantity to be considered, viz. lines, and areas or surfaces; and each kind has its own unit of measure.

When, therefore, the linear measures of ground are feet, yards, rods, or chains, the superficial measures will be square feet, square yards, square rods, or square chains; and the number expressing the area will be nothing else than the number of times which the unit of superficial measure is contained in the land measured.

It has been already observed (*Art. 83*), that Gunter's chain of four rods or 66 feet in length, and which is divided into 100 links, is the chain in general use among surveyors. We shall, therefore, take the length of this chain for the unit of linear measure.

105. An *acre* is a surface equal in extent to 10 square chains; that is, equal to a rectangle of which one side is ten chains, and the other side one chain.

One-quarter of an acre, is called a *rood*.

Since the chain is 4 rods in length, 1 square chain contains 16 square rods; and therefore, an acre, which is 10 square chains, contains 160 square rods, and a rood contains 40 square rods. The square rods are called *perches*.

106. Land is generally computed in acres, roods, and perches, which are respectively designated by the letters *A. R. P.*

When the linear dimensions of a survey are chains or links, the area will be expressed in square chains or square links, and it is necessary to form a rule for reducing this area to acres, roods, and perches. For this purpose, let us form the following

TABLE.

1 square chain	=	10000 square links.
1 acre	=	10 square chains = 100000 square links.
1 acre	=	4 roods = 160 perches.
1 square mile	=	6400 square chains = 640 acres.

Now, when the linear dimensions are links, the area will be expressed in square links, and may be reduced to acres by dividing by 100000, the number of square links in an acre: that is, by pointing off five decimal places from the right hand.

If the decimal part be then multiplied by 4, and five places of decimals pointed off from the right hand, the figures to the left will express the roods.

If the decimal part of this result be now multiplied by 40, and five places for decimals pointed off, as before, the figures to the left will express the perches.

If one of the dimensions be in links, and the other in chains, the chains may be reduced to links by annexing two ciphers: or, the multiplication may be made without annexing the ciphers, and the product reduced to acres and decimals of an acre, by pointing off three decimal places at the right hand.

When both the dimensions are in chains, the product is reduced to acres by dividing by 10, or pointing off one decimal place



From which we conclude ; that,

1st. *If links be multiplied by links, the product is reduced to acres by pointing off five decimal places from the right hand.*

2d. *If chains be multiplied by links, the product is reduced to acres by pointing off three decimal places from the right hand.*

3d. *If chains be multiplied by chains, the product is reduced to acres by pointing off one decimal place from the right hand.*

107. Since there are 16.5 feet in a rod, a square rod is equal to  $16.5 \times 16.5 = 272.25$  square feet.

If the last number be multiplied by 160, we shall have

$$272.25 \times 160 = 43560 = \text{the square feet in an acre.}$$

Since there are 9 square feet in a square yard, if the last number be divided by 9, we obtain

$$4840 = \text{the number of square yards in an acre.}$$

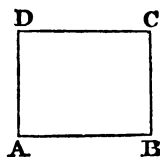
#### PROBLEM I.

108. To find the area of a square or rectangular piece of ground.

*Multiply the two sides together, and the product will express the area (Geom. Bk. IV, Prop. IV).*

1. To find the area of the rectangular field  $ABCD$ .

Measure the two sides  $AB, BC$ : let us suppose that we have found  $AB = 14$  chains 27 links, and  $BC = 9$  chains 75 links. Then,



$$AB = 1427 \text{ links,}$$

$$BC = 975 \text{ links,}$$

$$AB \times BC = 1391325 \text{ square links,}$$

$$= 13.91325 \text{ acres.}$$

$$\begin{array}{r} 4 \\ \hline 3.65300 \text{ rods,} \end{array}$$

$$\begin{array}{r} 40 \\ \hline 26.12000 \text{ perches.} \end{array}$$

*Ans. 13A 3R 26P.*

2. What is the area of a square field, of which the sides are each 33 ch 8 l ?

*Ans. 109A 1R 29P.*

3. What is the content of a rectangular field, of which the longest side is 49 ch 27 l, and the shorter 38 ch 7 l?

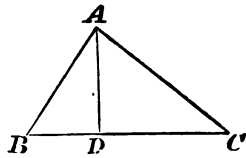
*Ans.* 187*A* 2*R* 11*P*.

PROBLEM II.

109. To find the content of a piece of land in the form of a triangle.

FIRST METHOD.

*Measure either side of the triangle as BC, and from the opposite angle A let fall a perpendicular AD, and measure this perpendicular; then, multiply the base and perpendicular together, and divide the product by 2, the result will express the area of the triangle. Or, the area is equal to the base multiplied by half the perpendicular, or to the perpendicular multiplied by half the base (Geom. Bk. IV, Prop. II).*



1. What is the content of a triangle whose base is 25 ch 1 l, and perpendicular 18 ch 14 l?

*Ans.* 22*A* 2*R* 29*P*.

2. What is the content of a triangle whose base is 15.48 chains, and altitude 9.67 chains?

*Ans.* 7*A* 1*R* 38*P*

SECOND METHOD.

*Measure two sides and their included angle. Then, add together the logarithms of the two sides and the logarithmic sine of their included angle; from this sum subtract the logarithm of the radius, which is 10, and the remainder will be the logarithm of double the area of the triangle. Find, from the table, the number answering to this logarithm, and divide it by 2; the quotient will be the required area (Geom. Mens. Prob. II).*

1. In a triangle *ABC*, suppose that we have found *AB* = 57.65 ch, *AC* = 125.81 ch, and the included angle *CAB* = 57° 25': required the area.

Let the required area be designated by  $Q$ : then

$$\log 2Q = \begin{cases} +\log AB \ 57.65 & . & . & 1.760799 \\ +\log AC \ 125.81 & . & . & 2.099715 \\ +\log \sin A \ 57^\circ 25' & . & . & 9.925626 \\ -\log R & . & . & 10 \\ \hline 2Q & . & . & 6111.4 & . & . & \underline{3.786140} \end{cases}$$

And  $Q = 3055.7$  square chains.

*Ans. 305.A 2R 11P.*

**REMARK.** In this example, the links are treated as decimal parts of the chain; the result, therefore, is in square chains and decimal parts of a square chain.

2. What is the area of a triangle whose sides are 30 and 40 chains, and their included angle  $28^\circ 57'$ ?

*Ans. 29.A 0R 7P.*

#### THIRD METHOD.

*Measure the three sides of the triangle. Then, add them together and take half their sum. From this half sum subtract each side separately. Then, multiply the half sum and the three remainders together, and extract the square root of the product: the result will be the area (Geom. Mens. Prob. II).*

*Or, after having obtained the three remainders, add together the logarithm of the half sum and the logarithms of the respective remainders, and divide their sum by 2: the quotient will be the logarithm of the area.*

1. Find the area of a triangular piece of ground whose sides are 20, 30, and 40 chains.

#### FIRST METHOD.

$$\begin{array}{r} 20 \qquad \qquad 45 \qquad \qquad 45 \qquad \qquad 45 \\ 30 \qquad \qquad -20 \qquad \qquad -30 \qquad \qquad -40 \\ \hline 40 \qquad \qquad 25 \text{ 1st rem.} \qquad \qquad 15 \text{ 2d rem.} \qquad \qquad 5 \text{ 3d rem.} \\ 2 \overline{)90} \end{array}$$

$45 =$  half sum. Then,

$$45 \times 25 \times 15 \times 5 = 84375 : \text{ and } \sqrt{84375} = 290.4737 = \text{the area.}$$

*Ans. 29.A 0R 8P.*

2. What is the area of a triangle whose sides are 2569, 4900, and 5035 links?

SECOND METHOD.

2569	6252	6252	6252
4900	-2569	-4900	-5035
5035	<u>3683</u> 1st rem.	<u>1352</u> 2d rem.	<u>1217</u> 3d rem.

2) 12504  
6252 = half sum.

	log 6252	.	.	3.796019
Then,	log 3683	.	.	3.566202
	log 1352	.	.	3.130977
	log 1217	.	.	3.085291

2) 13.578489

Area in square links, 6155225 . . . 6.789244

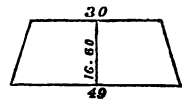
*Ans.* 61A 2R 8P.

PROBLEM III.

110. To find the area of a piece of land in the form of a trapezoid.

*Measure the two parallel sides, and also the perpendicular distance between them. Add the two parallel sides together, and take half the sum; then multiply the half sum by the perpendicular, and the product will be the area (Geom. Bk. IV. Prop. VII).*

1. What is the area of a trapezoid, of which the parallel sides are 30 and 49 chains, and the perpendicular distance between them 16 ch 60 l, or 16.60 chains?



30 + 49 = 79; dividing by 2, gives . . . 39.5  
 multiply by . . . . . 16.60  
 gives for the area in square chains, . . . 655.700

*Ans.* 65A 2R 11P.

2. Required the content, when the parallel sides are 20 and 32 ch, and the perpendicular distance between them 26 ch.

*Ans.* 67A 2R 16P.

PROBLEM IV.

111. To find the area of a piece of land in the form of a quadrilateral.

*Measure the four sides of the quadrilateral, and also one of the diagonals: the quadrilateral will thus be divided into*

two triangles, in both of which all the sides will be known. Then, find the areas of the triangles separately, and their sum will be the area of the quadrilateral.

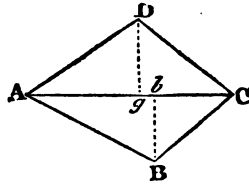
1. Suppose that we have measured the sides and diagonal  $AC$ , of the quadrilateral  $ABCD$ , and found

$$AB=40.05 \text{ ch, } CD=29.87 \text{ ch,}$$

$$BC=26.27 \text{ ch, } AD=37.07 \text{ ch,}$$

and  $AC=55 \text{ ch}$  :

required the area of the quadrilateral.



*Ans.* 101A 1R 15P.

**REMARK.** Instead of measuring the four sides of the quadrilateral, we may let fall the perpendiculars  $Bb$ ,  $Dg$ , on the diagonal  $AC$ . The area of the triangle may then be determined by measuring these perpendiculars and the diagonal  $AC$ . The perpendiculars are  $Dg=18.95 \text{ ch}$ , and  $Bb=17.92 \text{ ch}$ .

**PROBLEM V.**

112. To find the content of a field having any number of sides.

*Measure the sides of the field and also the diagonals : the three sides of each of the triangles into which the field will be thus divided will then be known, and the areas of the triangles may then be calculated by the preceding rules. Or, measure the diagonals, and from the angular points of the field draw perpendiculars to the diagonals and measure their lengths : the base and perpendicular of each of the triangles will then be known.*

1. Let it be required to determine the content of the field  $ABCDE$ , having five sides.

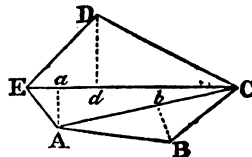
Let us suppose that we have measured the diagonals and perpendiculars, and found

$$AC=36.21 \text{ ch, } EC=39.11 \text{ ch,}$$

$$Bb=4.08 \text{ ch, } Dd=7.26 \text{ ch, } Aa=$$

$$4.19 \text{ ch ; also } Ea=4.00 \text{ ch, } Ed=13.60 \text{ ch, } Ab=20.30 \text{ ch :}$$

required the area of the field.



Area of triangle $ABC = 73.8684$	square chains
area of " $CDE = 141.9693$	" "
area of " $ACE = 81.7399$	" "
area of $ABCDE = \underline{297.5776}$	" "

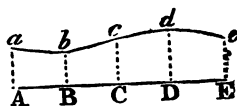
*Ans.* 29A 3R 12P

PROBLEM VI.

113. To find the content of a long and irregular figure, bounded on one side by a straight line.

Suppose the ground, of which the content is required, to be of the form  $ABEeda$ , bounded on one side by the right line  $AE$ , and on the other by the curve  $edca$ .

At  $A$  and  $E$ , the extremities of the right line  $AE$ , erect the two perpendiculars  $Aa$ ,  $Ee$ , and on each of them measure the breadth of the land. Then divide the base into any convenient number of equal parts and measure the breadth of the land at each point of division.



*Add together the intermediate breadths and half the sum of the two extreme ones: then multiply this sum by one of the equal parts of the base line, and the product will be the required area very nearly (Mens. Prob. VI).*

1. The breadths of an irregular figure, at five equidistant places, being 8.20 ch, 7.40 ch, 9.20 ch, 10.20 ch, and 8.60 chains, and the whole length 40 chains, required the area.

8.20		4)40	
8.60		<u>10</u>	one of the equal parts.
2)16.80			
<u>8.40</u>	mean of the extremes	35.20	sum
7.40		<u>10</u>	
9.20		area <u>352.00</u>	square ch.
10.20			
<u>35.20</u>	sum		

*Ans.* 35A 2R.

2. The length of an irregular piece of land being 21 ch, and the breadths, at six equidistant points, being 4.35 ch,

5.15 ch, 3.55 ch, 4.12 ch, 5.02 ch, and 6.10 chains : required the area.

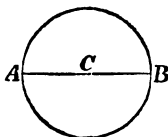
*Ans.* 9A 2R 30P.

**REMARK.** If it is not convenient to erect the perpendiculars at equal distances from each other, the areas of the trapezoids, into which the whole figure is divided, must be computed separately ; their sum will be the required area.

**PROBLEM VII.**

114. To find the area of a piece of ground in the form of a circle.

*Measure the radius AC : then multiply the square of the radius by 3.1416 (Mens. Prob. X).*



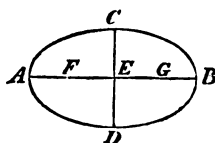
1. To find the area of a circular piece of land, of which the diameter is 25 ch.

*Ans.* 49A 0R 14P.

**PROBLEM VIII.**

115. To find the content of a piece of ground in the form of an ellipsis.

*Measure the semi-axes AE, CE. Then multiply them together, and their product by 3.1416.*



1. To find the area of an elliptical piece of ground, of which the transverse axis is 16.08 ch, and the conjugate axis 9.72 ch.

*Ans.* 12A 1R 4P.

**REMARK I.** The following is the manner of tracing an ellipse on the ground, when the two axes are known.

From C, one of the extremities of the conjugate axis as a centre, and AE half the transverse axis as a radius, describe the arc of a circle cutting AB in the two points F and G : these points are called the foci of the ellipse.

Then, take a tape, the length of which is equal to  $AB$ , and fasten the two ends, one at the focus  $F$ , the other at the focus  $G$ . Place a pin against the tape and move it around, keeping the tape tightly stretched: the extremity of the pin will trace the curve of the ellipse.

**REMARK II.** In determining the content of ground, in the examples which have been given, the linear dimensions have been taken in chains and decimals of a chain.

If the linear dimensions were taken in terms of any other unit, they may be readily reduced to chains. For, a chain is equal to 4 rods, equal to 22 yards, equal to 66 feet. Hence,

1st. *Rods may be reduced to chains and the decimal of a chain, by dividing by 4.*

2d. *Yards may be reduced to chains and the decimal of a chain, by dividing by 22.*

3d. *Feet may be reduced to chains and the decimal of a chain, by dividing by 66.*

**REMARK III.** If it is thought best to calculate the area, without reducing the linear dimensions to chains, the result can be reduced to acres.

1st. *By dividing it by 160 when it is in square rods (Art. 107).*

2d. *By dividing it by 4840 when it is in square yards (Art. 107).*

3d. *By dividing it by 43560 when it is in square feet (Art. 107).*

#### OF LAYING OUT AND DIVIDING LAND.

116. The surveyor is often required to lay off a given quantity of land, in such a way that its bounding lines shall form a particular figure, viz., a square, a rectangle, a triangle, &c. He is also often called upon to divide given pieces of land into parts containing given areas, or bearing certain relations with each other.

The manner of making such divisions must always depend on a judicious application of the principles of geometry to the particular case.



If, for example, it were required to lay out an acre of ground in a square form, it would first be necessary to find, by calculation, the side of such a square, and then to trace, on the ground, four equal lines at right angles to each other.

## PROBLEM I.

117. To lay out a given quantity of land in a square form.

*Reduce the given area to square chains, or square rods: then extract the square root, and the result will be the side of the required square. This square being described on the ground, will be the figure required.*

1. To trace a square which shall contain  $15A\ 0R\ 12P$

First, .  $15A = 60R = 2400P$

Add . . .  $12P$ ; hence,

$15A\ 0R\ 12P = \underline{2412P}$ ; the square root of

which is 49.11.

Therefore, if a square be traced on the ground, of which the side is 49.11 rods, it will be the required figure.

2. To trace a square which shall contain  $176A\ 1R\ 24P$ .

First, .  $176A = 1760$  square chains,

$1R = 2.5$  " "

$24P = 1.5$  " " ; hence,

$176A\ 1R\ 24P = 1764$  square chains: the square root of which is 42. Hence, if a square be traced on the ground, of which the side is 42 ch, it will be the required figure.

## PROBLEM II.

118. To lay out a given quantity of land in a rectangular form, having one of its sides given.

*Divide the given area, reduced to square chains or square rods, by the given side of the required rectangle, and the quotient will be the other side. Then trace the rectangle on the ground.*

1. To lay off 240 acres in a rectangular form, one of the sides being given, and equal to 80 rods.

First,  $240A = 2400$  square chains = 38400 square rods.

Then,  $80)38400(480$  rods; which is the required side of the rectangle.

119. A great number of similar problems might be proposed. The solution of them does not, however, properly belong to surveying. The laying out of the ground, and the tracing of lines, after the figure and area have been determined, are the only parts which appertain to a practical treatise. The manner of tracing lines having been already explained, it seems unnecessary to add the numerous examples often given under this head of the subject.

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## CHAPTER IV.

### *Of the Surveying Compass.—Of Surveying with the Compass.—Of the Plane-Table.*

120. Before considering the principles involved in the method of surveying now to be explained, it will be necessary to describe the instrument principally used in the field, and which is called

#### THE CIRCUMFERENTER, OR SURVEYOR'S COMPASS.

Pl. 2, Fig. 2. This instrument consists of a compass-box *DCE*, a magnetic needle, a brass plate *AB*, from twelve to fourteen inches long, two plain sights, *AF* and *BG*, one of which is more fully shown in Fig. 3; and a stand, which is sometimes a tripod, and sometimes a single staff pointed with iron at the lower end, so that it may be placed firmly in the ground.

The open sights, *AF* and *BG*, are placed at right angles to the plate *AB*, and fastened to it firmly by the screws *a* and *b*. In each sight there is a large and small aperture or slit; the larger aperture being above the smaller in one of the sights, and below it in the other. A hair or thread of silk is drawn vertically through the middle of the large aperture, as shown in Fig. 3.

The compass-box *DCE* is circular, and generally about six inches in diameter. At the centre is a small pin, on which the magnetic needle is poised. This needle, if allowed

to turn freely around the point of support, will settle to a state of rest: the direction which it then indicates, is called the *magnetic meridian*.

In the interior of the compass-box, there is a graduated circle divided to degrees, and sometimes to half degrees: the degrees are numbered from the extremities of the diameter *NS*, both ways to  $90^\circ$ .

The length of the magnetic needle is a little less than the diameter of the graduated circle, so that the needle can move freely around its centre, within the circle, and its positions be noted on the graduated arc.

The compass-box is turned about its centre, without moving the plate *AB*, by means of the milled screw *L*: it is fastened to the plate *AB*, by the screw *P*.

In using the compass, it is important to ascertain the exact angle which may be included between the magnetic meridian and the direction that may be given to the line drawn through the eye and the sights *AF* and *BG*.

To effect this, a small arc *HI* is described on the bar *AB*, having its centre at the centre of the compass-box. This arc is divided to degrees, and sometimes to the parts of a degree. A vernier is also used, which is permanently attached to the compass-box.

When the 0 point of this vernier coincides with the 0 point of the graduated arc *HI*, the line of the compass-box marked *NS*, has the same horizontal direction as the line along which the sights are directed.

Now, supposing the 0 of the vernier to coincide with the 0 of the arc *HI*, if the end of the needle does not stand at one of the lines of division of the graduated circle, let the whole degrees be read. Then, turn the compass-box by means of the screw *L*, until the needle points exactly to the line which marked the whole degrees: the space passed over by the 0 of the vernier, shows the minutes that are to be added.

#### OF SURVEYING WITH THE COMPASS.

121. The line about which the earth revolves is called its *axis*; and the two points in which the axis meets the surface of the earth are called the *poles*.

122. A meridian is a line traced on the surface of the earth, which would, if sufficiently produced in both directions, pass through the poles. Hence, all the meridian lines intersect each other at the two poles.

The poles, however, are so distant from each other, that no sensible error will arise in supposing the meridians to be parallel; and since, in all the surveys made with the compass, the surface of the ground is regarded as a horizontal plane, the meridians are represented by horizontal and parallel lines.

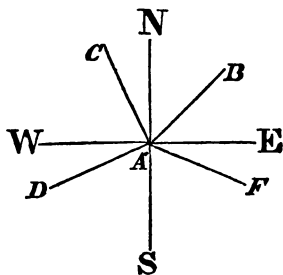
123. When the compass is placed on its stand, and the needle is allowed to settle to a state of rest, the direction it assumes has been named the *magnetic meridian*. Although this line is different from the true meridian, yet in the surveys made with the compass, we shall take for the meridian that line which is determined by the direction of the magnetic needle.

124. If the right hand be turned towards the point where the sun rises, the direction pointed by the farthest end of the needle is called *north*; the direction shown by the nearest end is called *south*, and the line thus indicated is called a north and south line, as well as a meridian.

125. A line perpendicular to the meridian is called an *east* and *west* line: the east point being on the right hand, and the west on the left.

126. A line traced or measured on the ground, is called a *course*; and the angle which this line makes with the meridian passing through the point of beginning, is called the *bearing*.

Thus, if we start from the point *A*, and measure in the direction *AB*, the line *AB* is the course, and the angle  $\angle NAB$  is the bearing.

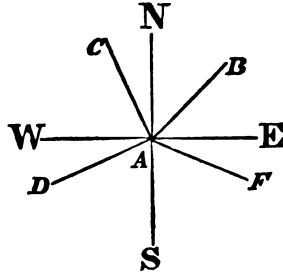


When the course, like *AB*, falls between the north and east points, the bearing is read, north  $46^\circ$  east, and is written, N  $46^\circ$  E.

When the course, like  $AC$ , falls between the north and west points, the bearing is read, north  $30^\circ$  west, and is written, N  $30^\circ$  W.

When the course, like  $AF$ , falls between the south and east points, the bearing is read, south  $70^\circ$  east, and is written, S  $70^\circ$  E.

When the course, like  $AD$ , falls between the south and west points, the bearing is read, south  $70^\circ$  west, and is written, S  $70^\circ$  W.

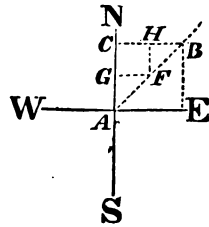


A course which runs due north, or due south, is designated by the letter N or S: and one which runs due east, or due west, by the letter E or W.

127. If, after having passed over a course, the bearing be taken to the back station, this bearing is called the *back sight*, or *reverse bearing*.

128. The perpendicular distance between the east and west lines, drawn through the extremities of a course, is called the *northing* or *southing*, according as the course is run towards the north or south. This distance is also called the *difference of latitude*, or simply the *latitude*, because it shows the distance which one of the points is north or south of the other.

Thus, in running the course from  $A$  to  $B$ ,  $AC$  is the difference of latitude, north.



129. The perpendicular distance between the meridians passing through the extremities of a course, is called the *departure* of that course, and is east or west, according as the course lies on the east or west side of the meridian passing through the point of beginning.

Thus, in running the course  $AB$ ,  $CB$  is the departure, east.

130. It will be found convenient, in explaining the rules for surveying with the compass, to attribute to the latitudes and departures the algebraic signs,  $+$  and  $-$ ; which are read plus and minus.

We shall, therefore, consider every northing as affected

with the sign  $+$ , and every southing as affected with the sign  $-$ . We shall also consider every easting as affected with the sign  $+$ , and every westing as affected with the sign  $-$ .

131. The meridian distance of a point is the perpendicular let fall on the meridian, from which the distance is estimated. This meridian is called the *assumed meridian*. Thus, if the distance be estimated from  $NS$ ,  $BC$  will be the meridian distance of the point  $B$ .

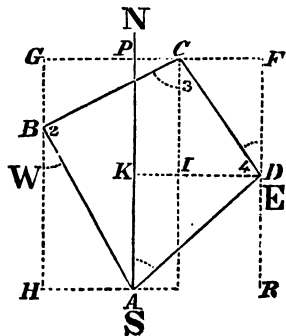
132. The meridian distance of a line, is the distance of the middle point of that line from an assumed meridian: and is east or west, according as this point lies on the east or west side of the assumed meridian. Thus,  $FG$  drawn through the middle point of  $AB$ , is the meridian distance of the line  $AB$ .

The sign  $+$  will always be given to the meridian distance of a point or line, when it lies on the east of the assumed meridian, and the sign  $-$ , when it lies on the west.

133. When a piece of ground is to be surveyed, we begin at some prominent corner of the field, and go entirely around the land, measuring the lengths of the bounding lines with the chain, and taking their bearings with the compass. It is not material whether the ground be kept on the right hand or on the left, and all the rules deduced for one of the cases, are equally applicable to the other. To preserve, however, an uniformity in the language of the rules, we shall suppose the land to be always kept on the right hand of the surveyor.

Let  $ABCD$  be a piece of ground to be surveyed,  $A$  the point where the work is to be begun, and  $NS$  a meridian.

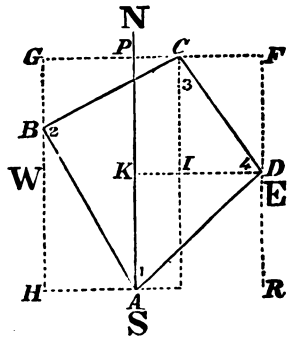
On a sheet of paper, rule three columns, as in next page, and head them stations, bearings, distances.



FIELD NOTES.

Stations.	Bearings.	Distances.
1	N $31\frac{1}{2}^{\circ}$ W	10.
2	N $62\frac{3}{4}^{\circ}$ E	9.25
3	S $36^{\circ}$ E	7.60
4	S $45\frac{1}{2}^{\circ}$ W	10.40

Place the compass at *A* and take the bearing to *B*, which is *PAB*: suppose this angle has been found to be  $31\frac{1}{2}^{\circ}$ . The bearing from *A* to *B* is then N  $31\frac{1}{2}^{\circ}$  W. Enter this bearing in the field notes opposite station 1. Then measure the distance from *A* to *B*, which we will suppose to be 10 ch, and insert that distance opposite station 1, in the column of distances.



We next take the bearing from *B* to *C*, N  $62\frac{3}{4}^{\circ}$  E, and then measure the distance *BC*=9 ch 25 l, both of which we insert in the notes opposite station 2.

At station *C* we take the bearing to *D*, S  $36^{\circ}$  E, and then measure the distance *CD*=7 ch 60 l, and place them in the notes opposite station 3.

At *D* we take the bearing to *A*, S  $45\frac{1}{2}^{\circ}$  W, and then measure the distance *DA*=10 ch 40 l. We have thus made all the measurements on the field which are necessary to determine the content of the ground.

134. REMARK I. The reverse bearing, or back sight, from *B* to *A*, is the angle *ABH*; and since the meridians *NS* and *HG* are parallel, this angle is equal to the bearing *NAB*. The reverse bearing is, therefore, S  $31\frac{1}{2}^{\circ}$  E.

The reverse bearing from *C*, is S  $63\frac{3}{4}^{\circ}$  W: that is, it is the angle *ICB*=*GBC*.

And generally, a reverse bearing, or back sight, is always equal to the forward bearing, and differs from it in both of the letters by which it is designated.

135. REMARK II. In taking the bearings with the compass, there are two sources of error. 1st. The inaccuracy of the observations: 2d. Local attractions, or the derangement which the needle experiences when brought into the vicinity of iron-ore beds, or any ferruginous substances.

To guard against these sources of error, the reverse bearing should be taken at every station: if this and the forward bearing are of the same value, the work is probably right; but if they differ considerably, they should both be taken again.

136. REMARK III. In passing over the course  $AB$ , the northing is found to be  $HB$ , and the departure, which is west, is represented by  $AH$ . Of the course  $BC$ , the northing is expressed by  $BG$ , and the departure, which is east, by  $GC$ . Of the course  $CD$ , the southing is expressed by  $CI$ , and the departure, which is east, by  $CF$ . Of the course  $DA$ , the southing is expressed by  $KA$ , and the departure, which is west, by  $DK$ . It is seen from the figure, that the sum of the northings is equal to  $HB+BG=HG$ ; and that the sum of the southings is equal to  $CI+KA=PA=HG$ : hence, the sum of the northings is equal to the sum of the southings.

If we consider the departures, it is apparent that the sum of the eastings is equal to  $GC+CF=GF$ ; and that the sum of the westings is equal to  $AH+DK=GF$ : hence also, the sum of the eastings is equal to the sum of the westings. We therefore conclude, that when any survey is correctly made, the sum of the northings will be equal to the sum of the southings, and the sum of the eastings to the sum of the westings.

It would indeed appear plain, even without a rigorous demonstration, that after having gone entirely round a piece of land, the distance passed over in the direction due north, must be equal to that passed over in the direction due south; and the distance passed over in the direction due east, equal to that passed over in the direction due west.

Having now explained the necessary operations on the field, we shall proceed to show the manner of computing the content of the ground. We shall first explain

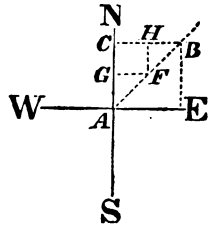


## THE TRAVERSE TABLE.

137. This table shows the difference of latitude, and the departure, corresponding to any bearing, and for courses less than 100.

Let  $AB$  denote any course,  $NS$  the meridian, and  $NAB$  the bearing of  $AB$ . Then will  $AC$  be the difference of latitude, and  $BC$  the departure.

It is evident that the course, the difference of latitude, and the departure, are respectively, the hypotenuse, the base, and the perpendicular of a right-angled triangle, of which the bearing is the angle at the base.



If there be two bearings, which are complements of each other, or of which the sum is  $90^\circ$ , the difference of latitude corresponding to the one, will be the departure of the other, and reciprocally. For, if  $BC$  were a meridian,  $CBA$  which is the complement of  $CAB$ , would be the bearing of  $BA$ ;  $CB$  would be the difference of latitude, and  $CA$  would be the departure.

In the traverse table, the figures at the top and bottom of each page, show the bearings to degrees and parts of a degree; and the columns on the left and right, the distances to which the latitudes and departures correspond.

If the bearing is less than  $45^\circ$ , the angle will be found at the top of the page; if greater, at the bottom. Then, if the distance is less than 50, it will be found in the column "distance," on the left hand page; if greater than 50, in the corresponding column of the right hand page. The table is calculated only to quarter degrees, for the bearings cannot be relied on to smaller parts of a degree.

The latitudes or departures of courses of different lengths, but which have the same bearing, will be proportional to the lengths of the courses. Thus, in the last figure, the latitudes  $AG$ ,  $AC$ , or the departures  $GF$ ,  $CB$ , are to each other as the courses  $AF$ ,  $AB$ .

Therefore, when the distance is greater than 100, it may be divided by any number which will give an exact quotient, less than 100: then the latitude and departure being

found and multiplied by the divisor, the products will be the latitude and departure of the whole course. It is also plain, that the latitude or departure of two or more courses, having the same bearing, is equal to the sum of the latitudes or departures of the courses taken separately.

Hence, if we have any number greater than 100, as 614, we have only to regard the last figure as a cipher, and recollect that,  $610 \div 4 = 614$ ; and also, that the latitude and departure of 610, are ten times greater, respectively, than the latitude and departure of 61: that is, equal to the latitude and departure of 61 multiplied by 10, or with the decimal point removed one place to the right.

1. To find the latitude and departure for the bearing  $29\frac{1}{2}^\circ$ , and the course 614.

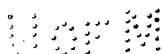
Latitude for 610 . . . 530.90	Departure for 610 . . . 300.40
Latitude for <u>4</u> . . . <u>3.48</u>	Departure for <u>4</u> . . . <u>1.97</u>
Latitude for 614 . . . <u>534.38</u>	Departure for 614 . . . <u>302.37</u>

In this example, the latitude and departure answering to the bearing  $29\frac{1}{2}^\circ$ , and to the distance 61, are first taken from the table, and the decimal point removed one place to the right: this gives the latitude and departure for the distance 610; the latitude and departure answering to the same bearing and the distance 4, are then taken from the table and added.

2. To find the latitude and departure for the bearing  $62\frac{1}{2}^\circ$ , and the course 7855 chains.

Latitude for 7800 . . . 3602.00	Departure for 7800 . . . 6919.00
Latitude for <u>55</u> . . . <u>25.40</u>	Departure for <u>55</u> . . . <u>48.79</u>
Latitude for 7855 . . . <u>3627.40</u>	Departure for 7855 . . . <u>6967.79</u>

**REMARK.** When the distances are expressed in whole numbers and decimals, the manner of finding the latitudes and departures is still the same, except in pointing off the places for decimals: but this is not difficult, when it is remembered that the column of distances in the table, may be regarded as decimals, by removing the decimal point to the left in the other columns.



3. To find the latitude and departure for the bearing  $47\frac{1}{2}^\circ$ , and the course 37.57.

Latitude for 37.00 . . .	24.88	Departure for 37.00 . . .	27.39
Latitude for 57 . . .	38	Departure for 57 . . .	42
Latitude for 37.57 . . .	<u>25.26</u>	Departure for 37.57 . . .	<u>27.81</u>

*Of Balancing the work.*

138. The use of the traverse table being explained, we can proceed to compute the area of the ground.

The field notes having been completed, rule a new table, as below, with four additional columns, two for latitude, and two for departure.

Then find, from the traverse table, the latitude and departure of each course, and enter them in the proper columns opposite the station.

Then add up the column of northings, and also the column of southings: the two sums should be equal to each other. If they are not, subtract the less from the greater, and the remainder is called the *error in latitude*. This error takes the name of that column which is the least. For example, if the sum of the northings is less than the sum of the southings, the error is called, *error in northing*: but if the sum of the southings is less than the sum of the northings, the error is called, *error in southing*. We find the error for each particular course by the following proportion.

As the sum of the courses  
Is to the error of latitude,  
So is each particular course  
To its correction.

The error of each course, thus found, may be entered in a separate column; after which, add it to the latitude of the course, when the error and latitude are of the *same name*, but subtract it, when they are of *different names*. This will make the sum of the northings equal to the sum of the southings, and is called *balancing the work*. The northings and southings, thus corrected, are entered in columns on the right, under the head, *balanced*. Having done this, balance the eastings and westings in the very same manner. The difference between their sums, is called the *error in departure*.



For an example, we will resume the same example that has already been considered.

Sta.	Bearings.	Distan- ces.	LATITUDE.		DEPARTURE.		Cor. Lat.	Cor. Dep.	BALANCED.				
			N.	S.	E.	W.			N.	S.	E.	W.	
			+	-	+	-			+	-	+	-	
1	N 31½° W	10.	8.53			5.22	+0.18	+0.02	8.71				5.24
2	N 62¼° E	9.25	4.23		8.22		+0.17	-0.01	4.40		8.21		
3	S 36° E	7.60		6.15	4.47		-0.14	-0.01		6.01	4.46		
4	S 45½° W	10.40		7.29		7.41	-0.19	+0.02		7.10			7.43
Sum of courses, 37.25			12.76	13.44	12.69	12.63			13.11	13.11	12.67	12.67	

Error in Northing, . . . 0.68 | 0.06 Error in Westing.

As 37.25 : 0.68 :: 10 : 0.18 error in lat. of 1st course.

As 37.25 : 0.68 :: 9.25 : 0.17 error in lat. of 2d course.

As 37.25 : 0.68 :: 7.60 : 0.14\* error in lat. of 3d course.

As 37.25 : 0.68 :: 10.40 : 0.19 error in lat. of 4th course.

As 37.25 : 0.06 :: 10 : 0.02\* error in dep. of 1st course.

As 37.25 : 0.06 :: 9.25 : 0.01 error in dep. of 2d course.

As 37.25 : 0.06 :: 7.60 : 0.01 error in dep. of 3d course.

As 37.25 : 0.06 :: 10.40 : 0.02 error in dep. of 4th course.

139. REMARK I. In finding the error in latitude or departure, for a particular course, the last figure is sometimes doubtful ; in which case it is best to mark it, as in the third proportion for error in latitude, and the first for error in departure ; and then, if the figures taken do not balance the work, let each be increased or diminished by 1.

140. REMARK II. It has already been observed (Art. 136), that if the measurements on the field are correctly made, the sums of the northings and southings will be equal to each other, as also those of the eastings and westings. It is the opinion of some surveyors, that when the error in latitude or departure exceeds one link for every five chains of the courses, the field notes ought not to be relied on. This, perhaps, is a higher degree of accuracy than can be attained. The error, however, should always be made considerably less than one link to a chain.

*Of the double meridian distances of the courses.*

141. After the work has been balanced, the next thing to be done is to calculate the double meridian distance of each course.

For this purpose, a meridian line is assumed, lying either wholly without the land, or passing through any point within it. It is, however, most convenient to take that meridian which passes through the most easterly or westerly station of the survey; and these two stations are readily determined by inspecting the field notes.

Having chosen the meridian, let the station through which it passes, be called the *principal station*, and the course which begins at this point, *the first course*. Care, however, must be taken, not to confound this with the course which begins at station 1, and which is the first course that is entered in the field notes.

It has already been remarked (Art. 132), that all departures in the direction east, are considered as *plus*, and all departures in the direction west, as *minus*: then, through whatever station of the survey the assumed meridian be taken, we shall have for the calculation of the double meridian distances, the following

## RULE.

I. *The double meridian distance of the first course is equal to its departure.*

II. *The double meridian distance of the next course is equal to the double meridian distance of the first course, plus its departure, plus the departure of the second course.*

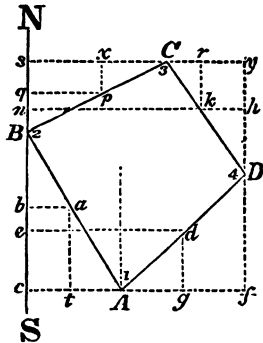
III. *The double meridian distance of the third course is equal to the double meridian distance of the second, plus its departure, plus the departure of the third course.*

IV. *And, the double meridian distance of any course is equal to the double meridian distance of the preceding course, plus its departure, plus the departure of the course itself.*

REMARK. It should be recollected that *plus* is here used in its algebraic sense, and that when double the meridian distance of a course and the departure which is to be added to it, are of different names, that is, one east and the other west, they will have contrary algebraic signs; hence, their algebraic sum will be expressed by their difference, with the sign of the greater prefixed to it.

*Demonstration of the Rule.*

Let the figure  $ABCD$ , which we have already surveyed with the compass, be resumed. By inspecting the field notes, it will be seen that  $B$ , or station 2, is the most westerly station. Through this point let the assumed meridian  $NS$  be supposed to pass. Then,  $B$  will be the principal station, and  $BC$  the first course. By what has been already said, every departure towards the east is to be considered as plus, and every departure towards the west, as minus.



Now, since  $p$ ,  $k$ ,  $d$  and  $a$ , are the middle points of the courses  $BC$ ,  $CD$ ,  $DA$  and  $AB$ , we have, by similar triangles,

- $2 qp = 2 sx = sC =$  the first departure.
- $2 Cr = 2 hk = Cy =$  the second departure.
- $2 fg = 2 gA = Af =$  the third departure.
- $2 At = 2 ab = Ac =$  the fourth departure.

We also have,

- $2 qp = sC =$  doub. mer. dis. of  $BC$ .
- $2 qp + 2 xC + 2 Cr = 2 kn =$  doub. mer. dis. of  $CD$ .
- $2 kn + 2 kh - 2 gf = 2 de =$  doub. mer. dis. of  $DA$ .
- $2 de - 2 gA - 2 At = 2 ab =$  doub. mer. dis. of  $AB$ .

The departure of the courses  $BC$ ,  $CD$ , are east, and therefore positive; while the departures of the courses  $DA$ ,  $AB$ , are west, and consequently negative.

Since the course of reasoning just pursued is applicable to all figures, we may regard the rule as demonstrated for every case which can occur.

**REMARK.** The double meridian distance of the last course should be equal to the departure of that course. A verification of the work is, therefore, obtained by comparing this double meridian distance with the departure of the course.

142. To apply the above rule to the particular example already considered, rule a new table, as below, in which are entered the *balanced* northings and southings, and the *balanced* eastings and westings.

In this table there is but a single column for the difference of latitude, and a single column for the departures. The + sign shows when the difference of latitude is north, and the - sign, when it is south. The + sign also shows when the departure is east, and the - sign, when it is west.

Stations.	Bearings.	Distances.	Dif. Lat.	Dep.	D. M. D.
1	N 31½° W	10.	+8.71	-5.24	+17.91 - 7.43 - 5.24 +5.24
2*	N 62½° E	9.25	+4.40	+8.21	8.21
3	S 36° E	7.60	-6.01	+4.46	+8.21 +8.21 +1.46 +20.88
4	S 45½° W	10.40	-7.10	-7.43	+20.88 + 1.46 - 7.43 +17.91

We see, from inspecting the notes, that 2 is the most westerly, and 4 the most easterly station. Either of them may, therefore, be taken for the principal station. Let us assume 2 for the principal station, and distinguish it by a star, thus\*.

Having done so, we enter the departure 8.21 in the column of double meridian distances, which gives the double meridian distance of the first course. The double meridian distances of the other courses are calculated according to the rule; and as the last, opposite to station 1, is equal to the departure of the course, the work is known to be right.

#### *Of the Area.*

143. Having calculated the double meridian distance of each course, the next and last operation for finding the content of the ground, is explained in the following

#### RULE.

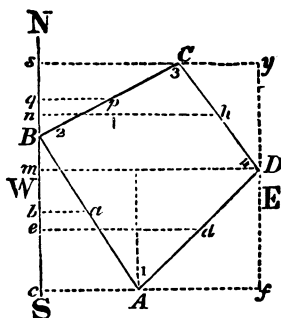
I. *Multiply the double meridian distance of each course by its northing or southing, observing that like signs in the multiplicand and multiplier give plus in the product, and that unlike signs give minus in the product.*

II. *Place all the products which have a plus sign in one column, and all the products which have a minus sign in another.*

III. *Add up each of the columns separately and take their difference: this difference will be double the area of the land.*

*Demonstration of the Rule.*

Let us again resume the example which we have been considering, and write the difference of latitude and the double meridian distances of the courses, in the following table.



Stations.	Dif. of Latitude.	D. M. D.	Area. +	Area. -
1	$+cB$	$+2ba$	$2cAB$	
2*	$+Bs$	$+2qp$	$2BsC$	
3	$-yD$	$+2nh$		$2msCD$
4	$-Df$	$+2ed$		$2cmDA$

It is now evident, that  $cB$  multiplied by  $2ba=cA$ , will give double the area of the triangle  $cAB$ . But  $cB$  and  $ba$  are both plus; hence, the product will be plus, and must be put in the column of plus areas. Double the area of the triangle  $BsC$ , is equal to  $Bs$  multiplied by  $2qp$ , which product is also plus.

The area of the trapezoid  $msCD$  is equal to  $yD=ms$  multiplied by  $nh$  (Geom. Bk. IV, Prop. VII); hence, double the area is equal to  $yD$  into  $2nh$ . But since  $yD$  is minus, and  $2nh$  plus, it follows that the product will be negative; hence, it must be placed in the column of negative areas.

Double the area of the trapezoid  $cADm$ , is equal to  $Df=mc$  multiplied by  $2de$ : but, since  $Df$  is negative and  $2de$  positive, the product will be negative.

It is now evident that the difference between the two columns is equal to twice the content of the figure  $ABCD$ :



and as the same may be shown for any figure whatever, we may regard the rule as demonstrated for all cases.

We will now make the calculations in numbers. Having balanced the work, we can place it in the following table.

Sta.	Bear.	Dist.	Dif. Lat.	Dep.	D. M. D.	Area. +	Area. -
1	N $31\frac{1}{2}^{\circ}$ W	10.	+8.71	-5.24	+5.24	45.6404	
2*	N $62\frac{1}{4}^{\circ}$ E	9.25	+4.40	+8.21	+8.21	36.1240	
3	S $36^{\circ}$ E	7.60	-6.01	+4.46	+20.88		125.4888
4	S $45\frac{1}{4}^{\circ}$ W	10.40	-7.10	-7.43	+17.91		127.1610

| 81.7644 | 252.6498

81.7644

2) 170.8854

Area in square chains, . . . 85.4427

Dividing by 10, . . . 8.54427

4

2.17708

40

*Ans. 8A 2R 7P.* . . . 7.05320

Observing in the field notes that station 2 is the most westerly point of the land, we assume the meridian which passes through this point, as the one from which the meridian distances are calculated. We mark the principal station with a star.

Opposite station 2, we enter, in the column of double meridian distances, headed D. M. D., the departure of the course from 2 to 3, which is the double meridian distance of that course, and plus. To this we add the departure of the course, and also the departure of the next course: their sum is the double meridian distance of the course from 3 to 4.

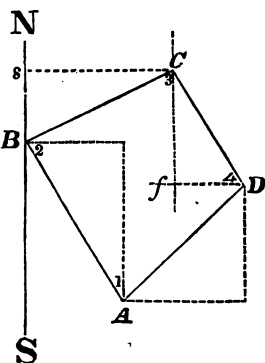
To the last sum add the departure opposite station 3, and the minus departure opposite station 4: their algebraic sum is the double meridian distance from 4 to 1.

To the last sum add the last departure, which is minus, also the next departure which is likewise minus: this will give the double meridian distance of the course from 1 to 2, which is also equal to its departure.

Then forming the products, adding them together, taking their difference, and dividing it by 2, according to the rule, we obtain the content of the ground.

144. It only remains to make a plot of the ground.

For this purpose, draw any line, as  $NS$ , to represent the meridian passing through the principal station, on which take any point, as  $B$ , to represent that station.



#### FIRST METHOD OF PLOTTING.

Having fixed upon the scale on which the plot is to be made, lay off from  $B$  on the meridian, a distance  $Bs$  equal to the difference of latitude of the first course, and at  $s$  erect a perpendicular to the meridian, and make it equal to the departure of the first course: then draw  $BC$ , which will be the first course.

Through  $C$  draw a meridian, and make  $Cf$  equal to the difference of latitude of the second course, and through  $f$  draw a perpendicular  $fd$ , and make it equal to the departure of the second course: draw  $CD$ , and it will be the second course.

Lay down, in the same manner, the courses  $DA$  and  $AB$ , and the entire plot will be completed.

#### SECOND METHOD OF PLOTTING.

The work may be plotted in another manner, thus. At the principal station  $B$ , lay off an angle equal to the bearing from  $B$  to  $C$ , which will give the direction of  $BC$ . Then, from the scale of equal parts, make  $BC$  equal to the first course: this will give the station  $C$ .

Through  $C$  draw a meridian, and lay off an angle equal to the bearing from  $C$  to  $D$ , and then lay off the course  $CD$ . Do the same for the bearing at  $D$  and the course  $DA$ ; also, for the bearing at  $A$  and the course  $AB$ , and a complete plot of the ground will thus be obtained. If the work is all right, the last line  $AB$  will exactly close the figure. This plot is made on a scale of 40 chains to an inch.

9. It is required to determine the content and plot of a piece of land, of which the following are the field notes, viz.

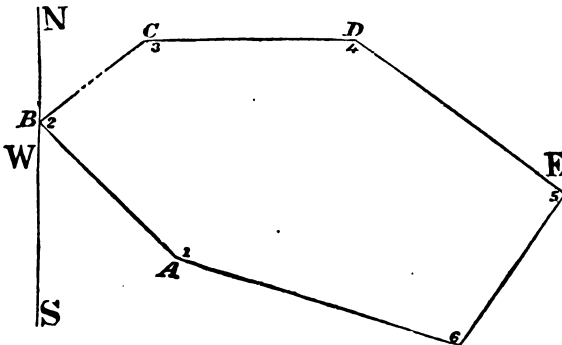
Station.	Bearings.	Distances.
1	N 46½° W	20 ch.
2	N 51½° E	13.80
3	E	21.25
4	S 56° E	27.60
5	S 33½° W	18.80
6	N 74½° W	30.95

CALCULATION.

Sta- tions	Bearings.	Dist.	Lat.		Dep.		BALANCED.		D.M.D. +	AREA +	AREA -
			N +	S -	E +	W -	Lat.	Dep.			
1	N 46½° W	20 ch.	13.77			14.51	+13.88	-14.56	14.56	202.0928	
2*	N 51½° E	13.80	8.54		10.84		+8.61	+10.81	10.81	93.0741	
3	E	21.25			21.25		...	+21.20	42.82	....	
4	S 56° E	27.60		15.44	22.88		-15.29	+22.82	86.84		1327.7836
5	S 33½° W	18.80		15.72		10.31	-15.63	-10.36	99.30		1552.0590
6	N 74½° W	30.95	8.27			29.83	+8.43	-29.91	59.03	497.6220	

Sum of courses . . 132.40 30.58 | 31.16 54.97 | 54.65  
 Error in Northing . . 0.58 | 0.32 Error in Westing  
 Ans. 104A 1R 16P . . . . . 1043.5264

Plot of the above example.



REMARK. When a bearing is due east or west, the error in latitude is nothing, and the course must be subtracted from

the sum of the courses, before balancing the columns of latitude. In the last example, the 3d bearing is due east, and the first term of the several proportions for error in latitude, was  $132.40 - 21.25 = 111.15$ .

In like manner, if a bearing is due north or south, the error in departure is nothing; and the sum of the courses must be diminished by this course, before balancing the columns of departure.

3. Required the content and plot of a piece of land, of which the following are the field notes.

Stations	Bearings.	Distances.
1	S 34° W	3.95 ch.
2	S	4.60
3	S 36½° E	8.14
4	N 59½° E	3.72
5	N 25° E	6.24
6	N 16° W	3.50
7	N 65° W	8.20

1

*Ans. 10A 0R 5P.*

4. Required the content and plot of a piece of land, from the following field notes.

Stations.	Bearings.	Distances.
1	S 40° W	70 rods
2	N 45° W	89
3	N 36° E	125
4	N	54
5	S 81° E	186
6	S 8° W	137
7	W	130

10

*Ans. 207A 3R 33P.*

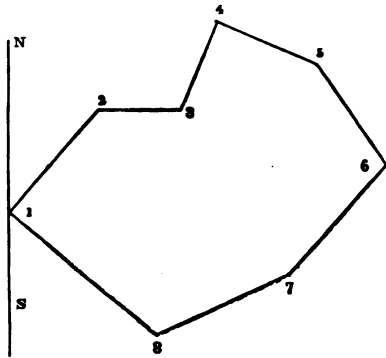
5. Required the content and plot of a piece of land, from the following field notes.

Stations.	Bearings.	Distances.
1	S 40 $\frac{1}{2}$ <sup>o</sup> E	31.80 ch.
2	N 54 <sup>o</sup> E	2.08
3	N 29 $\frac{1}{4}$ <sup>o</sup> E	2.21
4	N 28 $\frac{3}{4}$ <sup>o</sup> E	35.35
5	N 57 <sup>o</sup> W	21.10
6	S 47 <sup>o</sup> W	31.30

*Ans. 92A 3R 32P.*

6. Required the area of a survey of which the following are the field notes.

Stations.	Bearings.	Distances.
2	East.	4.00 ch.
3	N 9 <sup>o</sup> E	4.00
4	S 69 <sup>o</sup> E	5.56
5	S 36 <sup>o</sup> E	7.00
6	S 42 <sup>o</sup> W	4.00
7	S 75 <sup>o</sup> W	10.00
8	N 39 <sup>o</sup> W	7.50
1	N 42 <sup>o</sup> E	5.00



If, in this example, we assume 1 as the principal station, the double meridian distances will all be plus, and the positive area will exceed the negative.

In balancing we shall find the area in southing to be .28 ch. and in westing .22 ch. The area is 13A 0R 11P. It should however be remarked, that in all the examples the answers may be slightly varied by distributing the corrections.

7. What is the area of a survey of which the following are the field notes.

Stations.	Bearings.	Distances.
1	N 75° 00' E	54.8 rods.
2	N 20° 30' E	41.2
3	East.	64.8
4	S 33° 30' W	141.2
5	S 76° 00' W	64.0
6	North.	36.0
7	S 84° 00' W	46.4
8	N 53° 15' W	46.4
9	N 36° 45' E	76.8
10	N 22° 30' E	56.0
11	S 76° 45' E	48.0
12	S 15° 00' W	43.4
13	S 16° 45' W	40.5

In this survey 4 is the most easterly and 9 the most westerly station. The area is equal to  $110A\ 2R\ 23P$ . It may vary a little, on account of the way in which the balancing is done

8. What is the content of a piece of land of which the following are the field notes.

Stations.	Bearings.	Distances.
1	S 75° W	13.70 ch.
2	S 20½° W	10.30
3	West.	16.20
4	N 33½° E	35.30
5	N 76° E	16.00
6	South.	9.00
7	N 84° E	11.60
8	S 53¼° E	11.60
9	S 36¾° W	19.20
10	S 22½° W	14.00
11	N 76¾° W	12.00
12	N 15° E	10.85
13	N 16¾° E	10.12

In this survey 4 is the most westerly station and 9 the most easterly. The area is 110A 2R 23P. The result may, however, as in the other examples, be slightly varied by the balancing.

9. What is the area of a survey of which the following are the notes ?

Stations.	Bearings.	Distances.
1	S $46\frac{1}{2}^{\circ}$ E	80 rods.
2	S $51\frac{3}{4}^{\circ}$ W	34.16
3	West.	85
4	N $56^{\circ}$ W	110.40
5	N $33\frac{1}{4}^{\circ}$ E	75.20
6	S $74\frac{1}{2}^{\circ}$ E	123.80

*Ans.* 104A 1R 16P.

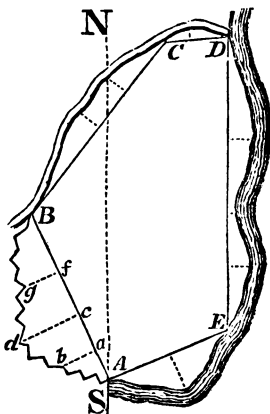
PROBLEM.

To determine the content and boundary of a piece of land, by means of offsets from the principal lines.

145. An offset is a line drawn perpendicular to a course, and may lie either on the right or left of it.

146. Let *ABCDE* be a piece of ground to be surveyed. Let us suppose it to be bounded on the west and north by a fence and road, and on the east and south by a creek or river.

Place stations at the principal points, as *A, B, C, D* and *E*. Take, with the compass, the bearings from *A* to *B*, from *B* to *C*, from *C* to *D*, from *D* to *E*, and from *E* to *A*; and measure the distances *AB, BC, CD, DE*, and *EA*.



At convenient points of the course *AB*, as *a, c* and *f*, make the offsets *ab, cd, fg*. Then, having measured these lines, as also the distances *Aa, ac, cf* and *fB*, enough will be known to determine the area which lies without the station



line  $AB$ . The points  $b$ ,  $d$ , and  $g$ , of the fence which runs from  $A$  to  $B$ , are also determined.

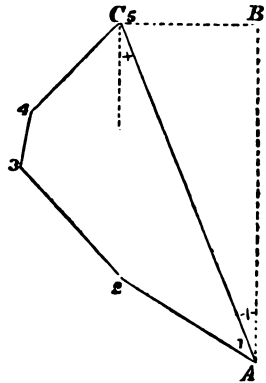
Erect, in a similar manner, offsets to the other courses, and determine the areas which lie without the station lines. These several areas being added to the area within the station lines, will give the entire area of the ground.

If the offsets fall within the station lines, the corresponding area must be subtracted from the area which is bounded by the station lines.

#### PROBLEM.

*To determine the bearing and distance from one point to another, when the points are so situated that one cannot be seen from the other.*

147. Let  $AB$  be a meridian, and  $A$  and  $C$  the two points. From either of them, as  $A$ , measure a course  $A2$ , of a convenient length in the direction towards  $C$ , and take the bearing with the compass. At  $2$ , take the bearing of a second course, and measure the distance to  $3$ . At  $3$ , take a third bearing and measure to  $4$ . At  $4$ , take the bearing to  $C$ , and measure the distance from  $4$  to  $C$ .



Then, the difference between the sum of the northings and the sum of the southings will be represented by  $AB$ , and the difference between the sum of the eastings and the sum of the westings by  $BC$ . The base  $AB$ , and the perpendicular  $BC$  of the right-angled triangle  $ABC$ , are then known. The angle at the base,  $BAC$ , is the bearing from  $A$  to  $C$ ; or the equal alternate angle at  $C$  is the bearing from  $C$  to  $A$ , and the hypotenuse  $AC$  is the distance.

Having measured the bearings and courses on the field, form a table, and find the base and perpendicular of the right-angled triangle, in numbers

Stations.	Bearings.	Distances.	N.	S.	E.	W.
1	N 61° W	40 ch.	19.39			34.98
2	N 42° W	41.	30.47			27.43
3	N 12° E	16.10	15.75		3.35	
4	N 47° E	32.50	22.16		23.77	
			$\overline{AB}=87.77$		27.12	62.41
					<u>27.12</u>	
						$\overline{CB}=35.29$ ch.

**REMARK.** Had any of the courses run south,  $\overline{AB}$  would have been equal to the sum of the northings, minus the sum of the southings.

To find the angle  $BAC$ , or the bearing from  $A$  to  $C$ .

As radius :  $\tan A$  ::  $\overline{AB}$  :  $\overline{BC}$ ,

or  $\overline{AB}$  :  $\overline{BC}$  ::  $R$  :  $\tan A$  :

that is,

As $\overline{AB}$ 87.77	.	ar. comp.	.	8.056654
: $\overline{BC}$ 35.29	.	.	.	1.547652
:: $R$	.	.	.	10.
: $\tan A$ 21° 54' 12".	.	.	.	<u>9.604306</u>

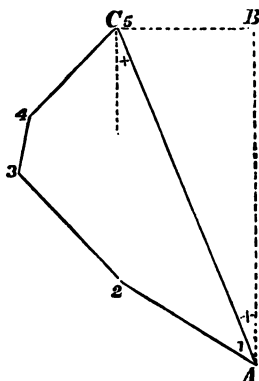
To find the distance  $\overline{AC}$ .

As $\sin A$ 21° 54' 12"	.	ar. comp.	.	0.428242
: $R$	.	.	.	10.
:: $\overline{BC}$ 35.29	.	.	.	1.547652
: $\overline{AC}$ 94.6	.	.	.	<u>1.975894</u>

Hence, the bearing and distance are both found.

*Of supplying omissions in the field notes.*

148. The last problem affords an easy method of finding the bearing and length of one of the courses of a survey, when the bearings and lengths of all the others are known. It may be necessary to use this method when there are obstacles which prevent the measuring of a course, or when the



bearing cannot be taken. Indeed, any *two omissions* may always be supplied by calculation. It is far better, however, if possible, to take all the notes on the field. For, when any of them are supplied by calculation, there are no test by which the accuracy of the work can be ascertained, and all the errors of the notes affect also the parts which are supplied.

1. In a survey we have the following notes.

Stations.	Bearings.	Distances.
1	N $31\frac{1}{2}^{\circ}$ W	10 ch.
2	N $62\frac{3}{4}^{\circ}$ E	9.25
3	Lost.	Lost.
4	S $45\frac{1}{4}^{\circ}$ W	10.40

What is the bearing and distance from station 3 to 4.

*Ans.* { Bearing, S  $36^{\circ}$  E.  
 { Distance, 7.60 ch.

2. In a survey we have the following notes :

Stations.	Bearings.	Distances.
1	S $40\frac{1}{2}^{\circ}$ E	31.80 ch.
2	N $54^{\circ}$ E	2.08
3	Lost.	Lost.
4	N $28\frac{3}{4}^{\circ}$ E	35.35
5	N $57^{\circ}$ W	21.10
6	S $47^{\circ}$ W	31.30

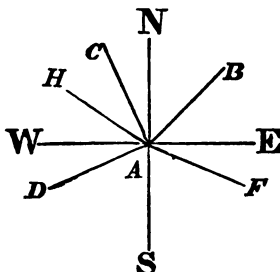
What is the bearing and distance from 3 to 4 ?

*Ans.* { Bearing,  $29\frac{1}{4}^{\circ}$  E.  
 { Distance, 2.21 ch.

To determine the angle included between any two courses, when their bearings are known.

149. Let NS be a meridian passing through A.

Let AB, AC, AD and AH be four courses running from A. We readily deduce the following



RULES.

AC is N 26° W  
 AH is N 65° W  
 $\overline{CAH} = 39^\circ$

} When the meridional letters are alike, and those of departure also alike, the difference of the bearings will be the angle between the courses.

AB is N 46° E  
 AC is N 26° W  
 $\overline{CAB} = 72^\circ$

} When the meridional letters are alike, and those of departure unlike, the sum of the bearings will be the angle between the courses.

AC is N 26° W  
 AD is S 66° W  
 $\overline{CAD} = 180^\circ - 92^\circ = 88^\circ$

} When the meridional letters are unlike, and those of departure alike the angle between the courses will be equal to 180° minus the sum of the bearings.

AC is N 26° W  
 AF is S 66° E  
 $\overline{CAF} = 180^\circ - 40^\circ = 140^\circ$

} When the meridional letters are unlike, and those of departure also unlike, the angle between the courses will be equal to the difference of the bearings taken from 180°.

**REMARK.** The above rules are determined, under the supposition that the two courses are both run from the angular point. Hence, if it be required to apply the rules to two courses run in the ordinary way, as we go around the field, the bearing of one of them must be reversed before the calculation for the angle is made.

1. The bearings of two courses, from the same point, are N 37° E, and S 85° W : what is the angle included between them ?

*Ans.* 132°.

2. The bearings of two adjacent courses, in going round a piece of land, are  $N\ 39^\circ\ W$ , and  $S\ 48^\circ\ W$ : what is the angle included between them?

*Ans.*  $87^\circ$ .

3. The bearings of two adjacent courses, in going round a piece of land, are  $S\ 85^\circ\ W$ , and  $N\ 69^\circ\ W$ : what is the angle included between them?

*Ans.*  $154^\circ$ .

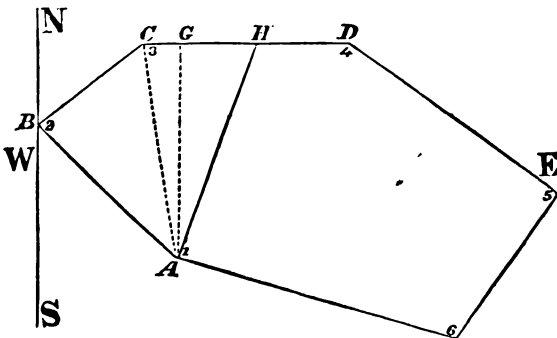
4. The bearings of two adjacent courses, in going round a piece of land, are  $N\ 55^\circ\ 30'\ E$ , and  $S\ 69^\circ\ 20'\ E$ : what is the angle included between them?

*Ans.*  $124^\circ\ 50'$ .

PROBLEM.

To run a line from a given point in the boundary of a piece of land, so as to cut off on either side of it a given portion of the field.

150. Make a complete survey of the field, by the rules already given. Let us take, as an example, the field whose area is computed at page 106. That field contains  $104A\ 1R\ 16P$ , and the following is a plot of it.



Let it now be required to run a line from station  $A$ , in such a manner as to cut off on the left any part of the field; say,  $26A\ 2R\ 31P$ .

It is seen, by examining the field, that the division line will probably terminate on the course  $CD$ . Therefore, draw a line from  $A$  to  $C$ , which we will call the first closing line.

The bearings and lengths of the courses  $AB$ ,  $BC$ , are always known; and in the present example are found in the

table on page 106 : hence, the bearing and distance from *C* to *A*, can be calculated by the last problem : they are in this example,

Bear. S 9° 28' E : Course 22.8 ch.

Having calculated the bearing and length of the closing line, find, by the general method, the area which it cuts off : that area, in the present case, is

13*A* 3*R* 3*P*.

It is now evident that the division line must fall on the right of the closing line *AC*, and must cut off an area *ACH*, equal to the difference between that already cut off, and the given area : that is, an area equal

26*A* 2*R* 31*P* given area.

13*A* 3*R* 3*P* area already cut off.

to . . . 12*A* 3*R* 28*P*.

Since the bearing of the next course *CD*, and the bearing of the closing line *AC* are known, the angle *ACD* which they form with each other, can be calculated, and is in this example 80° 32'. Hence, knowing the hypotenuse *AC*, and the angle *ACG* at the base, the length *AG* of the perpendicular let fall on the course *CD*, can be found, and is 22.49 chains.

Since the area of a triangle is equal to its base multiplied by half its altitude, it follows, that the base is equal to the area divided by half the altitude. Therefore, if the area

12*A* 3*R* 28*P*

be reduced to square chains, and divided by 11.24½ chains, which is half the perpendicular *AG*, the quotient, which is 11.58 chains, will be the base *CH*. Hence, if we lay off from *C*, on *CD*, a distance *CH*, equal to 11.5 chains, and then run the line *AH*, it will cut off from the land the required area.

**REMARK I.** If the part cut off by the first closing line, should exceed the given area, the division line will fall on the left of *AC*.

**REMARK II.** If the difference between the given area and the first area cut off, divided by half the perpendicular *AG*, gives a quotient larger than the course *CD* ; then, draw a

line from  $A$  to  $D$ , and consider it as the first closing line, and let fall a perpendicular on  $DE$ .

**REMARK III.** When the point from which the division line is to be drawn, falls between the extremities of a course, dividing the course into two parts, consider one of the parts as an entire course, and the other as forming a new course, having the same bearing. The manner of making the calculation will then be the same as before.

*Method of determining the area of a Survey by means of the Table of Natural Sines and Cosines.*

If, in a circle of which the radius is 1, we calculate the sine and cosine for every minute of the quadrant, they form what is called a Table of Natural Sines and Cosines. The natural sine is the perpendicular, and the natural cosine the base of a right angled triangle of which the hypotenuse, or radius of the circle, is 1.

Since either leg of a right angled triangle is less than the hypotenuse, it follows that the natural sine or cosine of every arc of the quadrant is less than 1. These sines and cosines are expressed in decimals of the radius 1, and although the decimal point is not written in the table, yet it must always be prefixed to the number before using it.

Thus in page 67, the sine of $5^{\circ} 30'$	is	.09585.
The cosine of $5^{\circ} 30'$	„	.99540.
Sine of $40^{\circ} 25'$ (page 71)	„	.64834.
Cosine of $40^{\circ} 25'$	„	.76135.

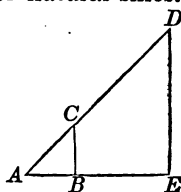
When the angle exceeds  $45^{\circ}$ , the degrees are found at the bottom of the page, and the minutes are counted upwards in the right hand column of the page, as in the table of logarithmic sines.

Thus, sine of $84^{\circ} 20'$ (page 64)	is	.99511.
The cosine of $84^{\circ} 20'$	„ -	.09874.
Sine of $79^{\circ} 37'$ (page 65)	„ -	.98362.
Cosine of $79^{\circ} 37'$	- „ -	.18023.
Sine of $69^{\circ} 25'$	- „ -	.93016.
Cosine of $69^{\circ} 25'$	- „ -	.35157.
Sine of $57^{\circ} 59'$	- „ -	.84789.
Cosine of $57^{\circ} 59'$	- „ -	.53017

If the Surveying Compass has a vernier which enables you to read the bearings to smaller parts of a degree than 15', greater accuracy may be attained by using the table of natural sines, instead of the Traverse Table, for computing the area.

We shall now show the method of calculating the latitude and departure of any course, from the table of natural sines.

Let  $AD$ , for example be any course,  $DAE$  the bearing, and  $AC=1$  the radius of the table of natural sines.



Having formed the right angled triangles  $ACB$ ,  $ADE$ , we have  $DAE$ =bearing,  
 $AE$ =dif. of latitude and  $ED$ =departure,  
 $AB$ =cosine of bearing and  $BC$ =sine of bearing.

From similar triangles, we have,

$$AC : AB :: AD : AE; \text{ that is,}$$

1 : cosine of bear. :: course : dif. of lat. ; hence,  
 dif. of latitude = course  $\times$  cosine of bearing ; that is ;

*The difference of latitude is equal to the length of the course multiplied by the cosine of the bearing.*

Again,

$$AC : CB :: AD : DE; \text{ that is,}$$

1 : sine of bearing :: course : departure ; hence,  
 departure = course  $\times$  sine of bearing, that is,

*The departure is equal to the length of the course multiplied by the sine of the bearing.*

*Ex. 1.* Find, from the Table of natural sines, the latitude and departure of the course 49 yards and bearing  $35^{\circ} 18'$

Natural cosine of	$35^{\circ} 18'$	-	-	-	.81614
Length of the course		-	-	-	49
Product, which is the dif. of latitude		-	39.99086.		

Natural sine of	$35^{\circ} 18'$	-	-	-	.57786
Length of the course		-	-	-	49
Product, which is the departure		-	28.31514.		



2. The bearing is  $65^{\circ} 39'$ , the course 69.41 chains: what is the latitude, and what the departure?

Natural cosine of $65^{\circ} 39'$	-	-	-	.41231
Length of the course	-	-	-	69.41
Product, which is the Dif. of Latitude				<u>28.6184371.</u>
Natural sine of $65^{\circ} 39'$	-	-	-	.91104
Length of the course	-	-	-	69.41
Product, which is the Departure	-			<u>63.2352864.</u>

3. The bearing is  $75^{\circ} 47'$ , the course 89.75 chains: what is the latitude, and what the departure?

Natural cosine of $75^{\circ} 47'$	-	-	-	.24559
Length of course	-	-	-	89.75
Product, which is the Dif. of Latitude				<u>22.0417025.</u>
Natural sine of $75^{\circ} 47'$	-	-	-	.96937
Length of course	-	-	-	89.75
Product, which is the Departure	-			<u>87.0009575.</u>

4. Find the area of a piece of land from the following notes.

Stations.	Bearings.	Distances.
1	N $45^{\circ} 55'$ W	53 ch.
2	N $4^{\circ} 50'$ E	74.40
3	N $89^{\circ} 05'$ E	125.50
4	S $1^{\circ} 50'$ W	71.80
5	S $7^{\circ} 40'$ E	31.20
6	N $89^{\circ} 25'$ W	35.50
7	S $84^{\circ} 35'$ W	40.
8	S $74^{\circ} 35'$ W	21.

Calculating the latitude and departure of each course by the rules already given, we have

Sta.	Bearings.	Dist.	Dif. of Latitude.		Departure.		Balanced.			
			N.	S.	E.	W.	N.	S.	E.	W.
1	N 45° 55' W	53 ch.	36.87210			38.07149	36.65908			38.07149
2	N 4° 50' E	74.40	74.13513		6.26894		73.72813		6.26894	
3	N 89° 05' E	125.50	2.00800		125.48368		1.96126		125.49228	
4	S 1° 50' W	71.80		71.76338		2.29689		72.17110		2.29688
5	S 7° 40' E	31.20		30.92107	4.16239			31.12138	4.16239	
6	N 89° 25' W	35.50	0.36139			35.49822	0.36139			35.49822
7	S 84° 35' W	40.		3.77600		39.82120		3.80352		39.81260
8	S 74° 35' W	21.		5.58264		20.24442		5.61385		20.24442
			113.37662 112.04309	112.04309	135.91501	135.93221 135.91501	112.70956	112.70985	135.92361	135.92361

Error in Southing  
Half Error

1.33353  
0.66676

0.01720 Error in Easting.  
0.00860 Half Error.

Instead of balancing by the method explained in Art. 138, we divide each error by two. Now if we subtract half the error in southing from the column of northings and at the same time add it to the column of southings, these two columns will exactly balance. In like manner, if we subtract half the error in easting from the column of westings and at the same time add it to the column of eastings, these columns will also balance.

The errors should be distributed in proportion to the lengths of the courses, but this may be done with sufficient accuracy without making the proportions. If any of the courses have been run over rough ground, the probability is that the errors belong to these courses and they should be distributed among them.

In this example we separate the half error in southing into the three parts .40700, .21302 and .04674, and subtract them respectively from the northings of courses 2, 1 and 3, and then place the northings in the balanced columns. For the southings, we separate the error into the four parts .40772, .20031, .03121, and .02752, and add them respectively to the southings of the courses 4, 5, 8 and 7. We then enter the southings in the balanced columns. As the error in easting is so small we add half of it to the easting of course 3, and subtract half from the westing of course 7.

Forming a new table and entering the balanced latitudes and departures with their proper signs, we have,

Sta.	Bearing.	Dist.	Lat.	Dep.	D. M. D.	Area. +	Area. -
1	N 45° 55' W	53 ch.	+36.65908	- 38.07149	+ 38.07149	1395.66579	
2	N 4° 50' E	74.40	+73.72813	+ 6.26894	+ 6.26894	462.19722	
3	N 89° 05' E	125.50	+ 1.96126	+125.49228	+138.03016	270.71303	
4	S 1° 50' W	71.80	-72.17110	- 2.29688	+261.22556		18854.24214
5	S 7° 40' W	31.20	-31.12138	+ 4.16239	+263.09107		6187.75716
6	N 69° 25' W	35.50	+ 0.36139	- 35.49822	+231.75524	83.75402	
7	S 84° 35' W	40.	- 3.80352	- 39.81260	+156.44442		595.03948
8	S 74° 35' W	21.	- 5.61385	- 20.24442	+ 96.38740		541.10440
						2212.33006	28178.14318
							2212.33006
							225965.81312
							12982.90656

*An. 1298.A. 1R. 6P.*

Having entered the balanced latitudes and departures we seek for the most easterly or westerly station. We see at once that station 2 is the most westerly.

Assuming this for the principal station (see Art. 141), the double meridian distances will all be east, and consequently will be plus.

We then enter the departure of course 2 in the column of double meridian distances, and then calculate the double meridian distance of each course, according to the rule given in Art. 141.

Having done this we multiply each departure by the double meridian distance of its course and place the product in the column of plus or minus areas, according as the signs of the factors are like or unlike. We enter but five decimal places in the columns of areas. This will give the result with sufficient accuracy. We then add up the columns of area, take the difference of the two sums, divide it by two and reduce the quotient to acres, roods and perches.

We thus find the area to be 1298 acres, 1 rood and 6 perches.

*Ex. 5.* Find the area of a piece of land of which the following are the field notes.

Stations.	Bearings.	Distances.
1	N 52° 36' W	20 ch.
2	N 45° 39' E	13.80
3	N 83° 54' E	21.25
4	S 62° 06' E	27.60
5	S 27° 09' W	18.80
6	N 80° 36' W	30.95

In this example station 2 is the most westerly and station 5 the most easterly point of the land.

6. Find the content of a piece of land from the following field notes.

Stations.	Bearings.	Distances.
1	W.	35.25 ch.
2	S 88° 15' W	45.65
3	N 30' W	32.55
4	N 88° 45' E	20.25
5	N 1° 15' W	25.40
6	N 88° 30' E	60.00
7	S 1° 00' E	25.50
8	S 1° 45' E	33.10

In this example station 1 is the most easterly and station 4 the most westerly point of the land. If the meridian distances of the courses be calculated from the meridian passing through station 1 they will all be west: if from the meridian passing through 4, they will all be east.

*Method of Surveying the Public Lands.*

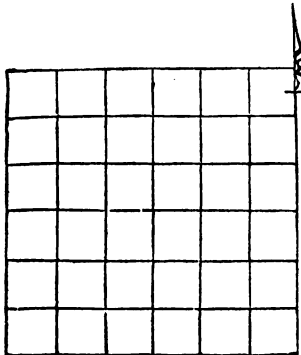
151. Soon after the organization of the present government, several of the states ceded to the United States large tracts of wild land, and these together with the lands since acquired by treaty and purchase, constitute what is called the public lands or public domain. Previous to the year 1802 these lands were parcelled out without reference to any general plan, in consequence of which the titles often conflicted with each other, and in many cases, several grants covered the same premises.

In the year 1802, the following method of surveying the public lands, was adopted by Colonel Jared Mansfield, then surveyor-general of the North-Western Territory.

152. The country to be surveyed is first divided by parallel meridians, six miles distant from each other; and then again, by a system of east and west lines, also six miles from each other. The whole country is thus divided into equal squares, which are called *townships*. Hence, each township is a square, six miles on a side, and contains 36 square miles. The townships which lie along the same meridian, are called a *range*, and are numbered, to distinguish them from each other.

Each township is divided into equal squares, by meridians one mile apart, and by east and west lines at the same distance from each other. Hence, each township is divided into 36 square miles, each one of which is called a *section*. The sections of a township are numbered from 1 to 36, and each contains 640 acres.

The diagram exhibits the 36 sections of a township.



To describe a section accurately, we say, section number 5, in township number 4, in range 3d, west of a known meridian, the one, for example, drawn through the mouth of the Great Miami river. This description fixes precisely the place of the section. Go to the 3d range of townships, west of the known meridian, find township number 4 in this range, and lastly, section number 5 of that township. The corners of the sections should be marked by permanent corner-posts, or by lines blazed on trees.

The sections are divided into half sections, quarter sections, and even into eighths of sections. The following table shows the content of a township, and its subdivisions.

1 township = 36 sections = 23040 acres.

1 section = 640 acres.

$\frac{1}{2}$  section = 320 acres.

$\frac{1}{4}$  section = 160 acres.

$\frac{1}{8}$  section = 80 acres.

The principal meridians, and the principal east and west lines, have been established by astronomical observation, and the lines of subdivision run with the compass.

#### VARIATION OF THE NEEDLE.

153. The line indicated by the magnetic needle, when allowed to move freely about the point of support, and settle to a state of rest, has been called the magnetic meridian. This, in general, is a different line from the true meridian, which always passes through the poles of the earth, when sufficiently produced in both directions.

154. The angle which the magnetic meridian makes with the true meridian, at any place on the surface of the earth, is called the *variation of the needle* at that place, and is east or west, according as the north end of the needle lies on the east or west side of the true meridian.

155. The variation is different at different places, and even at the same place it does not remain constant for any length of time. The variation is ascertained by comparing the magnetic, with the true meridian.

156. The best practical method of determining the true meridian of a place, is by observing the north star. If this star were precisely at the point in which the axis of the earth,

produced, pierces the heavens, then, the intersection of the vertical plane passing through it and the place, with the surface of the earth, would be the true meridian. But, the star being at a distance from the pole, equal to  $1^{\circ} 34'$  nearly, it performs a revolution about the pole in a circle, the polar distance of which is  $1^{\circ} 34'$ : the time of revolution is 23 h. and 56 min.

To the eye of an observer, this star is continually in motion, and is due north but twice in 23 h. 56 min.; and is then said to be on the meridian. Now, when it departs from the meridian, it apparently moves east or west, for 5 h. and 59 min., and then returns to the meridian again. When at its greatest distance from the meridian, east or west, it is said to be at its greatest *eastern* or *western* elongation.

The following tables show the times of its greatest eastern and western elongations.

## EASTERN ELONGATIONS.

Days	April	May	June	July	August	Sept
	H. M.	H. M.	H. M.	H. M.	H. M.	H. M.
1	18 18	16 26	14 24	12 20	10 16	8 20
7	17 56	16 03	14 00	11 55	9 53	7 58
13	17 34	15 40	13 35	11 31	9 30	7 36
19	17 12	15 17	13 10	11 07	9 08	7 15
25	16 49	14 53	12 45	10 43	8 45	6 53

## WESTERN ELONGATIONS.

Days	Oct.	Nov.	Dec.	Jan.	Feb.	March
	H. M.	H. M.	H. M.	H. M.	H. M.	H. M.
1	18 18	16 22	14 19	12 02	9 50	8 01
7	17 56	15 59	13 53	11 36	9 26	7 38
13	17 34	15 35	13 27	11 10	9 02	7 16
19	17 12	15 10	13 00	10 44	8 39	6 54
25	16 49	14 45	12 34	10 18	8 16	6 33

The eastern elongations are put down from the first of April to the first of October; and the western, from the first of October to the first of April; the time is computed from 12 at noon. The western elongations in the first case, and the eastern in the second, occurring in the daytime, cannot

be used. Some of those put down are also invisible, occurring in the evening, before it is dark, or after daylight in the morning. In such case, if it be necessary to determine the meridian at that particular season of the year, let 5 h. and 59 min. be added to, or subtracted from, the time of greatest eastern or western elongation, and the observation be made at night, when the star is on the meridian.

The following table exhibits the angle which the meridian plane makes with the vertical plane passing through the pole-star, when at its greatest eastern or western elongation : such angle is called the *azimuth*. The mean angle only is put down, being calculated for the first of July of each year

AZIMUTH TABLE.

Years	Lat. 32° Azimuth	Lat. 34° Azimuth	Lat. 36° Azimuth	Lat. 38° Azimuth	Lat. 40° Azimuth	Lat. 42° Azimuth	Lat. 44° Azimuth
1836	1° 50'	1° 52½'	1° 56'	1° 58½'	2° 2½'	2° 6'	2° 10½'
1837	1° 50½'	1° 52½'	1° 55½'	1° 58½'	2° 2'	2° 5½'	2° 10'
1838	1° 50'	1° 52½'	1° 55'	1° 58'	2° 1½'	2° 5'	2° 9½'
1839	1° 49½'	1° 52'	1° 54½'	1° 57½'	2° 1'	2° 4½'	2° 9'
1840	1° 49'	1° 51½'	1° 54'	1° 57½'	2° 0½'	2° 4'	2° 8½'
1841	1° 48½'	1° 51'	1° 53½'	1° 57½'	2° 0'	2° 3½'	2° 8'
1842	1° 48'	1° 50½'	1° 53'	1° 56½'	1° 59½'	2° 3'	2° 7½'
1843	1° 47½'	1° 50'	1° 52½'	1° 56'	1° 59'	2° 2½'	2° 7'
1844	1° 47'	1° 49½'	1° 52'	1° 55½'	1° 58½'	2° 2'	2° 6½'
1845	1° 46½'	1° 49'	1° 51½'	1° 55'	1° 58'	2° 1½'	2° 6'
1846	1° 46'	1° 48½'	1° 51'	1° 54½'	1° 57½'	2° 1'	2° 5½'

The use of the above tables, in finding the true meridian, will soon appear.

*To find the true meridian with the theodolite.*

157. Take a board, of about one foot square, paste white paper upon it, and perforate it through the centre ; the diameter of the hole being somewhat larger than the diameter of the telescope of the theodolite. Let this board be so fixed



to a vertical staff, as to slide up and down freely : and let a small piece of board, about three inches square, be nailed to the lower edge of it, for the purpose of holding a candle.

About twenty-five minutes before the time of the greatest eastern or western elongation of the pole-star, as shown by the tables of elongations, let the theodolite be placed at a convenient point and levelled. Let the board be placed about one foot in front of the theodolite, a lamp or candle placed on the shelf at its lower edge ; and let the board be slipped up or down, until the pole-star can be seen through the hole. The light reflected from the paper will show the cross hairs in the telescope of the theodolite.

Then, let the vertical spider's line be brought exactly upon the pole-star, and, if it is an eastern elongation that is to be observed, and the star has not yet reached the most easterly point, it will move from the line towards the east, and the reverse when the elongation is west.

At the time the star attains its greatest elongation, it will appear to coincide with the vertical spider's line for some time, and then leave it, in the direction contrary to its former motion.

As the star moves towards the point of greatest elongation, the telescope must be continually directed to it, by means of the tangent-screw of the vernier plate ; and when the star has attained its greatest elongation, great care should be taken that the instrument be not afterwards moved.

Now, if it be not convenient to leave the instrument in its place until daylight, let a staff, with a candle or small lamp upon its upper extremity, be arranged at thirty or forty yards from the theodolite, and in the same vertical plane with the axis of the telescope. This is easily effected, by revolving the vertical limb about its horizontal axis without moving the vernier plate, and aligning the staff to coincide with the vertical hair. Then mark the point directly under the theodolite ; the line passing through this point and the staff, makes an angle with the true meridian equal to the azimuth of the pole-star.

From the table of azimuths, take the azimuth corresponding to the year and nearest latitude. If the observed elongation were east, the true meridian lies on the west of the line which has been found, and makes with it an angle equal to

the azimuth. If the elongation were west, the true meridian lies on the east of the line : and, in either case, laying off the azimuth angle with the theodolite, gives the true meridian.

*To find the true meridian with the compass.*

158. 1. Drive two posts firmly into the ground, in a line nearly east and west ; the uppermost ends, when driven firmly, being about three feet above the surface, and the posts about four feet apart : then lay a plank, or piece of timber three or four inches in width, and smooth on the upper side, upon the posts, and let it be pinned or nailed, to hold it firmly.

2. Prepare a piece of board four or five inches square, and smooth on the under side. Let one of the compass-sights be placed at right angles to the upper surface of the board, and let a nail be driven through the board, so that it can be tacked to the timber resting on the posts.

3. At about twelve feet from the stakes, and in the direction of the pole-star, let a plumb be suspended from the top of an inclined stake or pole. The top of the pole should be of such a height that the pole-star will appear about six inches below it ; and the plumb should be swung in a vessel of water to prevent it from vibrating.

This being done, about twenty minutes before the time of elongation, place the board, to which the compass-sight is fastened, on the horizontal plank, and slide it east or west, until the aperture of the compass-sight, the plumb line, and the star, are brought into the same range. Then if the star depart from the plumb-line, move the compass-sight, east or west, along the timber, as the case may be, until the star shall attain its greatest elongation, when it will continue behind the plumb-line for several minutes ; and will then recede from it in the direction contrary to its motion before it became stationary. Let the compass-sight be now fastened to the horizontal plank. During this observation it will be necessary to have the plumb-line lighted : this may be done by an assistant holding a candle near it.

Let now a staff, with a candle or lamp upon it, be placed at a distance of thirty or forty yards from the plumb-line, and in the same direction with it and the compass-sight. The line so determined, makes, with the true meridian, an angle

equal to the azimuth of the pole-star; and, from this line, the variation of the needle is readily determined, even without tracing the true meridian on the ground.

Place the compass upon this line, turn the sights in the direction of it, and note the angle shown by the needle. Now, if the elongation, at the time of observation, were west, and the north end of the needle on the west side of the line, the azimuth, plus the angle shown by the needle, is the true variation. But should the north end of the needle be found on the east side of the line, the elongation being west, the difference between the azimuth and the angle would show the variation: and the reverse when the elongation is east.

1. Elongation west, azimuth	. . .	2° 04'
North end of the needle on the west, angle		4° 06'
	Variation	<u>6° 10'</u> west.

2. Elongation west, azimuth	. . .	1° 59'
North end of the needle on the east, angle		4° 50'
	Variation	<u>2° 51'</u> east.

3. Elongation east, azimuth	. . .	2° 05'
North end of the needle on the west, angle		8° 30'
	Variation	<u>6° 25'</u> west.

4. Elongation east, azimuth	. . .	1° 57'
North end of the needle on the east, angle		8° 40'
	Variation	<u>10° 37'</u> east.

REMARK I. The variation at West Point, in September, 1835, was 6° 32' west.

REMARK II. The variation of the needle should always be noted on every survey made with the compass, and then if the land be surveyed at a future time, the old lines can always be re-run.

159. It has been found by observation, that heat and cold sensibly affect the magnetic needle, and that the same needle will, at the same place, indicate different lines at different hours of the day.

If the magnetic meridian be observed early in the morning, and again at different hours of the day, it will be found that the needle will continue to recede from the meridian as the day advances, until about the time of the highest tempera-

ture, when it will begin to return, and at evening will make the same line as in the morning. This change is called the *diurnal variation*, and varies, during the summer season, from one-fourth to one-fifth of a degree.

## OF THE PLAIN-TABLE.

160. Pl. 3, Fig. 1. The plain-table consists of two parts ; a rectangular board *CDBA*, and a tripod *EHG*, to which it is firmly secured.

Directly under the rectangular board are four milled screws which pass through sockets inserted in a horizontal brass plate : these screws are worked against a second horizontal plate, for the purpose of levelling the table ; the table having a ball and socket motion, similar to the limb of the theodolite.

For the purpose of levelling the table, a small detached spirit-level is used. This level being placed over the centre, and also over two of the levelling screws, the screws are turned contrary ways until the level is horizontal ; after which, it is placed over the other two screws, and made horizontal in the same manner.

Between the upper horizontal plate and the table, there is a clamp-screw, similar to the clamp-screw of the theodolite, which being loosened, the table can be turned freely about its axis. There is, also, a small tangent-screw, by which the smaller motions of the table are regulated, after the clamp-screw is made fast. Neither of these screws can be seen in the figure.

The upper side of the table is bordered by four brass plates, about one inch in width, and the centre of the table is marked by a small pin, *F*. About this centre, and tangent to the sides of the table, conceive a circle to be described. Suppose the circumference of the circle to be divided into degrees and parts of a degree, and radii to be drawn through the centre and the points of division. The points in which these radii intersect the outer edge of the brass border, are marked by lines on the brass plates, and the degrees are numbered in the direction from left to right, from the point *L* to the point *I*,  $180^\circ$ , and from the point *I* to the point *L*,  $180^\circ$ . In some plain-tables, however, they are numbered from 0 to  $360^\circ$ .

There are, generally, diagonal scales of equal parts cut on

the plates *DLC* and *AIB*, the use of which will be explained hereafter.

Near the two other edges of the table, two small grooves are made, into which the plates of brass *DB* and *CA* are fitted, and these plates are drawn to their places by means of milled screws which pass through the table from the under side, and screw firmly into the plates. The heads of two of the screws, *Q* and *S*, are seen in the figure, as also one of the plates and its two screws in Fig. 3. The object of these plates is to confine a sheet of paper on the table. By loosening the screws, and pressing them upwards, the plates are raised above the surface of the table; the edges of the paper can then be placed under them: then, by turning the screws back again, the plates are drawn down and the paper held tightly. Fig. 1 represents the table with the paper partly put upon it: one edge of the paper has been placed under the plate *DB*, and the screws *S* and *Q*, tightened. The paper, before being put on, should be moistened, in order to expand it; and then, after it has been dried, it will fit closely to the table.

A ruler, *AB* (Fig. 2), with open vertical sights, is used with the plain-table. This ruler has a fiducial edge, which is in the same vertical plane with the hairs of the sights. A ruler with a telescope, and a vertical limb, similar to the vertical limb of the theodolite, is sometimes used with the plain-table. A compass, also, is often attached to the table, to show the bearings of the lines.

The plain-table is used for two distinct objects.

1st. For the measurement of horizontal angles.

2dly. For the determination of the shorter lines of a survey, both in extent and position.

#### *To measure a horizontal angle.*

161. Place, by means of a plumb, the centre of the table directly over the angular point: then level the table; after which, place the fiducial edge of the ruler against the small pin at the centre: direct the sights to one of the objects, and note the degrees on the brass plate; then turn the ruler and sights to the other object, and note the degrees as before. If the ruler has not passed over the 0 point, the difference of the readings is the angle sought; but, if it has, the larger

taken from  $180^\circ$ , and the remainder added to the smaller, gives the required angle.

*Of the determination of lines in extent and position.*

162. Having placed a paper on the table, examine the objects and lines which are to be determined, and measure a base line in such a direction, if possible, that all the objects can be seen from its extremities. Then place the plain-table with its centre, nearly, though not accurately, over one extremity of the base; make it truly horizontal, and turn it until the larger part of the paper lies on the same side of the base with the objects.

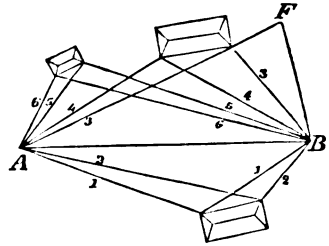
Then, tighten the clamp-screw, and mark with a pin the point of the paper directly over the station, which point is determined most accurately by suspending a plumb from the lower side of the table. Press the pin firmly on this point, bring the fiducial edge of the ruler against it, and sight to the other extremity of the base line, and mark with the pin or pencil, the direction of the line on the paper. Sight in like manner to every other object, and draw on the paper the corresponding lines, numbering them from the base line, 1, 2, 3, 4, &c.

Then, with a pair of dividers, take from the scale a certain number of equal parts to represent the base, and lay off the distance on the base line from the place of the pin. Take up the table, carry it to the other extremity of the base, and place the point of the paper corresponding to that extremity, directly over it. Place the fiducial edge of the ruler on the base line, and turn the table, by means of the tangent-screw, until the sights are directed to the first station. If, however, in bringing the table to this position, the corresponding point of the paper has been moved from over the extremity of the base line, move the legs of the tripod until it is brought back to its place. Let the table be then levelled, after which, place the ruler again on the base line, and bring the table to its proper position by the tangent-screw, and continue the adjustment until the extremity of the base line on the paper is directly over the station, and in the same vertical plane with the base line on the ground. Then direct the sights to all the objects sighted to from the other station, and mark the lines 1, 2, 3, 4, &c. from the base line, as before. The inter

sections of the corresponding lines 1,1, 2,2, 3,3, 4,4, &c., determine, on the paper, the positions of the several objects; and a reference of these lines to the scale of equal parts, determines the true distances.

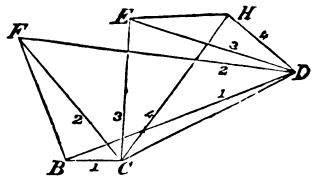
163. Let it be required, for example, to determine, by means of the plain-table, the relative position of several houses.

Measure the base line  $AB$ , which we will suppose equal to 300 yards. Place the plain-table at  $A$ , and sight to the corners of the houses, and mark the lines 1, 2, 3, 4, &c. Then remove the table to  $B$ , and sight to the same corners as before, and draw the lines as in the figure. The points at which they intersect the corresponding lines before drawn, determine the corners of the houses. The front lines of the houses may then be drawn on the paper. Draw lines at right angles to the front lines, and on them lay off the depths of the houses, with the same scale as that used for the base line.



To find the length of any line drawn on the paper, as the line 1, drawn through  $A$ , for example, place the dividers at  $A$  and extend them to the other extremity of the line, and then apply the line to the scale. The length of the line 1 is equal to 198 yards.

164. In this example, we determine from the base line  $CD$ , the positions of the points  $B$ ,  $F$ ,  $E$ , and  $H$ .



#### *Of changing the Paper.*

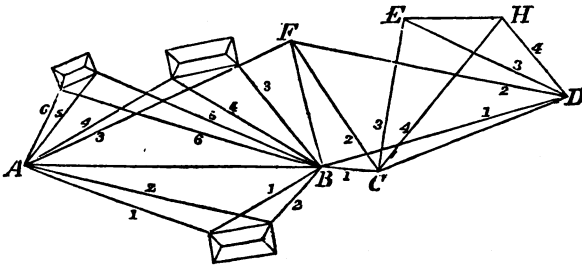
165. When one paper is filled, and there is yet more work to be done, let the paper be removed, and a second paper put on the table; after which, the table may be used as before.

Now, in order that the two papers may be put together and form one entire plan, it is necessary that two points determined on the first paper, be also determined on the second; and then, by placing the lines joining these points upon each other, all the lines on the two papers will have the same

relative position as the corresponding lines on the ground ; and the same for as many papers as it may be necessary to use. If different scales are used, the corresponding points will not join, and then the work must be reduced to the same scale, before the papers can be put together.

In the first example, the position of the point *F* was determined, in order to unite the first paper with the second.

In the second example, we sighted from *C* and *D*, the extremities of the base line, to the points *B* and *F*; we thus determined the line *BF* on the second paper. Placing the line *BF* of the one paper on *BF* of the other, we have the following plan.



In this plan, all the points and lines are accurately laid down. Any number of papers may be joined in the same manner.

The plain-table is used to great advantage when only a plot of the ground is wanted. It ought not to be used for the determination of long lines, nor can it be relied on in determining extended areas.

## CHAPTER V.

### *Of Levelling.*

166. If all the points of the earth's surface were equidistant from the centre, it would be perfectly even, and present to the eye an unbroken level.

. Intersected, however, as it is, by valleys and ridges of mountains, it becomes an important problem to ascertain the *difference* between the distances of given points from the centre of the earth ; such difference is called the *difference*



of level; and a line, all the points of which are equally distant from the centre, is called *the line of true level*.\*

167. One point is said to be *above* another, when it is farther from the centre of the earth; and *below* it, when it is nearer.

168. Let  $C$  (Pl. 4, Fig. 1), represent the centre of the earth.  $A$  a point of its surface, and  $AEF$  the line of true level. If, at the point  $A$ , a tangent line  $ABD$  be drawn to the surface, such line is called *the line of apparent level*.

169. Now, if an instrument were placed at  $A$ , and brought into a horizontal position so as to indicate a horizontal line, this line would be tangent to the earth at  $A$ , and would be the line  $ABD$  of apparent level.

170. When, therefore, we have ascertained the direction of a tangent, or horizontal line, we have found the line of apparent level only; the line of true level is yet to be determined.

If at the points  $E$  and  $F$ , vertical staves be placed, the line of apparent level passing through  $A$  will cut them at  $B$  and  $D$ , while the line of true level cuts them at  $E$  and  $F$ . Therefore,  $BE$  and  $DF$  are, respectively, the differences between the apparent levels of the points  $E$  and  $F$ , as determined by the horizontal line passing through  $A$ , and the true levels of those points.

But  $AB^2 = BE (BE + 2EC)$ , and  $AD^2 = DF (DF + 2FC)$  (Geom. Bk. IV, Prop. XXX). In the common operations of levelling, the arcs  $AE$ ,  $AF$ , are small; and since the difference between small arcs and their tangents is very inconsiderable, the arcs  $AE$ ,  $AF$  may be substituted for the tangents  $AB$ ,  $AD$ . And since the external parts of the secants  $BE$  and  $DF$  are very small in comparison with the diameter of the earth, they may be neglected without sensible error: the expressions above will then become,

$$AE^2 = BE \times 2EC, \text{ and } AF^2 = DF \times 2FC,$$

$$\text{or, } BE = \frac{AE^2}{2EC}; \text{ and } DF = \frac{AF^2}{2FC};$$

and since the diameter of the earth is constant,  $BE$  and  $DF$  are proportional to  $AE^2$  and  $AF^2$ .

\* The spheroidal form of the earth is not considered, as it affects the results too inconsiderably to be regarded in the common operations of levelling.

But  $BE$  and  $DF$  are respectively the differences between the true levels of the points  $E$  and  $F$ , and their apparent levels, as determined from the point  $A$ : hence, the difference between the apparent and true level of any point, is equal to the square of the distance of that point from the place where the apparent level was made, divided by the diameter of the earth; or, the diameter being constant, the rise of the apparent above the true level, is proportional to the square of the distance.

171. The mean diameter of the earth being about 7919 miles, if  $AE$  be taken equal to 1 mile, then the excess

$$BE = \frac{AE^2}{2AC} \text{ becomes equal to } \frac{1}{7919} = 8.001 \text{ inches.}$$

If the excess  $FD$ , for any other distance  $AF$ , were required,  $AE^2 : AF^2 :: BE : FD$ ;

and by similar proportions the following table is calculated.

*Table showing the differences in inches between the true and apparent level, for distances between 1 and 100 chains.*

Chains.	Inches.	Chains.	Inches.	Chains.	Inches.	Chains.	Inches.
1	.001	26	.845	51	3.255	76	7.221
2	.005	27	.911	52	3.380	77	7.412
3	.011	28	.981	53	3.511	78	7.605
4	.020	29	1.051	54	3.645	79	7.802
5	.031	30	1.125	55	3.781	80	8.001
6	.045	31	1.201	56	3.925	81	8.202
7	.061	32	1.280	57	4.061	82	8.406
8	.080	33	1.360	58	4.205	83	8.612
9	.101	34	1.446	59	4.351	84	8.832
10	.125	35	1.531	60	4.500	85	9.042
11	.151	36	1.620	61	4.654	86	9.246
12	.180	37	1.711	62	4.805	87	9.462
13	.211	38	1.805	63	4.968	88	9.681
14	.245	39	1.901	64	5.120	89	9.902
15	.281	40	2.003	65	5.281	90	10.126
16	.320	41	2.101	66	5.443	91	10.351
17	.361	42	2.208	67	5.612	92	10.587
18	.405	43	2.311	68	5.787	93	10.812
19	.451	44	2.420	69	5.955	94	11.046
20	.500	45	2.531	70	6.125	95	11.233
21	.552	46	2.646	71	6.302	96	11.521
22	.605	47	2.761	72	6.480	97	11.763
23	.661	48	2.880	73	6.662	98	12.017
24	.720	49	3.004	74	6.846	99	12.246
25	.781	50	3.125	75	7.032	100	12.502

We cannot proceed farther in the discussion of the principles of levelling, until we have described the instruments which are to be used, and explained the particular objects which they are to answer.

#### OF THE LEVEL.

172. The level is an instrument used to determine horizontal lines, and the difference of level of any points on the surface of the earth.

The part of the instrument shown in Pl. 4, Fig. 2, rests on a tripod to which it is permanently attached at *Z*. *HH* is a horizontal brass plate, through which four levelling screws with milled heads are passed, and worked against a second horizontal plate *GG*. Two of these screws, *K* and *I*, are seen in the figure. *S* is a clamp-screw, which, being loosened, allows the upper part of the instrument to turn freely around its axis. *Q* is a tangent-screw, by means of which the upper part of the instrument is moved gently, after the clamp-screw *S* has been made fast. *EE* is a horizontal bar, perpendicular to which are the wyes, designated *Y*'s, that support the telescope *LB*. This telescope is confined in the *Y*'s by the loops *r, r*, which are fastened by the pins *p* and *p*. The object-glass *B*, is adjusted to its focus by the screw *X*; the eye-glass *L* slides out and in freely. The screws *f, f*, work the slide which carries the horizontal hair; and two horizontal screws, only one of which, *a*, is seen, work the slide that carries the vertical hair. *CD* is an attached spirit level. The screw *N* elevates and depresses the *Y*, nearest the eye-glass. In some instruments this *Y* is elevated and depressed, by means of two screws at *M* and *R*.

Before using the level, it must be adjusted. The adjustment consists in bringing the different parts to their proper places.

The line of *collimation* is the axis of the telescope. With this axis, the line drawn through the centre of the eye-glass, and the intersection of the spider's lines, within the barrel of the telescope, ought to coincide.

**FIRST ADJUSTMENT.\*** *To fix the intersection of the spider's lines in the axis of the telescope.*

Having screwed the tripod to the instrument, extend the

\* This, and some of the following adjustments, are so similar to those of the theodolite, that they would not be repeated, but that some may use the level without wishing to study a more complicated instrument.

legs, and place them firmly. Then loosen the clamp-screw  $S$ , and direct the telescope to a small, well-defined, and distant object. Then slide the eye-glass till the spider's lines are seen distinctly; after which, with the screw  $X$ , adjust the object-glass to its proper focus, when the object and the spider's lines will be distinctly seen. Note now the precise point covered by the intersection of the spider's lines.

Having done this, revolve the telescope in the  $Y$ 's, half round, when the attached level  $CD$  will come to the upper side. See if, in this position, the horizontal hair appears above or below the point, and in either case, loosen the one, and tighten the other, of the two screws which work the horizontal hair, until it has been carried over half the space between its last position and the observed point. Carry the telescope back to its place; direct again, by the screws at  $M$  and  $R$ , the intersection of the spider's lines to the point, and repeat the operation, till the horizontal hair neither ascends nor descends while the telescope is revolved. A similar process will arrange the vertical hair, and the line of collimation is then adjusted.

**SECOND ADJUSTMENT.** *To make the axis of the attached level  $CD$  parallel to the line of collimation.*

Turn the screw  $N$ , or the screws  $M$  and  $R$ , until the bubble of the level  $DC$  stands at the middle of the tube. Then open the loops, and reverse the telescope. If the bubble still stands at the middle of the tube, the axis of the level is horizontal; but if not, it is inclined, the bubble being at the elevated end. In such case, raise the depressed, or depress the elevated end, by means of the screw  $h$ , half the inclination; and then with the screw  $N$ , bring the level to a horizontal position. Reverse the telescope in the  $Y$ 's, and make the same correction again; and proceed thus, until the bubble stands in the middle of the tube, in both positions of the telescope; the axis of the level is then horizontal.

Let the telescope be now revolved in the  $Y$ 's. If the bubble continue in the middle of the tube, the axis of the level is not only horizontal, but also parallel to the line of collimation. If, however, the bubble recedes from the centre, the axis of the level is inclined to the line of collimation, and

must be made parallel to it, by means of two small screws, which work horizontally ; one of these screws is seen at *q*. By loosening one of them, and tightening the other, the level is soon brought parallel to the line of collimation ; and then, if the telescope be revolved in the *Y*'s, the bubble will continue at the middle point of the tube. It is, however, difficult to make the first part of this adjustment, while the axis of the level is considerably inclined to the line of collimation : for, allowing the level to be truly horizontal in one position of the telescope, after it is reversed, there will be but one corresponding position in which the bubble will stand at the middle of the tube. This suggests the necessity of making the first part of the adjustment with tolerable accuracy ; then, having made the second with care, re-examine the first, and proceed thus till the adjustment is completed.

**THIRD ADJUSTMENT.** *To make the level  $CD$  and the line of collimation perpendicular to the axis of the instrument, or parallel to the horizontal bar  $EE$ .*

Loosen the clamp-screw *S*, and turn the bar *EE*, until the level *DC* comes directly over two of the levelling screws. By means of these screws, make the level *CD* truly horizontal. Then, turn the level quite round ; if, during the revolution, it continue horizontal, it must be at right angles to the axis of the instrument about which it has been revolved. But if, after the revolution, the level *CD* be not horizontal, rectify half the error with the screws at *M* and *R*, and half with the levelling screws. Then place the bar *EE* over the other two levelling screws, and make the same examinations and corrections as before ; and proceed thus, until the level can be turned entirely around without displacing the bubble at the centre. When this can be done, it is obvious that the level *DC* and the line of collimation, are at right angles to the axis of the instrument about which they revolve ; and since the axis is carefully adjusted by the maker, at right angles to the bar *EE*, it follows, that the line of collimation, the level *DC*, and the bar *EE*, are parallel to each other.

The level is now adjusted. When used, however, it is best to re-examine it every day or two, as the work will be erroneous unless the adjustments are accurate.

*Of Levelling Staves.*

173. The levelling staves are used to determine the points at which a given horizontal line intersects lines that are perpendicular to the surface of the earth, and to show the distance of such points of intersection from the ground.

They are thus constructed. *AB* (Pl. 4, Fig. 3) is a rectangular piece of wood, in the middle of which is a groove *abcd*. Into this groove a slide *lnst* enters, and is moved freely along the groove. At the upper end of the slide is a rectangular board *fhov*, called a *vane*, six inches, in the direction *hi*. The vane is divided into four equal parts, by the lines *fg*, *hi*: the two rectangles *fh*, *ig*, are usually painted black, and the other two, *if*, *hg*, white; so that the lines *fg* and *hi* may be distinguished with great accuracy. The slide from *fg* to *ln*, is of the same length with the body of the staff *AB*: hence, when the line *fg* coincides with *bc*, the lower end of the slide *ln*, will coincide with *ad*. The pins *p* and *q*, which work in grooves, and are largest at the ends *p* and *q*, are pressed in to hold the slide in any position at which it may be placed. The length of the staff is generally six feet, and it is usually divided into eighths or tenths of an inch. The slide is divided in the same way. The longer lines show the feet, the shorter, the inches. *The object to be attained by these divisions, is, to ascertain the distance of the line fg from the ground.*

When the line *fg* is brought to the top of the staff, to coincide with *bc*, the lower line *wio* of the vane, coincides with the line marked 6, on the left of the staff: which shows, the staff standing upright, that the line *fg* is six feet above the ground. From the line marked 6, to the lower end of the staff, is, indeed, but 5 feet 9 inches; but the line *fg* is three inches above the line *wio*, so that *fg* is six feet from the ground.

If, from the last position, the slide be run up until the line *wio* coincides with the division marked 1, on the left of the staff, the line *fg* will be six feet and one inch from the ground: if, till it coincides with *bc*, it will be six feet and three inches, the inches being marked on the staff. If the slide be still run up, until 7 on the slide coincides with *bc*, the line *fg* will be seven feet from the ground. In the figure, the line *fg* is

seven feet from the bottom of the staff. The count above 6 feet 3 inches is always made on the slide. The manner of counting off, for the parts of an inch, is too plain to require particular explanation.

Having run down the slide till the upper line  $h$ , of the vane, coincides with  $bc$ , place  $bB$  on the ground, and the staff vertical. It is now plain, that the line  $fg$  is three inches above the ground. These three inches are marked on the right of the staff. If the slide be run up till the lower line  $h$  coincides with 1, on the right of the staff, the line  $fg$  will be one foot from the ground, and similarly, until six feet be shown at the other end of the staff.

The feet are marked 1, 2, 3, &c., from the upper end, and are reversed in the present position of the staff; but are upright when the staff is placed for use. In the last position of the staff, the count is made at the *lower line of the vane*.

174. There is a method of testing the adjustments of the level, which ought not to be neglected, since all the results depend on the accuracy of the instrument. The method is this:

The level being adjusted, place it at any convenient point, as  $G$  (Fig. 4). At equal distances of about 100 yards, on either side, and in the same line with the level, place the levelling staves  $CE$ ,  $BF$ . Make the level horizontal with the levelling screws. Then, turn it towards either staff, as  $BF$ , and run the vane up or down, as required, until the intersection of the hairs strikes the centre: then make the slide fast, and note carefully the height of the vane. Turn the level half round, and do the same in respect of the staff  $CE$ . Let the telescope be now reversed in the  $Y$ 's. Sight again to the staff  $BF$ , and note the exact height of the vane. Let the telescope be now turned half round, and the same be done for the staff  $CE$ . If the two heights last observed, are equal to those first noted, each to each, the line of collimation will be perpendicular to the axis of the instrument, and if the bubble has, at the same time, preserved its place at the middle point of the tube, the instrument is truly adjusted.

For, had the line of collimation been inclined to the axis of the level, it would, in the first instance, have taken the direction  $AF$  or  $Ad$ ; and when turned half round, it would have taken the direction  $Ab$  or  $AE$ . The telescope being

reversed in the  $Y$ 's, and again directed to the staff  $BF$ , the line of collimation would take the direction  $Ad$  or  $AF$ , and when turned to the staff  $CE$ , it would take the direction  $AE$  or  $Ab$ : and the two distances  $BF$ ,  $Bd$ , or  $Cb$ ,  $CE$ , can only be equal to each other when the line of collimation falls on the horizontal line  $gf$ .

175. Having described the instruments used in levelling, we will explain the practical operations on the field.

When it is proposed to find the difference of level of any two objects, or stations, all levels made in the direction of the station at which the work is begun, are, for the sake of distinction merely, called *back-sights*; and levels taken in the direction of the other station, *fore-sights*.

Before going on the field with the level, rule three columns, as below, and head them, stations, back-sights, fore-sights.

Stations.	Back-Sights.	Fore-Sights.
1	10	3
2	11-6	0
3	6-8	4-9
4	3-9	8-3
Sums . . . .	31-11 16-00	16-0
Dif. of level . . .	15-11	

#### PROBLEM.

176. To find the difference of level between any two points, as  $A$  and  $G$  (Pl. 4, Fig. 5).

The level being adjusted, place it at any point as  $B$ , as nearly in the line joining  $A$  and  $G$  as may be convenient. Place a levelling staff at  $A$ , and another at  $N$ , a point lying as near as may be in the direction of  $G$ . Make the level horizontal, by means of the levelling screws; turn the telescope to the staff at  $A$ , and direct the person at the staff to slide up the vane until the horizontal line  $ab$  cuts its centre; then note the distance  $Ab$  (equal to 10 feet in the present example), and enter it in the column of back-sights, opposite station 1. Sight also to the staff at  $N$ , and enter the distance



$\mathcal{N}a$ , equal to 3 feet, in the column of fore-sights, opposite station 1.

Take up the level, and place it at some other convenient station, as  $C$ , and remove the staff at  $A$ , to  $M$ . Having levelled the instrument, sight to the staff at  $\mathcal{N}$ , and enter the distance  $\mathcal{N}d$ , 11 feet 6 inches, in the column of back-sights, opposite station 2: sight also to the staff at  $M$ , and enter the distance  $Mf$ , equal 0, in the column of fore-sights, opposite station 2.

Let the level be now removed to any other station, as  $D$ , and the staff at  $\mathcal{N}$ , to some other point, as  $P$ . Let the distance  $Mg$ , equal to 6 feet 8 inches, be entered in the column of back-sights, opposite station 3, and the distance  $Ph$ , equal to 4 feet 9 inches, in the column of fore-sights. Let the instrument be now placed at  $E$ , and the distance  $Pm$ , equal to 3 feet 9 inches, and  $Gn$ , equal to 8 feet 3 inches, be entered opposite station 4, in their proper columns.

By adding up the columns, we find, that the sum of the back-sights is equal to 31 feet 11 inches, and the sum of the fore-sights, 16 feet; the difference, 15 feet and 11 inches, is the difference of level of the points  $A$  and  $G$ .

#### DEMONSTRATION.

Let the back-sights be called plus, and the fore-sights, minus.

Then, having let fall the perpendiculars  $\mathcal{N}F$ ,  $MH$ ,  $PI$ , and  $GL$ , on the horizontal line  $AL$ , it remains to be proved, that the difference of level,

$$GL = Ab + \mathcal{N}d + Mg + Pm - \mathcal{N}a - 0 - hP - nG.$$

$$\text{Now, } Ab + \mathcal{N}d - \mathcal{N}a = Ab + ad = Fd;$$

$$\text{Therefore, } GL = Fd + Mg + Pm - hP - nG.$$

$$\text{But } Fd + Mg = Hg, \text{ and } +Pm - hP = -hm,$$

$$\text{Therefore, } GL = Hg - hm - nG = hI - (hm + nG) = GL.$$

As the same may be shown in every example, we conclude that, *the difference between the sum of the fore-sights and the sum of the back-sights is, in all cases, equal to the difference of level.*

It is also evident that, when the sum of the back-sights exceeds the sum of the fore-sights, the last station is more elevated than the first; and, conversely, if the sum of the

back-sights is less than the sum of the fore-sights, the second station is lower than the first.

177. In this example, we have not regarded the difference between the true and apparent level. If it be necessary to ascertain the result with extreme accuracy, this difference must be considered; and then, the horizontal distances between the level, at each of its positions, and the staves, must be measured, and the apparent levels diminished by the differences of level; which differences can be found from the table.

*The following is such an Example.*

Stat.	Back-sts.	Distances.	Fore-st.	Distances.	Cor. back-sights.	Cor. fore-sts.
1	9-8	20 ch.	1-6	32 ch.	9-7.500	1-4.720
2	8-7	25 ch.	2-4	28 ch.	8-6.219	2-3.019
3	5-2	18 ch.	3-1	16 ch.	5-1.595	3-0.680
4	10-3	29 ch.	1-9	87 ch.	10-1.949	0-11.538
5	11-0	45 ch.	2-5	72 ch.	10-9.469	1-10.520
					44-2.732	9-6.477

In this example, the first column shows the stations; the second, the back-sights; the third, the distances from the level in each of its positions to the back staff; the fourth, the fore-sights; the fifth, the distances from the level to the forward staff; the sixth and seventh, are the columns of back and fore sights, corrected by the difference of level. The corrections are thus made:—The difference of level in the table corresponding to 20 chains, is 5 tenths of an inch, which being subtracted from 9 feet 8 inches, leaves 9 feet 7.5 inches for the corrected back-sight; this is entered opposite station 1 in the sixth column. The difference of level corresponding to 32 chains, is 1.280 inches, which being subtracted from the apparent level, 1 foot 6 inches, leaves 1 foot 4.720 inches for the true fore-sight from station 1. The other corrections are made in the same manner.

The sum of the back-sights being 44 feet 2.732 inches, and the sum of the fore-sights 9 feet 6.477 inches, it follows,

that the difference, 34 feet 8.255 inches, is the true difference of level.

178. In finding the true from the apparent level, we have not regarded the effect caused by refraction on the apparent elevation of objects, as well because the refraction is different in different states of the atmosphere, as because the corrections are inconsiderable in themselves.

179. The small errors that would arise from regarding the apparent as the true level, may be avoided by placing the levelling staves at equal distances from the level. In such case, it is plain, 1st, that equal corrections must be made in the fore and back sights; and, 2dly, that when the fore and back sights are diminished equally, the result, which is always the difference of their sums, will not be affected.

This method should always be followed, if practicable, as it avoids the trouble of making corrections for the difference of true and apparent level.

The differences between the true and apparent level, being very inconsiderable for short distances, if only ordinary accuracy be required, it will be unnecessary to make measurements at all. Care, however, ought to be taken, in placing the levelling staves, to have them as nearly at equal distances from the level as can be determined by the eye; and if the distances are unequal, let the next distances also be made unequal; that is, if the back-sight was the longest in the first case, let it be made proportionably shorter in the second, and the reverse.

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## CHAPTER VI.

*Of the methods of showing the contour and accidents of ground.*

180. Besides the surveys that are made to determine the area of land and the relative positions of objects, it is frequently necessary to make minute and careful examinations for the purpose of ascertaining the form and accidents of the ground, and to make such a plan as will distinguish the

swelling hill from the sunken valley, and the course of the rivulet from the unbroken plain.

181. This branch of surveying is called Topography. In surveys made with a view to the location of extensive works, the determination of the slopes and irregularities of the ground is of the first importance: indeed, the examinations would otherwise be useless.

182. The manner of ascertaining these irregularities is, to intersect the surface of the ground by a system of horizontal planes at equal distances from each other; the curves determined by these secant planes, being lines of the surface, will indicate its form at the places of section, and, as the curves are more or less numerous, the form of the surface will be more or less accurately ascertained.

If such a system of curves be determined, and then projected or let fall on a horizontal plane, it is obvious that the curves on such plane will be nearer together or farther apart, as the ascent of the hill is steep or gentle.

If, therefore, such intersections be made, and the curves so determined be accurately delineated on paper, the map will present such a representation of the ground as will show its form, its inequalities, and its striking characteristics.

183. The subject divides itself, naturally, into two parts.

First, To make the necessary examinations and measurements on the field.

And, 2dly, to make the delineations on paper.

For the former of these objects, the theodolite is the best instrument; the common level, however, will answer all the purposes, though it is less convenient.

Before going on the field, it is necessary to provide a number of wooden stakes, about two feet in length, with heads. These stakes are used to designate particular points, and are to be driven to the surface of the ground. A nail should then be driven into the head of each of them, to mark its centre.

184. We shall, perhaps, be best understood, by giving an example or two, and then adding such general remarks as will extend the particular cases to all others that can occur.

Let *A* (Pl. 4, Fig. 6), be the summit of a hill, the contour of

which it is required to represent. At  $A$ , let a stake be driven, and let the axis of the theodolite, or level, be placed directly over the nail which marks its centre. From  $A$ , measure any line down the hill, as  $AB$ , using the telescope of the theodolite or level to arrange all its points in the same vertical plane. Great care must be taken to keep the measuring chain horizontal, for it is the *horizontal distances* that are required. At different points of this line, as  $a, b, c, d$ , &c., let stakes be driven, and let the horizontal distances  $Aa, ab, bc$ , and  $cd$ , be carefully measured. In placing the stakes, reference must be had to the abruptness of the declivity, and the accuracy with which the surface is to be delineated: their differences of level ought not to exceed once and a half, or twice, the distance between the horizontal planes of section.

Having placed stakes, and measured all the distances along the line  $AB$ , run another line down the hill, as  $AC$ , placing stakes at the points  $e, f, g$ , and  $h$ , and measuring the horizontal distances  $Ae, ef, fg$ , and  $gh$ . Run also the line  $AD$ , placing stakes at  $i, l, m$ , and  $n$ , and measuring the horizontal distances  $Ai, il, lm$ , and  $mn$ .

Each line,  $AB, AC, AD$ , running down the hill from  $A$ , may be regarded as the intersection of the hill by a vertical plane; and these secant planes are to be continued over all the ground which is to be surveyed. If the work is done with a theodolite, or with a level having a compass, the angles  $DAB$  and  $BAC$ , contained by the vertical secant planes, can be measured; if it is done with a level, having no needle, let any of the distances  $ae, bf, ai, bl$ , &c. be measured with the chain, and there will then be known the three sides of the triangles  $Aae, Abf, Aai, Abl$ , &c.

Let now, the difference of level of the several points marked in each of the lines  $AB, AD, AC$ , be determined.

In the present example the results of the measurements and levelling, are—

#### Line $AB$ .

Distances.		Difference of Level.
$Aa = 40$ feet		$A$ above $a$ 12 feet
$ab = 50$ "		$a$ above $b$ 8 "
$bc = 30$ "		$b$ above $c$ 9 "
$cd = 46$ "		$c$ above $d$ 11 "

Line *AC*.

Distances.	Difference of Level
<i>Ae</i> = 28 feet	<i>A</i> above <i>e</i> 11 feet
<i>ef</i> = 45 "	<i>e</i> above <i>f</i> 9 "
<i>fg</i> = 55 "	<i>f</i> above <i>g</i> 12 "
<i>gh</i> = 49 "	<i>g</i> above <i>h</i> 14 "

Line *AD*.

Distances.	Difference of Level.
<i>Ai</i> = 25 feet	<i>A</i> above <i>i</i> 9 feet
<i>il</i> = 55 "	<i>i</i> above <i>l</i> 13 "
<i>lm</i> = 38 "	<i>l</i> above <i>m</i> 7 "
<i>mn</i> = 48 "	<i>m</i> above <i>n</i> 14 "

Angle *CAB* = 25°, Angle *DAB* = 30°.

These data are sufficient, not only to find the intersections of horizontal planes with the surface of the hill, but also for delineating such curves of section on paper.

Having drawn on the paper the line *AB*, lay off the angle *BAC* = 25°, and the angle *BAD* = 30°. Then, from a convenient scale of equal parts, lay off the distances *Aa*, *ab*, *bc*, *cd*, *Ae*, *ef*, *fg*, *gh*, *Ai*, *il*, *lm*, and *mn*.

Let it be required that the horizontal planes be at a distance of eight feet from each other. Since *A* is the highest point of the hill, and the difference of level of the points *A* and *a*, is 12 feet, the first plane, reckoning downwards, will intersect the line traced on the ground from *A* to *B*, between *A* and *a*. Regarding the descent as uniform, which we may do for small distances without sensible error, we have this proportion; as the difference of level of the points *A* and *a*, is to the horizontal distance *Aa*, so is 8 feet, to the horizontal distance from *A* to where the first horizontal plane will cut the line from *A* to *B*. This distance being thus found, and laid off from *A* to *o*, gives *o*, a point of the curve in which the first plane intersects the ground. The points at which it cuts the line from *A* to *C*, and the line from *A* to *D*, are determined similarly, and three points in the first curve are thus found.

By the aid of the sector, the graphic operations are greatly facilitated. Let it be borne in mind, that the descent from *A* to *a*, is 12 feet, and that it is required, upon the supposition

of the descent being uniform, to find that part of the distance corresponding to a descent of 8 feet. Take the distance from  $A$  to  $a$ , in the dividers, and open the arms of the sector until the dividers will reach from 12 on the line of equal parts, on one side, to 12 on the line of equal parts, on the other. Then, without changing the angle, extend the dividers from 8 on one side, to 8 on the other; this will give the proportional distance to be laid off from  $A$  to  $o$ . Or, if the dividers be extended from 4 to 4, the proportional distance may be laid off from  $a$  to  $o$ .

If the distances to be taken from the sector fall too near the joint, let multiples of them be used; as for instance, on the French sectors, let the arms be extended until the dividers reach from 120 on the one, to 120 on the other, then 80 or 40 will be the proportional numbers. Other multiples may be used, though it is generally more convenient to multiply by 10.

The second plane is to pass 8 feet below the first, that is, 16 feet below  $A$ , or 4 feet below  $a$ ,  $a$  being 12 feet below  $A$ . Take the distance  $ab$  in the dividers, and extend the sector, so that the dividers will reach from 8 to (the descent from  $a$  to  $b$  being 8 feet) 8, or from 80 to 80; then, the distance from 4 to 4, or from 40 to 40, being laid off from  $a$  to  $p$ , gives  $p$ , a point of the second curve.

The difference of level between  $a$  and  $b$  being 8 feet, and the difference of level between  $a$  and  $p$  being 4 feet, the difference of level between  $p$  and  $b$  must also be 4 feet: hence, the third plane will pass 4 feet below  $b$ , and  $q$ , determined as above, is a point of the third curve.

The difference of level between  $b$  and  $c$  being 9 feet, and consequently between  $q$  and  $c$ , 5 feet, the fourth plane will pass 3 feet below  $c$ , and  $r$  is a point of the fourth curve.

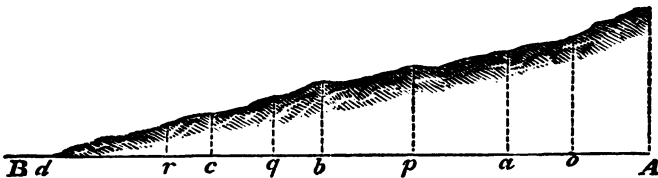
The difference of level between  $c$  and  $d$  being 11 feet, the difference of level between  $r$  and  $d$  is 8 feet; so that the fifth plane will pass through  $d$ , which is consequently a point of the fifth curve.

The points at which the horizontal planes cut the lines drawn from  $A$  to  $C$ , and from  $A$  to  $D$ , are determined in a manner entirely similar. Having thus made as many diverging sections from the point  $A$  as may be necessary, and found the points in which they are cut by horizontal planes, the

horizontal curves of section can be described through the several corresponding points. These curves being represented on paper, their curvature shows the form of the surface of the hill in the direction of a horizontal line traced around it; and the distances between them, the abruptness or gentleness of the declivity. The numbers (8), (16), &c. show the vertical distances of the respective planes below the point *A*.

Having drawn the horizontal curves, the next thing to be done is so to shade the drawing that it may represent accurately the surface of the ground. This is done by drawing a system of small broken lines, as in the figure, perpendicular in direction to the horizontal curves already described. In all topographical representations of undulating ground, the lines of shading are drawn perpendicular to the horizontal curves.

185. If it be required to show a profile of the ground, let the vertical plane passing through *A* and *B* be revolved about its intersection with a horizontal plane passing through *d*. Erect perpendiculars at *r*, *c*, *q*, *b*, *p*, *a*, *o*, and *A*, to the line *BA*, and make them equal to the respective distances of these points above the horizontal plane passing through *d*, viz. at *r*, 8 feet, at *c*, 11, at *q*, 16, at *b*, 20, at *p*, 24, at *a*, 28, at *o*, 32, and at *A*, 40; and through the extremities of the perpendiculars so determined, let a curve be traced: this curve will be the curve of the hill from *d* to *A*.



186. This method of finding the form of the surface of a hill, is perhaps the best, when the hill slopes gradually from its summit, and the declivity is sufficiently gentle to measure down it. If the surface were that of an undulating plain, the following method is preferable.

Measure a horizontal line, as *AB* (Pl. 4, Fig. 7), running along one side of the ground to be surveyed. At the extremities *A* and *B*, erect the perpendiculars *AD* and *BC*, and produce them until all the land to be surveyed shall be in-



cluded within the rectangle  $ABCD$ . On the line  $AB$ , measure the horizontal distances  $AE$ ,  $EF$ ,  $FG$ , and  $GB$ ; and on the line  $DC$ , the distances  $DH$ ,  $HI$ ,  $IL$ , and  $LC$ , respectively equal to the distances on  $AB$ : that is,  $DH=AE$ ,  $HI=EF$ , &c. The distances  $AE$ ,  $EF$ , &c. are regulated by the inequalities of the ground, being less if the changes in the surface are considerable, and greater if the changes are nearly uniform. In the present example, they are 100 feet each, which, upon ordinary ground, would render the work tolerably accurate.

Let stakes be driven at  $A$ ,  $E$ ,  $F$ ,  $G$ ,  $B$ ,  $C$ ,  $L$ ,  $I$ ,  $H$ , and  $D$ . Measure now the line  $AD$ , and place stakes at convenient distances, as  $a$ ,  $b$ ,  $c$ , and  $d$ : place stakes also along the other lines  $EH$ ,  $FI$ ,  $GL$ , and  $BC$ , at suitable points, and measure the respective distances  $Ef$ ,  $fg$ , &c. It is best to use the telescope of the theodolite or level, in order to run the lines and place the stakes truly. In placing the stakes, it should be borne in mind, that the difference of level of either two that follow each other, ought not to be very great; and also, that they ought not to be on the same horizontal plane.

After the stakes are all placed, and the distances measured, let the differences of level of all the points so designated be found. In the present example, the results of the measurements are—

$Aa = 80$	$AE = 100$	$EF = 100$	$FG = 100$	$GB = 100$
$ab = 60$	$Ef = 105$	$Fi = 74$	$Gm = 96$	$Bq = 76$
$bc = 90$	$fg = 85$	$ik = 115$	$mn = 76$	$qs = 85$
$cd = 55$	$gh = 71$	$kl = 60$	$np = 76$	$st = 127$
$dD = 50$	$hH = 74$	$li = 86$	$pL = 87$	$tC = 47$

### Of the Levelling.

Line $AD$ .	Line $EH$ .	Line $FI$ .	Line $GL$ .	Line $BC$ .
$A$ above $a$ 5	$E$ below $A$ 3	$F$ below $E$ 2	$G$ below $F$ 1	$B$ below $G$ 2
$a$ " $b$ 6	$E$ above $f$ 9	$F$ above $i$ 3	$G$ above $m$ 2	$B$ above $q$ 3
$b$ " $c$ 7	$f$ " $g$ 3	$i$ " $k$ 5	$m$ " $n$ 1	$q$ " $s$ 2
$c$ below $d$ 2	$g$ " $h$ 1	$k$ " $l$ 2	$n$ " $p$ 2	$s$ " $t$ 3
$d$ above $D$ 4	$h$ below $H$ 3	$l$ below $I$ 3	$p$ below $L$ 4	$t$ below $C$ 5

The heights of the points are here compared with each other, two and two. Before, however, we can conceive clearly their relative heights, we must assume some one point,

and compare all the others with it. Let the point *A* be taken. The height of

<i>A</i> above <i>u</i>	5	<i>A</i> above <i>f</i>	12	<i>A</i> above <i>k</i>	13	<i>A</i> above <i>p</i>	11
<i>A</i> " <i>b</i>	11	<i>A</i> " <i>g</i>	15	<i>A</i> " <i>l</i>	15	<i>A</i> " <i>L</i>	7
<i>A</i> " <i>c</i>	18	<i>A</i> " <i>h</i>	16	<i>A</i> " <i>I</i>	12	<i>A</i> " <i>B</i>	8
<i>A</i> " <i>d</i>	16	<i>A</i> " <i>H</i>	13	<i>A</i> " <i>G</i>	6	<i>A</i> " <i>q</i>	11
<i>A</i> " <i>D</i>	20	<i>A</i> " <i>F</i>	5	<i>A</i> " <i>m</i>	8	<i>A</i> " <i>s</i>	13
<i>A</i> " <i>E</i>	3	<i>A</i> " <i>i</i>	8	<i>A</i> " <i>n</i>	9	<i>A</i> " <i>t</i>	16

And of *A* above *C*, 11 feet.

This being done, a mere inspection shows us the highest and lowest points, as also the relative heights of the others, reckoning upwards or downwards: Let them be now written in the order of their heights above the lowest point, which is *D*. The difference of level between *A* and *D* being 20 feet, if the difference of level of each of the points below *A*, be taken from 20 feet, the remainder will be the height above *D*. Arranging them in their order, we have

<i>c</i> above <i>D</i>	2	<i>H</i> above <i>D</i>	7	<i>p</i> above <i>D</i>	9	<i>B</i> above <i>D</i>	12
<i>d</i> " <i>D</i>	4	<i>k</i> " <i>D</i>	7	<i>q</i> " <i>D</i>	9	<i>L</i> " <i>D</i>	13
<i>h</i> " <i>D</i>	4	<i>s</i> " <i>D</i>	7	<i>C</i> " <i>D</i>	9	<i>G</i> " <i>D</i>	14
<i>t</i> " <i>D</i>	4	<i>f</i> " <i>D</i>	8	<i>n</i> " <i>D</i>	11	<i>a</i> " <i>D</i>	15
<i>g</i> " <i>D</i>	5	<i>I</i> " <i>D</i>	8	<i>i</i> " <i>D</i>	12	<i>F</i> " <i>D</i>	15
<i>l</i> " <i>D</i>	5	<i>b</i> " <i>D</i>	9	<i>m</i> " <i>D</i>	12	<i>E</i> " <i>D</i>	17

*A* above *D*, 20 feet.

Let the surface be now intersected by a system of horizontal planes at 3 feet from each other,—the first plane being 3 feet above the point *D*. The point *b* being 9 feet above *D*, and the point *c*, 2 feet, the first plane will intersect the line *AD* between *b* and *c*: let the proportional distance be found, as in the last example, and one point *u*, of the first curve, will be known. The point *H* being 7 feet above *D*, the plane will cut the line *DC* between *H* and *D*, and finding the proportional distance as before, a second point, *v*, of the first curve, is determined. Now, in drawing this curve, it will be borne in mind, that the point *h* is but 4 feet above *D*, and consequently but 1 foot above the first curve, so that the curve must run from *u* towards *h*, and then turn around to the point *v*. The curve is marked (3), which is the number of feet that it is above the lowest point, and similarly for the

other curves of the figure; their number showing their distance in feet above  $D$ . Around the point  $d$ , there is a small curve, also marked (3). By inspecting the table, it will be seen that  $d$  is 4 feet above  $D$ , and that the ground descends from  $d$  towards  $D$  and  $c$ :  $d$  is therefore a small knoll, the top of which is cut off by the first plane. To show that the ground descends from  $d$ , even below the first curve (3), a plane is passed 1 foot below the first plane, or 2 feet above  $D$ ; the curve of section is marked (2).

The second of the system of curves, or the one marked (6), must cut the line  $AD$  between  $b$  and  $c$ , the line  $EH$  between  $f$  and  $g$ , the line  $FI$  between  $k$  and  $l$ , and also between  $l$  and  $I$ ; it also cuts  $EH$  again between  $h$  and  $H$ , and the line  $DC$  between  $H$  and  $D$ .

The third curve, or the one passing 9 feet above  $D$ , passes through  $b$ , cuts the line  $EH$  between  $E$  and  $f$ , the line  $FI$  between  $i$  and  $k$ ; thence it passes to  $p$ , and thence to the line  $DC$ , crossing it between  $I$  and  $L$ . There is also another curve determined by this plane, since it passes through the points  $C$  and  $q$ , leaving the points  $t$  and  $s$  below it. This curve runs from  $C$  to  $p$ , and from  $p$  to  $q$ , as drawn in the figure.

The fourth curve, marked (12), intersects the line  $AD$  between  $a$  and  $b$ ,  $EH$  between  $E$  and  $f$ ,  $FI$  at  $i$ ,  $GL$  at  $m$ , and  $BC$  at  $B$ . There is also another curve lying around the point  $L$ : for the plane cuts  $GL$  between  $p$  and  $L$ , the line  $DC$  between  $C$  and  $L$ , and again between  $I$  and  $L$ .

The fifth curve, marked (15), cuts  $AD$  at  $a$ ,  $EH$  between  $E$  and  $f$ , and  $AB$  at  $F$ . The sixth curve, marked (18), cuts  $AD$  between  $A$  and  $a$ , and  $AB$  between  $A$  and  $E$ . The proportional distances in all these cases are found as in the first example.

In looking on the little map that has been made, it is clearly indicated by the curves and shading, that the ground slopes from  $A$  to  $c$ , thence rises to  $d$ , and then slopes to  $D$ . It also slopes from  $A$  along the line  $AB$ ; from  $E$  in the directions  $f$  and  $i$ , from  $F$  in the directions  $i$  and  $m$ , from  $G$  in the directions  $m$  and  $B$ , and from  $B$  in the direction  $Bqs$ . The ground also slopes from  $L$  to  $p$ , thence to  $l$  and  $h$ , and along to curve (2), and the point  $D$ : and on the other side to  $t$  and  $s$ .

187. Thus far, we have said nothing of a *plane of reference*, which is any horizontal plane to which the levels of all the points are referred. In the first example, the plane of reference was assumed through the point *A* (Pl. 4, Fig. 6), and tangent to the surface of the hill: in the second example, it was taken through *D*, the lowest point of the work.

188. After having compared all the levels with any one point, the highest and the lowest points are at once discovered, and the plane of reference may be assumed through either of them. As, however, in comparing the heights of objects, the mind most readily refers the higher to the lower, it is considered preferable to take the plane of reference through the lowest point. We say, for example, that the summit of a hill is 200 feet above a given plain, and not that the plain is 200 feet below the summit of the hill; so we say that a plain is at a given distance above a river, and not that the river is below the plain. This habit of the mind of referring the higher to the lower objects, suggests the propriety of taking the plane of reference through the lowest point, where there is no other circumstance to influence its selection. If, however, there are fixed and permanent objects, to which, as points of comparison, the mind readily refers all others, such as the court-house or church of a village, the market-house of a town, or any public building or monument, it is best to assume the plane of reference through some such point; for, it must be kept in mind, that the ends proposed in the construction of maps, are, to present an accurate view of the ground, its form, its accidents, and the relative position of objects upon it.

189. When the plane of reference is so chosen that the points of the work fall on different sides of it, all the references on one side are called positive, and those on the other, negative. The curves having a negative reference are distinguished by placing the minus sign before the number; thus - ( ).

190. In topographical surveys, great care should be taken to leave some *permanent marks*, with their levels written on them in a durable manner. For example, if there are any rocks, let one or more of them be smoothed, and the vertical distance from the plane of reference marked thereon: or let

the vertical distance of a point on some prominent building, be ascertained and marked permanently on the building. Such points should also be noted on the map, so that a person, although unacquainted with the ground, could by means of the map, go upon it, and trace out all the points, together with their differences of level.

191. The manner of shading the map, so as to indicate the hills and slopes, consists in drawing the lines of shading perpendicular to the horizontal curves, as already explained.

192. In making topographical surveys, the great point is, to determine the curves which result from the intersection of the surface by horizontal planes.

Besides the methods of diverging and parallel sections, we may assume a point on the surface of a hill, place the level there, and run a line of level round the hill, measuring the angles at every turn or change of direction: such a line will be a horizontal curve. Then, levelling up or down the hill, a distance equal to the vertical distance between the horizontal curves, let a second curve be traced; and similarly for as many curves as may be necessary.

This method, however, is not as good as the methods before explained.

193. Besides representing the contour of the ground, it is often necessary to make a map which shall indicate the cultivated field, the woodland, the marsh, and the winding river. For this, certain characters, or conventional signs, have been agreed upon, as the representatives of things, and when these are once fixed in the mind, they readily suggest the objects for which they stand. Those which are given in Plates 5 and 6, have been adopted by the Engineer Department, and are used in all plans and maps made by the United States Engineers.

It is very desirable that a uniform method of delineation should be adopted, and none would seem to be of higher authority than that established by the Topographical Beaureau. It is, therefore, recommended, that the conventional signs given in Plates 5 and 6, be carefully studied and closely followed.

## CHAPTER VII.

*Of Surveying Harbours.*

194. There are two objects to be attained in the survey of a harbour.

1st. To survey the shore along high or low water mark, to trace its windings, to note the points and inlets, and to ascertain and fix the places at which rivers and creeks discharge themselves. And,

2dly. To discover the channels, their direction, depth, and width; the position of shoals, the depth of water upon them, the nature of the bottom, and in short, whatever may contribute to easy and safe navigation.

*To determine the principal points and trace the shore.*

195. Having provided a boat and crew, row once or twice around the harbour, mark the more important and prominent points; at which, let station-staves with flags upon them be erected.

Then, measure a base line, and form a series of triangles, having their angles at the stations already chosen. Let the angles of these triangles be measured with the theodolite, and their sides calculated; after which, the high or low water mark may be traced along the shore with the compass, as hereafter explained.

Let us suppose that Plate 6 is a map of a harbour to be surveyed.

We see, by inspecting it, that the upper end of the lake at *A*, the termination of the harbour at *B*, the rocks at *C*, the point at *D*, the fisheries at *E*, and the two bays at *F* and *G*, are all prominent points. At these points, therefore, let station-flags be placed. Then, measure the distance from *A* to *B*, for a base line, and let the work be begun at *A*.

Remove the staff at *A*, and place, by means of a plumb-line, the axis of the theodolite over the station. Then, having levelled the instrument, bring the 0 of the eyeglass vernier to coincide with the 0 of the limb, and tighten the clamp-screw of the vernier plate. Loosen the lower clamp-screw, and turn

the body of the instrument until the telescope comes nearly on the base line  $AB$ : then tighten the clamp-screw  $K$ , and by means of the lower tangent-screw  $L$ , and the thumb-screw  $Z$ , bring the intersection of the spider's lines to coincide with the bottom of the staff at  $B$ . Then, direct the lower telescope to the same point, without moving the limb.

Having thus placed the instrument, examine the opposite vernier, and if it stands exactly at  $180^\circ$ , enter the direction from  $A$  to  $B$ ,  $00$ , as in the field notes below.

But if the reading of the opposite vernier exceeds  $180^\circ$ , enter half the excess for the direction. If the reading is less than  $180^\circ$ , take half of what it falls short, from  $360^\circ$ , and enter the remainder for the direction from  $A$  to  $B$ .

The two verniers are used to avoid any error which might arise from a defective graduation of the limb, or from an imperfect centring. A false centring, is when the centre of the limb or vernier plate is out of the axis of the instrument, and when this is the case, it is a fruitful source of error.

Both verniers should be read at every observation, and a mean between the readings taken for the true direction.

Having thus placed the instrument, loosen the clamp-screw of the vernier plate, and direct the telescope to station  $E$ . Note the degrees, and take a mean between the readings of the two verniers for the minutes, and enter the result opposite direction  $AE$ , as in the field notes. Do the same for the station  $G$ , and then enter in a column to the right, the angle formed by the lines which join the stations. The angle will either be the difference of the readings, or the difference between  $360^\circ$  and the larger reading, plus the smaller reading.

*Station A.*

Direction $AB$ . . .	00	
Direction $AE$ . . .	$73^\circ 25'$	$BAE = 73^\circ 25'$
Direction $AG$ . . .	$138^\circ 35'$	$EAG = 65^\circ 10'$

Having sighted to all the stations which can be seen from  $A$ , remove the instrument and replace the station staff.

Take the theodolite to  $B$ , the other extremity of the base line. It is now required to place the instrument in such a manner that the horizontal limb shall have the same relative position with the base line  $AB$ , as it had at the station  $A$

For this purpose, after having levelled the instrument, add  $180^\circ$  to the direction from  $A$  to  $B$ , and place the 0 of the eyeglass vernier at the point so found. Then clamp the vernier plate, after which direct both the telescopes to station  $A$ . It is now plain that the line of the limb drawn through 0 and  $180^\circ$  will coincide with the base line  $AB$ , the 0 being towards  $A$ , as before; hence the theodolite is like placed.

Having clamped the limb, loosen the clamp-screw of the vernier plate, and sight to stations  $E$  and  $C$ , and enter the directions as below.

*Station B.*

Direction $BA$ . . .	$180^\circ 00'$	
Direction $BE$ . . .	$139^\circ 40'$	$ABE=40^\circ 20'$
Direction $BC$ . . .	$57^\circ 12'$	$EBC=82^\circ 28'$

Having sighted to all the stations which can be seen from  $B$ , replace the station-staff and remove the instrument to station  $C$ . To the direction  $BC=57^\circ 12'$  add  $180^\circ$ , and the sum is  $237^\circ 12'$ . Having levelled the instrument, place the 0 of the eyeglass vernier at  $237^\circ 12'$ , and then sight to station  $B$ . The limb of the theodolite will then have the same relative position as at the stations  $A$  and  $B$ . Then sight to  $E$  and  $D$ , and enter the directions as below.

*Station C.*

Direction $CB$ . . .	$237^\circ 12'$	
Direction $CE$ . . .	$180^\circ 27'$	$BCE=56^\circ 45'$
Direction $CD$ . . .	$150^\circ 27'$	$ECD=30^\circ 00'$

Remove the instrument to  $E$ . To the direction  $CE=180^\circ 27'$ , add  $180^\circ$ , and the sum will be  $360^\circ 27'$ . Then place the 0 of the vernier at  $27'$ , and direct the telescope to  $C$ . Or, the theodolite may be placed at  $E$  by adding  $180^\circ$  to the direction  $AE$ , as taken from  $A$ , or to the direction  $BE$ , as taken from  $B$ , and then directing the telescope to  $A$  or  $B$ .

By placing the instrument in a similar manner at every station, the line of the limb passing through 0 and  $180^\circ$ , continues parallel to the base  $AB$ , the 0 being constantly in the direction towards  $A$ . The instrument is thus placed at all the stations, and the following are the results of the measurements of the angles.



## Station E.

Direction <i>EC</i> . . . $0^{\circ} 27'$	
Direction <i>EB</i> . . $319^{\circ} 40'$	$CEB = 40^{\circ} 47'$
Direction <i>EA</i> . . $253^{\circ} 25'$	$BEA = 66^{\circ} 15'$
Direction <i>EG</i> . . $199^{\circ} 15'$	$AEG = 54^{\circ} 10'$
Direction <i>EF</i> . . $164^{\circ} 10'$	$GEF = 35^{\circ} 05'$
Direction <i>ED</i> . . $94^{\circ} 10'$	$FED = 70^{\circ} 00'$

## Station D.

Direction <i>DC</i> . . $330^{\circ} 27'$	
Direction <i>DE</i> . . $274^{\circ} 10'$	$CDE = 56^{\circ} 17'$
Direction <i>DF</i> . . $225^{\circ} 50'$	$EDF = 48^{\circ} 20'$

## Station F.

Direction <i>FD</i> . . . $45^{\circ} 50'$	
Direction <i>FE</i> . . $344^{\circ} 10'$	$DFE = 61^{\circ} 40'$
Direction <i>FG</i> . . $247^{\circ} 10'$	$EFG = 97^{\circ} 00'$

## Station G.

Direction <i>GF</i> . . . $67^{\circ} 10'$	
Direction <i>GE</i> . . . $19^{\circ} 15'$	$FGE = 47^{\circ} 55'$
Direction <i>GA</i> . . $318^{\circ} 35'$	$EGA = 61^{\circ} 40'$

The measurements which have been made, enable us to calculate the lengths of the lines joining the several stations. For, commencing with the triangle *AEB*, we know all the angles and the base line *AB*; we can, therefore, find the sides *EB*, *EA*. We shall then know one side and all the angles of the triangle *CEB*, and by pursuing the calculation, the sides of all the triangles can be readily found.

Since the third angle of a triangle can always be found when two of the angles are known, it may seem unnecessary to measure all the angles. But when the three angles are measured and their sum found equal to  $180^{\circ}$ , the work is proved to be right, and this verification should never be omitted.

It is not probable that the sum of the three measured angles will be exactly equal to  $180^{\circ}$ . But they ought not to differ much from it. If each of them be measured several

times, and a mean of the measurements be taken, the errors of observation and of the instrument will be much diminished.

196 The method of determining points by a series of consecutive triangles, is called the method by *triangulation*. It may be extended to any number of triangles, and if the three angles of every triangle be measured, and the work carefully verified at each step, there is little danger of error. We have applied the method only in the survey of a harbour, but it may be used with equal advantage in all surveys in which long lines are to be determined, and is, indeed, the only one that can be relied on, where great accuracy is required.

#### *Of the Manner of using the Compass.*

197. The compass is often used in connection with the theodolite, and although a rude instrument, may yet be relied on for the shorter lines and smaller parts of a survey. The following is the manner of keeping the field notes.

Divide a paper into two equal parts, by two parallel lines near to each other, and consider each part as a separate leaf or page. Each leaf is divided into three spaces, and the middle one is generally smaller than either of the others, which are equal.

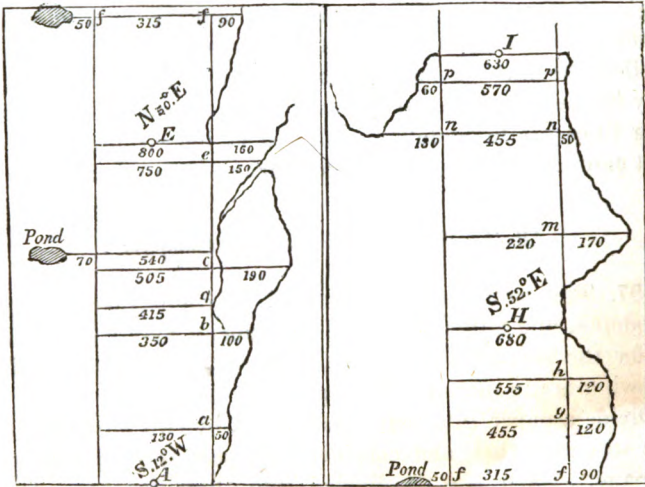
The notes begin at the bottom of the first page, and run up the page to the top. They then commence again at the bottom of the next page, and run up to the top; thence to the bottom of the third page, and thus, for as many pages as the work may require.

When the compass is used in the way we are about to explain, the distances to objects which lie on the right or left of the courses, are determined by means of offsets.

The beginning of every course is designated in the middle column by 0, and the bearing is entered directly above. The other figures of the middle column, express the distances from the beginning of each course to the offsets, and those in the side columns indicate the lengths of the offsets, or the distances to objects on the right or left of the compass lines.

The stations, at which the compass is placed, are designated by 0 in the middle column, and the bearing of each course is entered directly above.

To explain more definitely the manner of using the compass on the field, let us suppose that we have determined, with the theodolite, the prominent parts of the harbour. Place the compass at *A* (Plate 6), and take the bearing of the line *AE*, which S 12° W.



Enter this bearing at *A*. Then measure along the line *AE* any distance, as *Aa* equal to 130 yards, and make an offset to the lake, which we measure and find to be 50 yards. Enter the 130 in the middle column, and as the lake lies on the right (in going from *A* to *E*), we insert the 50 in the right hand column.

We then measure along the line *AE* to *b*, 350 yards from *A*. Here we make a second offset to the lake, and find it to be equal to 100 yards. Having entered the distances in the notes, we measure to *q*, the point where the line *AE* crosses the creek, and we enter the distance from *A*, 415 yards.

At *d*, we lay off an offset on the left, to the pond, 70 yards: at *e*, an offset to the mouth of the creek, 150 yards: and at *E*, where the course terminates, an offset to the lake, of 160 yards. The entire distance from *A* to *E* is 800 yards.

At *E*, we take the bearing to *H*, which is N 50° E. Having measured along this line to *f*, 315 yards, we make an offset to the pond, on the left, of 50 yards, and to the shore, on the right, of 90 yards. Having entered these distances,

we recommence the notes at 315 below, which we suppose to be at the bottom of the second page. Having reached *H*, the extremity of the course, we enter the entire distance from *E*, 680 yards. We next take the bearing to *I*, S 62° E. We then measure the distances to *m*, *n*, *p*, and *I*, and enter them, together with the offsets, as in the notes.

198. It is also well to make, in the columns on the right and left, such sketches of the ground, fields, houses, creeks and rivers, as will afford the means of making an accurate delineation on paper.

199. In making the plan of the harbour, it might be found convenient to use the plain-table in connexion with the theodolite and compass. For example, we might place the plain-table at *G*, and having fixed stations at the principal points of the shore, between *G* and *F*, we would sight to each of them: then remove the table to *F*, and do the same for that station: we should thus determine the points between *F* and *G*, with reference to the line *GF*.

### *Of Plotting.*

200. The lines of the triangles determined with the theodolite, can be plotted in the manner already explained. It would be better, however, to use the instrument which we are about to describe, and which is called

#### THE CIRCULAR PROTRACTOR.

201. This instrument consists of a brass circular limb (Pl. 2, Fig. 4), of about six inches in diameter, with a moveable index *AB*, having a vernier at one extremity *A*, and a milled screw at the other extremity *B*, with a concealed cog-wheel that works with the cogs of the limb, and thus moves the index *AB* about the centre of the protractor. At the centre of the protractor is a small circular glass plate, on which two lines are cut; the point of their intersection, is the exact centre of the instrument. The limb is generally divided to half degrees; the degrees are numbered from 0 to 360.

At the 0 point, and at the opposite extremity of the diameter passing through that point, are small lines on the inner edge of the limb; the two extremities of the diameter, perpendicular to this latter, are also designated in the same way.

Two angular pieces of brass, each having a small and sharp steel pin at its extremity, are fastened to the index, and revolve freely around the lines  $ab$  and  $cd$ . The small screws,  $a$ ,  $b$ ,  $c$ , and  $d$ , move them in the directions of the lines  $ab$ ,  $cd$ , for the purpose of bringing the steel pins exactly into the line which passes through the 0 of the index and the centre of the protractor.

To adjust them to their places, place the centre of the protractor over a marked point, and the 0 of the index to the 0 of the limb. Then mark the place of the index by the pins: after which, turn the index  $180^\circ$ , and see if the pins will mark the same points as before. If they do, the index is adjusted; if they do not, correct the error with the screws  $a$ ,  $b$ ,  $c$ , and  $d$ .

*To lay off an angle with the Protractor.*

202. Let its centre be placed over the angular point, and the diameter passing through 0 and  $180^\circ$ , on the given line. Turn the screw that works the index, until the 0 of the vernier coincides with the division corresponding to the given angle; then let the angular brass pieces be turned down; the points dotted by the steel pins will show the direction of the required line.

If this line does not pass through the angular point, the pins are out of place, and must be adjusted.

*First Method of Plotting.*

203. Suppose it were required to make the plan of the harbour on a scale of 450 yards to an inch.

Divide the length of the base line  $AB$ , which we will suppose equal to 1140 yards, by 450, and the quotient 2.53 will express the length which is to represent the base line on the paper (Art. 33).

Draw an indefinite line  $AB$ , to represent the base, and having chosen any point, as  $A$ , for the first station, lay off 2.53 inches to  $B$ . The other extremity of the base line will thus be determined.

Then, place the circular protractor at  $A$ , and lay off the angle  $BAE$ , and then the angle  $EAG$ . Next, place the protractor at  $B$ , and lay off the angles  $ABE$  and  $EBC$ . The intersection of the lines  $AE$  and  $BE$  will determine

the station *E*. Let the protractor be then placed at this point, and all the angles of station *E*, laid down.

The point *G*, where *EG* intersects *AG*, and the point *C*, where *EC* intersects *BC*, will then be found.

By placing the protractor at *C* and *G*, we can determine the points *D* and *F*, when the place, on the paper, of all the stations will be known.

To unite the work done with the compass, spread the compass-notes before you, and draw through *A* a line to represent the meridian. This line makes an angle of  $12^{\circ}$  with the course *AE*.

Then, lay off from the scale the distances *Aa*, *Ab*, *Aq*, *Ac*, *Ad*, *Ae*, and at the several points erect perpendiculars to *AE*. Lay off on these perpendiculars the lengths of the offsets, and the curve traced through the points so determined, will be the margin of the lake.

At *E*, draw a parallel to the meridian through *A*, and lay down the course *EH*, which makes an angle of  $50^{\circ}$  with the meridian. Then, lay down the several distances to the offsets, and draw the offsets and lay off their lengths. Do the same for the course *HI*, and all the compass-work will be plotted.

Had there been work done with the plain-table, it could easily be united to that done with the theodolite.

### *Second Method of Plotting.*

204. Place the centre of the protractor near the centre of the paper, and draw a line through the points 0 and  $180^{\circ}$ . This line will have the same position with the circular protractor that the base line *AB* had with the limb of the theodolite.

Lay off then from the 0 point an arc equal to the direction from *A* to *E*, also an arc equal to the direction *AG*, and through the centre point, and the points so determined, draw lines. Lay off in succession, in a similar manner, the directions taken at all the stations; and through the centre point, and the points so determined, draw lines, and designate each by the letters of the direction to which it corresponds.

Now, since all the lines drawn on the paper have the same position with the circular protractor, as the corresponding

lines on the ground have with the limb of the theodolite, it follows that each direction will be parallel to its corresponding line upon the ground.

Hence, any line may be drawn parallel to that passing through 0 and  $180^\circ$ , to represent the base line  $AB$ . Having drawn such a line, and marked a point for the station  $A$ , lay off the length of the base, and the extremity will be the station  $B$ .

Through  $A$  and  $B$ , so determined, draw parallels respectively to the lines corresponding to the directions  $AE$  and  $BE$ , and the point of intersection will determine station  $E$ . Through  $B$  and  $E$  draw parallels to the lines which correspond to the directions  $BC$ ,  $CE$ , and their point of intersection will determine station  $C$ . Through  $C$  and  $E$  draw lines parallel to the lines corresponding to the directions  $CE$  and  $ED$ , and the point of intersection will determine  $D$ . In a similar manner we may determine the stations  $F$  and  $G$ .

*Of surveying a harbour for the purpose of determining the depth of water, &c.*

205. When a harbour is surveyed for the second object, viz., for the purpose of ascertaining the channels, their depth and width, the positions of shoals, and the depth of water thereon, other means must be used, and other examinations made in addition to those already referred to.

Let buoys be anchored on the principal shoals and along the edges of the channel, and using any of the lines already determined as a base, let the angles subtended by lines drawn from its extremities, to the buoys respectively, be measured with the theodolite. Then, there will be known in each triangle the base and angles at the base, from which the distances to the buoys are easily found; and hence, their positions become known.

Having made the soundings, and ascertained the exact depth of the water at each of the buoys, several points of the harbour are established, at which the precise depth of the water is known; and by increasing the number of the buoys, the depth of the water can be found at as many points as may be deemed necessary.

206. If a person with a theodolite, or with any other instrument adapted to the measurement of horizontal angles, be

stationed at each extremity of the base line, it will not be necessary to establish buoys. A boat, provided with an anchor, a sounding line, and a signal flag, has only to throw its anchor, hoist its signal flag, and make the sounding, while the persons at the extremities of the base line measure the angles ;—from these data, the precise place of the boat can be determined.

207. There is also another method of determining the places at which the soundings are made, that admits of great despatch, and which, if the observations be made with care, affords results sufficiently accurate.

Having established, trigonometrically, three points which can be seen from all parts of the harbour, and having provided a sextant, let the sounding be made at any place in the harbour, and at the same time the three angles subtended by lines drawn to the three fixed points, measured with the sextant.

The problem, to find from these data the place of the boat at the time of the sounding, is the same as example 6, page 74.

It is only necessary to measure two of the angles, but it is safest to measure the third also, as it affords a verification of the work.

The great rapidity with which angles can be measured with the sextant, by one skilled in its use, renders this a most expeditious method of sounding and surveying a harbour.

The sextant is not described, nor are its uses explained in these Elements, because its construction combines many philosophical principles, with which the surveyor cannot be supposed conversant.

208. There is yet another method of finding the soundings, which, although not as accurate as those already explained, will, nevertheless, afford results approximating nearly to the truth. It is this :—Let a boat be rowed uniformly across the harbour, from one extremity to the other of any of the lines determined trigonometrically. Let soundings be made continually, and let the precise time of making each be carefully noted. Then, knowing the length of the entire line, the time spent in passing over it, as also the time of making each of the soundings, we can easily find the points of the line at which the several soundings were made ; and hence, the depth of water at those points becomes known. Sound-



ings may thus be made along any number of known lines, and a comparison of the depths found on different lines, at or near their points of intersection, will show with what degree of accuracy the work has been done.

209. If the soundings are made in tide-waters, the time of high tide must be carefully noted, as also the precise time of making the sounding, so that the exact depth at high or low water may be known. It is considered preferable to reduce the soundings to high-water mark, and the number of feet which the tide rises and falls should be noted on the map.

210. Having plotted the work done with the theodolite, as also the outline of the harbour traced with the compass, it remains to delineate the bottom of the harbour; and this is done by means of horizontal curves (Chap. VI), which have already been used to represent broken or undulating ground.

Let the plane of reference be taken through high-water mark, or to coincide with the surface of the water at high tide. The accuracy with which the bottom of the harbour is to be delineated, will guide us in fixing the distance between the horizontal planes of section.

The first horizontal plane should be passed at a distance below the shallowest point that has been sounded, equal to the number of feet fixed upon for the distance between the planes of section; and the curve, in which it intersects the bottom of the harbour determined as in Chapter VI. And similarly, for the other horizontal planes of section.

Having thus delineated the bottom of the harbour, and noted on the map the distance of each intersecting plane below the plane of reference, let such lines be drawn as will indicate the channels, shoals, sunken rocks, and direction of the current.

In the example given in plate 6, soundings have been made in three directions from the sand-bar in the harbour, and also from the rocky shore across to the light-house.

## CHAPTER VIII.

*Of Navigation.*

1. We have given, in the preceeding chapters of this work, various applications of Trigonometry. We propose, in the following chapter to explain the best methods of determining the place of a ship at sea. This application constitutes the science of *Navigation*.

There are two methods of determining the place of a ship at sea.

1st. When a ship departs on her voyage, if we note her courses and the distance sailed, we may, at any time, by means of Plane Trigonometry, determine her place very nearly.

2nd. By means of observations on the heavenly bodies and the aid of Spherical Trigonometry, we may determine with great accuracy, the exact place of the ship. This method is called *Nautical Astronomy*.

The first part of Navigation, viz. the cases which can be solved without the aid of observations on the heavenly bodies, will be alone treated of in this chapter.

2. The earth is nearly spherical. For the purposes of Navigation it may be considered as perfectly so. It revolves round one of its diameters, called the *axis*, in about twenty-four hours.

3. The great circle, whose poles are the extremities of the axis, is called the *equator*. The poles of the equator are called the poles of the earth—the one is called the north pole, and the other the south pole.

4. Every great circle which passes through the poles cuts the equator at right angles, and is called a *meridian circle*. Every place on the surface of the earth has its own meridian; but for the purposes of Geography and Navigation, all these meridians are reckoned from a particular meridian, which is called the *first meridian*. The English have fixed on the meridian of Greenwich Observatory for the first meridian.

5. The *longitude* of any place is the arc of the equator intercepted between the meridian of that place and the first meridian, and is east or west, according as the place lies east or west of the first meridian.

6. The *difference of longitude* of two places is the arc of the equator included between their meridians; this arc is equal to the difference of longitudes when they are of the same name, and to their sum, when they are of different names.

7. The *latitude* of a place is its distance from the equator,

measured on the meridian of the place, and is north or south according as the place lies north or south of the equator.

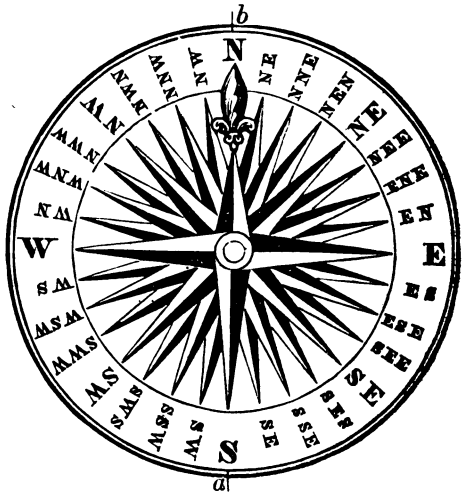
8. The small circles drawn parallel to the equator, are called *parallels* of latitude. The arc of any meridian intercepted between the parallels passing through any two places, measures the difference of latitude of those places; this difference is found by subtracting their latitudes when they are of the same name, and by adding them when they are of different names.

9. The *sensible horizon* of any place is an imaginary plane, supposed to touch the earth at that place, and to be extended to the heavens. A plane passing through the centre of the earth, and parallel to the sensible horizon, is called the *rational horizon*. The north and south line, is the intersection of the plane of the meridian circle with the sensible horizon, and the line which is drawn perpendicular to this, is called the east and west line.

10. The *course* of a ship, at any point, is the angle which her track makes with the meridian. So long as the course is unchanged, the ship would sail in a straight line, provided the meridians were truly parallel; but as the meridians bend constantly toward the pole, the direction of her path is continually changing, and she moves in a curve called the *rhumb line*. The course of a ship is indicated by the mariner's compass.

11. The *mariner's compass* consists of a circular card, whose circumference is divided into thirty-two equal parts called *points*; each point being subdivided into four equal parts called *quarter points*.

To the under side of this card a slender bar of magnetized steel, called a *needle*, is permanently attached. The direction of the needle corresponds to the diameter NS. The diameter EW, at right angles to NS, is intended to indicate the east and west points. The points of the compass are thus read: beginning at the north point, and going east, we say, *north and*



by east, north north east, north east and by north, north east; and so on, round the compass, as indicated by the letters.

The card being permitted to turn freely on the pin, on which it is poised as a centre, the line NS will always indicate the true magnetic meridian, but this, as we have seen it Art. 153, page 127, is not the *true* meridian, and hence, the variation must always be allowed for.

On the interior of the compass box, in which the card swings, are two marks, *a* and *b*, which lie in a line passing through the centre of the card, and the compass box is so placed that this line shall be parallel to the keel of the ship. Consequently, if *a* be placed towards the bow of the vessel, the point which it marks on the card will show the compass course, for the line NS is always north and south, and EW east and west. The course is generally read to quarter points, and as a quadrant contains eight points, each point will be equal to  $90^\circ \div 8 = 11^\circ 15'$ ; and a quarter point =  $11^\circ 15' \div 4 = 2^\circ 48' 45''$ . The table of Rhumbs, after the Traverse Table, shows the degrees of each course to quarter points.

12. A ship's *rate* of sailing is determined by means of an instrument, called the *log*, and an attached line called the log line. The log is a piece of wood in the form of a sector of a circle, the rim of which is loaded with lead, so that when it is heaved into the sea it assumes a vertical position. The log line is so attached as to draw the log square against the water, that it may not be drawn along after the ship as the line unwinds from the reel, by the ship's forward motion.

The time in which the log line unwinds from the reel, is noted by a sand-glass, through which the sand passes in *half* a minute; that is, in the *one hundred and twentieth part of an hour*.

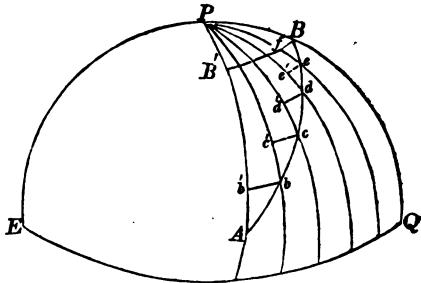
For convenience, the log line is divided into equal parts, marked by *knots*, and each part is equal to the one hundred and twentieth part of a nautical or geographical mile.\*

Now, since half a minute is the one hundred and twentieth part of an hour, and each knot measures the one hundred and twentieth part of a mile, it follows that the *number* of knots reeled off while the half minute glass runs out, will indicate how fast the ship sails per hour.

\* A geographical mile is one minute, or one-sixtieth of a degree, measured on the equator. Taking the diameter at 7916 English miles, the geographical mile will be about 6079 feet; that is, about one-sixth greater than the English mile, which is 5280 feet.

*Of Plane Sailing.*

13. Let the diagram  $EPQ$  represent a portion of the earth's surface,  $P$  the pole, and  $EQ$  the equator. Let  $AB$  be any rhumb line, or track described by a ship in sailing from  $A$  to  $B$ .



Conceive the path of the ship to be divided into very small parts, and through the points of division draw meridians, and also the parallels of latitude  $b'b, c'c, d'd, e'e$ , and  $B'B$ : a series of triangles will thus be formed, but so small that each may be considered as a plane triangle.

In these triangles, the sum of the bases

$$Ab' + bc' + cd' + de' + ef = AB',$$

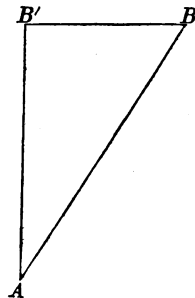
which is equal to the difference of latitude between the points  $A$  and  $B$ . Also,

$$b'b + c'c + d'd + e'e + fB' = BB',$$

which is equal to the distance that the ship has departed from the meridian  $AB'P$ , and is called the departure in sailing from  $A$  to  $B$ .

Therefore, the *distance* sailed, the *difference of latitude* made, and the *departure*, are correctly represented by the hypotenuse and sides of a right angled triangle, of which the angle opposite the departure is the course.

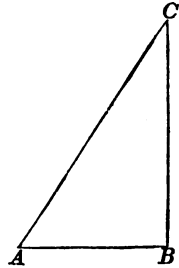
When any two of the four things above named are given, the other two can be determined. This method of determining the place of a ship reduces all the elements to the parts of a plane triangle, and hence is called *plane sailing*.



EXAMPLES.

1. A ship from latitude  $47^\circ 30'$  N. has sailed S. W. by S. 98 miles. What latitude is she in, and what departure has she made?

Let  $C$  be the place sailed from,  $CB$  the meridian, and  $BCA$  the course, which we find from the table of rhumbs to be equal to  $33^\circ 45'$ ; then  $AC$  will be the distance sailed, equal to 98 miles. Also,  $AB$  will be the departure, and  $CB$  the difference of latitude.



Then by the formulas for the solution of right angled triangles,

As radius	10.000000	As radius	10.000000
: $AC$ 98	1.991226	: $CB$ 98	1.991226
:: $\cos. C$ $33^\circ 45'$	9.919846	:: $\sin. C$ $33^\circ 45'$	9.744739
: $CB$ 81.48	1.911072	: $AB$ 54.45	1.735965

Latitude left  $47^\circ 30' N.$   
 Dif. lat. = 81.48 miles = 81.48 minutes =  $1^\circ 22' S.$   
In latitude  $46^\circ 08'.$

Departure 54.45 miles.

2. A ship sails 24 hours on a direct course, from latitude  $38^\circ 32' N.$  till she arrives at latitude  $36^\circ 56' N.$  The course is between S. and E. and the rate  $5\frac{1}{2}$  miles an hour. Required the course, distance, and departure.

Lat. left  $38^\circ 32' N.$   $24 \times 5\frac{1}{2} = 132$  miles = distance.  
 In lat.  $36^\circ 56'$   
 Diff.  $1^\circ 36'$  = 96 miles.

As dist. 132	2.120574	As radius	10.000000
: radius	10.000000	: dist. 132	2.120574
:: diff. lat. 96	1.982271	:: $\sin.$ course $43^\circ 20'$	9.836477
: $\cos.$ course $43^\circ 20'$	9.861697	: dep. 90.58	1.957051

Hence, the course is S.  $43^\circ 20' E.$ , and the departure 90.58 miles east.

3. A ship sails from latitude  $3^\circ 52' S.$  to latitude  $4^\circ 30' N.$ , the course being N. W. by W.  $\frac{1}{2}W$ : required the distance and departure. *Ans.* Dist. 1065 miles; dep. 938.9 miles W.

4. Two points are under the same meridian, one in latitude  $52^\circ 30' N.$ , the other in latitude  $47^\circ 10' N.$  A ship from the southern place sails due east, at the rate of 9 miles an hour, and two days after meets a sloop that had sailed from the other: required the sloop's direct course, and distance run.

*Ans.* Course S.  $53^\circ 28' E.$ ; dist. 537.6 miles.

5. If a ship from latitude  $48^\circ 27' S.$ , sail S. W. by W. 7 miles an hour, in what time will she reach the parallel of  $50^\circ$  south? *Ans.* 23.914 hours.

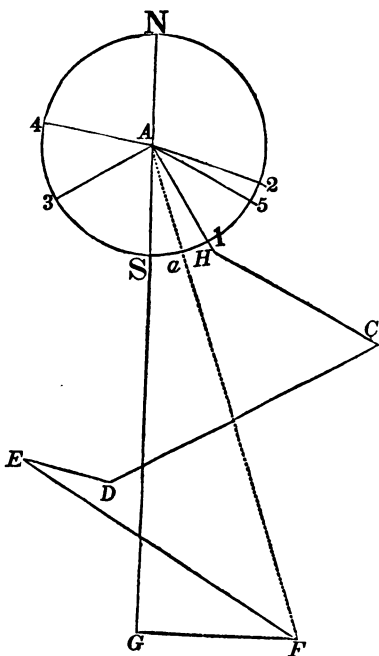
## Of Traverse Sailing.

14. When a ship, in going from one place to another, sails on different courses, it is called *Traverse Sailing*. The determination of the distance and course, from the place of departure to the place of termination, is called *compounding* or *working* the traverse. This is done by the aid of the "Traverse Table," which has already been explained, and the method is in all respects similar to that adopted in the Prob. of Art. 147, p. 115.

## EXAMPLES.

1. A ship from Cape Clear, in lat.  $51^{\circ} 25' N.$ , sails, 1st, S. S. E.  $\frac{1}{4}$  E. 16 miles; 2nd, E. S. E. 23 miles; 3rd, S. W. by W.  $\frac{1}{4}$  W. 36 miles; 4th, W.  $\frac{3}{4}$  N. 12 miles; 5th, S. E. by E.  $\frac{1}{4}$  E. 41 miles: required the distance run, the direct course, and the latitude.

We first form the table below, in which we enter the courses, from the table of rhumbs, omitting the seconds, and then enter the latitudes and departures, taken from the traverse table, to the nearest quarter degree. Thus, in taking the latitude and departure for  $25^{\circ} 18'$  we take for  $25\frac{1}{4}^{\circ}$ . The difference of latitudes gives the line  $AG$ , and the difference of departures the line  $GF$ .



Traverse Table.

Courses.		Angle.	Dist's.	Diff. of Latitude.		Departure.	
No.				N.	S.	E.	W.
1	S. S. E. $\frac{1}{4}$ E. . .	$25^{\circ} 18'$	16		14.47	6.83	
2	E. S. E. . . . .	$67^{\circ} 30'$	23		8.80	21.25	
3	S. W. by W. $\frac{1}{4}$ W.	$61^{\circ} 52'$	36		17.04		31.71
4	W. $\frac{3}{4}$ N. . . . .	$81^{\circ} 33'$	12	1.77			11.87
5	S. E. by E. $\frac{1}{4}$ E.	$59^{\circ} 3'$	41		21.12	35.14	
				1.77	61.43	63.22	43.58
					1.77	43.58	
				Diff.	59.66	19.64	

Latitude left  $51^{\circ} 25' N.$   
 Difference of latitude 59.66 miles =  $1^{\circ} 00' S.$   
 In latitude  $50^{\circ} 25' N.$

Then, by formulas for the solution of right angled triangles, we have,

As $AG$ , diff. lat. 59.66	1.775683	As sin. course $18^{\circ} 13'$	9.495005
: radius,	10.000000	: departure	19.64 1.293141
: : departure 19.64	1.293141	: : radius	10.000000
: : tangt. course $18^{\circ} 13'$	<u>9.517458</u>	: : distance	62.83 <u>1.798136</u>

Therefore the direct course is  $S. 18^{\circ} 13' E.$ , and the distance 62.83 miles.

### Of Plotting.

15. There is yet another method of finding the direct course and distance, much practiced by seamen, although it does not afford a high degree of accuracy. It is a method by plotting, which requires the use of a mariner's scale and a pair of dividers.

One of the scales marked on the mariner's scale, is a scale of chords, commonly called a scale of rhumbs, being divided to every quarter point of the compass; and there is also a second scale of chords divided to degrees. Both of these scales are constructed in reference to the same common radius, so that the chords on the scale of rhumbs correspond to those on the scale of marked chords. The manner of using the scales will appear in plotting the last example.

To construct this traverse, describe a circle with a radius equal to the chord of  $60^{\circ}$  and draw the meridian  $NS$ . Then take from the line of rhumbs the chord of the first course  $2\frac{1}{4}$  points, and apply it from  $S$  to 1, to the right of  $NS$ , since the course is southeasterly, and draw  $S1$ ; take, in like manner, the chord of the second course, 6 points, from  $S$  to 2, and lay it off also to the right of the meridian line. Apply the chord of the third course,  $5\frac{1}{2}$  points, from  $S$  to 3, to the left of the meridian; the fourth course,  $7\frac{1}{4}$  points from  $N$  to 4, to the left of  $NS$ , this course being northwesterly; and, lastly, apply the chord of the fifth course,  $5\frac{1}{4}$  points, from  $S$  to 5, to the right of  $NS$ , and join all the lines as in the figure.

In the direction  $A1$ , lay off the distance  $AH=16$  miles from a scale of equal parts, and through the extremity  $H$ , draw  $HC$  parallel to  $A2$ , and lay off  $HC=23$  miles. Draw  $CD$  parallel to  $A3$ , and lay off  $CD=36$  miles; then draw  $DE$  parallel to  $A4$ , and lay off 12 miles; and lastly draw  $EF$  parallel to  $A5$ , and lay off 41 miles, and  $F$  will be the place of the ship. Hence, we conclude that  $AF$  will be the distance made good, and  $GAF$  will be the course.



Applying, then, the distance  $AF$  to the scale of equal parts, we find it equal to  $62\frac{3}{4}$  miles; and applying the chord  $Sa$  to the scale of chords we find the course  $GAF = 18\frac{1}{4}^\circ$ .

2. A ship sails from a place in latitude  $24^\circ 32' N.$ , and runs the following courses and distances, viz. 1st, S. W. by W. dist. 45 miles; 2nd, E. S. E. dist. 50 miles; 3rd, S. W. dist. 30 miles; 4th, S. E. by E. dist. 60 miles; 5th, S. W. by S.  $\frac{1}{4}$  W. dist. 63 miles: required her latitude, and the direct course and distance from the place left to the place arrived at, and the construction of the traverse.

*Ans.*  $\left\{ \begin{array}{l} \text{Lat. } 22^\circ 3' N., \text{ course S.} \\ \text{Dist. } 149.2 \text{ miles.} \end{array} \right.$

3. A ship from lat.  $28^\circ 32' N.$  has run the following courses, viz. 1st, N. W. by N. 20 miles; 2nd, S. W. 40 miles; 3rd, N. E. by E. 60 miles; 4th, S. E. 55 miles; 5th, W. by S. 41 miles; 6th, E. N. E. 66 miles: required her latitude, the distance made good, and the direct course, also the construction of the traverse.

*Ans.* Dist. 70.2 miles, course E.

4. A ship from lat.  $41^\circ 12' N.$  sails S. W. by W. 21 miles; S. W.  $\frac{1}{2}$  S. 31 miles; W. S. W.  $\frac{1}{2}$  S. 16 miles; S.  $\frac{3}{4}$  E. 18 miles; S. W.  $\frac{1}{4}$  W. 14 miles; then W.  $\frac{1}{2}$  N. 30 miles: required the latitude, the direct course, and the distance.

*Ans.*  $\left\{ \begin{array}{l} \text{Lat. } 40^\circ 05', \text{ course S. } 52^\circ 49' W. \\ \text{Dist. } 111.7 \text{ miles.} \end{array} \right.$

5. A ship runs the following courses, viz.

1st, S. E. 40 miles; 2d, N. E. 28 miles; 3d, S. W. by W. 52 miles; 4th, N. W. by W. 30 miles; 5th, S. S. E. 36 miles; 6th, S. E. by E. 58 miles: required the direct course, and distance made good.

*Ans.*  $\left\{ \begin{array}{l} \text{Direct course S. } 25^\circ 59' E., \text{ or S. S. E. } \frac{1}{4} E., \text{ nearly.} \\ \text{Distance } 95.87 \text{ miles.} \end{array} \right.$

6. A ship sails, 1st, N. W. by W.  $\frac{1}{2}$  W. 40 miles; 2nd, N. W. by  $\frac{1}{4}$  N., 41 miles; 3rd, N. by E. 16.1 miles; and 4th, N. E.  $\frac{1}{4}$  E. 32.5 miles: required the distance made, and the direct course.

*Ans.* Course  $21^\circ 54'$  West of North. Dist. 94.6 miles.

These examples will, perhaps, suffice to illustrate the principles of plane sailing.

The longitude, made on any course, cannot be determined by these methods, for this being the arc of the equator intercepted between two meridians, cannot be found under the supposition that the meridians are parallel.

The most simple case of finding the difference of longitude is when the ship sails due east or due west: this is called *Parallel Sailing*.

*Parallel Sailing.*

16. The entire theory of parallel sailing is comprehended in the following proposition, viz.

*The cosine of the latitude of the parallel, is to the distance run, as radius to the difference of longitude.*

Let  $IQH$  represent the equator, and  $FDN$  any parallel of latitude: then,  $CI$  will be the radius of the equator, and  $EF$  the radius of the parallel.

Suppose  $FD$  to be the distance sailed, then the difference of longitude will be measured by  $IQ$ , the arc intercepted on the equator. Then, since similar arcs are to each other as their radii (Bk. V. Prop. xi. Cor.), we have,

$$EF : CI :: \text{dist. } FD : \text{diff. long. } IQ.$$

But  $EF$  is the sine of  $PF$ , or cosine of  $FI$ , the latitude, and  $CI$  is the radius of the sphere: hence,

$$\cos. \text{ lat.} : R :: \text{distance} : \text{diff. longitude.}$$

*Corollary.* If we denote by  $D$  the distance between any two meridians, measured on the parallel whose latitude is  $L$ ; and by  $D'$  the distance between the same meridians measured on the parallel whose latitude is  $L'$ , the arcs will be similar, and we shall have (Bk. V. Prop. xi. Cor.),

$$\cos. L : D :: \cos. L' : D',$$

that is,  $\cos. L : \cos. L' :: D : D'.$

Hence, *when the longitude made on different parallels is the same, the distances sailed are proportional to the cosines of the parallels of latitude.*

By referring to Th. V. page 45, we see that in any right angled triangle

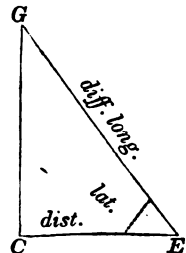
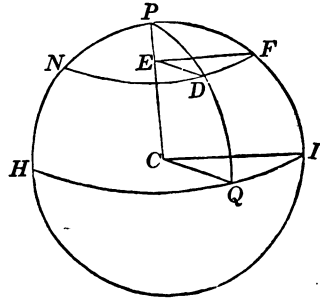
$$R : \cos. \text{ angle at base} :: \text{hyp.} : \text{base,}$$

or  $\cos. E : R :: EG : EC;$

and by comparing this with the proportion,

$$\cos. \text{ lat.} : R :: \text{dist.} : \text{diff. long.}$$

We see, that if one leg of a right angled triangle represent the distance run on any parallel, and the adjacent acute angle be made equal



to the degree of latitude of that parallel, then the hypotenuse will represent the difference of longitude. It follows therefore, that any problem in parallel sailing, may be solved as a simple case of plane sailing. For, if we regard the latitude as the course, the distance run as the base, the difference of longitude will be the hypotenuse of the corresponding right angled triangle.

## EXAMPLES.

1. A ship from latitude  $53^{\circ} 56' N.$ , longitude  $10^{\circ} 18' E.$ , has sailed due west, 236 miles : required her present longitude.

By the rule

As cos. lat.	$53^{\circ} 56'$	-	-	-	-	9.769913
: radius	-	-	-	-	-	10.000000
: : distance	236	-	-	-	-	<u>2.372912</u>
: diff. long.	400.8	-	-	-	-	<u>2.602999</u>

Long. left - -  $10^{\circ} 18' E.$

Diff. long. =  $\frac{400}{60}$  degrees =  $6^{\circ} 40' W.$

Long. in - -  $3^{\circ} 38' E.$

2. If a ship sails E. 126 miles, from the North Cape, in lat.  $71^{\circ} 10' N.$ , and then due N., till she reaches lat.  $73^{\circ} 26' N.$ ; how far must she sail W. to reach the meridian of the North Cape?

Here the ship sails on two parallels of latitude, first on the parallel of  $71^{\circ} 10'$ , and then on the parallel of  $73^{\circ} 26'$ , and makes the same difference of longitude on each parallel.

Hence, by the corollary,

As cos. lat.	$71^{\circ} 10'$	arith. comp.	0.491044
: distance	126	-	2.100371
: : cos. lat.	$43 26$	-	<u>9.455044</u>
: distance	111.3	-	<u>2.046459</u>

3. A ship in latitude  $32^{\circ} N.$  sails due E. till her difference of longitude is 384 miles : required the distance run.

*Ans.* 325.6 miles.

4. If two ships in latitude  $44^{\circ} 30' N.$ , distant from each other 216 miles, should both sail directly S. till their distance is 256 miles, what latitude would they arrive at?

*Ans.*  $32^{\circ} 17' S.$

5. Two ships in the parallel of  $47^{\circ} 54' N.$ , have  $9^{\circ} 35'$  difference of longitude, and they both sail directly S., a distance of 836 miles : required their distance from each other at the parallel left, and at that reached.

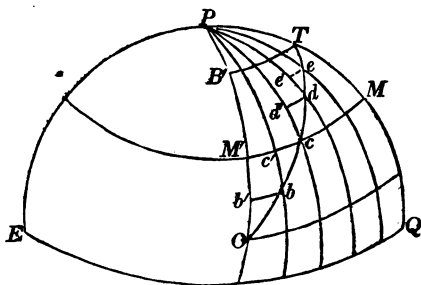
*Ans.* 385.5 miles, and 479.9 miles.

*Middle Latitude Sailing.*

17. Having seen how the longitude which a ship makes when sailing on a parallel of latitude may be determined, we come now to examine the more general problem, viz. to find the longitude which a ship makes when sailing upon any oblique rhumb.

There are two methods of solving this problem, the one by what is called *middle latitude sailing*, and the other by *Mercator's sailing*. The first of these methods is confined in its application, and is moreover somewhat inaccurate even where applicable; the second is perfectly general, and rigorously true; but still there are cases in which it is advisable to employ the method of middle latitude sailing, in preference to that of Mercator's sailing. It is, therefore, proper that middle latitude sailing should be explained, especially since, by means of a correction to be hereafter noticed, the usual inaccuracy of this method may be rectified.

Middle latitude sailing proceeds on the supposition that the departure or sum of all the meridional distances,  $b'b$ ,  $c'c$ ,  $d'd$ , &c. from  $O$  to  $T$ , is equal to the distance  $M'M$  of the meridians of  $O$  and  $T$ , measured on the middle parallel of latitude between  $O$  and  $T$ .



The middle latitude is *half the sum* of the two extreme latitudes, if they are both of the same name, and to *half their difference* if they are of contrary names.

This supposition becomes very inaccurate when the course is small, and the distance run great; for it is plain that the middle latitude distance will receive a much greater accession than the departure, if the track  $OT$  cuts the successive meridians at a very small angle.

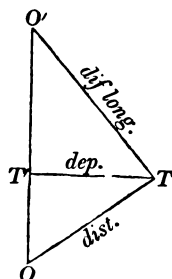
The principal approaches nearer to accuracy as the angle  $O$  of the course increases, because then as but little advance is made in latitude, the several component departures lie more in the immediate vicinity of the middle parallel  $M'M$ . But still, in very high latitudes, a small advance in latitude makes a considerable difference in meridional distance; hence, this principle is not to be used in such latitudes, if much accuracy is required.

By means, however, of a small table of corrections, constructed by *Mr. Wakeman*, the imperfections of the middle lat-

itude method may be removed, and the results of it rendered in all cases accurate. This table we have given at the end of this work.

The rules for middle latitude sailing may be thus deduced.

We have seen, in the first case of plane sailing, that if a ship sails on an oblique rhumb from  $O$  to  $T$ , that the hypotenuse  $OT$  will represent the distance;  $OT'$  the difference of latitude, and  $T'T$ , the departure. Now, by the present hypothesis, the departure  $T'T$  is equal to the middle parallel of latitude between the meridians of the places sailed from and arrived at: so that the difference of longitude of these two places is the same as if the ship had sailed the distance  $T'T$  on the middle parallel of latitude. The determination of the difference of longitude is, therefore, reduced to the case of parallel sailing: for,  $T'T$  now representing the distance on the parallel, if the angle  $T'TO$  be made equal to the latitude of that parallel, we shall have, by the last case, the difference of longitude represented by the hypotenuse  $O'T$ . We therefore have the following theorem:



I. In the triangle  $O'TT'$

$$\cos. O'TT' : TT' :: R : TO';$$

that is,

$$\cos. \text{mid. lat.} : \text{departure} :: R : \text{diff. longitude.}$$

II. In the triangle  $O'TO$

$$\sin. O' : OT :: \sin O : O'T';$$

that is, since  $\sin. O' = \cos. O'TT'$

$$\cos. \text{mid. lat.} : \text{distance} :: \sin. \text{course} : \text{diff. longitude.}$$

III. In the triangle  $OTT'$ , we have

$$R : \text{tangent } O :: OT' : TT';$$

comparing this with the first proportion, and observing that the extremes of this are the means of that, we have

$$OT' : O'T :: \cos. O'TT' : \text{tangt. } O;$$

that is,

$$\text{diff. lat.} : \text{diff. long.} :: \cos. \text{mid. lat.} : \text{tangt. course.}$$

These three propositions comprise the theory of middle latitude sailing; and when to the middle latitude sailing, the proper correction, taken from Mr. Workman's table, is applied, these theorems will be rendered accurate.

In the table of pages 93 and 94, the middle latitude is to be found in the first column to the left. Then, along in the horizontal line, and under the given difference of latitude, is inserted

the proper correction to be *added* to the middle latitude to obtain the latitude in which the meridian distance is accurately equal to the departure. Thus, if the middle latitude be  $37^\circ$ , and the difference of latitude  $18^\circ$ , the correction will be found on page 94, and is equal to  $0^\circ 40'$ .

EXAMPLES.

1. A ship, in latitude  $51^\circ 18' N.$ , longitude  $22^\circ 6' W.$ , is bound to a place in the S. E. quarter, 1024 miles distant, and in lat.  $37^\circ N.$ : what is her direct course and distance, as also the difference of longitude between the two places?

Lat. from $51^\circ 18' N.$	}	Sum of latitudes	-	-	-	$88^\circ 18'$
Lat. to <u><math>37^\circ 0' N.</math></u>		Mid. lat.	-	-	-	$44^\circ 9'$
Diff. lat. $14^\circ 18' = 858$ miles.						

As distance 1024	. . .	3.010300	Cos. mid. lat. $44^\circ 9'$ ar. comp.	0.144167
: radius . . . . .		10.000000	: tang. course $33^\circ 5'$	9.813899
: : diff. lat. 858 . . . . .		2.933487	: : diff. lat. 858 . . . . .	2.933487
: cos. course $33^\circ 5'$ . . . . .		<u>9.923187</u>	: diff. long. 779 . . . . .	<u>2.891552</u>

In this operation the middle latitude has not been corrected, so that the difference of longitude here determined is not without error. To find the proper correction, look for the given middle latitude, viz.  $44^\circ 9'$ , in the table of corrections, the nearest to which we find to be  $45^\circ$ ; against this and under  $14^\circ$  diff. of lat. we find  $27'$ , and also under  $15^\circ$  we find  $31'$ , the difference between the two being  $4'$ ; hence, corresponding to  $14^\circ 18'$  the correction will be about  $28'$ . Hence, the corrected middle latitude is  $44^\circ 37'$ , therefore,

Cos. corrected mid. lat. $44^\circ 37'$	ar. comp.	0.147629
: tangt. course	$33^\circ 5'$	9.813899
: : diff. lat.	858	3.933487
: diff. long.	785.3	<u>2.895015</u>

therefore, the error in the former result is about  $6\frac{1}{2}$  miles.

2. A ship sails in the N. W. quarter, 248 miles, till her departure is 135 miles, and her difference of longitude 310 miles: required her course, the latitude left, and the latitude come to.

*Ans.* { Course N.  $32^\circ 59' W.$ ;  
 { Lat. left  $62^\circ 27' N.$ ; lat. in  $65^\circ 55' N.$

3. A ship, from latitude  $37^\circ N.$ , longitude  $9^\circ 2' W.$ , having sailed between the N. and W., 1027 miles, reckons that she has made 564 miles of departure: what was her direct course, and the latitude and longitude reached?

*Ans.* { Course N.  $33^\circ 19' W.$ , or N. W. nearly;  
 { Lat.  $51^\circ 18' N.$ ; long.  $22^\circ 8' W.$

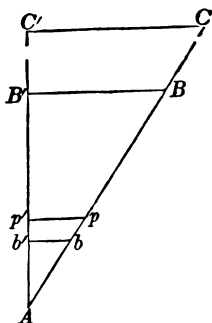
4. Required the course and distance from the east point of St. Michael's, lat.  $37^{\circ} 48' N.$ , long.  $25^{\circ} 13' W.$ , to the Start Point, lat.  $50^{\circ} 13' N.$ , long.  $3^{\circ} 38' W.$ ; the middle latitude being corrected by Workman's tables.

*Ans.* Course N.  $57^{\circ} 11' E$ ; dist. 1189 miles.

### *Mercator's Sailing.*

18. It has already been observed, that when a ship sails on an oblique rhumb, the departure, the difference of latitude, and the distance run, are truly represented by the sides of a right angled triangle.

Thus, if a ship sails from  $A$  to  $B$ , the departure  $B'B$  will represent the sum of all the very small meridian distances, or elementary departures,  $b'b$ ,  $p'p$ , &c.; the difference of latitude  $AB'$  will represent, in like manner, the small differences of latitude  $Ab'$ ,  $b'p'$ , &c; and the hypotenuse  $AB$ , will express the sum of the distances corresponding to these several differences of latitude and departure. Each of these elements is supposed to be taken so small, as to form on the surface of the sphere a series of triangles, differing insensibly from plane triangles.



Let  $Ab'b$  represent one of these elementary triangles;  $b'b$  will then be one of the elements of departure; and  $Ab'$  the corresponding difference of latitude. Now, as  $b'b$  is a small arc of a parallel of latitude, it will be to a portion of the equator or of a meridian containing an equal number of degrees, as the cosine of its latitude is to radius (Art. 16). This similar portion of the equator, or of the meridian, will be the difference of longitude between  $b'$  and  $b$ .

Let us now suppose  $Ab$  to be prolonged until the perpendicular  $p'p$  shall become equal to the difference of longitude between  $b'$  and  $b$ : then,

$bb'$  will be to  $p'p$ , as the cosine of the latitude of  $b'b$ , to radius.

But,  $b'b : p'p :: Ab' : Ap'$ :

hence,  $Ab' : Ap' :: \cos. \text{lat. of } b'b : \text{radius};$

that is, if the latitude be so increased that  $p'p$  shall become the true difference of longitude, then,

true diff. lat.  $Ab' : \text{increased lat. } Ap' :: \cos. \text{lat.} : \text{radius.}$

The increased latitude  $Ap'$  is called the *meridional* difference of latitude. Denoting, therefore, the true difference of latitude

by  $d$ , the increased or meridional difference of latitude by  $D$ , the latitude of  $b'b$  by  $l$ , and the radius by 1, which is, indeed, the radius of the tables of natural sines, and we shall have

$$d : D :: \cos. l : 1,$$

which gives

$$D = d \secant l, \quad \text{since} \quad \frac{1}{\cos. l} = \sec. l.$$

It then, we know the latitude  $l$  of the beginning of a course, and the true difference of latitude  $d$  of the extremity of the course, we can easily find the meridional latitude  $D$  corresponding to that course.

Conceiving each elementary distance to be increased in this manner, giving the meridional differences of latitude on the line  $AC'$ , the sum of all the corresponding elements will be the entire meridional departure during the course.

To represent, therefore, the difference of longitude due to any departure, as  $B'B$ , and to its corresponding difference of latitude  $AB'$ , we must produce  $AB'$  till  $AC'$  is equal to the meridional difference of latitude; the perpendicular  $C'C$  will then be the difference of longitude actually made in sailing from  $A$  to  $B$ .

The determination of  $AC'$  requires the determination of all its elementary parts. If  $d$  be taken equal to 1', we shall have from the equation above

$$D = 1' \sec l. \quad \text{or} \quad D = \sec. l,$$

it being understood that  $l$  expresses minutes or geographical miles.

From this equation, the value of  $D$ , corresponding to every minute of  $l$ , from the equator to the pole, may be calculated; and from the continued addition of these there may be obtained, in succession, the meridional parts corresponding to 1', 2', 3', 4', &c. of true latitude, and when registered in a table, they form a table of meridional parts, given in all books on Navigation.

The following may serve as a specimen of the manner in which such a table may be constructed, and, indeed, of the manner in which the first table of meridional parts was actually formed by Mr. Wright, the proposer of this valuable method.

Mer. pts. of 1' = nat. sec. 1'.

Mer. pts. of 2' = nat. sec. 1' + nat. sec. 2'.

Mer. pts. of 3' = nat. sec. 1' + nat. sec. 2' + nat. sec. 3'.

Mer. pts. of 4' = nat. sec. 1' + nat. sec. 2' + nat. sec. 3' + &c.

Hence, by means of a table of natural secants we have

	Nat. Secs.	Mer. Pts.
Mer. pts. of 1' =	1.000000	= 1.0000000
Mer. pts. of 2' =	1.0000000 + 1.0000000	= 2.0000002
Mer. pts. of 3' =	2.0000002 + 1.0000004	= 3.0000006
Mer. pts. of 4' =	3.0000006 + 1.0000007	= 4.0000013 &c.



There are other methods of construction, but this is the most simple and obvious. The meridional parts thus determined, are all expressed in geographical miles, because in the general expression

$$D = 1' \text{ sec. } l.$$

1' is a geographical mile.

Having thus formed the table of meridional parts, if we enter it, and find the meridional parts corresponding to the latitudes of the place left and the place arrived at, their difference will be the meridional difference of latitude, or the line  $AC'$  in the diagram. The difference of longitude  $C'C$  may then be found by the following proportion.

I. *As radius is to the tangent of the course, so is the meridional difference of latitude to the difference of longitude.*

But if the departure be given instead of the course, then,

II. *As the true difference of latitude, is to the departure, so is the meridional difference of latitude to the tangent of the course.*

Other proportions may also be deduced from the diagram.

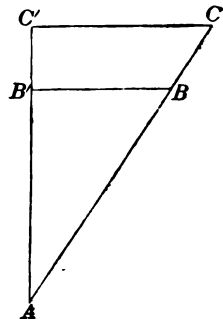
EXAMPLES.

As an example of Mercator's or rather Wright's, sailing, let us take the following:

1. Required the course and distance from the east point of St. Michael's to the Start point: the latitudes being  $37^\circ 48' \text{ N.}$ , and  $50^\circ 13' \text{ N.}$ , and the longitudes  $25^\circ 13' \text{ W.}$ , and  $3^\circ 38' \text{ W.}$

Start Point, lat. $50^\circ 13' \text{ N.}$	Mer. pts. 3495
St. Michael's, lat. $37^\circ 48' \text{ N.}$	Mer. pts. 2453
True difference of lat. $12^\circ 25'$	Mer. diff. <u>1042</u>
	Diff. of long. $21^\circ 35'$
Diff. in miles <u>745</u>	60
	Diff. in miles <u>1295</u>

Now, let us suppose that we have sailed from  $A$  to  $B$ : we shall then know  $AB'$  equal true diff. lat. = 745 miles;  $AC'$  = meridional diff. of lat. = 1042; and  $C'C$  = the difference of longitude equal to 1295 miles. It is required to find the course  $B'AB$ , and the distance  $AB$ .



For the Course.			For the Distance.		
As $AC'$	1042	3.017868	As $\cos. A. 51^\circ 11'$		9.797150
: radius . . . . .	10.000000		: $AB'$	745	2.872156
:: $C'C$	1295	3.112270	:: radius . . . . .		10.000000
: tangt. $A 51^\circ 11' E.$		<u>16.094402</u>	: $AB$	1189	<u>3.075006</u>

2. A ship sails from latitude  $37^\circ N.$  longitude  $22^\circ 56' W.$ , on the course  $N: 33^\circ 19' E:$  till she arrives at  $51^\circ 18' N.$ : required the distance sailed, and the longitude arrived at.

*Ans.* Dis. 1027 miles; long.  $9^\circ 45' W.$

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*Mercator's Chart.*

MERCATOR'S CHART is a Map constructed for the use of Navigators. In this chart all the meridians are represented by straight lines drawn parallel to each other, and the parallels of latitude are also represented by parallel straight lines drawn at right angles to the meridians.

The chart may be thus constructed. Draw on the lower part of the paper a horizontal line to represent the parallel of latitude which is to bound the southern portion of the chart. From a scale of equal parts, corresponding in size to the extent of the map to be made, lay off, on this line, any number of equal distances and through the points draw a series of parallels to represent the meridians.

Then draw a line on the side of the map, and for the second parallel of latitude, find from the table of meridional parts the meridional difference of latitude corresponding to the degrees between the first and second parallel, and lay off this distance for the interval between the two parallels. Then find the meridional difference between the second and third, and lay it off in the same way for the third parallel, and so on, for the fourth, fifth, &c.

A place whose latitude and longitude is known, may be laid down in the same manner; for it will always be determined by the intersection of the meridian and parallel of latitude.

If the chart is constructed on a small scale the divisions on the graduated lines, may be *degrees* instead of minutes; and the meridians and parallels may be drawn only for every fifth or tenth degree.

We have already seen (Art. 18.), that the meridional difference of latitude bears a constant ratio to the difference of longitude, so long as the course remains unchanged: and hence we see that on Mercator's chart, every rhumb will be represented by a straight line.

*Line of Meridional Parts on Gunter's Scale.*

This scale corresponds exactly with the table of meridional parts, excepting, that in the table the circle is divided to minutes, while the scale is divided only to degrees. A scale of equal parts is placed directly beneath the scale of meridional parts; if the former corresponds to divisions of longitude, the latter will represent those of latitude. Hence, a chart may be constructed from these scales by using the scale of equal parts for the lines of longitude, and the scale of meridional parts for those of latitude.

THE END.

# A TABLE

OF

## LOGARITHMS OF NUMBERS

FROM 1 TO 10,000.

---

N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.000000	26	1.414973	51	1.707570	76	1.880814
2	0.301030	27	1.431364	52	1.716003	77	1.886491
3	0.477121	28	1.447158	53	1.724276	78	1.892095
4	0.602060	29	1.462398	54	1.732394	79	1.897627
5	0.698970	30	1.477121	55	1.740363	80	1.903090
6	0.778151	31	1.491362	56	1.748188	81	1.908485
7	0.845098	32	1.505150	57	1.755875	82	1.913814
8	0.903090	33	1.518514	58	1.763428	83	1.919078
9	0.954243	34	1.531479	59	1.770852	84	1.924279
10	1.000000	35	1.544068	60	1.778151	85	1.929419
11	1.041393	36	1.556303	61	1.785330	86	1.934498
12	1.079181	37	1.568202	62	1.792392	87	1.939519
13	1.113943	38	1.579784	63	1.799341	88	1.944483
14	1.146128	39	1.591065	64	1.806180	89	1.949390
15	1.176091	40	1.602060	65	1.812913	90	1.954243
16	1.204120	41	1.612784	66	1.819544	91	1.959041
17	1.230449	42	1.623249	67	1.826075	92	1.963788
18	1.255273	43	1.633468	68	1.832509	93	1.968483
19	1.278754	44	1.643453	69	1.838849	94	1.973128
20	1.301030	45	1.653213	70	1.845098	95	1.977724
21	1.322219	46	1.662758	71	1.851258	96	1.982271
22	1.342423	47	1.672098	72	1.857333	97	1.986772
23	1.361728	48	1.681241	73	1.863323	98	1.991226
24	1.380211	49	1.690196	74	1.869232	99	1.995635
25	1.397940	50	1.698970	75	1.875061	100	2.000000

N. B. In the following table, in the last nine columns of each page, where the first or leading figures change from 9's to 0's, points or dots are introduced instead of the 0's through the rest of the line, to catch the eye, and to indicate that from thence the annexed first two figures of the Logarithm in the second column stand in the next lower line.



N.	0	1	2	3	4	5	6	7	8	9	D.
100	000000	0434	0868	1301	1734	2166	2598	3029	3461	3891	432
101	4321	4751	5181	5609	6038	6466	6894	7321	7748	8174	428
102	8600	9026	9451	9876	.300	.724	1147	1570	1993	2415	424
103	012837	3259	3680	4100	4521	4940	5360	5779	6197	6616	419
104	7033	7451	7868	8284	8700	9116	9532	9947	.361	.775	416
105	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896	412
106	5306	5715	6125	6533	6942	7350	7757	8164	8571	8978	408
107	9384	9789	.195	.600	1004	1408	1812	2216	2619	3021	404
108	033424	3826	4227	4628	5029	5430	5830	6230	6629	7028	400
109	7426	7825	8223	8620	9017	9414	9811	.207	.602	.998	396
110	041393	1787	2182	2576	2969	3362	3755	4148	4540	4932	393
111	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830	389
112	9218	9606	9993	.380	.766	1153	1538	1924	2309	2694	386
113	053078	3463	3846	4230	4613	4996	5378	5760	6142	6524	382
114	6905	7286	7666	8046	8426	8805	9185	9563	9942	.320	379
115	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083	376
116	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815	372
117	8186	8557	8928	9298	9668	.38	.407	.776	1145	1514	369
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
119	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819	363
120	079181	9513	9904	.266	.626	.987	1347	1707	2067	2426	360
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
122	6360	6716	7071	7426	7781	8136	8490	8845	9198	9552	355
123	9905	.258	.611	.963	1315	1667	2018	2370	2721	3071	351
124	093422	3772	4122	4471	4820	5169	5518	5866	6215	6562	349
125	6910	7257	7604	7951	8298	8644	8990	9335	9681	.26	346
126	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462	343
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	340
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	.253	338
129	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609	335
130	113943	4277	4611	4944	5278	5611	5943	6276	6608	6940	333
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	.245	330
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
133	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781	325
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	.112	323
135	130334	0655	0977	1298	1619	1939	2260	2580	2900	3219	321
136	3539	3858	4177	4496	4814	5133	5451	5769	6086	6403	318
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	315
138	9879	.194	.508	.822	1136	1450	1763	2076	2389	2702	314
139	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140	146128	6438	6748	7058	7367	7676	7985	8294	8603	8911	309
141	9219	9527	9835	.142	.449	.756	1063	1370	1676	1982	307
142	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032	305
143	5336	5640	5943	6246	6549	6852	7154	7457	7759	8061	303
144	8362	8664	8965	9266	9567	9868	.168	.469	.769	1069	301
145	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055	299
146	4353	4650	4947	5244	5541	5838	6134	6430	6726	7022	297
147	7317	7613	7908	8203	8497	8792	9086	9380	9674	9968	295
148	170262	0555	0848	1141	1434	1726	2019	2311	2603	2895	293
149	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802	291
150	176091	6381	6670	6959	7248	7536	7825	8113	8401	8689	289
151	8977	9264	9552	9839	.126	.413	.699	.985	1272	1558	287
152	181844	2129	2415	2700	2985	3270	3555	3839	4123	4407	285
153	4691	4975	5259	5542	5825	6108	6391	6674	6956	7239	283
154	7521	7803	8084	8366	8647	8928	9209	9490	9771	.51	281
155	190332	0612	0892	1171	1451	1730	2010	2289	2567	2846	279
156	3125	3403	3681	3959	4237	4514	4792	5069	5346	5623	278
157	5899	6176	6453	6729	7005	7281	7556	7832	8107	8382	276
158	8657	8932	9206	9481	9755	.29	.303	.577	.850	1124	274
159	201397	1670	1943	2216	2488	2761	3033	3305	3577	3848	272

N.	0	1	2	3	4	5	6	7	8	9	D.
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A TABLE OF LOGARITHMS FROM 1 TO 10,000.

N.	0	1	2	3	4	5	6	7	8	9	D.
160	204120	4391	4663	4934	5204	5475	5746	6016	6286	6556	271
161	6826	7096	7365	7634	7904	8173	8441	8710	8979	9247	269
162	9515	9783	.51	.319	.586	.853	1121	1388	1654	1921	267
163	212188	2454	2720	2986	3252	3518	3783	4049	4314	4579	266
164	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221	264
165	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846	262
166	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456	261
167	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051	259
168	5309	5568	5826	6084	6342	6600	6858	7115	7372	7630	258
169	7837	8144	8400	8657	8913	9170	9426	9682	9938	.193	256
170	230449	0704	0960	1215	1470	1724	1979	2234	2488	2742	254
171	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276	253
172	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795	252
173	8046	8297	8548	8799	9049	9299	9550	9800	.50	.300	250
174	240549	0799	1048	1297	1546	1795	2044	2293	2541	2790	249
175	3038	3286	3534	3782	4030	4277	4525	4772	5019	5266	248
176	5513	5759	6006	6252	6499	6745	6991	7237	7482	7728	246
177	7973	8219	8464	8709	8954	9198	9443	9687	9932	.176	245
178	250420	0664	0908	1151	1395	1638	1881	2125	2368	2610	243
179	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031	242
180	255273	5514	5755	5996	6237	6477	6718	6958	7198	7439	241
181	7679	7918	8158	8398	8637	8877	9116	9355	9594	9833	239
182	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	238
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	237
184	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	235
185	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	234
186	9513	9746	9980	.213	.446	.679	.912	1144	1377	1609	233
187	271842	2074	2306	2538	2770	3001	3233	3464	3696	3927	232
188	4158	4389	4620	4850	5081	5311	5542	5772	6002	6232	230
189	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229
190	278754	8982	9211	9439	9667	9895	.123	.351	.578	.806	228
191	281033	1261	1488	1715	1942	2169	2396	2622	2849	3075	227
192	3301	3527	3753	3979	4205	4431	4656	4882	5107	5332	226
193	5557	5782	6007	6232	6456	6681	6905	7130	7354	7578	225
194	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812	223
195	290035	0257	0480	0702	0925	1147	1369	1591	1813	2034	222
196	2256	2478	2699	2920	3141	3363	3584	3804	4025	4246	221
197	4466	4687	4907	5127	5347	5567	5787	6007	6226	6446	220
198	6665	6884	7104	7323	7542	7761	7979	8198	8416	8635	219
199	8853	9071	9289	9507	9725	9943	.161	.378	.595	.813	218
200	301030	1247	1464	1681	1898	2114	2331	2547	2764	2980	217
201	3196	3412	3628	3844	4059	4275	4491	4706	4921	5136	216
202	5351	5566	5781	5996	6211	6425	6639	6854	7068	7282	215
203	7496	7710	7924	8137	8351	8564	8778	8991	9204	9417	213
204	9630	9843	.56	.268	.481	.693	.906	1118	1330	1542	212
205	311754	1966	2177	2389	2600	2812	3023	3234	3445	3656	211
206	3867	4078	4289	4499	4710	4920	5130	5340	5551	5760	210
207	5970	6180	6390	6599	6809	7018	7227	7436	7646	7854	209
208	8063	8272	8481	8689	8898	9106	9314	9522	9730	9938	208
209	329146	0354	0562	0769	0977	1184	1391	1598	1805	2012	207
210	322219	2426	2633	2839	3046	3252	3458	3665	3871	4077	206
211	4282	4488	4694	4899	5105	5310	5516	5721	5926	6131	205
212	6336	6541	6745	6950	7155	7359	7563	7767	7972	8176	204
213	8380	8583	8787	8991	9194	9398	9601	9805	.8	.211	203
214	330414	0617	0819	1022	1225	1427	1630	1832	2034	2236	202
215	2438	2640	2842	3044	3246	3447	3649	3850	4051	4253	202
216	4454	4655	4856	5057	5257	5458	5658	5859	6059	6260	201
217	6460	6660	6860	7060	7260	7459	7659	7858	8058	8257	200
218	8456	8656	8855	9054	9253	9451	9650	9849	.47	.246	199
219	340444	0642	0841	1039	1237	1435	1632	1830	2028	2225	198

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220	342423	2620	2817	3014	3212	3409	3606	3802	3999	4196	197
221	4392	4589	4785	4981	5178	5374	5570	5766	5962	6157	196
222	6353	6549	6744	6939	7135	7330	7525	7720	7915	8110	195
223	8305	8500	8694	8889	9083	9278	9472	9666	9860	.54	194
224	350248	0442	0636	0829	1023	1216	1410	1603	1796	1989	193
225	2183	2375	2568	2761	2954	3147	3339	3532	3724	3916	193
226	4108	4301	4493	4685	4876	5068	5260	5452	5643	5834	192
227	6026	6217	6408	6599	6790	6981	7172	7363	7554	7744	191
228	7935	8125	8316	8506	8696	8886	9076	9266	9456	9646	190
229	9835	.25	.215	.404	.593	.783	.972	1161	1350	1539	189
230	361728	1917	2105	2294	2482	2671	2859	3048	3236	3424	188
231	3612	3800	3988	4176	4363	4551	4739	4926	5113	5301	188
232	5488	5675	5862	6049	6236	6423	6610	6796	6983	7169	187
233	7356	7542	7729	7915	8101	8287	8473	8659	8845	9030	186
234	9216	9401	9587	9772	9958	.143	.328	.513	.698	.883	185
235	371068	1253	1437	1622	1806	1991	2175	2360	2544	2728	184
236	2912	3096	3280	3464	3647	3831	4015	4198	4382	4565	184
237	4748	4932	5115	5298	5481	5664	5846	6029	6212	6394	183
238	6577	6759	6942	7124	7306	7488	7670	7852	8034	8216	182
239	8398	8580	8761	8943	9124	9306	9487	9668	9849	.30	181
240	380211	0392	0573	0754	0934	1115	1296	1476	1656	1837	181
241	2017	2197	2377	2557	2737	2917	3097	3277	3456	3636	180
242	3815	3995	4174	4353	4533	4712	4891	5070	5249	5428	179
243	5606	5785	5964	6142	6321	6499	6677	6856	7034	7212	178
244	7390	7568	7746	7923	8101	8279	8456	8634	8811	8989	178
245	9166	9343	9520	9698	9875	.51	.228	.405	.582	.759	177
246	390935	1112	1288	1464	1641	1817	1993	2169	2345	2521	176
247	2697	2873	3048	3224	3400	3575	3751	3926	4101	4277	176
248	4452	4627	4802	4977	5152	5326	5501	5676	5850	6025	175
249	6199	6374	6548	6722	6896	7071	7245	7419	7592	7766	174
250	397940	8114	8287	8461	8634	8808	8981	9154	9328	9501	173
251	9674	9847	.20	.192	.365	.538	.711	.883	1056	1228	173
252	401401	1573	1745	1917	2089	2261	2433	2605	2777	2949	172
253	3121	3292	3464	3635	3807	3978	4149	4320	4492	4663	171
254	4834	5005	5176	5346	55.7	5688	5858	6029	6199	6370	171
255	6540	6710	6881	7051	7221	7391	7561	7731	7901	8070	170
256	8240	8410	8579	8749	8918	9087	9257	9426	9595	9764	169
257	9933	.102	.271	.440	.609	.777	.946	1114	1283	1451	169
258	411620	1788	1956	2124	2293	2461	2629	2796	2964	3132	168
259	3300	3467	3635	3803	3970	4137	4305	4472	4639	4806	167
260	411973	5140	5307	5474	5641	5808	5974	6141	6308	6474	167
261	6641	6807	6973	7139	7306	7472	7638	7804	7970	8135	166
262	8301	8467	8633	8798	8964	9129	9295	9460	9625	9791	165
263	9956	.121	.286	.451	.616	.781	.945	1110	1275	1439	165
264	421604	1708	1933	2097	2261	2426	2590	2754	2918	3082	164
265	3246	3410	3574	3737	3901	4065	4228	4392	4555	4718	164
266	4882	5045	5208	5371	5534	5697	5860	6023	6186	6349	163
267	6511	6674	6836	6999	7161	7324	7486	7648	7811	7973	162
268	8135	8297	8459	8621	8783	8944	9106	9268	9429	9591	162
269	9752	9914	.75	.236	.398	.559	.720	.881	1042	1203	161
270	431364	1525	1685	1846	2007	2167	2328	2488	2649	2809	161
271	2969	3130	3290	3450	3610	3770	3930	4090	4249	4409	160
272	4569	4729	4888	5048	5207	5367	5526	5685	5844	6004	159
273	6163	6322	6481	6640	6798	6957	7116	7275	7433	7592	159
274	7751	7909	8067	8226	8384	8542	8701	8859	9017	9175	158
275	9333	9491	9648	9806	9964	.122	.279	.437	.594	.752	158
276	440909	1066	1224	1381	1538	1695	1852	2009	2166	2323	157
277	2480	2637	2793	2950	3106	3263	3419	3576	3732	3889	157
278	4045	4201	4357	4513	4669	4825	4981	5137	5293	5449	156
279	5604	5760	5915	6071	6226	6382	6537	6692	6848	7003	155

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280	447158	7313	7468	7623	7778	7933	8088	8242	8397	8552	155
281	8706	8861	9015	9170	9324	9478	9633	9787	9941	. .95	154
282	450249	0403	0557	0711	0865	1018	1172	1326	1479	1633	154
283	1786	1940	2093	2247	2400	2553	2706	2859	3012	3165	153
284	3318	3471	3624	3777	3930	4082	4235	4387	4540	4692	153
285	4845	4997	5150	5302	5454	5606	5758	5910	6062	6214	152
286	6366	6518	6670	6821	6973	7125	7276	7428	7579	7731	152
287	7882	8033	8184	8336	8487	8638	8789	8940	9091	9242	151
288	9392	9543	9694	9845	9995	.146	.296	.447	.597	.748	151
289	460898	1048	1198	1348	1499	1649	1799	1948	2098	2248	150
290	462398	2548	2697	2847	2997	3146	3296	3445	3594	3744	150
291	3893	4042	4191	4340	4490	4639	4788	4936	5085	5234	149
292	5383	5532	5680	5829	5977	6126	6274	6423	6571	6719	149
293	6868	7016	7164	7312	7460	7608	7756	7904	8052	8200	148
294	8347	8495	8643	8790	8938	9085	9233	9380	9527	9675	148
295	9822	9969	.116	.263	.410	.557	.704	.851	.998	1145	147
296	471292	1438	1585	1732	1878	2025	2171	2318	2464	2610	146
297	2756	2903	3049	3195	3341	3487	3633	3779	3925	4071	146
298	4216	4362	4508	4653	4799	4944	5090	5235	5381	5526	146
299	5671	5816	5962	6107	6252	6397	6542	6687	6832	6976	145
300	477121	7266	7411	7555	7700	7844	7989	8133	8278	8422	145
301	8566	8711	8855	8999	9143	9287	9431	9575	9719	9863	144
302	480007	0151	0294	0438	0582	0725	0869	1012	1156	1299	144
303	1443	1586	1729	1872	2016	2159	2302	2445	2588	2731	143
304	2874	3016	3159	3302	3445	3587	3730	3872	4015	4157	143
305	4300	4442	4585	4727	4869	5011	5153	5295	5437	5579	142
306	5721	5863	6005	6147	6289	6430	6572	6714	6855	6997	142
307	7138	7280	7421	7563	7704	7845	7986	8127	8269	8410	141
308	8551	8692	8833	8974	9114	9255	9396	9537	9677	9818	141
309	9958	. .99	.239	.380	.520	.661	.801	.941	1081	1222	140
310	491362	1502	1642	1782	1922	2062	2201	2341	2481	2621	140
311	2760	2900	3040	3179	3319	3458	3597	3737	3876	4015	139
312	4155	4294	4433	4572	4711	4850	4989	5128	5267	5406	139
313	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791	139
314	6930	7068	7206	7344	7483	7621	7759	7897	8035	8173	138
315	8311	8448	8586	8724	8862	8999	9137	9275	9412	9550	138
316	9687	9824	9962	. .99	.236	.374	.511	.648	.785	.922	137
317	501059	1196	1333	1470	1607	1744	1880	2017	2154	2291	137
318	2427	2564	2700	2837	2973	3109	3246	3382	3518	3655	136
319	3791	3927	4063	4199	4335	4471	4607	4743	4878	5014	136
320	505150	5286	5421	5557	5693	5828	5964	6099	6234	6370	136
321	6505	6640	6776	6911	7046	7181	7316	7451	7586	7721	135
322	7856	7991	8126	8260	8395	8530	8664	8799	8934	9068	135
323	9203	9337	9471	9606	9740	9874	. . .9	.143	.277	.411	134
324	510545	0679	0813	0947	1081	1215	1349	1482	1616	1750	134
325	1883	2017	2151	2284	2418	2551	2684	2818	2951	3084	133
326	3218	3351	3484	3617	3750	3883	4016	4149	4282	4414	133
327	4548	4681	4813	4946	5079	5211	5344	5476	5609	5741	133
328	5874	6006	6139	6271	6403	6535	6668	6800	6932	7064	132
329	7196	7328	7460	7592	7724	7855	7987	8119	8251	8382	132
330	518514	8646	8777	8909	9040	9171	9303	9434	9566	9697	131
331	9828	9959	. .90	.221	.353	.484	.615	.745	.876	1007	131
332	521138	1269	1400	1530	1661	1792	1922	2053	2183	2314	131
333	2444	2575	2705	2835	2966	3096	3226	3356	3486	3616	130
334	3746	3876	4006	4136	4266	4396	4526	4656	4786	4915	130
335	5045	5174	5304	5434	5563	5693	5822	5951	6081	6210	129
336	6339	6469	6598	6727	6856	6985	7114	7243	7372	7501	129
337	7630	7759	7888	8016	8145	8274	8402	8531	8660	8788	129
338	8917	9045	9174	9302	9430	9559	9687	9815	9943	. .72	128
339	530200	0328	0456	0584	0712	0840	0968	1096	1223	1351	128



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340	531479	1607	1734	1862	1990	2117	2245	2372	2500	2627	128
341	2754	2882	3009	3136	3264	3391	3518	3645	3772	3899	127
342	4026	4153	4280	4407	4534	4661	4787	4914	5041	5167	127
343	5294	5421	5547	5674	5800	5927	6053	6180	6306	6432	126
344	6558	6685	6811	6937	7063	7189	7315	7441	7567	7693	126
345	7819	7945	8071	8197	8322	8448	8574	8699	8825	8951	126
346	9076	9202	9327	9452	9578	9703	9829	9954	. . 79	. 204	125
347	540329	0455	0580	0705	0830	0955	1080	1205	1330	1454	125
348	1579	1704	1829	1953	2078	2203	2327	2452	2576	2701	125
349	2825	2950	3074	3199	3323	3447	3571	3696	3820	3944	124
350	544068	4192	4316	4440	4564	4688	4812	4936	5060	5183	124
351	5307	5431	5555	5678	5802	5925	6049	6172	6296	6419	124
352	6543	6666	6789	6913	7036	7159	7282	7405	7529	7652	123
353	7775	7898	8021	8144	8267	8389	8512	8635	8758	8881	123
354	9003	9126	9249	9371	9494	9616	9739	9861	9984	. 106	123
355	550228	0351	0473	0595	0717	0840	0962	1084	1206	1328	122
356	1450	1572	1694	1816	1938	2060	2181	2303	2425	2547	122
357	2668	2790	2911	3033	3155	3276	3398	3519	3640	3762	121
358	3883	4004	4126	4247	4368	4489	4610	4731	4852	4973	121
359	5094	5215	5336	5457	5578	5699	5820	5940	6061	6182	121
360	556303	6423	6544	6664	6785	6905	7026	7146	7267	7387	120
361	7507	7627	7748	7868	7988	8108	8228	8349	8469	8589	120
362	8709	8829	8948	9068	9188	9308	9428	9548	9667	9787	120
363	9907	. . 26	. 146	. 265	. 385	. 504	. 624	. 743	. 863	. 982	119
364	561101	1221	1340	1459	1578	1698	1817	1936	2055	2174	119
365	2293	2412	2531	2650	2769	2887	3006	3125	3244	3362	119
366	3481	3600	3718	3837	3955	4074	4192	4311	4429	4548	119
367	4666	4784	4903	5021	5139	5257	5376	5494	5612	5730	118
368	5848	5966	6084	6202	6320	6437	6555	6673	6791	6909	118
369	7026	7144	7262	7379	7497	7614	7732	7849	7967	8084	118
370	568202	8319	8436	8554	8671	8788	8905	9023	9140	9257	117
371	9374	9491	9608	9725	9842	9959	. . 76	. 193	. 309	. 426	117
372	570543	0660	0776	0893	1010	1126	1243	1359	1476	1592	117
373	1709	1825	1942	2058	2174	2291	2407	2523	2639	2755	116
374	2872	2988	3104	3220	3336	3452	3568	3684	3800	3915	116
375	4031	4147	4263	4379	4494	4610	4726	4841	4957	5072	116
376	5188	5303	5419	5534	5650	5765	5880	5996	6111	6226	115
377	6341	6457	6572	6687	6802	6917	7032	7147	7262	7377	115
378	7492	7607	7722	7836	7951	8066	8181	8295	8410	8525	115
379	8639	8754	8868	8983	9097	9212	9326	9441	9555	9669	114
380	579784	9898	. . 12	. 126	. 241	. 355	. 469	. 583	. 697	. 811	114
381	580925	1039	1153	1267	1381	1495	1608	1722	1836	1950	114
382	2063	2177	2291	2404	2518	2631	2745	2858	2972	3085	114
383	3199	3312	3426	3539	3652	3765	3879	3992	4105	4218	113
384	4331	4444	4557	4670	4783	4896	5009	5122	5235	5348	113
385	5461	5574	5686	5799	5912	6024	6137	6250	6362	6475	113
386	6587	6700	6812	6925	7037	7149	7262	7374	7486	7599	112
387	7711	7823	7935	8047	8160	8272	8384	8496	8608	8720	112
388	8832	8944	9056	9167	9279	9391	9503	9615	9726	9838	112
389	9950	. . 61	. 173	. 284	. 396	. 507	. 619	. 730	. 842	. 953	112
390	591065	1176	1287	1399	1510	1621	1732	1843	1955	2066	111
391	2177	2288	2399	2510	2621	2732	2843	2954	3064	3175	111
392	3286	3397	3508	3618	3729	3840	3950	4061	4171	4282	111
393	4393	4503	4614	4724	4834	4945	5055	5165	5276	5386	110
394	5496	5606	5717	5827	5937	6047	6157	6267	6377	6487	110
395	6597	6707	6817	6927	7037	7146	7256	7366	7476	7586	110
396	7695	7805	7914	8024	8134	8243	8353	8462	8572	8681	110
397	8791	8900	9009	9119	9228	9337	9446	9556	9665	9774	109
398	9883	9992	. 101	. 210	. 319	. 428	. 537	. 646	. 755	. 864	109
399	600973	1082	1191	1299	1408	1517	1625	1734	1843	1951	109

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A TABLE OF LOGARITHMS FROM 1 TO 10,000.

N.	0	1	2	3	4	5	6	7	8	9	D
400	602060	2169	2277	2386	2494	2603	2711	2819	2928	3036	108
401	3144	3253	3361	3469	3577	3686	3794	3902	4010	4118	108
402	4226	4334	4442	4550	4658	4766	4874	4982	5089	5197	108
403	5305	5413	5521	5628	5736	5844	5951	6059	6166	6274	108
404	6381	6489	6596	6704	6811	6919	7026	7133	7241	7348	107
405	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419	107
406	8526	8633	8740	8847	8954	9061	9167	9274	9381	9488	107
407	9594	9701	9808	9914	. 21	. 128	. 234	. 341	. 447	. 554	107
408	610660	0767	0873	0979	1086	1192	1298	1405	1511	1617	106
409	1723	1829	1936	2042	2148	2254	2360	2466	2572	2678	106
410	612784	2890	2996	3102	3207	3313	3419	3525	3630	3736	106
411	3842	3947	4053	4159	4264	4370	4475	4581	4686	4792	106
412	4897	5003	5108	5213	5319	5424	5529	5634	5740	5845	105
413	5950	6055	6160	6265	6370	6476	6581	6686	6790	6895	105
414	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943	105
415	8048	8153	8257	8362	8466	8571	8676	8780	8884	8989	105
416	9093	9198	9302	9406	9511	9615	9719	9824	9928	. 32	104
417	620136	0240	0344	0448	0552	0656	0760	0864	0968	1072	104
418	1176	1280	1384	1488	1592	1695	1799	1903	2007	2110	104
419	2214	2318	2421	2525	2628	2732	2835	2939	3042	3146	104
420	623249	3353	3456	3559	3663	3766	3869	3973	4076	4179	103
421	4282	4385	4488	4591	4695	4798	4901	5004	5107	5210	103
422	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238	103
423	6340	6443	6546	6648	6751	6853	6956	7058	7161	7263	103
424	7366	7468	7571	7673	7775	7878	7980	8082	8185	8287	102
425	8389	8491	8593	8695	8797	8900	9002	9104	9206	9308	102
426	9410	9512	9613	9715	9817	9919	. 21	. 123	. 224	. 326	102
427	630428	0530	0631	0733	0835	0936	1038	1139	1241	1342	102
428	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356	101
429	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367	101
430	633468	3569	3670	3771	3872	3973	4074	4175	4276	4376	100
431	4477	4578	4679	4779	4880	4981	5081	5182	5283	5383	100
432	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388	100
433	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390	100
434	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389	99
435	8489	8589	8689	8789	8888	8988	9088	9188	9287	9387	99
436	9486	9586	9686	9785	9885	9984	. 84	. 183	. 283	. 382	99
437	640481	0581	0680	0779	0879	0978	1077	1177	1276	1375	99
438	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366	99
439	2465	2563	2662	2761	2860	2959	3058	3156	3255	3354	99
440	643153	3551	3650	3749	3847	3946	4044	4143	4242	4340	98
441	4439	4537	4636	4734	4832	4931	5029	5127	5226	5324	98
442	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306	98
443	6404	6502	6600	6698	6796	6894	6992	7089	7187	7285	98
444	7383	7481	7579	7676	7774	7872	7969	8067	8165	8262	98
445	8360	8458	8555	8653	8750	8848	8945	9043	9140	9237	97
446	9335	9432	9530	9627	9724	9821	9919	. 16	. 113	. 210	97
447	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181	97
448	1278	1375	1472	1569	1666	1762	1859	1956	2053	2150	97
449	2246	2343	2440	2536	2633	2730	2826	2923	3019	3116	97
450	653213	3309	3405	3502	3598	3695	3791	3888	3984	4080	96
451	4177	4273	4369	4465	4562	4658	4754	4850	4946	5042	96
452	5139	5235	5331	5427	5523	5619	5715	5810	5906	6002	96
453	6098	6194	6290	6386	6482	6577	6673	6769	6864	6960	96
454	7056	7152	7247	7343	7438	7534	7629	7725	7820	7916	96
455	8011	8107	8202	8298	8393	8488	8584	8679	8774	8870	95
456	8965	9060	9155	9250	9346	9441	9536	9631	9726	9821	95
457	9916	. 11	. 106	. 201	. 296	. 391	. 486	. 581	. 676	. 771	95
458	660365	0960	1055	1150	1245	1339	1434	1529	1623	1718	95
459	1813	1907	2002	2096	2191	2286	2380	2475	2569	2663	95

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160	662159	2532	2247	3041	3135	3220	3324	3418	3512	3607	94
161	3791	3775	3859	3943	4078	4172	4266	4360	4454	4548	94
162	4642	4736	4830	4924	5018	5112	5206	5294	5383	5487	94
163	5581	5675	5769	5862	5956	6050	6143	6237	6331	6424	94
164	6519	6612	6705	6799	6892	6986	7079	7173	7266	7360	94
165	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293	94
166	8386	8479	8572	8665	8759	8852	8945	9038	9131	9224	93
167	9317	9410	9503	9596	9689	9782	9875	9967	1.60	1.53	93
168	670246	0229	0431	0524	0617	0710	0802	0895	0988	1080	93
169	1173	1265	1358	1451	1543	1636	1728	1821	1913	2005	93
170	672028	2160	2253	2345	2437	2530	2622	2714	2806	2899	92
171	3021	3113	3205	3297	3390	3482	3574	3666	3758	3850	92
172	3942	4034	4126	4218	4310	4402	4494	4586	4677	4769	92
173	4861	4953	5045	5137	5228	5320	5412	5503	5595	5687	92
174	5778	5870	5962	6053	6145	6236	6328	6419	6511	6602	92
175	6694	6785	6876	6968	7059	7151	7242	7333	7424	7516	91
176	7607	7698	7789	7881	7972	8063	8154	8245	8336	8427	91
177	8518	8609	8700	8791	8882	8973	9064	9155	9246	9337	91
178	9428	9519	9610	9700	9791	9882	9973	1.63	1.54	1.45	91
179	680036	0426	0517	0607	0698	0789	0879	0970	1060	1151	91
180	681241	1332	1422	1513	1603	1693	1784	1874	1964	2055	90
181	2145	2235	2326	2416	2506	2596	2686	2777	2867	2957	90
182	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857	90
183	3-17	4137	4127	4217	4307	4396	4486	4576	4666	4756	90
184	4845	4935	5025	5114	5204	5294	5383	5473	5563	5652	90
185	5742	5831	5921	6010	6100	6189	6279	6368	6458	6547	89
186	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440	89
187	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331	89
188	8420	8509	8598	8687	8776	8865	8953	9042	9131	9220	89
189	9309	9398	9486	9575	9664	9753	9841	9930	1.19	1.107	89
190	690196	0285	0373	0462	0550	0639	0728	0816	0905	0993	89
191	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877	88
192	1965	2053	2142	2230	2318	2406	2494	2583	2671	2759	88
193	2847	2935	3023	3111	3199	3287	3375	3463	3551	3639	88
194	3727	3815	3903	3991	4078	4166	4254	4342	4430	4517	88
195	4605	4693	4781	4868	4956	5044	5131	5219	5307	5394	88
196	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269	87
197	6356	6444	6531	6618	6706	6793	6880	6968	7055	7142	87
198	7229	7317	7404	7491	7578	7665	7752	7839	7926	8014	87
199	8101	8188	8275	8362	8449	8535	8622	8709	8796	8883	87
200	698970	9057	9144	9231	9317	9404	9491	9578	9664	9751	87
501	9838	9924	1.11	1.98	1.84	2.71	3.58	4.44	5.31	6.17	87
502	700704	0790	0877	0963	1050	1136	1222	1309	1395	1482	86
503	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344	86
504	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205	86
505	3291	3377	3463	3549	3635	3721	3807	3893	3979	4065	86
506	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922	86
507	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778	86
508	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632	85
509	6718	6803	6888	6974	7059	7144	7229	7315	7400	7485	85
510	707570	7655	7740	7826	7911	7996	8081	8166	8251	8336	85
511	8421	8506	8591	8676	8761	8846	8931	9015	9100	9185	85
512	9270	9355	9440	9524	9609	9694	9779	9863	9948	1.33	85
513	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879	85
514	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723	84
515	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566	84
516	2650	2734	2818	2902	2986	3070	3154	3238	3323	3407	84
517	3491	3575	3659	3742	3826	3910	3994	4078	4162	4246	84
518	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084	84
519	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920	84
N.	0	1	2	3	4	5	6	7	8	9	D.

A TABLE OF LOGARITHMS FROM 1 TO 10,000.

N.	0	1	2	3	4	5	6	7	8	9	D.
520	716003	6087	6170	6254	6337	6421	6504	6588	6671	6754	83
521	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587	83
522	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419	83
523	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248	83
524	9331	9414	9497	9580	9663	9745	9828	9911	9994	. . 77	83
525	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903	83
526	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728	82
527	1811	1893	1975	2058	2140	2222	2305	2387	2469	2552	82
528	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374	82
529	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194	82
530	724276	4358	4440	4522	4604	4685	4767	4849	4931	5013	82
531	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830	82
532	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646	82
533	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460	81
534	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273	81
535	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084	81
536	9165	9246	9327	9408	9489	9570	9651	9732	9813	9893	81
537	9974	. . 55	. 136	. 217	. 298	. 378	. 459	. 540	. 621	. 702	81
538	730782	0893	0914	1024	1105	1186	1266	1347	1428	1508	81
539	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313	81
540	732394	2474	2555	2635	2715	2796	2876	2956	3037	3117	80
541	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919	80
542	3999	4079	4160	4240	4320	4400	4480	4560	4640	4720	80
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519	80
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317	80
545	6397	6476	6556	6635	6715	6795	6874	6954	7034	7113	80
546	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908	79
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701	79
548	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493	79
549	9572	9651	9721	9810	9889	9968	. . 47	. 126	. 205	. 284	79
550	740363	0442	0521	0600	0678	0757	0836	0915	0994	1073	79
551	1152	1230	1309	1388	1467	1546	1624	1703	1782	1860	79
552	1939	2018	2096	2175	2254	2332	2411	2489	2568	2646	79
553	2725	2804	2882	2961	3039	3118	3196	3275	3353	3431	78
554	3510	3588	3667	3745	3823	3902	3980	4058	4136	4215	78
555	4293	4371	4449	4528	4606	4684	4762	4840	4919	4997	78
556	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777	78
557	5855	5933	6011	6089	6167	6245	6323	6401	6479	6556	78
558	6634	6712	6790	6868	6945	7023	7101	7179	7256	7334	78
559	7412	7489	7567	7645	7722	7800	7878	7955	8033	8110	78
560	748188	8266	8343	8421	8498	8576	8653	8731	8808	8885	77
561	8963	9040	9118	9195	9272	9350	9427	9504	9582	9659	77
562	9736	9814	9891	9968	. . 45	. 123	. 200	. 277	. 354	. 431	77
563	750508	0586	0663	0740	0817	0894	0971	1048	1125	1202	77
564	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972	77
565	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740	77
566	2816	2893	2970	3047	3123	3200	3277	3353	3430	3506	77
567	3583	3660	3736	3813	3889	3966	4042	4119	4195	4272	77
568	4348	4425	4501	4578	4654	4730	4807	4883	4960	5036	76
569	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799	76
570	755875	5951	6027	6103	6180	6256	6332	6408	6484	6560	76
571	6636	6712	6788	6864	6940	7016	7092	7168	7244	7320	76
572	7396	7472	7548	7624	7700	7775	7851	7927	8003	8079	76
573	8155	8230	8306	8382	8458	8533	8609	8685	8761	8836	76
574	8912	8988	9063	9139	9214	9290	9366	9441	9517	9592	76
575	9698	9773	9849	9924	. . 45	. 121	. 196	. 272	. 347	. 422	75
576	760422	0498	0573	0649	0724	0799	0875	0950	1025	1101	75
577	1176	1251	1326	1402	1477	1552	1627	1702	1778	1853	75
578	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604	75
579	2679	2754	2829	2904	2978	3053	3128	3203	3278	3353	75
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N.	0	1	2	3	4	5	6	7	8	9	D.
580	763428	3503	3578	3653	3727	3802	3877	3952	4027	4101	75
581	4176	4251	4326	4400	4475	4550	4624	4699	4774	4848	75
582	4923	4998	5072	5147	5221	5296	5370	5445	5520	5594	75
583	5669	5743	5818	5892	5966	6041	6115	6190	6264	6338	74
584	6413	6487	6562	6636	6710	6785	6859	6933	7007	7082	74
585	7156	7230	7304	7379	7453	7527	7601	7675	7749	7823	74
586	7898	7972	8046	8120	8194	8268	8342	8416	8490	8564	74
587	8638	8712	8786	8860	8934	9008	9082	9156	9230	9303	74
588	9377	9451	9525	9599	9673	9746	9820	9894	9968	. . 42	74
589	770115	0189	0263	0336	0410	0484	0557	0631	0705	0778	74
590	770852	0926	0999	1073	1146	1220	1293	1367	1440	1514	74
591	1587	1661	1734	1808	1881	1955	2029	2102	2175	2248	73
592	2322	2395	2468	2542	2615	2688	2762	2835	2908	2981	73
593	3055	3128	3201	3274	3348	3421	3494	3567	3640	3713	73
594	3786	3860	3933	4006	4079	4152	4225	4298	4371	4444	73
595	4517	4590	4663	4736	4809	4882	4955	5028	5100	5173	73
596	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902	73
597	5974	6047	6120	6193	6265	6338	6411	6483	6556	6629	73
598	6701	6774	6846	6919	6992	7064	7137	7209	7282	7354	73
599	7427	7499	7572	7644	7717	7789	7862	7934	8006	8079	72
600	778151	8224	8296	8368	8441	8513	8585	8658	8730	8802	72
601	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524	72
602	9596	9669	9741	9813	9885	9957	. . 29	1.01	1.73	.245	72
603	780317	0389	0461	0533	0605	0677	0749	0821	0893	0965	72
604	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684	72
605	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401	72
606	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117	72
607	3189	3260	3332	3403	3475	3546	3618	3689	3761	3832	71
608	3904	3975	4046	4118	4189	4261	4332	4403	4475	4546	71
609	4617	4689	4760	4831	4902	4974	5045	5116	5187	5259	71
610	785330	5401	5472	5543	5615	5686	5757	5828	5899	5970	71
611	6041	6112	6183	6254	6325	6396	6467	6538	6609	6680	71
612	6751	6822	6893	6964	7035	7106	7177	7248	7319	7390	71
613	7460	7531	7602	7673	7744	7815	7885	7956	8027	8098	71
614	8168	8239	8310	8381	8451	8522	8593	8663	8734	8804	71
615	8875	8946	9016	9087	9157	9228	9299	9369	9440	9510	71
616	9581	9651	9722	9792	9863	9933	. . . 4	. . 74	1.44	.215	70
617	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918	70
618	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620	70
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322	70
620	792392	2462	2532	2602	2672	2742	2812	2882	2952	3022	70
621	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721	70
622	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418	70
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115	70
624	5185	5254	5324	5393	5463	5532	5602	5672	5741	5811	70
625	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505	69
626	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198	69
627	7268	7337	7406	7475	7545	7614	7683	7752	7821	7890	69
628	7960	8029	8098	8167	8236	8305	8374	8443	8513	8582	69
629	8651	8720	8789	8858	8927	8996	9065	9134	9203	9272	69
630	799341	9409	9478	9547	9616	9685	9754	9823	9892	9961	69
631	800029	0098	0167	0236	0305	0373	0442	0511	0580	0648	69
632	0717	0786	0854	0923	0992	1061	1129	1198	1266	1335	69
633	1404	1472	1541	1609	1678	1747	1815	1884	1952	2021	69
634	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705	69
635	2774	2842	2910	2979	3047	3116	3184	3252	3321	3389	68
636	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071	68
637	4139	4208	4276	4344	4412	4480	4548	4616	4685	4753	68
638	4821	4889	4957	5025	5093	5161	5229	5297	5365	5433	68
639	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112	68

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640	806180	6248	6316	6384	6451	6519	6587	6655	6723	6790	68
641	6858	6926	6994	7061	7129	7197	7264	7332	7400	7467	68
642	7535	7603	7670	7738	7806	7873	7941	8008	8076	8143	68
643	8211	8279	8346	8414	8481	8549	8616	8684	8751	8818	67
644	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492	67
645	9560	9627	9694	9762	9829	9896	9964	. . 31	. . 98	. 165	67
646	810233	0300	0367	0434	0501	0569	0636	0703	0770	0837	67
647	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508	67
648	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178	67
649	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847	67
650	812913	2980	3047	3114	3181	3247	3314	3381	3448	3514	67
651	3581	3648	3714	3781	3848	3914	3981	4048	4114	4181	67
652	4248	4314	4381	4447	4514	4581	4647	4714	4780	4847	67
653	4913	4980	5046	5113	5179	5246	5312	5378	5445	5511	66
654	5578	5644	5711	5777	5843	5910	5976	6042	6109	6175	66
655	6241	6308	6374	6440	6506	6573	6639	6705	6771	6838	66
656	6904	6970	7036	7102	7169	7235	7301	7367	7433	7499	66
657	7565	7631	7698	7764	7830	7896	7962	8028	8094	8160	66
658	8226	8292	8358	8424	8490	8556	8622	8688	8754	8820	66
659	8885	8951	9017	9083	9149	9215	9281	9346	9412	9478	66
660	819544	9610	9676	9741	9807	9873	9939	. . . 4	. . 70	. 136	66
661	820201	0267	0333	0399	0464	0530	0595	0661	0727	0792	66
662	0858	0924	0989	1055	1120	1186	1251	1317	1382	1448	66
663	1514	1579	1645	1710	1775	1841	1906	1972	2037	2103	65
664	2168	2233	2299	2364	2430	2495	2560	2626	2691	2756	65
665	2822	2887	2952	3018	3083	3148	3213	3279	3344	3409	65
666	3474	3539	3605	3670	3735	3800	3865	3930	3996	4061	65
667	4126	4191	4256	4321	4386	4451	4516	4581	4646	4711	65
668	4776	4841	4906	4971	5036	5101	5166	5231	5296	5361	65
669	5426	5491	5556	5621	5686	5751	5815	5880	5945	6010	65
670	826705	6140	6204	6269	6334	6399	6464	6528	6593	6658	65
671	6723	6787	6852	6917	6981	7046	7111	7175	7240	7305	65
672	7369	7434	7499	7563	7628	7692	7757	7821	7886	7951	65
673	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595	64
674	8660	8724	8789	8853	8918	8982	9046	9111	9175	9239	64
675	9304	9368	9432	9497	9561	9625	9690	9754	9818	9882	64
676	9947	. . 11	. . 75	. 139	. 204	. 268	. 332	. 396	. 460	. 525	64
677	830589	0653	0717	0781	0845	0909	0973	1037	1102	1166	64
678	1230	1294	1358	1422	1486	1550	1614	1678	1742	1806	64
679	1870	1934	1998	2062	2126	2189	2253	2317	2381	2445	64
680	832509	2573	2637	2700	2764	2828	2892	2956	3020	3083	64
681	3147	3211	3275	3338	3402	3466	3530	3593	3657	3721	64
682	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357	64
683	4421	4484	4548	4611	4675	4739	4802	4866	4929	4993	64
684	5056	5120	5183	5247	5310	5373	5437	5500	5564	5627	63
685	5691	5754	5817	5881	5944	6007	6071	6134	6197	6261	63
686	6324	6387	6451	6514	6577	6641	6704	6767	6830	6894	63
687	6957	7020	7083	7146	7210	7273	7336	7399	7462	7525	63
688	7588	7652	7715	7778	7841	7904	7967	8030	8093	8156	63
689	8219	8282	8345	8408	8471	8534	8597	8660	8723	8786	63
690	838849	8912	8975	9038	9101	9164	9227	9289	9352	9415	63
691	9478	9541	9604	9667	9729	9792	9855	9918	9981	. . 43	63
692	840106	0169	0232	0294	0357	0420	0482	0545	0608	0671	63
693	0733	0796	0859	0921	0984	1046	1109	1172	1234	1297	63
694	1359	1422	1485	1547	1610	1672	1735	1797	1860	1922	63
695	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547	62
696	2609	2672	2734	2796	2859	2921	2983	3046	3108	3170	62
697	3233	3295	3357	3420	3482	3544	3606	3669	3731	3793	62
698	3855	3918	3980	4042	4104	4166	4229	4291	4353	4415	62
699	4477	4539	4601	4664	4726	4788	4850	4912	4974	5036	62
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701	5718	5780	5842	5904	5966	6028	6090	6151	6213	6275	62
702	6337	6399	6461	6523	6585	6646	6708	6770	6832	6894	62
703	6955	7017	7079	7141	7202	7264	7326	7388	7449	7511	62
704	7573	7634	7696	7758	7819	7881	7943	8004	8066	8128	62
705	8189	8251	8312	8374	8435	8497	8559	8620	8682	8743	62
706	8805	8866	8928	8989	9051	9112	9174	9235	9297	9358	61
707	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972	61
708	850033	0095	0156	0217	0279	0340	0401	0462	0524	0585	61
709	0646	0707	0769	0830	0891	0952	1014	1075	1136	1197	61
710	851258	1320	1381	1442	1503	1564	1625	1686	1747	1809	61
711	1870	1931	1992	2053	2114	2175	2236	2297	2358	2419	61
712	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029	61
713	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637	61
714	3698	3759	3820	3881	3941	4002	4063	4124	4185	4245	61
715	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852	61
716	4913	4974	5034	5095	5156	5216	5277	5337	5398	5459	61
717	5519	5580	5640	5701	5761	5822	5882	5943	6003	6064	61
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668	60
719	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272	60
720	857332	7393	7453	7513	7574	7634	7694	7755	7815	7875	60
721	7935	7995	8056	8116	8176	8236	8297	8357	8417	8477	60
722	8537	8597	8657	8718	8778	8838	8898	8958	9018	9078	60
723	9138	9198	9258	9318	9379	9439	9499	9559	9619	9679	60
724	9739	9799	9859	9918	9978	. . 38	. . 98	. 158	. 218	. 278	60
725	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877	60
726	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475	60
727	1534	1594	1654	1714	1773	1833	1893	1952	2012	2072	60
728	2131	2191	2251	2310	2370	2430	2489	2549	2608	2668	60
729	2728	2787	2847	2906	2966	3025	3085	3144	3204	3263	60
730	863323	3382	3442	3501	3561	3620	3680	3739	3799	3858	59
731	3917	3977	4036	4096	4155	4214	4274	4333	4392	4452	59
732	4511	4570	4630	4689	4748	4808	4867	4926	4985	5045	59
733	5104	5163	5222	5282	5341	5400	5459	5519	5578	5637	59
734	5696	5755	5814	5874	5933	5992	6051	6110	6169	6228	59
735	6287	6346	6405	6465	6524	6583	6642	6701	6760	6819	59
736	6878	6937	6996	7055	7114	7173	7232	7291	7350	7409	59
737	7467	7526	7585	7644	7703	7762	7821	7880	7939	7998	59
738	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586	59
739	8644	8703	8762	8821	8879	8938	8997	9056	9114	9173	59
740	869232	9290	9349	9408	9466	9525	9584	9642	9701	9760	59
741	9818	9877	9935	9994	. . 53	. 111	. 170	. 228	. 287	. 345	59
742	870404	0462	0521	0579	0638	0696	0755	0813	0872	0930	58
743	0989	1047	1106	1164	1223	1281	1339	1398	1456	1515	58
744	1573	1631	1690	1748	1806	1865	1923	1981	2040	2098	58
745	2156	2215	2273	2331	2389	2448	2506	2564	2622	2681	58
746	2739	2797	2855	2913	2972	3030	3088	3146	3204	3262	58
747	3321	3379	3437	3495	3553	3611	3669	3727	3785	3844	58
748	3902	3960	4018	4076	4134	4192	4250	4308	4366	4424	58
749	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003	58
750	875061	5119	5177	5235	5293	5351	5409	5466	5524	5582	58
751	5640	5698	5756	5813	5871	5929	5987	6045	6102	6160	58
752	6218	6276	6333	6391	6449	6507	6564	6622	6680	6737	58
753	6795	6853	6910	6968	7026	7083	7141	7199	7256	7314	58
754	7371	7429	7487	7544	7602	7659	7717	7774	7832	7889	58
755	7947	8004	8062	8119	8177	8234	8292	8349	8407	8464	57
756	8522	8579	8637	8694	8752	8809	8866	8924	8981	9039	57
757	9096	9153	9211	9268	9325	9383	9440	9497	9555	9612	57
758	9669	9726	9784	9841	9898	9956	. . 13	. 70	. 127	. 185	57
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762	1955	2012	2069	2126	2183	2240	2297	2354	2411	2468	57
763	2525	2581	2638	2695	2752	2809	2866	2923	2980	3037	57
764	3093	3150	3207	3264	3321	3377	3434	3491	3548	3605	57
765	3661	3718	3775	3832	3888	3945	4002	4059	4115	4172	57
766	4229	4285	4342	4399	4455	4512	4569	4625	4682	4739	57
767	4795	4852	4909	4965	5022	5078	5135	5192	5248	5305	57
768	5361	5418	5474	5531	5587	5644	5700	5757	5813	5870	57
769	5926	5983	6039	6096	6152	6209	6265	6321	6378	6434	56
770	886491	6547	6604	6660	6716	6773	6829	6885	6942	6998	56
771	7054	7111	7167	7223	7280	7336	7392	7449	7505	7561	56
772	7617	7674	7730	7786	7842	7898	7955	8011	8067	8123	56
773	8179	8236	8292	8348	8404	8460	8516	8573	8629	8685	56
774	8741	8797	8853	8909	8965	9021	9077	9134	9190	9246	56
775	9302	9358	9414	9470	9526	9582	9638	9694	9750	9806	56
776	9862	9918	9974	.30	.86	.141	.197	.253	.309	.365	56
777	890421	0477	0533	0589	0645	0700	0756	0812	0868	0924	56
778	0980	1035	1091	1147	1203	1259	1314	1370	1426	1482	56
779	1537	1593	1649	1705	1760	1816	1872	1928	1983	2039	56
780	892095	2150	2206	2262	2317	2373	2429	2484	2540	2595	56
781	2651	2707	2762	2818	2873	2929	2985	3040	3096	3151	56
782	3207	3262	3318	3373	3429	3484	3540	3595	3651	3706	56
783	3762	3817	3873	3928	3984	4039	4094	4150	4205	4261	55
784	4316	4371	4427	4482	4538	4593	4648	4704	4759	4814	55
785	4870	4925	4980	5036	5091	5146	5201	5257	5312	5367	55
786	5423	5478	5533	5588	5644	5699	5754	5809	5864	5920	55
787	5975	6030	6085	6140	6195	6251	6306	6361	6416	6471	55
788	6526	6581	6636	6692	6747	6802	6857	6912	6967	7022	55
789	7077	7132	7187	7242	7297	7352	7407	7462	7517	7572	55
790	897627	7682	7737	7792	7847	7902	7957	8012	8067	8122	55
791	8176	8231	8286	8341	8396	8451	8506	8561	8616	8670	55
792	8725	8780	8835	8890	8944	8999	9054	9109	9164	9218	55
793	9273	9328	9383	9437	9492	9547	9602	9656	9711	9766	55
794	9821	9875	9930	9985	.39	.94	.149	.203	.258	.312	55
795	900367	0422	0476	0531	0586	0640	0695	0749	0804	0859	55
796	0913	0968	1022	1077	1131	1186	1240	1295	1349	1404	55
797	1458	1513	1567	1622	1676	1731	1785	1840	1894	1948	54
798	2003	2057	2112	2166	2221	2275	2329	2384	2438	2492	54
799	2547	2601	2655	2710	2764	2818	2873	2927	2981	3036	54
800	903090	3144	3199	3253	3307	3361	3416	3470	3524	3578	54
801	3633	3687	3741	3795	3849	3904	3958	4012	4066	4120	54
802	4174	4229	4283	4337	4391	4445	4499	4553	4607	4661	54
803	4716	4770	4824	4878	4932	4986	5040	5094	5148	5202	54
804	5256	5310	5364	5418	5472	5526	5580	5634	5688	5742	54
805	5796	5850	5904	5958	6012	6066	6119	6173	6227	6281	54
806	6335	6389	6443	6497	6551	6604	6658	6712	6766	6820	54
807	6874	6927	6981	7035	7089	7143	7196	7250	7304	7358	54
808	7411	7465	7519	7573	7626	7680	7734	7787	7841	7895	54
809	7949	8002	8056	8110	8163	8217	8270	8324	8378	8431	54
810	908485	8539	8592	8646	8699	8753	8807	8860	8914	8967	54
811	9021	9074	9128	9181	9235	9289	9342	9396	9449	9503	54
812	9556	9610	9663	9716	9770	9823	9877	9930	9984	.37	53
813	910091	0144	0197	0251	0304	0358	0411	0464	0518	0571	53
814	0624	0678	0731	0784	0838	0891	0944	0998	1051	1104	53
815	1158	1211	1264	1317	1371	1424	1477	1530	1584	1637	53
816	1690	1743	1797	1850	1903	1956	2009	2063	2116	2169	53
817	2222	2275	2328	2381	2435	2488	2541	2594	2647	2700	53
818	2753	2806	2859	2913	2966	3019	3072	3125	3178	3231	53
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822	4872	4925	4977	5030	5083	5136	5189	5241	5294	5347	53
823	5400	5453	5505	5558	5611	5664	5716	5769	5822	5875	53
824	5927	5980	6033	6085	6138	6191	6243	6296	6349	6401	53
825	6154	6507	6559	6612	6664	6717	6770	6822	6875	6927	53
826	6940	7033	7085	7138	7190	7243	7295	7348	7400	7453	53
827	7506	7558	7611	7663	7716	7768	7820	7873	7925	7978	52
828	8030	8083	8135	8188	8240	8293	8345	8397	8450	8502	52
829	8555	8607	8659	8712	8764	8816	8869	8921	8973	9026	52
830	019078	9130	9183	9235	9287	9340	9392	9444	9496	9549	52
831	9601	9653	9706	9758	9810	9862	9914	9967	. . 19	. . 71	52
832	920123	0176	0228	0280	0332	0384	0436	0489	0541	0593	52
833	0645	0697	0749	0801	0853	0905	0958	1010	1062	1114	52
834	1166	1218	1270	1322	1374	1426	1478	1530	1582	1634	52
835	1686	1738	1790	1842	1894	1946	1998	2050	2102	2154	52
836	2206	2258	2310	2362	2414	2466	2518	2570	2622	2674	52
837	2725	2777	2829	2881	2933	2985	3037	3089	3140	3192	52
838	3244	3296	3348	3399	3451	3503	3555	3607	3658	3710	52
839	3762	3814	3865	3917	3969	4021	4072	4124	4176	4228	52
840	924279	4331	4383	4434	4486	4538	4589	4641	4693	4744	52
841	4796	4848	4899	4951	5003	5054	5106	5157	5209	5261	52
842	5312	5364	5415	5467	5518	5570	5621	5673	5725	5776	52
843	5828	5879	5931	5982	6034	6085	6137	6188	6240	6291	51
844	6342	6394	6445	6497	6548	6600	6651	6702	6754	6805	51
845	6857	6908	6959	7011	7062	7114	7165	7216	7268	7319	51
846	7370	7422	7473	7524	7576	7627	7678	7730	7781	7832	51
847	7883	7935	7986	8037	8088	8140	8191	8242	8293	8345	51
848	8396	8447	8498	8549	8601	8652	8703	8754	8805	8857	51
849	8908	8959	9010	9061	9112	9163	9215	9266	9317	9368	51
850	929419	9470	9521	9572	9623	9674	9725	9776	9827	9879	51
851	9930	9981	. . 32	. . 83	. 134	. 185	. 236	. 287	. 338	. 389	51
852	930440	0491	0542	0592	0643	0694	0745	0796	0847	0898	51
853	0949	1000	1051	1102	1153	1204	1254	1305	1356	1407	51
854	1458	1509	1560	1610	1661	1712	1763	1814	1865	1915	51
855	1966	2017	2068	2118	2169	2220	2271	2322	2372	2423	51
856	2474	2524	2575	2626	2677	2727	2778	2829	2879	2930	51
857	2981	3031	3082	3133	3183	3234	3285	3335	3386	3437	51
858	3487	3538	3589	3639	3690	3740	3791	3841	3892	3943	51
859	3993	4044	4094	4145	4195	4246	4296	4347	4397	4448	51
860	934498	4549	4599	4650	4700	4751	4801	4852	4902	4953	50
861	5003	5054	5104	5154	5205	5255	5306	5356	5406	5457	50
862	5507	5558	5608	5658	5709	5759	5809	5860	5910	5960	50
863	6011	6061	6111	6162	6212	6262	6313	6363	6413	6463	50
864	6514	6564	6614	6665	6715	6765	6815	6865	6916	6966	50
865	7016	7066	7117	7167	7217	7267	7317	7367	7418	7468	50
866	7518	7568	7618	7668	7718	7769	7819	7869	7919	7969	50
867	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470	50
868	8520	8570	8620	8670	8720	8770	8820	8870	8920	8970	50
869	9020	9070	9120	9170	9220	9270	9320	9369	9419	9469	50
870	9395; 9	9569	9619	9669	9719	9769	9819	9869	9918	9968	50
871	940018	0068	0118	0168	0218	0267	0317	0367	0417	0467	50
872	0516	0566	0616	0666	0716	0765	0815	0865	0915	0964	50
873	1014	1064	1114	1163	1213	1263	1313	1362	1412	1462	50
874	1511	1561	1611	1660	1710	1760	1809	1859	1909	1958	50
875	2008	2058	2107	2157	2207	2256	2306	2355	2405	2455	50
876	2504	2554	2603	2653	2702	2752	2801	2851	2901	2950	50
877	3000	3049	3099	3148	3198	3247	3297	3346	3396	3445	49
878	3495	3544	3593	3643	3692	3742	3791	3841	3890	2939	49
879	3989	4038	4088	4137	4186	4236	4285	4335	4384	4433	49
N.	0	1	2	3	4	5	6	7	8	9	D.

A TABLE OF LOGARITHMS FROM 1 TO 10,000.

N.	0	1	2	3	4	5	6	7	8	9	D.
880	944483	4532	4581	4631	4680	4729	4779	4828	4877	4927	49
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	49
882	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912	49
883	5961	6010	6059	6108	6157	6207	6256	6305	6354	6403	49
884	6452	6501	6551	6600	6649	6698	6747	6796	6845	6894	49
885	6943	6992	7041	7090	7140	7189	7238	7287	7336	7385	49
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	49
887	7924	7973	8022	8070	8119	8168	8217	8266	8315	8364	49
888	8413	8462	8511	8560	8609	8657	8706	8755	8804	8853	49
889	8902	8951	8999	9048	9097	9146	9195	9244	9292	9341	49
890	949390	9439	9488	9536	9585	9634	9683	9731	9780	9829	49
891	9878	9926	9975	.24	.73	.121	.170	.219	.267	.316	49
892	950365	04.4	0462	0511	0560	0608	0657	0706	0754	0803	49
893	0851	0900	0949	0997	1046	1095	1143	1192	1240	1289	49
894	1338	1386	1435	1483	1532	1580	1629	1677	1726	1775	49
895	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260	48
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	48
897	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228	48
898	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711	48
899	3760	3808	3856	3905	3953	4001	4049	4098	4146	4194	48
900	954243	4291	4339	4387	4435	4484	4532	4580	4628	4677	48
901	4725	4773	4821	4869	4918	4966	5014	5062	5110	5158	48
902	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640	48
903	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120	48
904	6168	6216	6265	6313	6361	6409	6457	6505	6553	6601	48
905	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080	48
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559	48
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	48
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516	48
909	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994	48
910	959041	9039	9137	9185	9232	9280	9328	9375	9423	9471	48
911	9518	9566	9614	9661	9709	9757	9804	9852	9900	9947	48
912	9995	.42	.90	.138	.185	.233	.280	.328	.376	.423	48
913	960471	0518	0566	0613	0661	0709	0756	0804	0851	0899	48
914	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374	47
915	1421	1469	1516	1563	1611	1658	1706	1753	1801	1848	47
916	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322	47
917	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795	47
918	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268	47
919	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741	47
920	963788	3835	3882	3929	3977	4024	4071	4118	4165	4212	47
921	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684	47
922	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155	47
923	5202	5249	5296	5343	5390	5437	5484	5531	5578	5625	47
924	5672	5719	5766	5813	5860	5907	5954	6001	6048	6095	47
925	6142	6189	6236	6283	6329	6376	6423	6470	6517	6564	47
926	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033	47
927	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501	47
928	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969	47
929	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436	47
930	968483	8530	8576	8623	8670	8716	8763	8810	8856	8903	47
931	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369	47
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835	47
933	9882	9928	9975	.21	.68	.114	.161	.207	.254	.300	47
934	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765	46
935	0812	0858	0904	0951	0997	1044	1090	1137	1183	1229	46
936	1276	1322	1369	1415	1461	1508	1554	1601	1647	1693	46
937	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157	46
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619	46
939	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082	46
N.	0	1	2	3	4	5	6	7	8	9	D.

A TABLE OF LOGARITHMS FROM 1 TO 10,000

N.	0	1	2	3	4	5	6	7	8	9	D.
940	973128	3174	3220	3266	3313	3359	3405	3451	3497	3543	46
941	3590	3636	3682	3728	3774	3820	3866	3913	3959	4005	46
942	4051	4097	4143	4189	4235	4281	4327	4374	4420	4466	46
943	4512	4558	4604	4650	4696	4742	4788	4834	4880	4926	46
944	4972	5018	5064	5110	5156	5202	5248	5294	5340	5386	46
945	5432	5478	5524	5570	5616	5662	5707	5753	5799	5845	46
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304	46
947	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763	46
948	6808	6854	6900	6946	6992	7037	7083	7129	7175	7220	46
949	7266	7312	7358	7403	7449	7495	7541	7586	7632	7678	46
950	977724	7769	7815	7861	7906	7952	7998	8043	8089	8135	46
951	8181	8226	8272	8317	8363	8409	8454	8500	8546	8591	46
952	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047	46
953	9093	9138	9184	9230	9275	9321	9366	9412	9457	9503	46
954	9548	9594	9639	9685	9730	9776	9821	9867	9912	9958	46
955	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412	45
956	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867	45
957	0912	0957	1003	1048	1093	1139	1184	1229	1275	1320	45
958	1366	1411	1456	1501	1547	1592	1637	1683	1728	1773	45
959	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226	45
960	982271	2316	2362	2407	2452	2497	2543	2588	2633	2678	45
961	2723	2769	2814	2859	2904	2949	2994	3040	3085	3130	45
962	3175	3220	3265	3310	3356	3401	3446	3491	3536	3581	45
963	3626	3671	3716	3762	3807	3852	3897	3942	3987	4032	45
964	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482	45
965	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932	45
966	4977	5022	5067	5112	5157	5202	5247	5292	5337	5382	45
967	5426	5471	5516	5561	5606	5651	5696	5741	5786	5830	45
968	5875	5920	5965	6010	6055	6100	6144	6189	6234	6279	45
969	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727	45
970	986772	6817	6861	6906	6951	6996	7040	7085	7130	7175	45
971	7219	7264	7309	7353	7398	7443	7488	7532	7577	7622	45
972	7666	7711	7756	7800	7845	7890	7934	7979	8024	8068	45
973	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514	45
974	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960	45
975	9005	9049	9094	9138	9183	9227	9272	9316	9361	9405	45
976	9450	9494	9539	9583	9628	9672	9717	9761	9806	9850	44
977	9895	9939	9983	..28	..72	.117	.161	.206	.250	.294	44
978	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738	44
979	0783	0827	0871	0916	0960	1004	1049	1093	1137	1182	44
980	991226	1270	1315	1359	1403	1448	1492	1536	1580	1625	44
981	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067	44
982	2111	2156	2200	2244	2288	2333	2377	2421	2465	2509	44
983	2554	2598	2642	2686	2730	2774	2819	2863	2907	2951	44
984	2995	3039	3083	3127	3172	3216	3260	3304	3348	3392	44
985	3436	3480	3524	3568	3613	3657	3701	3745	3789	3833	44
986	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273	44
987	4317	4361	4405	4449	4493	4537	4581	4625	4669	4713	44
988	4757	4801	4845	4889	4933	4977	5021	5065	5108	5152	44
989	5196	5240	5284	5328	5372	5416	5460	5504	5547	5591	44
990	995635	5679	5723	5767	5811	5854	5898	5942	5986	6030	44
991	6074	6117	6161	6205	6249	6293	6337	6380	6424	6468	44
992	6512	6555	6599	6643	6687	6731	6774	6818	6862	6906	44
993	6949	6993	7037	7080	7124	7168	7212	7255	7299	7343	44
994	7386	7430	7474	7517	7561	7605	7648	7692	7736	7779	44
995	7823	7867	7910	7954	7998	8041	8085	8129	8172	8216	44
996	8259	8303	8347	8390	8434	8477	8521	8564	8608	8652	44
997	8695	8739	8782	8826	8869	8913	8956	9000	9043	9087	44
998	9131	9174	9218	9261	9305	9348	9392	9435	9479	9522	44
999	9565	9609	9652	9696	9739	9783	9826	9870	9913	9957	44
N.	0	1	2	3	4	5	6	7	8	9	D.

**A TABLE**  
**OF**  
**LOGARITHMIC**  
**SINES AND TANGENTS**  
**FOR EVERY**  
**DEGREE AND MINUTE**  
**OF THE QUADRANT.**

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**N. B** The minutes in the left-hand column of each page, increasing downwards, belong to the degrees at the top; and those increasing upwards, in the right-hand column, belong to the degrees below.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	0.000000		10.000000		0.000000		Infinite	60
1	6.463726	501717	000000	00	6.463726	501717	13.536274	59
2	761756	293485	000000	00	764756	293483	235244	58
3	940847	208231	000000	00	940847	208231	059153	57
4	7.065786	161517	000000	00	7.065786	161517	12.934214	56
5	162696	131968	000000	00	162696	131969	837504	55
6	241877	111575	9.999999	01	241878	111578	758122	54
7	308824	96653	999999	01	308825	96653	691175	53
8	366816	85254	999999	01	366817	85254	633183	52
9	417968	76263	999999	01	417970	76263	582030	51
10	463725	68988	999998	01	463727	68988	536273	50
11	7.505118	62981	9.999998	01	7.505120	62981	12.494880	49
12	542906	57336	999997	01	542909	57333	457091	48
13	577668	53641	999997	01	577672	53642	422328	47
14	609853	49938	999996	01	609857	49939	390143	46
15	639816	46714	999996	01	639820	46715	360180	45
16	667845	43881	999995	01	667849	43882	332151	44
17	691173	41372	999995	01	694179	41373	305821	43
18	718997	39135	999994	01	719003	39136	280997	42
19	742477	37127	999993	01	742484	37128	257516	41
20	764754	35315	999993	01	764761	35316	235239	40
21	7.785943	33672	9.999992	01	7.785951	33673	12.214449	39
22	806146	32175	999991	01	806155	32176	193845	38
23	825451	30805	999990	01	825460	30806	174540	37
24	843934	29547	999989	02	843944	29549	156956	36
25	861662	28388	999988	02	861674	28390	142826	35
26	878595	27317	999988	02	878708	27318	121292	34
27	895085	26323	999987	02	895099	26325	101301	33
28	910879	25399	999986	02	910894	25401	089106	32
29	926119	24538	999985	02	926134	24540	073866	31
30	940842	23733	999983	02	940858	23735	059142	30
31	7.955082	22980	9.999982	02	7.955100	22981	12.044900	29
32	968870	22273	999981	02	968889	22275	031111	28
33	982233	21608	999980	02	982253	21610	017747	27
34	995198	20981	999979	02	995219	20983	004781	26
35	8.007787	20390	999977	02	8.007809	20392	11.992191	25
36	020021	19831	999976	02	020045	19833	979955	24
37	031919	19202	999975	02	031945	19205	968055	23
38	043501	18801	999973	02	043527	18803	956473	22
39	054781	18325	999972	02	054809	18327	945191	21
40	065776	17872	999971	02	065806	17874	934194	20
41	8.076500	17441	9.999969	02	8.076531	17444	11.923469	19
42	086965	17031	999968	02	086997	17034	913303	18
43	097183	16639	999966	02	097217	16642	902783	17
44	107167	16265	999964	03	107202	16268	892797	16
45	116926	15908	999963	03	116963	15910	883037	15
46	126471	15566	999961	03	126510	15568	873490	14
47	135810	15238	999959	03	135851	15241	864149	13
48	144953	14924	999958	03	144996	14927	855004	12
49	153907	14622	999956	03	153952	14627	846048	11
50	162681	14333	999954	03	162727	14336	837273	10
51	8.171280	14054	9.999952	03	8.171328	14057	11.828672	9
52	179713	13786	999950	03	179763	13790	829237	8
53	187985	13529	999948	03	188036	13532	811964	7
54	196102	13280	999946	03	196156	13284	803844	6
55	204070	13041	999944	3	204126	13044	795874	5
56	211895	12810	999942	4	211953	12814	788047	4
57	219581	12587	999940	04	219641	12590	780359	3
58	227134	12372	999938	04	227195	12376	772805	2
59	234557	12164	999936	04	234621	12168	765379	1
60	241855	11963	999934	04	241921	11967	758079	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (1 Degree.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.241855	11963	9.999934	04	8.241921	11967	11.758079	60
1	249033	11768	999932	04	249102	11772	750898	59
2	256094	11580	999929	04	256165	11584	743835	58
3	263042	11398	999927	04	263115	11402	736885	57
4	269881	11221	999925	04	269956	11225	730044	56
5	276614	11050	999922	04	276691	11054	723309	55
6	283242	10883	999920	04	283323	10887	716677	54
7	289773	10721	999918	04	289856	10726	710144	53
8	296207	10565	999915	04	296292	10570	703708	52
9	302516	10413	999913	04	302634	10418	697366	51
10	308794	10266	999910	04	308884	10270	691116	50
11	8.314954	10122	9.999907	04	8.315016	10126	11.684954	49
12	321027	9982	999905	04	321122	9987	678878	48
13	327016	9847	999902	04	327114	9851	672886	47
14	332924	9714	999899	05	333025	9719	666975	46
15	338753	9586	999897	05	338856	9590	661144	45
16	344504	9460	999894	05	344610	9465	655390	44
17	350181	9338	999891	05	350289	9343	649711	43
18	355783	9219	999888	05	355895	9224	644105	42
19	361315	9103	999885	05	361430	9108	638570	41
20	366777	8990	999882	05	366895	8995	633105	40
21	8.372171	8880	9.999879	05	8.372292	8885	11.627708	39
22	377499	8772	999876	05	377622	8777	622378	38
23	382762	8667	999873	05	382889	8672	617111	37
24	387962	8564	999870	05	388092	8570	611908	36
25	393101	8464	999867	05	393234	8470	606766	35
26	398179	8366	999864	05	398315	8371	601685	34
27	403199	8271	999861	05	403338	8276	596662	33
28	408161	8177	999858	05	408304	8182	591696	32
29	413068	8086	999854	05	413213	8091	586787	31
30	417919	7996	999851	06	418068	8002	581932	30
31	8.422717	7909	9.999848	06	8.422869	7914	11.577131	29
32	427462	7823	999844	06	427618	7830	572382	28
33	432156	7740	999841	06	432315	7745	567685	27
34	436800	7657	999838	06	436962	7663	563038	26
35	441394	7577	999834	06	441550	7583	558440	25
36	445941	7499	999831	06	446110	7505	553890	24
37	450440	7422	999827	06	450613	7428	549387	23
38	454893	7346	999823	06	455070	7352	544930	22
39	459301	7273	999820	06	459481	7279	540519	21
40	463665	7200	999816	06	463849	7206	536151	20
41	8.467985	7129	9.999812	06	8.468172	7135	11.531828	19
42	472263	7060	999809	06	472454	7066	527546	18
43	476498	6991	999805	06	476693	6998	523307	17
44	480693	6924	999801	06	480892	6931	519108	16
45	484848	6859	999797	07	485050	6865	514950	15
46	488963	6794	999793	07	489170	6801	510830	14
47	493040	6731	999790	07	493250	6738	506750	13
48	497078	6669	999786	07	497293	6676	502707	12
49	501080	6608	999782	07	501298	6615	498702	11
50	505045	6548	999778	07	505267	6555	494733	10
51	8.508974	6489	9.999774	07	8.509200	6496	11.490800	9
52	512867	6431	999769	07	513098	6439	486902	8
53	516726	6375	999765	07	516961	6382	483039	7
54	520551	6319	999761	07	520790	6326	479210	6
55	524343	6264	999757	07	524586	6272	475414	5
56	528102	6211	999753	07	528349	6218	471651	4
57	531828	6158	999748	07	532080	6165	467920	3
58	535523	6106	999744	07	535779	6113	464221	2
59	539186	6055	999740	07	539447	6062	460553	1
60	542819	6004	999735	07	543084	6012	456916	0
	Cosine		Sine		Cotang.		Tang	M.

88 Degrees  
DD\*

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	8.512819	6004	9.999735	07	8.543084	6012	11.456916	60
1	546422	5955	999731	07	546691	5962	453309	59
2	549395	5906	999726	07	550268	5914	449732	58
3	553539	5858	999722	08	553817	5866	446183	57
4	557054	5811	999717	08	557336	5819	442664	56
5	560540	5765	999713	08	560828	5773	439172	55
6	563999	5719	999708	08	564291	5727	435709	54
7	567431	5674	999704	08	567727	5682	432273	53
8	570836	5630	999699	08	571137	5638	428863	52
9	574214	5587	999694	08	574520	5595	425480	51
10	577566	5544	999689	08	577877	5552	422123	50
11	8.580892	5502	9.999685	08	8.581208	5510	11.418792	49
12	584193	5460	999680	08	584514	5468	415486	48
13	587469	5419	999675	08	587795	5427	412205	47
14	590721	5379	999670	08	591051	5387	408949	46
15	593948	5339	999665	08	594283	5347	405717	45
16	597152	5300	999660	08	597492	5308	402508	44
17	600332	5261	999655	08	600677	5270	399323	43
18	603489	5223	999650	08	603839	5232	396161	42
19	606623	5186	999645	09	606978	5194	393022	41
20	609734	5149	999640	09	610094	5158	389906	40
21	8.612823	5112	9.999635	09	8.613189	5121	11.386811	39
22	615891	5076	999629	09	616262	5085	383738	38
23	618937	5041	999624	09	619313	5050	380687	37
24	621962	5006	999619	09	622343	5015	377657	36
25	624965	4972	999614	09	625352	4981	374648	35
26	627948	4938	999608	09	628340	4947	371660	34
27	630911	4904	999603	09	631308	4913	368692	33
28	633854	4871	999597	09	634256	4880	365744	32
29	636776	4839	999592	09	637184	4848	362816	31
30	639680	4806	999586	09	640093	4816	359907	30
31	8.642563	4775	9.999581	09	8.642982	4784	11.357018	29
32	645428	4743	999575	09	645853	4753	354147	28
33	648274	4712	999570	09	648704	4722	351296	27
34	651102	4682	999564	09	651537	4691	348463	26
35	653911	4652	999558	10	654352	4661	345648	25
36	656702	4622	999553	10	657149	4631	342851	24
37	659475	4592	999547	10	659928	4602	340072	23
38	662230	4563	999541	10	662689	4573	337311	22
39	664968	4535	999535	10	665433	4544	334567	21
40	667689	4506	999529	10	668160	4526	331840	20
41	8.670393	4479	9.999524	10	8.670870	4488	11.329130	19
42	673080	4451	999518	10	673563	4461	326437	18
43	675751	4424	999512	10	676239	4434	323761	17
44	678405	4397	999506	10	678900	4417	321100	16
45	681043	4370	999500	10	681544	4380	318456	15
46	683665	4344	999493	10	684172	4354	315828	14
47	686272	4318	999487	10	686784	4328	313216	13
48	688863	4292	999481	10	689381	4303	310619	12
49	691438	4267	999475	10	691963	4277	308037	11
50	693998	4242	999469	10	694529	4252	305471	10
51	8.696543	4217	9.999463	11	8.697081	4228	11.302919	9
52	699073	4192	999456	11	699617	4203	300383	8
53	701589	4168	999450	11	702139	4179	297861	7
54	704090	4144	999443	11	704646	4155	295354	6
55	706577	4121	999437	11	707140	4132	292860	5
56	709049	4097	999431	11	709618	4108	290382	4
57	711507	4074	999424	11	712083	4085	287917	3
58	713952	4051	999418	11	714534	4062	285465	2
59	716383	4029	999411	11	716972	4040	283028	1
60	718800	4006	999404	11	719396	4017	280604	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (3 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	8.718800	4006	9.999404	11	8.719396	4017	11.280604	60
1	721204	3984	999398	11	721806	3995	278194	60
2	723595	3962	999391	11	724204	3974	275796	68
3	725972	3941	999384	11	726588	3952	273412	57
4	728337	3919	999378	11	728959	3930	271041	56
5	730688	3898	999371	11	731317	3909	268683	55
6	733027	3877	999364	12	733663	3889	266337	54
7	735354	3857	999357	12	735996	3868	264004	53
8	737667	3836	999350	12	738317	3848	261683	52
9	739969	3816	999343	12	740626	3827	259374	51
10	742259	3796	999336	12	742922	3807	257078	50
11	8.744536	3776	9.999329	12	8.745207	3787	11.254793	49
12	746802	3756	999322	12	747479	3768	252521	48
13	749055	3737	999315	12	749740	3749	250260	47
14	751297	3717	999308	12	751989	3729	248011	46
15	753528	3698	999301	12	754227	3710	245773	45
16	755747	3679	999294	12	756453	3692	243547	44
17	757955	3661	999286	12	758668	3673	241332	43
18	760151	3642	999279	12	760872	3655	239128	42
19	762337	3624	999272	12	763065	3636	236935	41
20	764511	3606	999265	12	765246	3618	234754	40
21	8.766675	3588	9.999257	12	8.767417	3600	11.232583	39
22	768828	3570	999250	13	769578	3583	230422	38
23	770970	3553	999242	13	771727	3565	228273	37
24	773101	3535	999235	13	773866	3548	226134	36
25	775223	3518	999227	13	775995	3531	224005	35
26	777333	3501	999220	13	778114	3514	221886	34
27	779434	3484	999212	13	780222	3497	219778	33
28	781524	3467	999205	13	782320	3480	217680	32
29	783605	3451	999197	13	784408	3464	215592	31
30	785675	3434	999189	13	786486	3447	213514	30
31	8.787736	3418	9.999181	13	8.788554	3431	11.211446	29
32	789787	3402	999174	13	790613	3414	209387	28
33	791828	3386	999166	13	792662	3399	207338	27
34	793859	3370	999158	13	794701	3383	205299	26
35	795881	3354	999150	13	796731	3368	203269	25
36	797891	3339	999142	13	798752	3352	201248	24
37	799897	3323	999134	13	800763	3337	199237	23
38	801892	3308	999126	13	802765	3322	197235	22
39	803876	3293	999118	13	804758	3307	195242	21
40	805852	3278	999110	13	806742	3292	193258	20
41	8.807819	3263	9.999102	13	8.808717	3278	11.191283	19
42	809777	3249	999094	14	810683	3262	189317	18
43	811726	3234	999086	14	812641	3248	187359	17
44	813667	3219	999077	14	814589	3233	185411	16
45	815599	3205	999069	14	816529	3219	183471	15
46	817522	3191	999061	14	818461	3205	181539	14
47	819436	3177	999053	14	820384	3191	179616	13
48	821343	3163	999044	14	822298	3177	177702	12
49	823240	3149	999036	14	824205	3163	175795	11
50	825130	3135	999027	14	826103	3150	173897	10
51	8.827011	3122	9.999019	14	8.827992	3136	11.172008	9
52	828884	3108	999010	14	828874	3123	170126	8
53	830749	3095	999002	14	831748	3110	168252	7
54	832607	3082	998993	14	833613	3096	166387	6
55	834456	3069	998984	14	835471	3083	164529	5
56	836297	3056	998976	14	837321	3070	162679	4
57	838130	3043	998967	15	839163	3057	160837	3
58	839956	3030	998958	15	840998	3045	159002	2
59	841774	3017	998950	15	842825	3032	157175	1
60	843585	3000	998941	15	844644	3019	155356	0
	Cosine		Sine		Cotang.		Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	8.843583	3005	9.998941	15	8.844644	3019	11.155356	60
1	845387	2992	998932	15	846455	3007	153545	59
2	847183	2980	998923	15	848260	2995	151740	58
3	848971	2967	998914	15	850057	2982	149943	57
4	850751	2955	998905	15	851846	2970	148154	56
5	852525	2943	998896	15	853628	2958	146372	55
6	854291	2931	998887	15	855403	2946	144597	54
7	856049	2919	998878	15	857171	2935	142829	53
8	857801	2907	998869	15	858932	2923	141068	52
9	859546	2896	998860	15	860686	2911	139314	51
10	861283	2884	998851	15	862433	2900	137567	50
11	8.863014	2873	9.998841	15	8.864173	2888	11.135827	49
12	864738	2861	998832	15	865906	2877	134904	48
13	866455	2850	998823	16	867632	2866	132368	47
14	868165	2839	998813	16	869351	2854	130649	46
15	869868	2828	998804	16	871064	2843	128936	45
16	871565	2817	998795	16	872770	2832	127230	44
17	873255	2806	998785	16	874469	2821	125531	43
18	874938	2795	998776	16	876162	2811	123838	42
19	876615	2786	998766	16	877849	2800	122151	41
20	878285	2773	998757	16	879529	2789	120471	40
21	8.879949	2763	9.998747	16	8.881202	2779	11.118798	39
22	881607	2752	998738	16	882869	2768	117131	38
23	883258	2742	998728	16	884530	2758	115470	37
24	884903	2731	998718	16	886185	2747	113815	36
25	886542	2721	998708	16	887833	2737	112167	35
26	888174	2711	998699	16	889476	2727	110524	34
27	889801	2700	998689	16	891112	2717	108889	33
28	891421	2690	998679	16	892742	2707	107258	32
29	893035	2680	998669	17	894366	2697	105634	31
30	894643	2670	998659	17	895984	2687	104016	30
31	8.896246	2660	9.998649	17	8.897596	2677	11.102404	29
32	897842	2651	998639	17	899203	2667	100797	28
33	899432	2641	998629	17	900803	2658	099197	27
34	901017	2631	998619	17	902398	2648	097692	26
35	902596	2622	998609	17	903987	2638	096013	25
36	904169	2612	998599	17	905570	2629	094430	24
37	905736	2603	998589	17	907147	2620	092853	23
38	907297	2593	998578	17	908719	2610	091281	22
39	908853	2584	998568	17	910285	2601	089715	21
40	910404	2575	998558	17	911846	2592	088154	20
41	8.911949	2566	9.998548	17	8.913401	2583	11.086599	19
42	913488	2556	998537	17	914951	2574	085049	18
43	915022	2547	998527	17	916495	2565	083505	17
44	916550	2538	998516	18	918034	2556	081966	16
45	918073	2529	998506	18	919568	2547	080432	15
46	919591	2520	998495	18	921096	2538	078904	14
47	921103	2512	998485	18	922619	2530	077381	13
48	922610	2503	998474	18	924136	2521	075864	12
49	924112	2494	998464	18	925649	2512	074351	11
50	925609	2486	998453	18	927156	2503	072844	10
51	8.927100	2477	9.998442	18	8.928658	2495	11.071312	9
52	928587	2469	998431	18	930155	2486	069845	8
53	930068	2460	998421	18	931647	2478	068353	7
54	931544	2452	998410	18	933134	2470	066866	6
55	933015	2443	998399	18	934616	2461	065384	5
56	934481	2435	998388	18	936093	2453	063907	4
57	935942	2427	998377	18	937565	2445	062435	3
58	937398	2419	998366	18	939032	2437	060968	2
59	938850	2411	998355	18	940494	2430	059506	1
60	940296	2403	998344	18	941952	2421	058048	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M
0	8.910296	2103	9.998344	19	8.941952	2421	11.058048	60
1	941738	2394	998333	19	943404	2413	056596	59
2	943174	2387	998322	19	944852	2405	055148	58
3	944606	2379	998311	19	946295	2397	053705	57
4	946034	2371	998300	19	947734	2390	052266	56
5	947456	2363	998289	19	949168	2382	050832	55
6	948874	2355	998277	19	950597	2374	049403	54
7	950287	2348	998266	19	952021	2366	047979	53
8	951696	2340	998255	19	953441	2360	046559	52
9	953100	2332	998243	19	954856	2351	045144	51
10	954499	2325	998232	19	956267	2344	043733	50
11	8.955894	2317	9.998220	19	8.957674	2337	11.042326	49
12	957284	2310	998209	19	959075	2329	040925	48
13	958670	2302	998197	19	960473	2323	039527	47
14	960052	2295	998186	19	961866	2314	038134	46
15	961429	2288	998174	19	963255	2307	036745	45
16	962801	2280	998163	19	964639	2300	035361	44
17	964170	2273	998151	19	966019	2293	033981	43
18	965534	2266	998139	20	967394	2286	032606	42
19	966893	2259	998128	20	968766	2279	031234	41
20	968249	2252	998116	20	970133	2271	029867	40
21	8.969600	2244	9.998104	20	8.971496	2265	11.028504	39
22	970947	2238	998092	20	972855	2257	027145	38
23	972289	2231	998080	20	974209	2251	025791	37
24	973628	2224	998068	20	975560	2244	024440	36
25	974962	2217	998056	20	976906	2237	023094	35
26	976293	2210	998044	20	978248	2230	021752	34
27	977619	2203	998032	20	979586	2223	020414	33
28	978941	2197	998020	20	980921	2217	019079	32
29	980259	2190	998008	20	982251	2210	017749	31
30	981573	2183	997996	20	983577	2204	016423	30
31	8.982883	2177	9.997984	20	8.984899	2197	11.015101	29
32	984189	2170	997972	20	986217	2191	013783	28
33	985491	2163	997959	20	987532	2184	012468	27
34	986789	2157	997947	20	988842	2178	011158	26
35	988083	2150	997935	21	990149	2171	009851	25
36	989371	2144	997922	21	991451	2165	008549	24
37	990660	2138	997910	21	992750	2158	007250	23
38	991943	2131	997897	21	994045	2152	005955	22
39	993222	2125	997885	21	995337	2146	004663	21
40	994497	2119	997872	21	996624	2140	003376	20
41	8.995768	2112	9.997860	21	8.997908	2134	11.002092	19
42	997036	2106	997847	21	999188	2127	000812	18
43	998299	2100	997835	21	9.000465	2121	10.999535	17
44	999560	2094	997822	21	001738	2115	998262	16
45	9.000816	2087	997809	21	003007	2109	996993	15
46	002069	2082	997797	21	004272	2103	995728	14
47	003318	2076	997784	21	005534	2097	994466	13
48	004563	2070	997771	21	006792	2091	993203	12
49	005805	2064	997758	21	008047	2085	991953	11
50	007044	2058	997745	21	009298	2080	990702	10
51	9.008278	2052	9.997732	21	9.010546	2074	10.989454	9
52	009510	2046	997719	21	011790	2068	988210	8
53	010737	2040	997706	21	013031	2062	986969	7
54	011962	2034	997693	22	014268	2056	985732	6
55	013182	2029	997680	22	015502	2051	984498	5
56	014400	2023	997667	22	016732	2045	983268	4
57	015613	2017	997654	22	017959	2040	982041	3
58	016824	2012	997641	22	019183	2033	980817	2
59	018031	2006	997628	22	020403	2028	979597	1
60	019235	2000	997614	22	021620	2023	978380	0
	Cosine		Sine		Cotang.		Tang.	M

84Degrees.

24 (6 Degrees.) A TABLE OF LOGARITHMIC

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.019235	2000	9.997614	22	9.021620	2023	10.978380	60
1	020435	1995	997601	22	022834	2017	977166	59
2	021632	1989	997588	22	024044	2011	975956	58
3	022825	1984	997574	22	025251	2006	974749	57
4	024016	1978	997561	22	026455	2000	973545	56
5	025203	1973	997547	22	027655	1995	972345	55
6	026386	1967	997534	23	028852	1990	971148	54
7	027567	1962	997520	23	030046	1985	969954	53
8	028744	1957	997507	23	031237	1979	968763	52
9	029918	1951	997493	23	032425	1974	967575	51
10	031089	1947	997480	23	033609	1969	966391	50
11	9.032257	1941	9.997466	23	9.034791	1964	10.965209	49
12	033421	1936	997452	23	035969	1958	964031	48
13	034582	1930	997439	23	037144	1953	962856	47
14	035741	1925	997425	23	038316	1948	961684	46
15	036896	1920	997411	23	039485	1943	960515	45
16	038048	1915	997397	23	040651	1938	959349	44
17	039197	1910	997383	23	041813	1933	958187	43
18	040342	1905	997369	23	042973	1928	957027	42
19	041485	1899	997355	23	044130	1923	955870	41
20	042625	1894	997341	23	045284	1918	954716	40
21	9.043762	1889	9.997327	24	9.046434	1913	10.953566	39
22	044895	1884	997313	24	047582	1908	952418	38
23	046026	1879	997299	24	048727	1903	951273	37
24	047154	1875	997285	24	049869	1898	950131	36
25	048279	1870	997271	24	051008	1893	948992	35
26	049400	1865	997257	24	052144	1889	947856	34
27	050519	1860	997242	24	053277	1884	946723	33
28	051635	1855	997228	24	054407	1879	945593	32
29	052749	1850	997214	24	055535	1874	944465	31
30	053859	1845	997199	24	056659	1870	943341	30
31	054966	1841	9.997185	24	9.057781	1865	10.942219	29
32	056071	1836	997170	24	058900	1869	941100	28
33	057172	1831	997156	24	060016	1855	939984	27
34	058271	1827	997141	24	061130	1851	938870	26
35	059367	1822	997127	24	062240	1846	937760	25
36	060460	1817	997112	24	063348	1842	936652	24
37	061551	1813	997098	24	064453	1837	935547	23
38	062639	1808	997083	25	065556	1833	934444	22
39	063724	1804	997068	25	066655	1828	933345	21
40	064806	1799	997053	25	067752	1824	932248	20
41	9.065885	1794	9.997039	25	9.068846	1819	10.931154	19
42	066962	1790	997024	25	069938	1815	930062	18
43	068036	1786	997009	25	071027	1810	928973	17
44	069107	1781	996994	25	072113	1806	927887	16
45	070176	1777	996979	25	073197	1802	926803	15
46	071242	1772	996964	25	074278	1797	925722	14
47	072306	1768	996949	25	075356	1793	924644	13
48	073366	1763	996934	25	076432	1789	923568	12
49	074424	1759	996919	25	077505	1784	922495	11
50	075480	1755	996904	25	078576	1780	921424	10
51	9.076533	1750	9.996889	25	9.079644	1776	10.920356	9
52	077583	1746	996874	25	080710	1772	919290	8
53	078631	1742	996858	25	081773	1767	918227	7
54	079676	1738	996843	25	082833	1763	917167	6
55	080719	1733	996828	25	083891	1759	916109	5
56	081759	1729	996812	26	084947	1755	915053	4
57	082797	1725	996797	26	086000	1751	914000	3
58	083832	1721	996782	26	087050	1747	912950	2
59	084864	1717	996766	26	088098	1743	911902	1
60	085894	1713	996751	26	089144	1738	910856	0
	Cosine		Sine		Co. ang.		Tang.	M.

63 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.085894	1713	9.996751	26	9.089144	1738	10.910856	60
1	086922	1709	996735	26	090187	1734	909813	59
2	087947	1704	996720	26	091228	1730	908772	58
3	088970	1700	996704	26	092266	1727	907734	57
4	089990	1696	996688	26	093302	1722	906698	56
5	091008	1692	996673	26	094336	1719	905664	55
6	092024	1688	996657	26	095367	1715	904633	54
7	093037	1684	996641	26	096395	1711	903605	53
8	094047	1680	996625	26	097422	1707	992578	52
9	095056	1676	996610	26	098446	1703	991554	51
10	096062	1673	996594	26	099468	1699	990532	50
11	9.097065	1668	9.996578	27	9.100487	1695	10.899513	49
12	098066	1665	996562	27	101504	1691	898496	48
13	099065	1661	996546	27	102519	1687	897481	47
14	100062	1657	996530	27	103532	1684	896468	46
15	101056	1653	996514	27	104542	1680	895458	45
16	102048	1649	996498	27	105550	1676	894450	44
17	103037	1645	996482	27	106556	1672	893444	43
18	104025	1641	996465	27	107559	1669	892441	42
19	105010	1638	996449	27	108560	1665	891440	41
20	105992	1634	996433	27	109559	1661	890441	40
21	9.106973	1630	9.996417	27	9.110556	1658	10.889444	39
22	107951	1627	996400	27	111551	1654	888449	38
23	108927	1623	996384	27	112543	1650	887457	37
24	109901	1619	996368	27	113533	1646	886467	36
25	110873	1616	996351	27	114521	1643	885479	35
26	111842	1612	996335	27	115507	1639	884493	34
27	112809	1608	996318	27	116491	1636	883509	33
28	113774	1605	996302	28	117472	1632	882528	32
29	114737	1601	996285	28	118452	1629	881548	31
30	115698	1597	996269	28	119429	1625	880571	30
31	9.116656	1594	9.996252	28	9.120404	1622	10.879596	29
32	117613	1590	996235	28	121377	1618	878623	28
33	118567	1587	996219	28	122348	1615	877652	27
34	119519	1583	996202	28	123317	1611	876683	26
35	120469	1580	996185	28	124284	1607	875716	25
36	121417	1576	996168	28	125249	1604	874751	24
37	122362	1573	996151	28	126211	1601	873789	23
38	123306	1569	996134	28	127172	1597	872828	22
39	124248	1566	996117	28	128130	1594	871870	21
40	125187	1562	996100	28	129087	1591	870913	20
41	9.126125	1559	9.996083	29	9.130041	1587	10.869959	19
42	127060	1556	996066	29	130994	1584	869006	18
43	127993	1552	996049	29	131944	1581	868056	17
44	128925	1549	996032	29	132893	1577	867107	16
45	129854	1545	996015	29	133839	1574	866161	15
46	130781	1542	995998	29	134784	1571	865216	14
47	131706	1539	995980	29	135726	1567	864274	13
48	132639	1535	995963	29	136667	1564	863333	12
49	133551	1532	995946	29	137605	1561	862395	11
50	134470	1529	995928	29	138542	1558	861458	10
51	9.135387	1525	9.995911	29	9.139476	1555	10.860524	9
52	136303	1522	995894	29	140409	1551	859591	8
53	137216	1519	995876	29	141340	1548	858666	7
54	138128	1516	995859	29	142269	1545	857731	6
55	139037	1512	995841	29	143196	1542	856804	5
56	139944	1509	995823	29	144121	1539	855879	4
57	140850	1506	995806	29	145044	1535	854956	3
58	141754	1503	995788	29	145966	1532	854034	2
59	142655	1500	995771	29	146885	1529	853115	1
60	143555	1496	995753	29	147803	1526	852197	0
	Cosine		Sine		Tang.		Cotang.	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.143555	1496	9.995753	30	9.147803	1526	10.852197	60
1	144453	1493	995735	30	148718	1523	851282	59
2	145319	1490	995717	30	149632	1520	850368	58
3	146243	1487	995699	30	150544	1517		
4	147136	1484	995681	30	151454	1514	848246	56
5	148026	1481	995664	30	152363	1511	847637	55
6	148915	1478	995646	30	153269	1508	846731	54
7	149802	1475	995628	30	154174	1505	845826	53
8	150686	1472	995610	30	155077	1502	844923	52
9	151569	1469	995591	30	155978	1499	844022	21
10	152451	1466	995573	30	156877	1496	843123	50
11	9.153330	1463	9.995555	30	9.157775	1493	10.842225	49
12	154208	1460	995537	30	158671	1490	841329	48
13	155083	1457	995519	30	159565	1487	840435	47
14	155957	1454	995501	31	160457	1484	839543	46
15	156830	1451	995482	31	161347	1481	838653	45
16	157700	1448	995464	31	162236	1479	837764	44
17	158569	1445	995446	31	163123	1476	836877	43
18	159435	1442	995427	31	164008	1473	835992	42
19	160301	1439	995409	31	164892	1470	835108	41
20	161164	1436	995390	31	165774	1467	834226	40
21	9.162025	1433	9.995372	31	9.166654	1464	10.833346	39
22	162885	1430	995353	31	167532	1461	832468	38
23	163743	1427	995334	31	168409	1458	831591	37
24	164600	1424	995316	31	169284	1455	830716	36
25	165454	1422	995297	31	170157	1453	829843	35
26	166307	1419	995278	31	171029	1450	828971	34
27	167159	1416	995260	31	171899	1447	828101	33
28	168008	1413	995241	32	172767	1444	827233	32
29	168856	1410	995222	32	173634	1442	826366	31
30	169702	1407	995203	32	174499	1439	825501	30
31	9.170547	1405	9.995184	32	9.175362	1436	10.824638	29
32	171389	1402	995165	32	176224	1433	823776	28
33	172230	1399	995146	32	177084	1431	822916	27
34	173070	1396	995127	32	177942	1428	822058	26
35	173908	1394	995108	32	178799	1425	821201	25
36	174744	1391	995089	32	179655	1423	820345	24
37	175578	1388	995070	32	180508	1420	819492	23
38	176411	1386	995051	32	181360	1417	818640	22
39	177242	1383	995032	32	182211	1415	817789	21
40	178072	1380	995013	32	183059	1412	816941	20
41	9.178900	1377	9.994993	32	9.183907	1409	10.816093	19
42	179726	1374	994974	32	184752	1407	815248	18
43	180551	1372	994955	32	185597	1404	814403	17
44	181374	1369	994935	32	186439	1402	813561	16
45	182196	1366	994916	33	187280	1399	812720	15
46	183016	1364	994896	33	188120	1396	811880	14
47	183834	1361	994877	33	188958	1393	811042	13
48	184651	1359	994857	33	189794	1391	810206	12
49	185466	1356	994838	33	190629	1389	809371	11
50	186280	1353	994818	33	191462	1386	808538	10
51	9.187092	1351	9.994798	33	9.192291	1384	10.807766	9
52	187903	1348	994779	33	193124	1381	806937	8
53	188712	1346	994759	33	193953	1379	806097	7
54	189519	1343	994739	33	194780	1376	805250	6
55	190325	1341	994719	33	195606	1374	804394	5
56	191130	1338	994700	33	196430	1371	803574	4
57	191933	1336	994680	33	197253	1369	802747	3
58	192734	1333	994660	33	198074	1366	801926	2
59	193534	1330	994640	33	198894	1364	801106	1
60	194332	1328	994620	33	199713	1361	800287	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.134332	1328	9.994620	33	9.199713	1361	10.800287	60
1	195129	1326	994600	33	200529	1359	799471	59
2	195925	1323	994580	33	201345	1356	798655	58
3	196719	1321	994560	34	202159	1354	797841	57
4	197511	1318	994540	34	202971	1352	797029	56
5	198302	1316	994519	34	203782	1349	796218	55
6	199091	1313	994499	34	204592	1347	795408	54
7	199879	1311	994479	34	205400	1345	794600	53
8	200666	1308	994459	34	206207	1342	793793	52
9	201451	1306	994438	34	207013	1340	792987	51
10	202234	1304	994418	34	207817	1338	792183	50
11	9.203017	1301	9.994397	34	9.208619	1335	10.791331	49
12	203797	1299	994377	34	209420	1333	790580	48
13	204577	1296	994357	34	210220	1331	789780	47
14	205354	1294	994336	34	211018	1328	788982	46
15	206131	1292	994316	34	211815	1326	788185	45
16	206906	1289	994295	34	212611	1324	787389	44
17	207679	1287	994274	35	213405	1321	786595	43
18	208452	1285	994254	35	214198	1319	785802	42
19	209222	1282	994233	35	214989	1317	785011	41
20	209992	1280	994212	35	215780	1315	784220	40
21	9.210760	1278	9.994191	35	9.216568	1312	10.783432	39
22	211526	1275	994171	35	217356	1310	782644	38
23	212291	1273	994150	35	218142	1308	781858	37
24	213055	1271	994129	35	218926	1305	781074	36
25	213818	1268	994108	35	219710	1303	780290	35
26	214579	1266	994087	35	220492	1301	779508	34
27	215338	1264	994066	35	221272	1299	778728	33
28	216097	1261	994045	35	222052	1297	777948	32
29	216854	1259	994024	35	222830	1294	777170	31
30	217609	1257	994003	35	223606	1292	776394	30
31	9.218363	1255	9.993981	35	9.224382	1290	10.775618	29
32	219116	1253	993960	35	225156	1288	774844	28
33	219868	1250	993939	35	225929	1286	774071	27
34	220618	1248	993918	35	226700	1284	773300	26
35	221367	1246	993896	36	227471	1281	772529	25
36	222115	1244	993875	36	228239	1279	771761	24
37	222861	1242	993854	36	229007	1277	770993	23
38	223606	1239	993832	36	229773	1275	770227	22
39	224345	1237	993811	36	230539	1273	769461	21
40	225092	1235	993789	36	231302	1271	768698	20
41	9.225833	1233	9.993768	36	9.232065	1269	10.767935	19
42	226573	1231	993746	36	232826	1267	767174	18
43	227311	1228	993725	36	233586	1265	766414	17
44	228048	1226	993703	36	234345	1262	765655	16
45	228784	1224	993681	36	235103	1260	764897	15
46	229518	1222	993660	36	235859	1258	764141	14
47	230252	1220	993638	36	236614	1256	763386	13
48	230984	1218	993616	36	237368	1254	762632	12
49	231714	1216	993594	37	238120	1252	761880	11
50	232444	1214	993572	37	238872	1250	761128	10
51	9.233172	1212	9.993550	37	9.239622	1248	10.760378	9
52	233899	1209	993528	37	240371	1246	759620	8
53	234625	1207	993506	37	241118	1244	758882	7
54	235349	1205	993484	37	241865	1242	758135	6
55	236073	1203	993462	37	242610	1240	757390	5
56	236795	1201	993440	37	243354	1238	756646	4
57	237515	1199	993418	37	244097	1236	755903	3
58	238235	1197	993396	37	244839	1234	755161	2
59	238953	1195	993374	37	245579	1232	754421	1
60	239670	1193	993351	37	246319	1230	753681	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.143555	1496	9.995753	30	9.147803	1526	10.852197	60
1	144453	1493	995735	30	148718	1523	851282	59
2	145349	1490	995717	30	149632	1520	850368	58
3	146243	1487	995699	30	150544	1517		
4	147136	1484	995681	30	151454	1514	848546	56
5	148026	1481	995664	30	152363	1511	847637	55
6	148915	1478	995646	30	153269	1508	846731	54
7	149802	1475	995628	30	154174	1505	845826	53
8	150686	1472	995610	30	155077	1502	844923	52
9	151569	1469	995591	30	155978	1499	844022	21
10	152451	1466	995573	30	156877	1496	843123	50
11	9.153330	1463	9.995555	30	9.157775	1493	10.842225	49
12	154208	1460	995537	30	158671	1490	841329	48
13	155083	1457	995519	30	159565	1487	840435	47
14	155957	1454	995501	31	160457	1484	839543	46
15	156830	1451	995482	31	161347	1481	838653	45
16	157700	1448	995464	31	162236	1479	837764	44
17	158569	1445	995446	31	163123	1476	836877	43
18	159435	1442	995427	31	164008	1473	835992	42
19	160301	1439	995409	31	164892	1470	835108	41
20	161164	1436	995390	31	165774	1467	834226	40
21	9.162025	1433	9.995372	31	9.166654	1464	10.833346	39
22	162885	1430	995353	31	167532	1461	832468	38
23	163743	1427	995334	31	168409	1458	831591	37
24	164600	1424	995316	31	169284	1455	830716	36
25	165454	1422	995297	31	170157	1453	829843	35
26	166307	1419	995278	31	171029	1450	828971	34
27	167159	1416	995260	31	171899	1447	828101	33
28	168008	1413	995241	32	172767	1444	827233	32
29	168856	1410	995222	32	173634	1442	826366	31
30	169702	1407	995203	32	174499	1439	825501	30
31	9.170547	1405	9.995184	32	9.175362	1436	10.824638	29
32	171389	1402	995165	32	176224	1433	823776	28
33	172230	1399	995146	32	177084	1431	822916	27
34	173070	1396	995127	32	177942	1428	822058	26
35	173908	1394	995108	32	178799	1425	821201	25
36	174744	1391	995089	32	179655	1423	820345	24
37	175578	1388	995070	32	180508	1420	819492	23
38	176411	1386	995051	32	181360	1417	818640	22
39	177242	1383	995032	32	182211	1415	817789	21
40	178072	1380	995013	32	183059	1412	816941	20
41	9.178900	1377	9.994993	32	9.183907	1409	10.816093	19
42	179726	1374	994974	32	184752	1407	815248	18
43	180551	1372	994955	32	185597	1404	814403	17
44	181374	1369	994935	32	186439	1402	813561	16
45	182196	1366	994916	33	187280	1399	812720	15
46	183016	1364	994896	33	188120	1396	811880	14
47	183834	1361	994877	33	188958	1393	811042	13
48	184651	1359	994857	33	189794	1391	810206	12
49	185466	1356	994838	33	190629	1389	809371	11
50	186280	1353	994818	33	191462	1386	808538	10
51	9.187092	1351	9.994798	33	9.192294	1384	10.807706	9
52	187903	1348	994779	33	193124	1381	806876	8
53	188712	1346	994759	33	193953	1379	806047	7
54	189519	1343	994739	33	194780	1376	805220	6
55	190325	1341	994719	33	195606	1374	804394	5
56	191130	1338	994700	33	196430	1371	803570	4
57	191933	1336	994680	33	197253	1369	802747	3
58	192734	1333	994660	33	198074	1366	801926	2
59	193534	1330	994640	33	198894	1364	801106	1
60	194332	1328	994620	33	199713	1361	800287	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.194332	1328	9.994620	33	9.199713	1361	10.800287	60
1	195129	1326	994600	33	200529	1359	799471	59
2	195925	1323	994580	33	201345	1356	798655	58
3	196719	1321	994560	34	202159	1354	797841	57
4	197511	1318	994540	34	202971	1352	797029	56
5	198302	1316	994519	34	203782	1349	796218	55
6	199091	1313	994499	34	204592	1347	795408	54
7	199879	1311	994479	34	205400	1345	794600	53
8	200666	1308	994459	34	206207	1342	793793	52
9	201451	1306	994438	34	207013	1340	792987	51
10	202234	1304	994418	34	207817	1338	792183	50
11	9.203017	1301	9.994397	34	9.208619	1335	10.791381	49
12	203797	1299	994377	34	209420	1333	790580	48
13	204577	1296	994357	34	210220	1331	789780	47
14	205354	1294	994336	34	211018	1328	788982	46
15	206131	1292	994316	34	211815	1326	788185	45
16	206906	1289	994295	34	212611	1324	787389	44
17	207679	1287	994274	35	213405	1321	786595	43
18	208452	1285	994254	35	214198	1319	785802	42
19	209222	1282	994233	35	214989	1317	785011	41
20	209992	1280	994212	35	215780	1315	784220	40
21	9.210760	1278	9.994191	35	9.216568	1312	10.783432	39
22	211526	1275	994171	35	217356	1310	782644	38
23	212291	1273	994150	35	218142	1308	781858	37
24	213055	1271	994129	35	218926	1305	781074	36
25	213818	1268	994108	35	219710	1303	780290	35
26	214579	1266	994087	35	220492	1301	779508	34
27	215338	1264	994066	35	221272	1299	778728	33
28	216097	1261	994045	35	222052	1297	777948	32
29	216854	1259	994024	35	222830	1294	777170	31
30	217609	1257	994003	35	223606	1292	776394	30
31	9.218363	1255	9.993981	35	9.224382	1290	10.775618	29
32	219116	1253	993960	35	225156	1288	774844	28
33	219868	1250	993939	35	225929	1286	774071	27
34	220618	1248	993918	35	226700	1284	773300	26
35	221367	1246	993896	36	227471	1281	772529	25
36	222115	1244	993875	36	228239	1279	771761	24
37	222861	1242	993854	36	229007	1277	770993	23
38	223606	1239	993832	36	229773	1275	770227	22
39	224349	1237	993811	36	230539	1273	769461	21
40	225092	1235	993789	36	231302	1271	768698	20
41	9.225833	1233	9.993768	36	9.232065	1269	10.767935	19
42	226573	1231	993746	36	232826	1267	767174	18
43	227311	1228	993725	36	233586	1265	766414	17
44	228048	1226	993703	36	234345	1262	765655	16
45	228784	1224	993681	36	235103	1260	764897	15
46	229518	1222	993660	36	235859	1258	764141	14
47	230252	1220	993638	36	236614	1256	763386	13
48	230984	1218	993616	36	237368	1254	762632	12
49	231714	1216	993594	37	238120	1252	761880	11
50	232444	1214	993572	37	238872	1250	761128	10
51	9.233172	1212	9.993550	37	9.239622	1248	10.760378	9
52	233899	1209	993528	37	240371	1246	759620	8
53	234625	1207	993506	37	241118	1244	758862	7
54	235349	1205	993484	37	241865	1242	758135	6
55	236073	1203	993462	37	242610	1240	757390	5
56	236795	1201	993440	37	243354	1238	756646	4
57	237515	1199	993418	37	244097	1236	755903	3
58	238235	1197	993396	37	244839	1234	755161	2
59	238959	1195	993374	37	245579	1232	754421	1
60	239670	1193	993351	37	246319	1230	753681	0
	Cosine		Sine		Cotang.		Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.239670	1193	9.993351	37	9.246319	1230	10.753681	60
1	240386	1191	993329	37	247057	1228	752943	59
2	241101	1189	993307	37	247794	1226	752206	58
3	241814	1187	993285	37	248530	1224	751470	57
4	242526	1185	993262	37	249264	1222	750736	56
5	243237	1183	993240	37	249998	1220	750002	55
6	243947	1181	993217	38	250730	1218	749270	54
7	244656	1179	993195	38	251461	1217	748539	53
8	245363	1177	993172	38	252191	1215	747809	52
9	246069	1175	993149	38	252920	1213	747080	51
10	246775	1173	993127	38	253648	1211	746352	50
11	9.247478	1171	9.993104	38	9.254374	1209	10.745626	49
12	248181	1169	993081	38	255100	1207	744900	48
13	248883	1.67	993059	38	255824	1205	744176	47
14	249583	1165	993036	38	256547	1203	743453	46
15	250282	1163	993013	38	257269	1201	742731	45
16	250980	1161	992990	38	257990	1200	742010	44
17	251677	1159	992967	38	258710	1198	741290	43
18	252373	1158	992944	38	259429	1196	740571	42
19	253067	1156	992921	38	260146	1194	739854	41
20	253761	1154	992898	38	260863	1192	739137	40
21	9.254453	1152	9.992875	38	9.261578	1190	10.738422	39
22	255144	1150	992852	38	262292	1189	737708	38
23	255834	1148	992829	39	263005	1187	736995	37
24	256523	1146	992806	39	263717	1185	736283	36
25	257211	1144	992783	39	264428	1183	735572	35
26	257898	1142	992759	39	265138	1181	734862	34
27	258583	1141	992736	39	265847	1179	734153	33
28	259268	1139	992713	39	266555	1178	733445	32
29	259951	1137	992690	39	267261	1176	732739	31
30	260633	1135	992666	39	267967	1174	732033	30
31	9.261314	1133	9.992643	39	9.268671	1172	10.731329	29
32	261994	1131	992619	39	269375	1170	730625	28
33	262673	1130	992596	39	270077	1169	729923	27
34	263351	1128	992572	39	270779	1167	729221	26
35	264027	1126	992549	39	271479	1165	728521	25
36	264703	1124	992525	39	272178	1164	727822	24
37	265377	1122	992501	39	272876	1162	727124	23
38	266051	1120	992478	40	273573	1160	726427	22
39	266723	1119	992454	40	274269	1158	725731	21
40	267395	1117	992430	40	274964	1157	725036	20
41	9.268065	1115	9.992406	40	9.275658	1155	10.724342	19
42	268734	1113	992382	40	276351	1153	723649	18
43	269402	1111	992359	40	277043	1151	722957	17
44	270069	1110	992335	40	277734	1150	722266	16
45	270735	1108	992311	40	278424	1148	721576	15
46	271400	1106	992287	40	279113	1147	720887	14
47	272064	1105	992263	40	279801	1145	720199	13
48	272728	1103	992239	40	280488	1143	719512	12
49	273388	1101	992214	40	281174	1141	718826	11
50	274049	1099	992190	40	281858	1140	718142	10
51	9.274708	1098	9.992166	40	9.282542	1138	10.717458	9
52	275367	1096	992142	40	283225	1136	716775	8
53	276024	1094	992117	41	283907	1135	716093	7
54	276681	1092	992093	41	284588	1133	715412	6
55	277337	1091	992069	41	285268	1131	714732	5
56	277991	1089	992044	41	285947	1130	714053	4
57	278644	1087	992020	41	286624	1128	713376	3
58	279297	1086	991996	41	287301	1126	712699	2
59	279948	1084	991971	41	287977	1125	712023	1
60	280599	1082	991947	41	288652	1123	711348	0

Cosine	Sine	Cotang.	Tang.	M.
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97 Degrees.

SINES AND TANGENTS. (11 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.280599	1082	9.991947	41	9.288652	1123	10.711348	60
1	281248	1081	991922	41	289326	1122	710674	59
2	281897	1079	991897	41	289999	1120	710001	58
3	282544	1077	991873	41	290671	1118	709329	57
4	283190	1076	991848	41	291342	1117	708658	56
5	283836	1074	991823	41	292013	1115	707987	55
6	284480	1072	991799	41	292682	1114	707318	54
7	285124	1071	991774	42	293350	1112	706650	53
8	285766	1069	991749	42	294017	1111	705983	52
9	286408	1067	991724	42	294684	1109	705316	51
10	287048	1066	991699	42	295349	1107	704651	50
11	9.287687	1064	9.991674	42	9.296013	1106	10.703987	49
12	288326	1063	991649	42	296677	1104	703323	48
13	288964	1061	991624	42	297339	1103	702661	47
14	289600	1059	991599	42	298001	1101	701999	46
15	290236	1058	991574	42	298662	1100	701338	45
16	290870	1056	991549	42	299322	1098	700678	44
17	291504	1054	991524	42	299980	1096	700020	43
18	292137	1053	991498	42	300633	1095	699362	42
19	292768	1051	991473	42	301295	1093	698705	41
20	293399	1050	991448	42	301951	1092	698049	40
21	9.293329	1048	9.991422	42	9.302507	1090	10.697393	39
22	294058	1046	991397	42	303261	1089	696739	38
23	294686	1045	991372	43	303914	1087	696085	37
24	295313	1043	991346	43	304567	1086	695433	36
25	295939	1042	991321	43	305218	1084	694782	35
26	296564	1040	991295	43	305869	1083	694131	34
27	297188	1039	991270	43	306519	1081	693481	33
28	297812	1037	991244	43	307165	1080	692832	32
29	298434	1036	991218	43	307815	1078	692185	31
30	299055	1034	991193	43	308463	1077	691537	30
31	9.309276	1032	9.991167	43	9.309109	1075	10.690891	29
32	300895	1031	991141	43	309754	1074	690246	28
33	301514	1029	991115	43	310398	1073	689602	27
34	302132	1028	991090	43	311042	1071	688958	26
35	302748	1026	991064	43	311685	1070	688315	25
36	303364	1025	991038	43	312327	1068	687673	24
37	303979	1023	991012	43	312967	1067	687033	23
38	304593	1022	990986	43	313605	1065	686392	22
39	305207	1020	990960	43	314241	1064	685753	21
40	305819	1019	990934	44	314885	1062	685115	20
41	9.305135	1017	9.990908	44	9.315521	1061	10.683177	19
42	307011	1016	990882	44	316159	1060	683841	18
43	307630	1014	990855	44	316795	1058	683205	17
44	308259	1013	990829	44	317430	1057	682570	16
45	308867	1011	990803	44	318064	1055	681936	15
46	309474	1010	990777	44	318697	1054	681303	14
47	310080	1008	990750	44	319329	1053	680671	13
48	310685	1007	990724	44	319961	1051	680039	12
49	311289	1005	990697	44	320592	1050	679408	11
50	311893	1004	990671	44	321222	1048	678778	10
51	9.312495	1003	9.990644	44	9.321851	1047	10.678149	9
52	313097	1001	990618	44	322479	1045	677521	8
53	313698	1000	990591	44	323106	1044	676894	7
54	314297	998	990565	44	323733	1043	676267	6
55	314897	997	990538	44	324358	1041	675642	5
56	315495	996	990511	45	324983	1040	675017	4
57	316092	994	990485	45	325607	1039	674393	3
58	316689	993	990458	45	326231	1037	673769	2
59	317284	991	990431	45	326853	1036	673147	1
60	317879	990	990404	45	327475	1035	672525	0
	Cosine		Sine		Cotang.		Tang.	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.317879	990	9.590404	45	9.327474	1035	10.672526	60
1	318473	988	990278	45	328095	1033	671905	59
2	319066	987	990351	45	328715	1032	671285	58
3	319658	986	990324	45	329334	1030	670666	57
4	320249	984	990297	45	329953	1029	670047	56
5	320840	983	990270	45	330570	1028	669430	55
6	321430	982	990243	45	331187	1026	668813	54
7	322019	980	990215	45	331803	1025	668197	53
8	322607	979	990188	45	332418	1024	667582	52
9	323194	977	990161	45	333033	1023	666967	51
10	323780	976	990134	45	333646	1021	666354	50
11	9.324366	975	9.990107	46	9.334259	1020	10.665741	49
12	324950	973	990079	46	334871	1019	665129	48
13	325534	972	990052	46	335482	1017	664518	47
14	326117	970	990025	46	336093	1016	663907	46
15	326700	969	989997	46	336702	1015	663298	45
16	327281	968	989970	46	337311	1013	662689	44
17	327862	966	989942	46	337919	1012	662081	43
18	328442	965	989915	46	338527	1011	661473	42
19	329021	964	989887	46	339133	1010	660867	41
20	329599	962	989860	46	339739	1008	660261	40
21	9.330176	961	9.989832	46	9.340344	1007	10.659656	39
22	330753	960	989804	46	340948	1006	659052	38
23	331329	958	989777	46	341552	1004	658448	37
24	331903	957	989749	47	342155	1003	657845	36
25	332478	956	989721	47	342757	1002	657243	35
26	333051	954	989693	47	343358	1000	656642	34
27	333624	953	989665	47	343958	999	656042	33
28	334195	952	989637	47	344558	998	655442	32
29	334766	950	989609	47	345157	997	654843	31
30	335337	949	989582	47	345755	996	654245	30
31	9.335906	948	9.989553	47	9.346353	994	10.653647	29
32	336475	946	989525	47	346949	993	653051	28
33	337043	945	989497	47	347545	992	652455	27
34	337610	944	989469	47	348141	991	651859	26
35	338176	943	989441	47	348735	990	651265	25
36	338742	941	989413	47	349329	988	650671	24
37	339306	940	989384	47	349922	987	650078	23
38	339871	939	989356	47	350514	986	649486	22
39	340434	937	989328	47	351106	985	648894	21
40	340996	936	989300	47	351697	983	648303	20
41	9.341558	935	9.989271	47	9.352287	982	10.647713	19
42	342119	934	989243	47	352876	981	647124	18
43	342679	932	989214	47	353465	980	646535	17
44	343239	931	989186	47	354053	979	645947	16
45	343797	930	989157	47	354640	977	645360	15
46	344355	929	989128	48	355227	976	644773	14
47	344912	927	989100	48	355813	975	644187	13
48	345469	926	989071	48	356398	974	643602	12
49	346024	925	989042	48	356982	973	643018	11
50	346579	924	989014	48	357566	971	642434	10
51	9.347134	922	9.988985	48	9.358149	970	10.641851	9
52	347687	921	988956	48	358731	969	641269	8
53	348240	920	988927	48	359313	968	640687	7
54	348792	919	988898	48	359893	967	640107	6
55	349343	917	988869	48	360474	966	639526	5
56	349893	916	988840	48	361053	965	638947	4
57	350443	915	988811	49	361632	963	638368	3
58	350992	914	988782	49	362210	962	637790	2
59	351540	913	988753	49	362787	961	637213	1
60	352088	911	988724	49	363364	960	636636	0
	Cosine		Sine		Cotang.		Tang	M.

SINES AND TANGENTS. (13 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.352088	911	9.989724	49	9.363364	960	10.636636	60
1	352635	910	988695	49	363940	959	636060	59
2	353181	909	988666	49	364515	958	635485	58
3	353726	908	988636	49	365090	957	634910	57
4	354271	907	988607	49	365664	955	634336	56
5	354815	905	988578	49	366237	954	633763	55
6	355358	904	988548	49	366810	953	633190	54
7	355901	903	988519	49	367382	952	632618	53
8	356443	902	988489	49	367953	951	632047	52
9	356984	901	988460	49	368524	950	631476	51
10	357524	899	988430	49	369094	949	630906	50
11	9.358064	898	9.988401	49	9.369663	948	10.630337	49
12	358603	897	988371	49	370232	946	629768	48
13	359141	896	988342	49	370799	945	629201	47
14	359678	895	988312	50	371367	944	628633	46
15	360215	893	988282	50	371933	943	628067	45
16	360752	892	988252	50	372499	942	627501	44
17	361287	891	988223	50	373064	941	626936	43
18	361822	890	988193	50	373629	940	626371	42
19	362356	889	988163	50	374193	939	625807	41
20	362889	888	988133	50	374756	938	625244	40
21	9.363122	887	9.988103	50	9.375319	937	10.624681	39
22	363654	885	988073	50	375881	935	624119	38
23	364185	884	988043	50	376442	934	623558	37
24	365016	883	988013	50	377003	933	622997	36
25	365546	882	987983	50	377563	932	622437	35
26	366075	881	987953	50	378122	931	621878	34
27	366604	880	987922	50	378681	930	621319	33
28	367131	879	987892	50	379239	929	620761	32
29	367659	877	987862	50	379797	928	620203	31
30	368185	876	987832	51	380354	927	619646	30
31	9.368711	875	9.987801	51	9.380910	926	10.619090	29
32	369236	874	987771	51	381466	925	618534	28
33	369761	873	987740	51	382020	924	617980	27
34	370285	872	987710	51	382575	923	617425	26
35	370808	871	987679	51	383129	922	616871	25
36	371330	870	987649	51	383682	921	616318	24
37	371852	869	987618	51	384234	920	615766	23
38	372373	867	987588	51	384786	919	615214	22
39	372894	866	987557	51	385337	918	614663	21
40	373414	865	987526	51	385888	917	614112	20
41	9.373933	864	9.987496	51	9.386438	915	10.613562	19
42	374452	863	987465	51	386937	914	613013	18
43	374970	862	987434	51	387536	913	612464	17
44	375487	861	987403	52	388084	912	611916	16
45	376003	860	987372	52	388631	911	611369	15
46	376519	859	987341	52	389178	910	610822	14
47	377035	858	997310	52	389724	909	610276	13
48	377549	857	987279	52	390270	908	609730	12
49	378063	856	987248	52	390815	907	609185	11
50	378577	854	987217	52	391360	906	608640	10
51	9.379089	853	9.987186	52	9.391903	905	10.608097	9
52	379601	852	987155	52	392447	904	607553	8
53	380113	851	987124	52	392989	903	607011	7
54	380624	850	987092	52	393531	902	606469	6
55	381134	849	987061	52	394073	901	605927	5
56	381643	848	987030	52	394614	900	605386	4
57	382152	847	986998	52	395154	899	604846	3
58	382661	846	986967	52	395694	898	604306	2
59	383168	845	986936	52	396233	897	603767	1
60	383675	814	986904	52	396771	896	603229	0
	Cosine		Sine		Cotang.		Tang.	M.

EE\*

78 Degrees.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.383675	814	9.986894	52	9.396771	896	10.603229	60
1	384182	813	986873	53	397309	896	602691	59
2	384687	812	986841	53	397846	895	602154	58
3	385192	811	986809	53	398383	894	601617	57
4	385697	840	986778	53	398919	893	601081	56
5	386201	839	986746	53	399455	892	600545	55
6	386704	838	986714	53	399990	891	600010	54
7	387207	837	986683	53	400524	890	599476	53
8	387709	836	986651	53	401058	889	598942	52
9	388210	835	986619	53	401591	888	598409	51
10	388711	834	986587	53	402124	887	597876	50
11	9.389211	833	9.986555	53	9.402656	886	10.597344	49
12	389711	832	986523	53	403187	885	596813	48
13	390210	831	986491	53	403718	884	596282	47
14	390708	830	986459	53	404249	883	595751	46
15	391206	828	986427	53	404778	882	595222	45
16	391703	827	986395	53	405308	881	594692	44
17	392199	826	986363	54	405836	880	594164	43
18	392695	825	986331	54	406364	879	593636	42
19	393191	824	986299	54	406892	878	593108	41
20	393685	823	986266	54	407419	877	592581	40
21	9.394179	822	9.986234	54	9.407945	876	10.592055	39
22	394673	821	986202	54	408471	875	591529	38
23	395166	820	986169	54	408997	874	591003	37
24	395658	819	986137	54	409521	874	590479	36
25	396150	818	986104	54	410045	873	589955	35
26	396641	817	986072	54	410569	872	589431	34
27	397132	817	986039	54	411092	871	588908	33
28	397621	816	986007	54	411615	870	588385	32
29	398111	815	985974	54	412137	869	587863	31
30	398600	814	985942	54	412658	868	587342	30
31	9.399088	813	9.985909	55	9.413179	867	10.586821	29
32	399575	812	985876	55	413699	866	586301	28
33	400062	811	985843	55	414219	865	585781	27
34	400549	810	985811	55	414738	864	585262	26
35	401035	809	985778	55	415257	864	584743	25
36	401520	808	985745	55	415775	863	584225	24
37	402005	807	985712	55	416293	862	583707	23
38	402489	806	985679	55	416810	861	583190	22
39	402972	805	985646	55	417326	860	582674	21
40	403455	804	985613	55	417842	859	582158	20
41	9.403938	803	9.985580	55	9.418358	858	10.581642	19
42	404420	802	985547	55	418873	857	581127	18
43	404901	801	985514	55	419387	856	580613	17
44	405382	800	985480	55	419901	855	580099	16
45	405862	799	985447	55	420415	855	579585	15
46	406341	798	985414	56	420927	854	579073	14
47	406820	797	985380	56	421440	853	578560	13
48	407299	796	985347	56	421952	852	578048	12
49	407777	795	985314	56	422463	851	577537	11
50	408254	794	985280	56	422974	850	577026	10
51	9.408731	794	9.985247	56	9.423484	849	10.576516	9
52	409207	793	985213	56	423993	848	576007	8
53	409682	792	985180	56	424503	848	575497	7
54	410157	791	985146	56	425011	847	574989	6
55	410632	790	985113	56	425519	846	574481	5
56	411106	789	985079	56	426027	845	573973	4
57	411579	788	985045	56	426534	844	573466	3
58	412052	787	985011	56	427041	843	572959	2
59	412524	786	984978	56	427547	843	572453	1
60	412996	785	984944	56	428052	842	571948	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (15 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.412996	785	9.984944	57	9.428052	842	10.571948	60
1	413467	784	984910	57	428557	841	571443	59
2	413938	783	984876	57	429062	840	570938	58
3	414408	783	984842	57	429566	839	570434	57
4	414878	782	984808	57	430070	838	569930	56
5	415347	781	984774	57	430573	838	569427	55
6	415815	780	984740	57	431075	837	568925	54
7	416283	779	984706	57	431577	836	568423	53
8	416751	778	984672	57	432079	835	567921	52
9	417217	777	984637	57	432580	834	567420	51
10	417684	776	984603	57	433080	833	566920	50
11	9.418150	775	9.984569	57	9.433580	832	10.566420	49
12	418615	774	984535	57	434080	832	565920	48
13	419079	773	984500	57	434579	831	565421	47
14	419544	773	984466	57	435078	830	564922	46
15	420007	772	984432	58	435576	829	564424	45
16	420470	771	984397	58	436073	828	563927	44
17	420933	770	984363	58	436570	828	563430	43
18	421395	769	984328	58	437067	827	562933	42
19	421857	768	984294	58	437563	826	562437	41
20	422318	767	984259	58	438059	825	561941	40
21	9.422778	767	9.984224	58	9.438554	824	10.561446	39
22	423238	766	984190	58	439048	823	560952	38
23	423697	765	984155	58	439543	823	560457	37
24	424156	764	984120	58	440036	822	559964	36
25	424615	763	984085	58	440529	821	559471	35
26	425073	762	984050	58	441022	820	558978	34
27	425530	761	984015	58	441514	819	558486	33
28	425987	760	983981	58	442006	819	557994	32
29	426443	760	983946	58	442497	818	557503	31
30	426899	759	983911	58	442988	817	557012	30
31	9.427354	758	9.983875	58	9.443479	816	10.556521	29
32	427809	757	983840	59	443968	816	556032	28
33	428263	756	983805	59	444458	815	555542	27
34	428717	755	983770	59	444947	814	555053	26
35	429170	754	983735	59	445435	813	554565	25
36	429623	753	983700	59	445923	812	554077	24
37	430075	752	983664	59	446411	812	553589	23
38	430527	752	983629	59	446898	811	553102	22
39	430978	751	983594	59	447384	810	552616	21
40	431429	750	983558	59	447870	809	552130	20
41	9.431879	749	9.983523	59	9.448356	809	10.551644	19
42	432329	749	983487	59	448841	808	551159	18
43	432778	748	983452	59	449326	807	550674	17
44	433226	747	983416	59	449810	806	550190	16
45	433675	746	983381	59	450294	806	549706	15
46	434122	745	983345	59	450777	805	549223	14
47	434569	744	983309	59	451260	804	548740	13
48	435016	744	983273	60	451743	803	548257	12
49	435462	743	983238	60	452225	802	547775	11
50	435908	742	983202	60	452706	802	547294	10
51	9.436353	741	9.983166	60	9.453187	801	10.546813	9
52	436798	740	983130	60	453668	800	546332	8
53	437242	740	983094	60	454148	799	545852	7
54	437686	739	983058	60	454628	799	545372	6
55	438129	738	983022	60	455107	798	544893	5
56	438572	737	982986	60	455586	797	544414	4
57	439014	736	982950	60	456064	796	543936	3
58	439456	736	982914	60	456542	796	543458	2
59	439897	735	982878	60	457019	795	542981	1
60	440338	734	982842	60	457496	794	542504	0
	Cosine		Sine		Cotang.		Tang.	M.

34 (16 Degrees.) A TABLE OF LOGARITHMIC

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.440338	734	9.982842	60	9.457496	794	10.542504	60
1	440778	733	982805	60	457973	793	542027	59
2	441218	732	982769	61	458449	793	541551	58
3	441658	731	982733	61	458925	792	541075	57
4	442096	731	982696	61	459400	791	540600	56
5	442535	730	982660	61	459875	790	540125	55
6	442973	729	982624	61	460349	790	539651	54
7	443410	728	982587	61	460823	789	539177	53
8	443847	727	982551	61	461297	788	538703	52
9	444284	727	982514	61	461770	788	538230	51
10	444720	726	982477	61	462242	787	537758	50
11	9.445155	725	9.982441	61	9.462714	786	10.537286	49
12	445590	724	982404	61	463186	785	536814	48
13	446025	723	982367	61	463658	785	536342	47
14	446459	723	982331	61	464129	784	535871	46
15	446893	722	982294	61	464599	783	535401	45
16	447326	721	982257	61	465067	783	534931	44
17	447759	720	982220	62	465539	782	534461	43
18	448191	720	982183	62	466008	781	533992	42
19	448623	719	982146	62	466476	780	533524	41
20	449054	718	982109	62	466945	780	533055	40
21	9.449485	717	9.982072	62	9.467413	779	10.532587	39
22	449915	716	982035	62	467880	778	532120	38
23	450345	716	981998	62	468347	778	531653	37
24	450775	715	981961	62	468814	777	531186	36
25	451204	714	981924	62	469280	776	530720	35
26	451632	713	981886	62	469746	775	530254	34
27	452060	713	981849	62	470211	775	529789	33
28	452488	712	981812	62	470676	774	529324	32
29	452915	711	981774	62	471141	773	528859	31
30	453342	710	981737	62	471605	773	528395	30
31	9.453768	710	9.981699	63	9.472068	772	10.527932	29
32	454194	709	981662	63	472532	771	527468	28
33	454619	708	981625	63	472995	771	527005	27
34	455044	707	981587	63	473457	770	526543	26
35	455469	707	981549	63	473919	769	526081	25
36	455893	706	981512	63	474381	769	525619	24
37	456316	705	981474	63	474842	768	525158	23
38	456739	704	981436	63	475303	767	524697	22
39	457162	704	981399	63	475763	767	524237	21
40	457584	703	981361	63	476223	766	523777	20
41	9.458006	702	9.981323	63	9.476683	765	10.523317	19
42	458427	701	981285	63	477142	765	522858	18
43	458848	701	981247	63	477601	764	522399	17
44	459268	700	981209	63	478059	763	521941	16
45	459688	699	981171	63	478517	763	521483	15
46	460108	698	981133	64	478975	762	521025	14
47	460527	698	981095	64	479432	761	520568	13
48	460946	697	981057	64	479889	761	520111	12
49	461364	696	981019	64	480345	760	519655	11
50	461782	695	980981	64	480801	759	519199	10
51	9.462199	695	9.980942	64	9.481257	759	10.518743	9
52	462616	694	980904	64	481712	758	518288	8
53	463032	693	980866	64	482167	757	517833	7
54	463448	693	980827	64	482621	757	517379	6
55	463864	692	980789	64	483075	756	516925	5
56	464279	691	980750	64	483529	755	516471	4
57	464694	690	980712	64	483982	755	516018	3
58	465108	690	980673	64	484435	754	515565	2
59	465522	689	980635	64	484887	753	515113	1
60	465935	688	980596	64	485339	753	514661	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (17 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.465935	688	9.980596	64	9.485339	755	10.514661	60
1	466348	688	980558	64	485791	752	514209	59
2	466761	087	980519	65	486242	751	513758	58
3	467173	686	980480	65	486693	751	513307	57
4	467585	685	980442	65	487143	750	512857	56
5	467996	685	980403	65	487593	749	512407	55
6	468407	684	980364	65	488043	749	511957	54
7	468817	683	980325	65	488492	748	511508	53
8	469227	683	980286	65	488941	747	511059	52
9	469637	682	980247	65	489390	747	510610	51
10	470046	681	980208	65	489838	746	510162	50
11	9.470455	680	9.980169	65	9.490286	746	10.509714	49
12	470863	680	980130	65	490733	745	509267	48
13	471271	679	980091	65	491180	744	508820	47
14	471679	678	980052	65	491627	744	508373	46
15	472086	678	980012	65	492073	743	507927	45
16	472492	677	979973	65	492519	743	507481	44
17	472898	676	979934	66	492965	742	507035	43
18	473304	676	979895	66	493410	741	506590	42
19	473710	675	979855	66	493854	740	506146	41
20	474115	674	979816	66	494299	740	505701	40
21	9.474519	674	9.979776	66	9.494743	740	10.505257	39
22	474923	673	979737	66	495186	739	504814	38
23	475327	672	979697	66	495630	738	504370	37
24	475730	672	979658	66	496073	737	503927	36
25	476133	671	979618	66	496515	737	503485	35
26	476536	670	979579	66	496957	736	503043	34
27	476938	669	979539	66	497399	736	502601	33
28	477340	669	979499	66	497841	735	502159	32
29	477741	668	979459	66	498282	734	501718	31
30	478142	667	979420	66	498722	734	501278	30
31	9.478542	667	9.979380	66	9.499163	733	10.500837	29
32	478942	666	979340	66	499603	733	500397	28
33	479342	665	979300	67	500042	732	499958	27
34	479741	665	979260	67	500481	731	499519	26
35	480140	664	979220	67	500920	731	499080	25
36	480539	633	979180	67	501359	730	498641	24
37	480937	663	979140	67	501797	730	498203	23
38	481334	662	979100	67	502235	729	497765	22
39	481731	661	979059	67	502672	728	497328	21
40	482128	661	979019	67	503109	728	496891	20
41	9.482525	660	9.978979	67	9.503546	727	10.496454	19
42	482921	659	978939	67	503982	727	496018	18
43	483316	659	978898	67	504418	726	495582	17
44	483712	658	978858	67	504854	725	495146	16
45	484107	657	978817	67	505289	725	494711	15
46	484501	657	978777	67	505724	724	494276	14
47	484895	656	978736	67	506159	724	493841	13
48	485289	655	978696	68	506593	723	493407	12
49	485682	655	978655	68	507027	722	492973	11
50	486075	654	978615	68	507460	722	492540	10
51	9.486467	653	9.978574	68	9.507893	721	10.492107	9
52	486860	653	978533	68	508326	721	491674	8
53	487251	652	978493	68	508759	720	491241	7
54	487643	651	978452	68	509191	719	490809	6
55	488034	651	978411	68	509622	719	490378	5
56	488424	650	978370	68	510054	718	489946	4
57	488814	650	978329	68	510485	718	489515	3
58	489204	649	978288	68	510916	717	489084	2
59	489593	648	978247	68	511346	717	488654	1
60	489982	648	978206	68	511776	716	488224	0
	Cosine		Sine		Cotang.		Tang.	M.

Corner 71 Degrees.  
Should be - 72 degrees



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.489982	648	9.978206	68	9.511776	716	10.488224	60
1	490371	648	978165	68	512206	716	487794	59
2	490759	647	978124	68	512635	715	487365	58
3	491147	646	978083	69	513064	714	486936	57
4	491535	646	978042	69	513493	714	486507	56
5	491922	645	978001	69	513921	713	486079	55
6	492308	644	977959	69	514349	713	485651	54
7	492695	644	977918	69	514777	712	485223	53
8	493081	643	977877	69	515204	712	484796	52
9	493466	642	977835	69	515631	711	484369	51
10	493851	642	977794	69	516057	710	483943	50
11	9.494236	641	9.977752	69	9.516484	710	10.483516	49
12	494621	641	977711	69	516910	709	483090	48
13	495005	640	977669	69	517335	709	482665	47
14	495388	639	977628	69	517761	708	482239	46
15	495772	639	977586	69	518185	708	481815	45
16	496154	638	977544	70	518610	707	481390	44
17	496537	637	977503	70	519034	706	480966	43
18	496919	637	977461	70	519458	706	480542	42
19	497301	636	977419	70	519882	705	480118	41
20	497682	636	977377	70	520305	705	479695	40
21	9.498064	635	9.977335	70	9.520728	704	10.479272	39
22	498444	634	977293	70	521151	703	478849	38
23	498825	634	977251	70	521573	703	478427	37
24	499204	633	977209	70	521995	703	478005	36
25	499584	632	977167	70	522417	702	477583	35
26	499963	632	977125	70	522838	702	477162	34
27	500342	631	977083	70	523259	701	476741	33
28	500721	631	977041	70	523680	701	476320	32
29	501099	630	976999	70	524100	700	475900	31
30	501476	629	976957	70	524520	699	475480	30
31	9.501854	629	9.976914	70	9.524939	699	10.475061	29
32	502231	628	976872	71	525359	698	474641	28
33	502607	628	976830	71	525778	698	474222	27
34	502984	627	976787	71	526197	697	473803	26
35	503360	626	976745	71	526615	697	473385	25
36	503735	626	976702	71	527033	696	472967	24
37	504110	625	976660	71	527451	696	472549	23
38	504485	625	976617	71	527868	695	472132	22
39	504860	624	976574	71	528285	695	471715	21
40	505234	623	976532	71	528702	694	471298	20
41	9.505608	623	9.976489	71	9.529119	693	0.470881	19
42	505981	622	976446	71	529535	693	470465	18
43	506354	622	976404	71	529950	693	470050	17
44	506727	621	976361	71	530366	692	469634	16
45	507099	620	976318	71	530781	691	469219	15
46	507471	620	976275	71	531196	691	468804	14
47	507843	619	976232	72	531611	690	468389	13
48	508214	619	976189	72	532025	690	467975	12
49	508585	618	976146	72	532439	689	467561	11
50	508956	618	976103	72	532853	689	467147	10
51	9.509326	617	9.976060	72	9.533266	688	10.466734	9
52	509696	616	976017	72	533679	688	466321	8
53	510065	616	975974	72	534092	687	465908	7
54	510434	615	975930	72	534504	687	465496	6
55	510803	615	975887	72	534916	686	465084	5
56	511172	614	975844	72	535328	686	464672	4
57	511540	613	975800	72	535739	685	464261	3
58	511907	613	975757	72	536150	685	463850	2
59	512275	612	975714	72	536561	684	463439	1
60	512642	612	975670	72	536972	684	463028	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.512642	612	9.975670	73	9.536972	684	10.463028	60
1	513009	611	975627	73	537382	683	462618	59
2	513375	611	975583	73	537792	683	462208	58
3	513741	610	975539	73	538202	682	461798	57
4	514107	609	975496	73	538611	682	461389	56
5	514472	609	975452	73	539020	681	460980	55
6	514837	608	975408	73	539429	681	460571	54
7	515202	608	975365	73	539837	680	460163	53
8	515566	607	975321	73	540245	680	459755	52
9	515930	607	975277	73	540653	679	459347	51
10	516294	606	975233	73	541061	679	458939	50
11	9.516657	605	9.975189	73	9.541468	678	10.458532	49
12	517020	605	975145	73	541875	678	458125	48
13	517382	604	975101	73	542281	677	457719	47
14	517745	604	975057	73	542688	677	457312	46
15	518107	603	975013	73	543094	676	456906	45
16	518468	603	974969	74	543499	676	456501	44
17	518829	602	974925	74	543905	675	456095	43
18	519190	601	974880	74	544310	675	455690	42
19	519551	601	974836	74	544715	674	455285	41
20	519911	600	974792	74	545119	674	454881	40
21	9.520271	600	9.974748	74	9.545524	673	10.454476	39
22	520631	599	974703	74	545928	673	454072	38
23	520990	599	974659	74	546331	672	453669	37
24	521349	598	974614	74	546735	672	453265	36
25	521707	598	974570	74	547138	671	452862	35
26	522066	597	974525	74	547540	671	452460	34
27	522424	596	974481	74	547943	670	452057	33
28	522781	596	974436	74	548345	670	451655	32
29	523138	595	974391	74	548747	669	451253	31
30	523495	595	974347	75	549149	669	450851	30
31	9.523852	594	9.974302	75	9.549550	668	10.450450	29
32	524208	594	974257	75	549951	668	450049	28
33	524564	593	974212	75	550352	667	449648	27
34	524920	593	974167	75	550752	667	449248	26
35	525275	592	974122	75	551152	666	448848	25
36	525630	591	974077	75	551552	666	448448	24
37	525984	591	974032	75	551952	665	448048	23
38	526339	590	973987	75	552351	665	447649	22
39	526693	590	973942	75	552750	665	447250	21
40	527046	589	973897	75	553149	664	446851	20
41	9.527400	589	9.973852	75	9.553543	664	10.446452	19
42	527753	588	973807	75	553946	663	446054	18
43	528105	588	973761	75	554344	663	445656	17
44	528458	587	973716	76	554741	662	445259	16
45	528810	587	973671	76	555139	662	444861	15
46	529161	586	973625	76	555536	661	444464	14
47	529513	586	973580	76	555933	661	444067	13
48	529864	585	973535	76	556329	660	443671	12
49	530215	585	973489	76	556725	660	443275	11
50	530565	584	973444	76	557121	659	442879	10
51	9.530915	584	9.973398	76	9.557517	659	10.442483	9
52	531265	583	973352	76	557913	659	442087	8
53	531614	582	973307	76	558308	658	441692	7
54	531963	582	973261	76	558702	658	441298	6
55	532312	581	973215	76	559097	657	440903	5
56	532661	581	973169	76	559491	657	440509	4
57	533009	580	973124	76	559885	656	440115	3
58	533357	580	973078	76	560279	656	439721	2
59	533704	579	973032	77	560673	655	439327	1
60	534052	578	972986	77	561066	655	438934	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.531052	578	9.972986	77	9.561066	655	10.438934	60
1	531399	577	972940	77	561459	654	438541	59
2	531745	577	972894	77	561851	654	438149	58
3	535092	577	972848	77	562244	653	437756	57
4	535438	576	972802	77	562636	653	437364	56
5	535783	576	972755	77	563028	653	436972	55
6	536129	575	972709	77	563419	652	436581	54
7	536474	574	972663	77	563811	652	436189	53
8	536818	574	972617	77	564202	651	435798	52
9	537163	573	972570	77	564592	651	435408	51
10	537507	573	972524	77	564983	650	435017	50
11	9.537851	572	9.972478	77	9.565373	650	10.431627	49
12	538194	572	972431	78	565763	649	434237	48
13	538538	571	972385	78	566153	649	433847	47
14	538880	571	972338	78	566542	649	433458	46
15	539223	570	972291	78	566932	648	433068	45
16	539565	570	972245	78	567320	648	432680	44
17	539907	569	972198	78	567709	647	432291	43
18	540249	569	972151	78	568098	647	431902	42
19	540590	568	972105	79	568486	646	431514	41
20	540931	568	972058	78	568873	646	431127	40
21	9.541272	567	9.972011	78	9.569261	645	10.430739	39
22	541613	567	971964	78	569648	645	430352	38
23	541953	566	971917	78	570035	645	429965	37
24	542293	566	971870	78	570422	644	429578	36
25	542632	565	971823	78	570809	644	429191	35
26	542971	565	971776	78	571195	643	428805	34
27	543310	564	971729	79	571581	643	428419	33
28	543649	564	971682	79	571967	642	428033	32
29	543987	563	971635	79	572352	642	427648	31
30	544325	563	971588	79	572738	642	427262	30
31	9.544663	562	9.971540	79	9.573123	641	10.426877	29
32	545000	562	971493	79	573507	641	426491	28
33	545338	561	971446	79	573892	640	426108	27
34	545674	561	971398	79	574276	640	425724	26
35	546011	560	971351	79	574660	639	425340	25
36	546347	560	971303	79	575044	639	424956	24
37	546683	559	971256	79	575427	639	424573	23
38	547019	559	971208	79	575810	638	424190	22
39	547354	558	971161	79	576193	638	423807	21
40	547689	558	971113	79	576576	637	423424	20
41	9.548024	557	9.971066	80	9.576958	637	10.423041	19
42	548359	557	971018	80	577341	636	422659	18
43	548693	556	970970	80	577723	636	422277	17
44	549027	556	970922	80	578104	636	421896	16
45	549360	555	970874	80	578486	635	421514	15
46	549693	555	970827	80	578867	635	421133	14
47	550026	554	970779	80	579248	634	420752	13
48	550359	554	970731	80	579629	634	420371	12
49	550692	553	970683	80	580009	634	419991	11
50	551024	553	970635	80	580389	633	419611	10
51	9.551356	552	9.970586	80	9.580769	633	10.419231	9
52	551687	552	970538	80	581149	632	418851	8
53	552018	552	970490	80	581528	632	418472	7
54	552349	551	970442	80	581907	632	418093	6
55	552680	551	970394	80	582286	631	417714	5
56	553010	550	970345	81	582665	631	417335	4
57	553341	550	970297	81	583043	630	416957	3
58	553670	549	970249	81	583422	630	416578	2
59	554000	549	970200	81	583800	629	416200	1
60	554329	548	970152	81	584177	629	415823	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang	D.	Cotang	M.
0	9.554329	548	9.970152	81	9.584177	629	10.415823	60
1	554658	548	970103	81	584555	629	415445	59
2	554987	547	970055	81	584932	628	415068	58
3	555315	547	970006	81	585309	628	414691	57
4	555643	546	969957	81	585686	627	414314	56
5	555971	546	969909	81	586062	627	413938	55
6	556299	545	969860	81	586439	627	413561	54
7	556626	545	969811	81	586815	626	413185	53
8	556953	544	969762	81	587190	626	412810	52
9	557280	544	969714	81	587566	625	412434	51
10	557606	543	969665	81	587941	625	412059	50
11	9.557932	543	9.969616	82	9.588316	625	10.411684	49
12	558258	543	969567	82	588691	624	411309	48
13	558583	542	969518	82	589066	624	410934	47
14	558909	542	969469	82	589440	623	410560	46
15	559234	541	969420	82	589814	623	410186	45
16	559558	541	969370	82	590188	623	409812	44
17	559883	540	969321	82	590562	622	409438	43
18	560207	540	969272	82	590935	622	409065	42
19	560531	539	969223	82	591308	622	408692	41
20	560855	539	969173	82	591681	621	408319	40
21	9.561178	538	9.969124	82	9.592054	621	10.407946	39
22	561501	538	969075	82	592426	620	407574	38
23	561824	537	969025	82	592798	620	407202	37
24	562146	537	968976	82	593170	619	406829	36
25	562468	536	968926	83	593542	619	406458	35
26	562790	536	968877	83	593914	618	406086	34
27	563112	536	968827	83	594285	618	405715	33
28	563433	535	968777	83	594656	618	405344	32
29	563755	535	968728	83	595027	617	404973	31
30	564075	534	968678	83	595398	617	404602	30
31	9.564396	534	9.968628	83	9.595768	617	10.404232	29
32	564716	533	968578	83	596138	616	403862	28
33	565036	533	968528	83	596508	616	403492	27
34	565356	532	968479	83	596878	616	403122	26
35	565676	532	968429	83	597247	615	402753	25
36	565995	531	968379	83	597616	615	402384	24
37	566314	531	968329	83	597985	615	402015	23
38	566632	531	968278	83	598354	614	401646	22
39	566951	530	968228	84	598722	614	401278	21
40	567269	530	968178	84	599091	613	400909	20
41	9.567587	529	9.968128	84	9.599459	613	10.400541	19
42	567904	529	968078	84	599827	613	400173	18
43	568222	528	968027	84	600194	612	399806	17
44	568539	528	967977	84	600562	612	399438	16
45	568856	528	967927	84	600929	611	399071	15
46	569172	527	967876	84	601296	611	398704	14
47	569488	527	967826	84	601662	611	398338	13
48	569804	526	967775	84	602029	610	397971	12
49	570120	526	967725	84	602395	610	397605	11
50	570435	525	967674	84	602761	610	397239	10
51	9.570751	525	9.967624	84	9.603127	609	10.396873	9
52	571066	524	967573	84	603493	609	396507	8
53	571380	524	967522	85	603858	609	396142	7
54	571695	523	967471	85	604223	608	395777	6
55	572009	523	967421	85	604588	608	395412	5
56	572323	523	967370	85	604953	607	395047	4
57	572636	522	967319	85	605317	607	394683	3
58	572950	522	967268	85	605682	607	394318	2
59	573263	521	967217	85	606046	606	393954	1
60	573575	521	967166	85	606410	606	393590	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.573575	521	9.967166	85	9.606410	606	10.393590	66
1	573888	520	967115	85	606773	606	393227	59
2	574200	520	967064	85	607137	605	392863	58
3	574512	519	967013	85	607500	605	392500	57
4	574824	519	966961	85	607863	604	392137	56
5	575136	519	966910	85	608225	604	391775	55
6	575447	518	966859	85	608588	604	391412	54
7	575758	518	966808	85	608950	603	391050	53
8	576069	517	966756	86	609312	603	390688	52
9	576379	517	966705	86	609674	603	390326	51
10	576689	516	966653	86	610036	602	389964	50
11	9.576999	516	9.966602	86	9.610397	602	10.389603	49
12	577309	516	966550	86	610759	602	389241	48
13	577618	515	966499	86	611120	601	388880	47
14	577927	515	966447	86	611480	601	388520	46
15	578236	514	966395	86	611841	601	388159	45
16	578545	514	966344	86	612201	600	387799	44
17	578853	513	966292	86	612561	600	387439	43
18	579162	513	966240	86	612921	600	387079	42
19	579470	513	966188	86	613281	599	386719	41
20	579777	512	966136	86	613641	599	386359	40
21	9.580085	512	9.966085	87	9.614000	598	10.386000	39
22	580392	511	966033	87	614359	598	385641	38
23	580699	511	965981	87	614718	598	385282	37
24	581005	511	965928	87	615077	597	384923	36
25	581312	510	965876	87	615435	597	384565	35
26	581618	510	965824	87	615793	597	384207	34
27	581924	509	965772	87	616151	596	383849	33
28	582229	509	965720	87	616509	596	383491	32
29	582535	509	965668	87	616867	596	383133	31
30	582840	508	965615	87	617224	595	382776	30
31	9.583145	508	9.965563	87	9.617582	595	10.382118	29
32	583449	507	965511	87	617939	595	382361	28
33	583754	507	965458	87	618295	594	381705	27
34	584058	506	965406	87	618652	594	381348	26
35	584361	506	965353	88	619008	594	380992	25
36	584665	506	965301	88	619364	593	380636	24
37	584968	505	965248	88	619721	593	380279	23
38	585272	505	965195	88	620076	593	379924	22
39	585574	504	965143	88	620432	592	379568	21
40	585877	504	965090	88	620787	592	379213	20
41	9.586179	503	9.965037	88	9.621142	592	10.378858	19
42	586482	503	964984	88	621497	591	378503	18
43	586783	503	964931	88	621852	591	378148	17
44	587085	502	964879	88	622207	590	377793	16
45	587386	502	964826	88	622561	590	377437	15
46	587688	501	964773	88	622915	590	377082	14
47	587989	501	964719	88	623269	589	376727	13
48	588289	501	964666	89	623623	589	376372	12
49	588590	500	964613	89	623976	589	376017	11
50	588890	500	964560	89	624330	588	375662	10
51	9.589190	499	9.964507	89	9.624683	588	10.375317	9
52	589489	499	964454	89	625036	588	374964	8
53	589789	499	964400	89	625388	587	374612	7
54	590088	498	964347	89	625741	587	374259	6
55	590387	498	964294	89	626093	587	373907	5
56	590686	497	964240	89	626445	586	373555	4
57	590984	497	964187	89	626797	586	373203	3
58	591282	497	964133	89	627149	586	372851	2
59	591580	496	964080	89	627501	585	372499	1
60	591878	496	964026	89	627852	585	372148	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (23 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.591878	496	9.964026	89	9.627852	585	10.372148	60
1	592176	495	963972	89	628203	585	371797	59
2	592473	495	963919	89	628554	585	371446	58
3	592770	495	963865	90	628905	584	371095	57
4	593067	494	963811	90	629255	584	370745	56
5	593363	494	963757	90	629606	583	370394	55
6	593659	493	963704	90	629956	583	370044	54
7	593955	493	963650	90	630306	583	369694	53
8	594251	493	963596	90	630656	583	369344	52
9	594547	492	963542	90	631005	582	368995	51
10	594842	492	963488	90	631355	582	368645	50
11	9.595137	491	9.963434	90	9.631704	582	10.368296	49
12	595432	491	963379	90	632053	581	367947	48
13	595727	491	963325	90	632401	581	367599	47
14	596021	490	963271	90	632750	581	367250	46
15	596315	490	963217	90	633098	580	366902	45
16	596609	489	963163	90	633447	580	366553	44
17	596903	489	963108	91	633795	580	366205	43
18	597196	489	963054	91	634143	579	365857	42
19	597490	488	962999	91	634490	579	365510	41
20	597783	488	962945	91	634838	579	365162	40
21	9.598075	487	9.962890	91	9.635185	578	10.364815	39
22	598368	487	962836	91	635532	578	364468	38
23	598660	487	962781	91	635879	578	364121	37
24	598952	486	962727	91	636226	577	363774	36
25	599244	486	962672	91	636572	577	363428	35
26	599536	485	962617	91	636919	577	363081	34
27	599827	485	962562	91	637265	577	362735	33
28	600118	485	962508	91	637611	576	362389	32
29	600409	484	962453	91	637956	576	362044	31
30	600700	484	962398	92	638302	576	361698	30
31	9.600990	484	9.962343	92	9.638647	575	10.361353	29
32	601280	483	962288	92	638992	575	361008	28
33	601570	483	962233	92	639337	575	360663	27
34	601860	482	962178	92	639682	574	360318	26
35	602150	482	962123	92	640027	574	359973	25
36	602439	482	962067	92	640371	574	359629	24
37	602728	481	962012	92	640716	573	359284	23
38	603017	481	961957	92	641066	573	358940	22
39	603305	481	961902	92	641404	573	358596	21
40	603594	480	961846	92	641747	572	358253	20
41	9.603882	480	9.961791	92	9.642091	572	10.357809	19
42	604170	479	961735	92	642434	572	357566	18
43	604457	479	961680	92	642777	572	357223	17
44	604745	479	961624	93	643120	571	356880	16
45	605032	478	961569	93	643463	571	356537	15
46	605319	478	961513	93	643806	571	356194	14
47	605606	478	961458	93	644148	570	355852	13
48	605892	477	961402	93	644490	570	355510	12
49	606179	477	961346	93	644832	570	355168	11
50	606465	476	961290	93	645174	569	354826	10
51	9.606751	476	9.961235	93	9.645516	569	10.354484	9
52	607036	476	961179	93	645857	569	354143	8
53	607322	475	961123	93	646199	569	353801	7
54	607607	475	961067	93	646540	568	353460	6
55	607892	474	961011	93	646881	568	353119	5
56	608177	474	960955	93	647222	568	352778	4
57	608461	474	960899	93	647562	567	352438	3
58	608745	473	960843	94	647903	567	352097	2
59	609029	473	960786	94	648243	567	351757	1
60	609313	473	960730	94	648583	566	351417	0
	Cosine		Sine		Cotang.		Tang.	M

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.609313	473	9.960730	94	9.648583	566	10.351417	60
1	609597	472	960674	94	648923	566	351077	59
2	609880	472	960618	94	649263	566	350737	58
3	610164	472	960561	94	649602	566	350398	57
4	610447	471	960505	94	649942	565	350058	56
5	610729	471	960448	94	650281	565	349719	55
6	611012	470	960392	94	650620	565	349380	54
7	611294	470	960335	94	650959	564	349041	53
8	611576	470	960279	94	651297	564	348703	52
9	611858	469	960222	94	651636	564	348364	51
10	612140	469	960165	94	651974	563	348026	50
11	9.612121	469	9.960109	95	9.652312	563	10.347688	49
12	612702	468	960052	95	652650	563	347350	48
13	612983	468	959995	95	652988	563	347012	47
14	613264	467	959938	95	653326	562	346674	46
15	613545	467	959882	95	653663	562	346337	45
16	613825	467	959825	95	654000	562	346000	44
17	614105	466	959768	95	654337	561	345663	43
18	614385	466	959711	95	654674	561	345326	42
19	614665	466	959654	95	655011	561	344989	41
20	614944	465	959596	95	655348	561	344652	40
21	9.615223	465	9.959539	95	9.655684	560	10.344316	39
22	615502	465	959482	95	655620	560	343980	38
23	615781	464	959425	95	655956	560	343644	37
24	616060	464	959368	95	656292	559	343308	36
25	616338	464	959310	96	656708	559	342972	35
26	616616	463	959253	96	657364	559	342636	34
27	616894	463	959195	96	657699	559	342301	33
28	617172	462	959138	96	658034	558	341966	32
29	617450	462	959081	96	658369	558	341631	31
30	617727	462	959023	96	658704	558	341296	30
31	9.618004	461	9.958965	96	9.659039	558	10.340961	29
32	618281	461	958908	96	659373	557	340627	28
33	618558	461	958850	96	659708	557	340292	27
34	618834	460	958792	96	660042	557	339958	26
35	619110	460	958734	96	660376	557	339624	25
36	619386	460	958677	96	660710	556	339290	24
37	619662	459	958619	96	661043	556	338957	23
38	619938	459	958561	96	661377	556	338623	22
39	620213	459	958503	97	661710	555	338290	21
40	620488	458	958445	97	662043	555	337957	20
41	9.620763	458	9.958387	97	9.662376	555	10.337624	19
42	621038	457	958329	97	662709	554	337291	18
43	621313	457	958271	97	663042	554	336958	17
44	621587	457	958213	97	663375	554	336625	16
45	621861	456	958154	97	663707	554	336293	15
46	622135	456	958096	97	664039	553	335961	14
47	622409	456	958038	97	664371	553	335629	13
48	622682	455	957979	97	664703	553	335297	12
49	622956	455	957921	97	665035	553	334965	11
50	623229	455	957863	97	665366	552	334634	10
51	9.623502	454	9.957804	97	9.665697	552	10.334303	9
52	623774	454	957746	98	666029	552	333971	8
53	624047	454	957687	98	666360	551	333640	7
54	624319	453	957628	98	666691	551	333309	6
55	624591	453	957570	98	667021	551	332979	5
56	624863	453	957511	98	667352	551	332648	4
57	625135	452	957452	98	667682	550	332318	3
58	625406	452	957393	98	668013	550	331987	2
59	625677	452	957335	98	668343	550	331657	1
60	625948	451	957276	98	668672	550	331328	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (25 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.625948	451	9.957276	98	9.668673	550	10.331327	60
1	626219	451	957217	98	669002	549	330998	59
2	626490	451	957158	98	669332	549	330668	58
3	626760	450	957099	98	669661	549	330339	57
4	627030	450	957040	98	669991	548	329909	56
5	627300	450	956981	98	670320	548	329680	55
6	627570	449	956921	99	670649	548	329351	54
7	627840	449	956862	99	670977	548	329023	53
8	628109	449	956803	99	671306	547	328694	52
9	628378	448	956744	99	671634	547	328366	51
10	628647	448	956684	99	671963	547	328037	50
11	9.628916	447	9.956625	99	9.672291	547	10.327709	49
12	629185	447	956566	99	672619	546	327381	48
13	629453	447	956506	99	672947	546	327053	47
14	629721	446	956447	99	673274	546	326726	46
15	629989	446	956387	99	673602	546	326398	45
16	630257	446	956327	99	673929	545	326071	44
17	630524	446	956268	99	674257	545	325743	43
18	630792	445	956208	100	674584	545	325416	42
19	631059	445	956148	100	674910	544	325090	41
20	631326	445	956089	100	675237	544	324763	40
21	9.631593	444	9.956029	100	9.675564	544	10.324436	39
22	631859	444	955969	100	675890	544	324110	38
23	632125	444	955909	100	676216	543	323784	37
24	632392	443	955849	100	676543	543	323457	36
25	632658	443	955789	100	676869	543	323131	35
26	632923	443	955729	100	677194	543	322806	34
27	633189	442	955669	100	677520	542	322480	33
28	633454	442	955609	100	677846	542	322154	32
29	633719	442	955548	100	678171	542	321829	31
30	633984	441	955488	100	678496	542	321504	30
31	9.634249	441	9.955428	101	9.678821	541	10.321179	29
32	634514	440	955368	101	679146	541	320854	28
33	634778	440	955307	101	679471	541	320529	27
34	635042	440	955247	101	679795	541	320205	26
35	635306	439	955186	101	680120	540	319880	25
36	635570	439	955126	101	680444	540	319556	24
37	635834	439	955065	101	680768	540	319232	23
38	636097	438	955005	101	681092	540	318908	22
39	636360	438	954944	101	681416	539	318584	21
40	636623	438	954883	101	681740	539	318260	20
41	9.636886	437	9.954823	101	9.682063	539	10.317937	19
42	637148	437	954762	101	682387	539	317613	18
43	637411	437	954701	101	682710	538	317290	17
44	637673	437	954640	101	683033	538	316967	16
45	637935	436	954579	101	683356	538	316644	15
46	638197	436	954518	102	683679	538	316321	14
47	638458	436	954457	102	684001	537	315999	13
48	638720	435	954396	102	684324	537	315676	12
49	638981	435	954335	102	684646	537	315354	11
50	639242	435	954274	102	684968	537	315032	10
51	9.639503	434	9.954213	102	9.685290	536	10.314710	9
52	639764	434	954152	102	685612	536	314388	8
53	640024	434	954090	102	685934	536	314066	7
54	640284	433	954029	102	686255	536	313745	6
55	640544	433	953968	102	686577	535	313423	5
56	640804	433	953906	102	686898	535	313102	4
57	641064	432	953845	102	687219	535	312781	3
58	641324	432	953783	102	687540	535	312460	2
59	641584	432	953722	103	687861	534	312139	1
60	641842	431	953660	103	688182	534	311818	0
	Cosine		Sine		Cotang.		Tang.	M.

64 Degrees.  
F F\*



44 (26 Degrees.) A TABLE OF LOGARITHMIC

M.	Sine	D.	Cosine	D.	Tang.	D	Cotang.	
0	9.641842	431	9.953660	103	9.688182	534	10.311818	60
1	642101	431	953599	103	688502	534	311498	59
2	642360	431	953537	103	688823	534	311177	58
3	642618	430	953475	103	689143	533	310857	57
4	642877	430	953413	103	689463	533	310537	56
5	643135	430	953352	103	689783	533	310217	55
6	643393	430	953290	103	690103	533	309897	54
7	643650	429	953228	103	690423	533	309577	53
8	643908	429	953166	103	690742	532	309258	52
9	644165	429	953104	103	691062	532	308938	51
10	644423	428	953042	103	691381	532	308619	50
11	9.644680	428	9.952980	104	9.691700	531	10.308300	49
12	644936	428	952918	104	692019	531	307981	48
13	645193	427	952855	104	692338	531	307662	47
14	645450	427	952793	104	692656	531	307344	46
15	645706	427	952731	104	692975	531	307025	45
16	645962	426	952669	104	693293	530	306707	44
17	646218	426	952606	104	693612	530	306388	43
18	646474	426	952544	104	693930	530	306070	42
19	646729	425	952481	104	694248	530	305752	41
20	646984	425	952419	104	694566	529	305434	40
21	9.647240	425	9.952356	104	9.694883	529	10.305117	39
22	647494	424	952294	104	695201	529	304799	38
23	647749	424	952231	104	695518	529	304482	37
24	648004	424	952168	105	695836	529	304164	36
25	648258	424	952106	105	696153	528	303847	35
26	648512	423	952043	105	696470	528	303530	34
27	648766	423	951980	105	696787	528	303213	33
28	649020	423	951917	105	697103	528	302897	32
29	649274	422	951854	105	697420	527	302580	31
30	649527	422	951791	105	697736	527	302264	30
31	9.649781	422	9.951728	105	9.698053	527	10.301947	29
32	650034	422	951665	105	698369	527	301631	28
33	650287	421	951602	105	698685	526	301315	27
34	650539	421	951539	105	699001	526	300999	26
35	650792	421	951476	105	699316	526	300684	25
36	651044	420	951412	105	699632	526	300368	24
37	651297	420	951349	106	699947	526	300053	23
38	651549	420	951286	106	700263	525	299737	22
39	651800	419	951222	106	700578	525	299422	21
40	652052	419	951159	106	700893	525	299107	20
41	9.652304	419	9.951096	106	9.701208	524	10.298792	19
42	652555	418	951032	106	701523	524	298477	18
43	652806	418	950968	106	701837	524	298163	17
44	653057	418	950905	106	702152	524	297848	16
45	653308	418	950841	106	702466	524	297534	15
46	653558	417	950778	106	702780	523	297220	14
47	653808	417	950714	106	703095	523	296905	13
48	654059	417	950650	106	703409	523	296591	12
49	654309	416	950586	106	703723	523	296277	11
50	654558	416	950522	107	704036	522	295964	10
51	9.654808	416	9.950458	107	9.704350	522	10.295650	9
52	655058	416	950394	107	704663	522	295337	8
53	655307	415	950330	107	704977	522	295023	7
54	655556	415	950266	107	705290	522	294710	6
55	655805	415	950202	107	705603	521	294397	5
56	656054	414	950138	107	705916	521	294084	4
57	656302	414	950074	107	706229	521	293772	3
58	656551	414	950010	107	706541	521	293459	2
59	656799	413	949945	107	706854	521	293146	1
60	657047	413	949881	107	707166	520	292834	0
	Cosine		Sine		Cotang.		Tang.	M.

63 Degrees.

M	Sine	D	Cosine	D.	Tang.	D.	Cotang.	M.
0	0.657047	413	9.949881	107	9.707166	520	10.292834	60
1	657295	413	949816	107	707478	520	292522	69
2	657542	412	949752	107	707790	520	292210	78
3	657790	412	949688	108	708102	520	291898	57
4	658037	412	949623	108	708414	519	291586	56
5	658284	412	949558	108	708726	519	291274	55
6	658531	411	949494	108	709037	519	290963	54
7	658778	411	949429	108	709349	519	290651	53
8	659025	411	949364	108	709660	519	290340	52
9	659271	410	949300	108	709971	518	290029	51
10	659517	410	949235	108	710282	518	289718	50
11	9.659763	410	9.949170	108	9.710593	518	10.289407	49
12	660009	409	949105	108	710904	518	289096	48
13	660255	409	949040	108	711215	518	288785	47
14	660501	409	948975	108	711525	517	288475	46
15	660746	409	948910	108	711836	517	288164	45
16	660991	408	948845	108	712146	517	287854	44
17	661236	408	948780	109	712456	517	287544	43
18	661481	408	948715	109	712766	516	287234	42
19	661726	407	948650	109	713076	516	286924	41
20	661970	407	948584	109	713386	516	286614	40
21	9.662214	407	9.948519	109	9.713696	516	10.286304	39
22	662459	407	948451	109	714005	516	285995	38
23	662703	406	948388	109	714314	515	285686	37
24	662946	406	948323	109	714624	515	285376	36
25	663190	406	948257	109	714933	515	285067	35
26	663433	405	948192	109	715242	515	284758	34
27	663677	405	948126	109	715551	514	284449	33
28	663920	405	948060	109	715860	514	284140	32
29	664163	405	947995	110	716168	514	283832	31
30	664406	404	947929	110	716477	514	283523	30
31	9.664648	404	9.947863	110	9.716785	514	10.283215	29
32	664891	404	947797	110	717093	513	282907	28
33	665133	403	947731	110	717401	513	282599	27
34	665375	403	947665	110	717709	513	282291	26
35	665617	403	947600	110	718017	513	281983	25
36	665859	402	947533	110	718325	513	281675	24
37	666100	402	947467	110	718633	512	281367	23
38	666342	402	947401	110	718940	512	281060	22
39	666583	402	947335	110	719248	512	280752	21
40	666824	401	947269	110	719555	512	280445	20
41	9.667065	401	9.947203	110	9.719862	512	10.280138	19
42	667305	401	947136	111	720169	511	279831	18
43	667546	401	947070	111	720476	511	279524	17
44	667786	400	947001	111	720783	511	279217	16
45	668027	400	946937	111	721089	511	278911	15
46	668267	400	946871	111	721396	511	278604	14
47	668506	399	946804	111	721702	510	278298	13
48	668746	399	946738	111	722009	510	277991	12
49	668986	399	946671	111	722315	510	277685	11
50	669225	399	946604	111	722621	510	277379	10
51	9.669464	398	9.946538	111	9.722927	510	10.277073	9
52	669703	398	946471	111	723232	509	276768	8
53	669942	398	946404	111	723538	509	276462	7
54	670181	397	946337	111	723844	509	276156	6
55	670419	397	946270	112	724149	509	275851	5
56	670658	397	946203	112	724454	509	275546	4
57	670896	397	946136	112	724759	508	275241	3
58	671134	396	946069	112	725065	508	274935	2
59	671372	396	946002	112	725369	508	274631	1
60	671609	396	945935	112	725674	508	274326	0
	Cosine	Sine	Cotang.		Tang.		M.	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.671609	396	9.945935	112	9.725674	508	10.274323	60
1	671847	395	945868	112	725979	508	274021	59
2	672084	395	945800	112	726284	507	273716	58
3	672321	395	945733	112	726588	507	273412	57
4	672558	395	945666	112	726892	507	273108	56
5	672795	394	945598	112	727197	507	272803	55
6	673032	394	945531	112	727501	507	272499	54
7	673268	394	945464	113	727805	506	272195	53
8	673505	394	945396	113	728109	506	271891	52
9	673741	393	945328	113	728412	506	271588	51
10	673977	393	945261	113	728716	506	271284	50
11	9.674213	393	9.945193	113	9.729020	506	10.270980	49
12	674448	392	945125	113	729323	505	270677	48
13	674684	392	945058	113	729626	505	270374	47
14	674919	392	944990	113	729929	505	270071	46
15	675155	392	944922	113	730233	505	269767	45
16	675390	391	944854	113	730535	505	269465	44
17	675624	391	944786	113	730838	504	269162	43
18	675859	391	944718	113	731141	504	268859	42
19	676094	391	944650	113	731444	504	268556	41
20	676328	390	944582	114	731746	504	268254	40
21	9.676562	390	9.944514	114	9.732048	504	10.267952	39
22	676796	390	944446	114	732351	503	267649	38
23	677030	390	944377	114	732653	503	267347	37
24	677264	389	944309	114	732955	503	267045	36
25	677498	389	944241	114	733257	503	266743	35
26	677731	389	944172	114	733558	503	266442	34
27	677964	388	944104	114	733860	502	266140	33
28	678197	388	944036	114	734162	502	265838	32
29	678430	388	943967	114	734463	502	265537	31
30	678663	388	943899	114	734764	502	265236	30
31	9.678895	387	9.943830	114	9.735066	502	10.264931	29
32	679128	387	943761	114	735367	502	264633	28
33	679360	387	943693	115	735668	501	264332	27
34	679592	387	943624	115	735969	501	264031	26
35	679824	386	943555	115	736269	501	263731	25
36	680056	386	943486	115	736570	501	263430	24
37	680288	386	943417	115	736871	501	263129	23
38	680519	385	943348	115	737171	500	262829	22
39	680750	385	943279	115	737471	500	262529	21
40	680982	385	943210	115	737771	500	262229	20
41	9.681213	385	9.943141	115	9.738071	500	10.261929	19
42	681443	384	943072	115	738371	500	261629	18
43	681674	384	943003	115	738671	499	261329	17
44	681905	384	942934	115	738971	499	261029	16
45	682135	384	942864	115	739271	499	260729	15
46	682365	383	942795	116	739570	499	260430	14
47	682595	383	942726	116	739870	499	260130	13
48	682825	383	942656	116	740169	499	259831	12
49	683055	383	942587	116	740468	498	259532	11
50	683284	382	942517	116	740767	498	259233	10
51	9.683514	382	9.942448	116	9.741066	498	10.258934	9
52	683743	382	942378	116	741365	498	258635	.8
53	683972	382	942308	116	741664	498	258336	7
54	684201	381	942239	116	741962	497	258038	6
55	684430	381	942169	116	742261	497	257739	5
56	684658	381	942099	116	742559	497	257441	4
57	684887	380	942029	116	742858	497	257142	3
58	685115	380	941959	116	743156	497	256844	2
59	685343	380	941889	117	743454	497	256546	1
60	685571	380	941819	117	743752	496	256248	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.685571	380	9.941819	117	9.743752	496	10.256218	60
1	685799	379	941749	117	744050	496	255950	59
2	686027	379	941679	117	744348	496	255652	58
3	686254	379	941609	117	744645	496	255355	57
4	686482	379	941539	117	744943	496	255057	56
5	686709	378	941469	117	745240	496	254750	55
6	686936	378	941398	117	745538	495	254452	54
7	687163	378	941328	117	745835	495	254165	53
8	687389	378	941258	117	746132	495	253868	52
9	687616	377	941187	117	746429	495	253571	51
10	687843	377	941117	117	746726	495	253274	50
11	9.688069	377	9.941046	118	9.747023	494	10.252977	49
12	688295	377	940975	118	747319	494	252681	48
13	688521	376	940905	118	747616	494	252384	47
14	688747	376	940834	118	747913	494	252087	46
15	688972	376	940763	118	748209	494	251791	45
16	689198	376	940693	118	748505	493	251495	44
17	689423	375	940622	118	748801	493	251199	43
18	689648	375	940551	118	749097	493	250903	42
19	689873	375	940480	118	749393	493	250607	41
20	690098	375	940409	118	749689	493	250311	40
21	9.690323	374	9.940338	118	9.749985	493	10.250015	39
22	690548	374	940267	118	750281	492	249719	38
23	690772	374	940196	118	750576	492	249424	37
24	690996	374	940125	119	750872	492	249128	36
25	691220	373	940054	119	751167	492	248833	35
26	691444	373	939982	119	751462	492	248538	34
27	691668	373	939911	119	751757	492	248243	33
28	691892	373	939840	119	752052	491	247948	32
29	692115	372	939768	119	752347	491	247653	31
30	692339	372	939697	119	752642	491	247358	30
31	9.692562	372	9.939625	119	9.752937	491	10.247063	29
32	692785	371	939554	119	753231	491	246769	28
33	693008	371	939482	119	753526	491	246474	27
34	693231	371	939410	119	753820	490	246180	26
35	693453	371	939339	119	754115	490	245885	25
36	693676	370	939267	120	754409	490	245591	24
37	693898	370	939195	120	754703	490	245297	23
38	694120	370	939123	120	754997	490	245003	22
39	694342	370	939052	120	755291	490	244709	21
40	694564	369	938980	120	755585	489	244415	20
41	9.694786	369	9.938908	120	9.755878	489	10.244122	19
42	695007	369	938836	120	756172	489	243828	18
43	695229	369	938763	120	756465	489	243535	17
44	695450	368	938691	120	756759	489	243241	16
45	695671	368	938619	120	757052	489	242948	15
46	695892	368	938547	120	757345	488	242655	14
47	696113	368	938475	120	757638	488	242362	13
48	696334	367	938402	121	757931	488	242069	12
49	696554	367	938330	121	758224	488	241776	11
50	696775	367	938258	121	758517	488	241483	10
51	9.696995	367	9.938185	121	9.758810	488	10.241190	9
52	697215	366	938113	121	759102	487	240898	8
53	697435	366	938040	121	759395	487	240605	7
54	697654	366	937967	121	759687	487	240313	6
55	697874	366	937895	121	759979	487	240021	5
56	698094	365	937822	121	760272	487	239728	4
57	698313	365	937749	121	760564	487	239436	3
58	698532	365	937676	121	760856	486	239144	2
59	698751	365	937604	121	761148	486	238852	1
60	698970	364	937531	121	761439	486	238561	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.698970	364	9.937531	121	9.761439	486	10.238561	60
1	699189	364	937458	122	761731	486	238269	59
2	699407	364	937385	122	762023	486	237977	58
3	699626	364	937312	122	762314	486	237686	57
4	699844	363	937238	122	762606	485	237394	56
5	700062	363	937165	122	762897	485	237103	55
6	700280	363	937092	122	763188	485	236812	54
7	700498	363	937019	122	763479	485	236521	53
8	700716	363	936946	122	763770	485	236230	52
9	700933	362	936872	122	764061	485	235939	51
10	701151	362	936799	122	764352	484	235648	50
11	9.701368	362	9.936725	122	9.764643	484	10.235357	49
12	701585	362	936652	123	764933	484	235067	48
13	701802	361	936578	123	765224	484	234776	47
14	702019	361	936505	123	765514	484	234486	46
15	702236	361	936431	123	765805	484	234195	45
16	702452	361	936357	123	766095	484	233905	44
17	702669	360	936284	123	766385	483	233615	43
18	702885	360	936210	123	766675	483	233325	42
19	703101	360	936136	123	766965	483	233035	41
20	703317	360	936062	123	767255	483	232745	40
21	9.703533	359	9.935988	123	9.767545	483	10.232455	39
22	703749	359	935914	123	767834	483	232166	38
23	703964	359	935840	123	768124	482	231876	37
24	704179	359	935766	124	768413	482	231587	36
25	704395	359	935692	124	768703	482	231297	35
26	704610	358	935618	124	768992	482	231008	34
27	704825	358	935543	124	769281	482	230719	33
28	705040	358	935469	124	769570	482	230430	32
29	705254	358	935395	124	769860	481	230140	31
30	705469	357	935320	124	770148	481	229852	30
31	9.705683	357	9.935246	124	9.770437	481	10.229563	29
32	705898	357	935171	124	770726	481	229274	28
33	706112	357	935097	124	771015	481	228985	27
34	706326	356	935022	124	771303	481	228697	26
35	706539	356	934948	124	771592	481	228408	25
36	706753	356	934873	124	771880	480	228120	24
37	706967	356	934798	125	772168	480	227832	23
38	707180	355	934723	125	772457	480	227543	22
39	707393	355	934649	125	772745	480	227255	21
40	707606	355	934574	125	773033	480	226967	20
41	9.707819	355	9.934499	125	9.773321	480	10.226679	19
42	708032	354	934424	125	773608	479	226392	18
43	708245	354	934349	125	773896	479	226104	17
44	708458	354	934274	125	774184	479	225816	16
45	708670	354	934199	125	774471	479	225529	15
46	708882	353	934123	125	774759	479	225241	14
47	709094	353	934048	125	775046	479	224954	13
48	709306	353	933973	125	775333	479	224667	12
49	709518	353	933898	126	775621	478	224379	11
50	709730	353	933822	126	775908	478	224092	10
51	9.709941	352	9.933747	126	9.776195	478	10.223805	9
52	710153	352	933671	126	776482	478	223518	8
53	710364	352	933596	126	776769	478	223231	7
54	710575	352	933520	126	777055	478	222945	6
55	710786	351	933445	126	777342	478	222658	5
56	710997	351	933369	126	777628	477	222372	4
57	711208	351	933293	126	777915	477	222085	3
58	711419	351	933217	126	778201	477	221799	2
59	711629	350	933141	126	778487	477	221512	1
60	711839	350	933066	126	778774	477	221226	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
9	9 711839	350	9.933066	126	9.778774	477	10.221226	60
1	712050	350	932990	127	779060	477	220940	59
2	712260	350	932914	127	779346	176	220654	58
3	712469	349	932838	127	779632	476	220368	57
4	712679	349	932762	127	779918	476	220082	56
5	712889	349	932685	127	780203	476	219797	55
6	713098	349	932609	127	780489	476	219511	54
7	713308	349	932533	127	780775	476	219225	53
8	713517	348	932457	127	781060	476	218940	52
9	713726	348	932380	127	781346	475	218654	51
10	713935	348	932304	127	781631	475	218369	50
11	9.714144	348	9.932228	127	9.781916	475	10.218084	49
12	714352	347	932151	127	782201	475	217799	48
13	714561	347	932075	128	782486	475	217514	47
14	714769	347	931998	128	782771	475	217229	46
15	714978	347	931921	128	783056	475	216944	45
16	715186	347	931845	128	783341	475	216659	44
17	715394	346	931768	128	783626	474	216374	43
18	715602	346	931691	128	783910	474	216090	42
19	715809	346	931614	128	784195	474	215805	41
20	716017	346	931537	128	784479	474	215521	40
21	9.716224	345	9.931460	128	9.784764	474	10.215236	39
22	716432	345	931383	128	785048	474	214952	38
23	716639	345	931306	128	785332	473	214668	37
24	716846	345	931229	129	785616	473	214384	36
25	717053	345	931152	129	785900	473	214100	35
26	717259	344	931075	129	786184	473	213816	34
27	717466	344	930998	129	786468	473	213532	33
28	717673	344	930921	129	786752	473	213248	32
29	717879	344	930843	129	787036	473	212964	31
30	718085	343	930766	129	787319	472	212681	30
31	9.718291	343	9.930688	129	9.787603	472	10.212397	29
32	718497	343	930611	129	787886	472	212114	28
33	718703	343	930533	129	788170	472	211830	27
34	718909	343	930456	129	788453	472	211547	26
35	719114	342	930378	129	788736	472	211261	25
36	719320	342	930300	130	789019	472	210981	24
37	719525	342	930223	130	789302	471	210698	23
38	719730	342	930145	130	789585	471	210415	22
39	719935	341	930067	130	789868	471	210132	21
40	720140	341	929989	130	790151	471	209849	20
41	9.720345	341	9.929911	130	9.790433	471	10.209567	19
42	720549	341	929833	130	790716	471	209284	18
43	720754	340	929755	130	790999	471	209001	17
44	720958	340	929677	130	791281	471	208719	16
45	721162	340	929599	130	791563	470	208437	15
46	721366	340	929521	130	791846	470	208154	14
47	721570	340	929442	130	792128	470	207872	13
48	721774	339	929364	131	792410	470	207590	12
49	721978	339	929286	131	792692	470	207308	11
50	722181	339	929207	131	792974	470	207026	10
51	9.722385	339	9.929129	131	9.793256	470	10.206744	9
52	722588	339	929050	131	793538	469	206462	8
53	722791	338	928972	131	793819	469	206181	7
54	722994	338	928893	131	794101	469	205899	6
55	723197	338	928815	131	794383	469	205617	5
56	723400	338	928736	131	794664	469	205336	4
57	723603	337	928657	131	794945	469	205055	3
58	723805	337	928578	131	795227	469	204773	2
59	724007	337	928499	131	795508	468	204492	1
60	724210	337	928420	131	795789	468	204211	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.721210	337	9.928420	132	9.795789	468	10.204211	60
1	721412	337	928312	132	796070	468	203930	59
2	721614	336	928263	132	796351	468	203649	58
3	721816	336	928183	132	796632	468	203368	57
4	722017	336	928104	132	796913	468	203087	56
5	722219	336	928025	132	797194	468	202806	55
6	722420	335	927946	132	797475	468	202525	54
7	722622	335	927867	132	797755	468	202245	53
8	722823	335	927787	132	798036	467	201964	52
9	723024	335	927708	132	798316	467	201684	51
10	723225	335	927629	132	798596	467	201404	50
11	9.723426	334	9.927549	132	9.798877	467	10.201123	49
12	723626	334	927470	133	799157	467	200843	48
13	723827	334	927390	133	799437	467	200563	47
14	724027	334	927310	133	799717	467	200283	46
15	724228	334	927231	133	799997	466	200003	45
16	724428	333	927151	133	800277	466	199723	44
17	724628	333	927071	133	800557	466	199443	43
18	724828	333	926991	133	800836	466	199164	42
19	725027	333	926911	133	801116	466	198884	41
20	725227	333	926831	133	801396	466	198604	40
21	9.725427	332	9.926751	133	9.801675	466	10.198325	39
22	725626	332	926671	133	801955	466	198045	38
23	725825	332	926591	133	802234	465	197766	37
24	726024	332	926511	134	802513	465	197487	36
25	726223	331	926431	134	802792	465	197208	35
26	726422	331	926351	134	803072	465	196928	34
27	726621	331	926270	134	803351	465	196649	33
28	726820	331	926190	134	803630	465	196370	32
29	727018	330	926110	134	803908	465	196092	31
30	727216	330	926025	134	804187	465	195813	30
31	9.727415	330	9.925949	134	9.804466	464	10.195534	29
32	727613	330	925868	134	804745	464	195255	28
33	727811	330	925788	134	805023	464	194977	27
34	728009	329	925707	134	805302	464	194698	26
35	728206	329	925626	134	805580	464	194420	25
36	728404	329	925545	135	805859	464	194141	24
37	728602	329	925465	135	806137	464	193863	23
38	728800	329	925384	135	806415	463	193585	22
39	729000	328	925303	135	806693	463	193307	21
40	729203	328	925222	135	806971	463	193029	20
41	9.729400	328	9.925141	135	9.807249	463	10.192751	19
42	729597	328	925060	135	807527	463	192473	18
43	729794	328	924979	135	807805	463	192195	17
44	729990	327	924897	135	808083	463	191917	16
45	730187	327	924816	135	808361	463	191639	15
46	730383	327	924735	136	808638	462	191362	14
47	730580	327	924654	136	808916	462	191084	13
48	730775	327	924572	136	809193	462	190807	12
49	730971	326	924491	136	809471	462	190529	11
50	731167	326	924409	136	809748	462	190252	10
51	9.731353	326	9.924328	136	9.810025	462	10.189975	9
52	731549	325	924246	136	810302	462	189698	8
53	731744	325	924164	136	810580	462	189420	7
54	731939	325	924083	136	810857	462	189143	6
55	732135	325	924001	136	811134	461	188866	5
56	732330	325	923919	136	811410	461	188590	4
57	732525	325	923837	136	811687	461	188313	3
58	732719	324	923755	137	811964	461	188036	2
59	732914	324	923673	137	812241	461	187759	1
60	733109	324	923591	137	812517	461	187483	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang	D.	Cotang.	M.
0	9.736109	324	9.923591	137	9.812517	461	10.187482	60
1	736303	324	923509	137	812794	461	187206	59
2	736498	324	923427	137	913070	461	186930	58
3	736692	323	923345	137	813347	460	186653	57
4	736886	323	923263	137	813623	460	186377	56
5	737080	323	923181	137	813899	460	186101	55
6	737274	323	923098	137	814175	460	185825	54
7	737467	323	923016	137	814452	460	185548	53
8	737661	322	922933	137	814728	460	185272	52
9	737855	322	922851	137	815004	460	184996	51
10	738048	322	922768	138	815279	460	184721	50
11	9.738241	322	9.922686	138	9.815555	459	10.184445	49
12	738434	322	922603	138	815831	459	284169	48
13	738627	321	922520	138	816107	459	183893	47
14	738820	321	922438	138	816382	459	183618	46
15	739013	321	922355	138	816658	459	183342	45
16	739206	321	922272	138	816933	459	183067	44
17	739398	321	922189	138	817209	459	182791	43
18	739590	320	922106	138	817484	459	182516	42
19	739783	320	922023	138	817759	459	182241	41
20	739975	320	921940	138	818035	458	181965	40
21	9.740167	320	9.921857	139	9.818310	458	10.181690	39
22	740359	320	921774	139	818585	458	181415	38
23	740550	319	921691	139	818860	458	181140	37
24	740742	319	921607	139	819135	458	180865	36
25	740934	319	921524	139	819410	458	180590	35
26	741125	319	921441	139	819684	458	180316	34
27	741316	319	921357	139	819959	458	180041	33
28	741508	318	921274	139	820234	458	179766	32
29	741699	318	921190	139	820508	457	179492	31
30	741889	318	921107	139	820783	457	179217	30
31	9.742080	318	9.921023	139	9.821057	457	10.178943	29
32	742271	318	920939	140	821332	457	178668	28
33	742462	317	920856	140	821606	457	178394	27
34	742652	317	920772	140	821880	457	178120	26
35	742842	317	920688	140	822154	457	177846	25
36	743033	317	920604	140	822429	457	177571	24
37	743223	317	920520	140	822705	457	177297	23
38	743413	316	920436	140	822977	456	177023	22
39	743602	316	920352	140	823250	456	176750	21
40	743792	316	920268	140	823524	456	176476	20
41	9.743982	316	9.920184	140	9.823798	456	10.176202	19
42	744171	316	920099	140	824072	456	175928	18
43	744361	315	920015	140	824345	456	175655	17
44	744550	315	919931	141	824619	456	175381	16
45	744739	315	919846	141	824893	456	175107	15
46	744928	315	919762	141	825166	456	174834	14
47	745117	315	919677	141	825439	455	174561	13
48	745306	314	919593	141	825713	455	174287	12
49	745494	314	919508	141	825986	455	174014	11
50	745683	314	919424	141	826259	455	173741	10
51	9.745871	314	9.919339	141	9.826532	455	10.173468	9
52	746059	314	919254	141	826805	455	173195	8
53	746248	313	919169	141	827078	455	172922	7
54	746436	313	919085	141	827351	455	172649	6
55	746624	313	919000	141	827624	455	172376	5
56	746812	313	918915	142	827897	454	172103	4
57	746999	313	918830	142	828170	454	171830	3
58	747187	312	918745	142	828442	454	171558	2
59	747374	312	918659	142	828715	454	171285	1
60	747562	312	918574	142	828987	454	171013	0
	Cosine		Sine		Cotang.		Tang.	M.



M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.747502	3.2	9.918574	142	9.828887	454	10.177113	60
1	747519	312	918489	142	828790	454	170749	59
2	747536	312	918404	142	828692	454	170668	58
3	748123	311	918318	142	828595	454	170585	57
4	748139	311	918233	142	828497	454	169923	56
5	748197	311	918147	142	828399	453	169851	55
6	748283	311	918062	142	828301	453	69373	54
7	748379	311	917976	143	828203	453	139107	53
8	748456	310	917891	143	828105	453	168855	52
9	748443	310	917805	143	828007	453	168593	51
10	748429	310	917719	143	827909	453	168291	50
11	9.748515	310	9.917634	143	9.827811	453	10.168039	49
12	748591	310	917548	143	827713	453	167747	48
13	748587	309	917462	143	827615	453	167475	47
14	750172	309	917376	143	827517	453	167204	46
15	750358	309	917290	143	827419	452	166932	45
16	750513	309	917204	143	827321	452	166661	44
17	750729	309	917118	144	827223	452	166389	43
18	750644	308	917032	144	827125	452	166118	42
19	751099	308	916946	144	827027	452	165846	41
20	751284	308	916859	144	826929	452	165575	40
21	9.751430	308	9.916773	144	9.826831	452	10.165391	39
22	751634	308	916687	144	826733	452	165033	38
23	751839	308	916600	144	826635	452	164762	37
24	752023	307	916514	144	826537	452	164491	36
25	752298	307	916427	144	826439	451	164220	35
26	752392	307	916341	144	826341	451	163949	34
27	752576	307	916254	144	826243	451	163678	33
28	752759	307	916167	145	826145	451	163407	32
29	752944	305	916081	145	826047	451	163136	31
30	753128	306	915994	145	825949	451	162866	30
31	9.753312	306	9.915907	145	9.825851	451	10.162595	29
32	753495	306	915820	145	825753	451	162325	28
33	753679	306	915733	145	825655	451	162054	27
34	753862	305	915646	145	825557	451	161784	26
35	754046	305	915559	145	825459	450	161513	25
36	754229	305	915472	145	825361	450	161243	24
37	754412	305	915385	145	825263	450	160973	23
38	754595	305	915297	145	825165	450	160703	22
39	754778	304	915210	145	825067	450	160432	21
40	754960	304	915123	146	824969	450	160162	20
41	9.755143	304	9.915035	146	9.824871	450	10.159892	19
42	755326	304	914948	146	824773	450	159622	18
43	755508	304	914860	146	824675	450	159353	17
44	755590	304	914773	146	824577	449	159083	16
45	755872	303	914685	146	824479	449	158813	15
46	756054	303	914598	146	824381	449	158543	14
47	756236	303	914510	146	824283	449	158274	13
48	756418	303	914422	146	824185	449	158004	12
49	756600	303	914334	146	824087	449	157734	11
50	756782	302	914246	147	823989	449	157465	10
51	9.756963	302	9.914158	147	9.823891	449	10.157195	9
52	757144	302	914070	147	823801	449	156926	8
53	757326	302	913982	147	823703	449	156657	7
54	757507	302	913894	147	823605	449	156388	6
55	757688	301	913806	147	823507	448	156118	5
56	757869	301	913718	147	823409	448	155849	4
57	758050	301	913630	147	823311	448	155580	3
58	758230	301	913541	147	823213	448	155311	2
59	758411	301	913453	147	823115	448	155042	1
60	758591	301	913365	147	823017	448	154773	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (35 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.758591	301	9.913365	147	9.845227	448	10.154773	90
1	758772	300	913276	147	845496	448	154504	59
2	758952	300	913187	148	845764	448	154236	58
3	759132	300	913099	148	846033	448	153967	57
4	759312	300	913010	148	846302	448	153698	56
5	759492	300	912922	148	846570	447	153430	55
6	759672	299	912833	148	846839	447	153161	54
7	759852	299	912744	148	847107	447	152893	53
8	760031	299	912655	148	847376	447	152624	52
9	760211	299	912566	148	847644	447	152356	51
10	760390	299	912477	148	847913	447	152087	50
11	9.760569	298	9.912388	148	9.848181	447	10.151819	49
12	760748	298	912299	149	848449	447	151551	48
13	760927	298	912210	149	848717	447	151283	47
14	761106	298	912121	149	848986	447	151014	46
15	761285	298	912031	149	849254	447	150746	45
16	761464	298	911942	149	849522	447	150478	44
17	761642	297	911853	149	849790	446	150210	43
18	761821	297	911763	149	850058	446	149942	42
19	761999	297	911674	149	850325	446	149675	41
20	762177	297	911584	149	850593	446	149407	40
21	9.762356	297	9.911495	149	9.850861	446	10.149139	39
22	762534	296	911405	149	851129	446	148871	38
23	762712	296	911315	150	851396	446	148604	37
24	762899	296	911226	150	851664	446	148336	36
25	763067	296	911136	150	851931	446	148069	35
26	763245	296	911046	150	852199	446	147801	34
27	763422	296	910956	150	852466	446	147534	33
28	763600	295	910866	150	852733	445	147267	32
29	763777	295	910776	150	853001	445	146999	31
30	763954	295	910686	150	853268	445	146732	30
31	9.764131	295	9.910596	150	9.853535	445	10.146465	29
32	764308	295	910506	150	853802	445	146198	28
33	764485	294	910415	150	854069	445	145931	27
34	764662	294	910325	151	854336	445	145664	26
35	764838	294	910235	151	854603	445	145397	25
36	765015	294	910144	151	854870	445	145130	24
37	765191	294	910054	151	855137	445	144863	23
38	765367	294	909963	151	855404	445	144596	22
39	765544	293	909873	151	855671	444	144329	21
40	765720	293	909782	151	855938	444	144062	20
41	9.765896	293	9.909691	151	9.856201	444	10.143796	19
42	766072	293	909601	151	856471	444	143529	18
43	766247	293	909510	151	856737	444	143263	17
44	766423	293	909419	151	857004	444	142996	16
45	766598	292	909328	152	857270	444	142730	15
46	766774	292	909237	152	857537	444	142463	14
47	766949	292	909146	152	857803	444	142197	13
48	767124	292	909055	152	858069	444	141931	12
49	767300	292	908964	152	858336	444	141664	11
50	767475	291	908873	152	858602	443	141398	10
51	9.767649	291	9.908781	152	9.858868	443	10.141132	9
52	767824	291	908690	152	859134	443	140866	8
53	767999	291	908599	152	859400	443	140600	7
54	768173	291	908507	152	859666	443	140334	6
55	768348	290	908416	153	859932	443	140068	5
56	768522	290	908324	153	860198	443	139802	4
57	768697	290	908233	153	860464	443	139536	3
58	768871	290	908141	153	860730	443	139270	2
59	769045	290	908049	153	860995	443	139005	1
60	769219	290	907958	153	861261	443	138739	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Star	D	Coef.	D	Tang.	D	Corang.	
0	9.769219	290	9.907958	153	9.861261	413	10.138739 50	
1	769393	289	907866	153	861527	413	138473 59	
2	769566	289	907774	153	861792	442	138208 58	
3	769740	289	907682	153	862058	442	137942 57	
4	769913	289	907590	153	862323	442	137677 56	
5	770087	289	907498	153	862589	442	137411 55	
6	770260	288	907406	153	862854	442	137146 54	
7	770433	288	907314	154	863119	442	136881 53	
8	770606	288	907222	154	863385	442	136615 52	
9	770779	288	907129	154	863650	442	136350 51	
10	770952	288	907037	154	863915	442	136085 50	
11	9.771125	288	9.906915	154	9.864180	442	10.135820 49	
12	771298	287	906825	154	864445	442	135555 48	
13	771470	287	906733	154	864710	442	135290 47	
14	771643	287	906641	154	864975	441	135025 46	
15	771815	287	906549	154	865240	441	134760 45	
16	771987	287	906457	154	865505	441	134495 44	
17	772159	287	906365	155	865770	441	134230 43	
18	772331	286	906273	155	866035	441	133965 42	
19	772503	286	906181	155	866300	441	133700 41	
20	772675	286	906089	155	866565	441	133436 40	
21	9.772847	286	9.905018	155	9.866829	441	10.133171 39	
22	773018	286	905925	155	867094	441	132906 38	
23	773190	286	905833	155	867358	441	132642 37	
24	773361	285	905741	155	867623	441	132377 36	
25	773533	285	905649	155	867887	441	132113 35	
26	773704	285	905557	155	868152	440	131848 34	
27	773875	285	905465	155	868416	440	131584 33	
28	774046	285	905373	156	868680	440	131320 32	
29	774217	285	905281	156	868945	440	131055 31	
30	774388	284	905189	156	869209	440	130791 30	
31	9.774558	284	9.905085	156	9.869473	440	10.130527 29	
32	774729	284	904992	156	869737	440	130263 28	
33	774899	284	904898	156	870001	440	129999 27	
34	775070	284	904804	156	870265	440	129735 26	
35	775240	284	904711	156	870529	440	129471 25	
36	775410	283	904617	156	870793	440	129207 24	
37	775580	283	904523	156	871057	440	128943 23	
38	775750	283	904429	157	871321	440	128679 22	
39	775920	283	904335	157	871585	440	128415 21	
40	776090	283	904241	157	871849	439	128151 20	
41	9.776259	283	9.904147	157	9.872112	439	10.127888 19	
42	776429	282	904053	157	872376	439	127624 18	
43	776598	282	903959	157	872640	439	127360 17	
44	776768	282	903864	157	872903	439	127097 16	
45	776937	282	903770	157	873167	439	126833 15	
46	777106	282	903676	157	873430	439	126570 14	
47	777275	281	903581	157	873694	439	126306 13	
48	777444	281	903487	157	873957	439	126043 12	
49	777613	281	903392	158	874220	439	125780 11	
50	777781	281	903298	158	874484	439	125516 10	
51	9.777950	281	9.903203	158	9.874747	439	10.125253 9	
52	778119	281	903108	158	875010	439	124990 8	
53	778287	280	903014	158	875273	438	124727 7	
54	778455	280	902919	158	875536	438	124464 6	
55	778624	280	902824	158	875800	438	124200 5	
56	778792	280	902729	158	876063	438	123937 4	
57	778960	280	902634	158	876326	438	123674 3	
58	779128	280	902539	159	876589	438	123411 2	
59	779295	279	902444	159	876851	438	123149 1	
60	779463	279	902349	159	877114	438	122886 0	
	Coef.		Sine		Corang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.779163	279	9.902319	159	9.877114	438	10.122386	60
1	779631	279	902253	159	877377	438	122623	59
2	779798	279	902158	159	877610	438	122360	58
3	779956	279	902063	159	877903	438	122097	57
4	780133	279	901967	159	878165	438	121835	56
5	780300	278	901872	159	878428	438	121572	55
6	780467	278	901776	159	878691	438	121309	54
7	780634	278	901681	159	878953	437	121047	53
8	780801	278	901585	159	879216	437	120784	52
9	780968	278	901490	159	879478	437	120522	51
10	781134	278	901394	160	879741	437	120259	50
11	9.781301	277	9.901298	160	9.880003	437	10.119997	49
12	781468	277	901202	160	880265	437	119735	48
13	781634	277	901106	160	880528	437	119472	47
14	781800	277	901010	160	880790	437	119210	46
15	781966	277	900914	160	881052	437	118948	45
16	782132	277	900818	160	881314	437	118686	44
17	782298	276	900722	160	881576	437	118424	43
18	782464	276	900626	160	881839	437	118161	42
19	782630	276	900529	160	882101	437	117899	41
20	782796	276	900433	161	882363	436	117637	40
21	9.782961	274	9.900337	161	9.882625	436	10.117375	39
22	783127	276	900240	161	882887	436	117113	38
23	783292	275	900144	161	883148	436	116852	37
24	783458	275	900047	161	883410	436	116590	36
25	783623	275	899951	161	883672	436	116328	35
26	783788	275	899854	161	883934	436	116066	34
27	783953	275	899757	161	884196	436	115804	33
28	784118	275	899660	161	884457	436	115543	32
29	784282	274	899564	161	884719	436	115281	31
30	784447	274	899467	162	884980	436	115020	30
31	9.784612	274	9.899370	162	9.885242	436	10.114758	29
32	784776	274	899273	162	885503	436	114497	28
33	784941	274	899176	162	885765	436	114235	27
34	785105	274	899078	162	886026	436	113974	26
35	785269	273	898981	162	886288	436	113712	25
36	785433	273	898884	162	886549	435	113451	24
37	785597	273	898787	162	886810	435	113190	23
38	785761	273	898689	162	887072	435	112928	22
39	785925	273	898592	162	887333	435	112667	21
40	786089	273	898494	163	887594	435	112406	20
41	9.786252	272	9.898397	163	9.887855	435	10.112145	19
42	786416	272	898299	163	888116	435	111884	18
43	786579	272	898202	163	888377	435	111623	17
44	786742	272	898104	163	888639	435	111361	16
45	786906	272	898006	163	888900	435	111100	15
46	787069	272	897908	163	889160	435	110840	14
47	787232	271	897810	163	889421	435	110579	13
48	787395	271	897712	163	889682	435	110318	12
49	787557	271	897614	163	889943	435	110057	11
50	787720	271	897516	163	890204	434	109796	10
51	9.787883	271	9.897418	164	9.890465	434	10.109535	9
52	788045	271	897320	164	890725	434	109274	8
53	788208	271	897222	164	890986	434	109014	7
54	788370	270	897123	164	891247	434	108753	6
55	788532	270	897025	164	891507	434	108493	5
56	788694	270	896926	164	891768	434	108232	4
57	788856	270	896828	164	892028	434	107972	3
58	789018	270	896729	164	892289	434	107711	2
59	789180	270	896631	164	892549	434	107451	1
60	789342	269	896532	164	892810	434	107190	0
1	Cosine		Sine		Cotang.		Tang.	

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.789342	269	9.895532	164	9.892810	434	10.107190	60
1	789504	269	896433	165	893070	434	105930	59
2	789665	269	896335	165	893331	434	106569	58
3	789827	269	896236	165	893591	434	106409	57
4	789988	269	896137	165	893851	434	106149	56
5	790149	269	896038	165	894111	434	105889	55
6	790310	268	895939	165	894371	434	105629	54
7	790471	268	895840	165	894632	433	105368	53
8	790632	268	895741	165	894892	433	105108	52
9	790793	268	895641	165	895152	433	104848	51
10	790954	268	895542	165	895412	433	104588	50
11	9.791115	268	9.895443	166	9.895672	433	10.10328	49
12	791275	267	895343	166	895932	433	104068	48
13	791436	267	895244	166	896192	433	103808	47
14	791596	267	895145	166	896452	433	103548	46
15	791757	267	895045	166	896712	433	103288	45
16	791917	267	894945	166	896971	433	103029	44
17	792077	267	894846	166	897231	433	102769	43
18	792237	266	894746	166	897491	433	102509	42
19	792397	266	894646	166	897751	433	102249	41
20	792557	266	894546	166	898010	433	101990	40
21	9.792716	266	9.894446	167	9.898270	433	10.101730	39
22	792876	266	894346	167	898530	433	101470	38
23	793035	266	894246	167	898789	433	101211	37
24	793195	265	894146	167	899049	432	100951	36
25	793354	265	894046	167	899308	432	100692	35
26	793514	265	893946	167	899568	432	100432	34
27	793673	265	893846	167	899827	432	100173	33
28	793832	265	893745	167	900086	432	099914	32
29	793991	265	893645	167	900346	432	099654	31
30	794150	264	893544	167	900605	432	099395	30
31	9.794308	264	9.893444	168	9.900864	432	10.099136	29
32	794467	264	893343	168	901124	432	098876	28
33	794626	264	893243	168	901383	432	098617	27
34	794784	264	893142	168	901642	432	098358	26
35	794942	264	893041	168	901901	432	098099	25
36	795101	264	892940	168	902160	432	097840	24
37	795259	263	892839	168	902419	432	097581	23
38	795417	263	892739	168	902679	432	097321	22
39	795575	263	892638	168	902938	432	097062	21
40	795733	263	892536	168	903197	431	096803	20
41	9.795891	263	9.892435	169	9.903455	431	10.096545	19
42	796049	263	892334	169	903714	431	096285	18
43	796206	263	892233	169	903973	431	096027	17
44	796364	262	892132	169	904232	431	095768	16
45	796521	262	892030	169	904491	431	095509	15
46	796679	262	891929	169	904750	431	095250	14
47	796836	262	891827	169	905008	431	094992	13
48	796993	262	891726	169	905267	431	094733	12
49	797150	261	891624	169	905526	431	094474	11
50	797307	261	891523	170	905784	431	094216	10
51	9.797464	261	9.891421	170	9.906043	431	10.093957	9
52	797621	261	891319	170	906302	431	093698	8
53	797777	261	891217	170	906560	431	093440	7
54	797934	261	891115	170	906819	431	093181	6
55	798091	261	891013	170	907077	431	092923	5
56	798247	261	890911	170	907336	431	092664	4
57	798403	260	890809	170	907594	431	092406	3
58	798560	260	890707	170	907852	431	092148	2
59	798716	260	890605	170	908111	430	091889	1
60	798872	260	890503	170	908369	430	091631	0
	Cosine		Sine		Cotang.		Tang.	M.

M.	Sine.	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.798872	260	9.890503	170	9.908369	430	10.091631	60
1	799028	260	890400	171	908628	430	091372	59
2	799184	260	890298	171	908886	430	091114	58
3	799339	259	890195	171	909144	430	090856	57
4	799495	259	890093	171	909402	430	090598	56
5	799651	259	889990	171	909660	430	090340	55
6	799806	259	889888	171	909918	430	090082	54
7	799962	259	889785	171	910177	430	089823	53
8	800117	259	889682	171	910435	430	089565	52
9	800272	258	889579	171	910693	430	089307	51
10	800427	258	889477	171	910951	430	089049	50
11	9.800582	258	9.889374	172	9.911209	430	10.088791	49
12	800737	258	889271	172	911467	430	088533	48
13	800892	258	889168	172	911724	430	088276	47
14	801047	258	889064	172	911982	430	088018	46
15	801201	258	888961	172	912240	430	087760	45
16	801356	257	888858	172	912498	430	087502	44
17	801511	257	888755	172	912756	430	087244	43
18	801665	257	888651	172	913014	429	086986	42
19	801819	257	888548	172	913271	429	086729	41
20	801973	257	888444	173	913529	429	086471	40
21	9.802128	257	9.888341	173	9.913787	429	10.086213	39
22	802282	256	888237	173	914044	429	085956	38
23	802436	256	888134	173	914302	429	085698	37
24	802589	256	888030	173	914560	429	085440	36
25	802743	256	887926	173	914817	429	085183	35
26	802897	256	887822	173	915075	429	084925	34
27	803050	256	887718	173	915332	429	084668	33
28	803204	256	887614	173	915590	429	084410	32
29	803357	255	887510	173	915847	429	084153	31
30	803511	255	887406	174	916104	429	083896	30
31	9.803664	255	9.887302	174	9.916362	429	10.083638	29
32	803817	255	887198	174	916619	429	083381	28
33	803970	255	887093	174	916877	429	083123	27
34	804123	255	886989	174	917134	429	082866	26
35	804276	254	886885	174	917391	429	082609	25
36	804428	254	886778	174	917648	429	082352	24
37	804581	254	886666	174	917905	429	082095	23
38	804734	254	886571	174	918163	428	081837	22
39	804886	254	886466	174	918420	428	081580	21
40	805039	254	886362	175	918677	428	081323	20
41	9.805191	254	9.886257	175	9.918934	428	10.081066	19
42	805343	253	886152	175	919191	428	080809	18
43	805495	253	886047	175	919448	428	080552	17
44	805647	253	885942	175	919705	428	080295	16
45	805799	253	885837	175	919962	428	080038	15
46	805951	253	885732	175	920219	428	079781	14
47	806103	253	885627	175	920476	428	079524	13
48	806254	253	885522	175	920733	428	079267	12
49	806406	252	885416	175	920990	428	079010	11
50	806557	252	885311	176	921247	428	078753	10
51	9.806709	252	9.885205	176	9.921503	428	10.078497	9
52	806860	252	885100	176	921760	428	078240	8
53	807011	252	884994	176	922017	428	077983	7
54	807163	252	884889	176	922274	428	077726	6
55	807314	252	884783	176	922530	428	077470	5
56	807465	251	884677	176	922787	428	077213	4
57	807615	251	884572	176	923044	428	076956	3
58	807766	251	884466	176	923300	428	076700	2
59	807917	251	884360	176	923557	427	076443	1
60	808067	251	884254	177	923813	427	076187	0
	Cosine		Sine		Co.ang.		Tang.	M.

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.808067	251	9.884254	177	9.923913	427	10.076187	60
1	808218	251	884148	177	924070	427	075930	59
2	808368	251	884042	177	924327	427	075673	58
3	808519	250	883936	177	924583	427	075417	57
4	808669	250	883829	177	924840	427	075160	56
5	808819	250	883723	177	925096	427	074904	55
6	808969	250	883617	177	925352	427	074648	54
7	809119	250	883510	177	925609	427	074391	53
8	809269	250	883404	177	925865	427	074135	52
9	809419	249	883297	178	926122	427	073878	51
10	809569	249	883191	178	926378	427	073622	50
11	9.809718	249	9.883084	178	9.926634	427	10.073366	49
12	809868	249	882977	178	925990	427	073110	48
13	810017	249	882871	178	927147	427	072853	47
14	810167	249	882764	178	927403	427	072597	46
15	810316	248	882657	178	927659	427	072341	45
16	810465	248	882550	178	927915	427	072085	44
17	810614	248	882443	178	928171	427	071829	43
18	810763	248	882336	179	928427	427	071573	42
19	810912	248	882229	179	928683	427	071317	41
20	811061	248	882121	179	928940	427	071060	40
21	9.811210	248	9.882014	179	9.929196	427	10.070804	39
22	811358	247	881907	179	929452	427	070548	38
23	811507	247	881799	179	929708	427	070292	37
24	811655	247	881692	179	929964	426	070036	36
25	811804	247	881584	179	930220	426	069780	35
26	811952	247	881477	179	930475	426	069525	34
27	812100	247	881369	179	930731	426	069269	33
28	812248	247	881261	180	930987	426	069013	32
29	812396	246	881153	180	931243	426	068757	31
30	812544	246	881046	180	931499	426	068501	30
31	9.812692	246	9.880938	180	9.931755	426	10.068245	29
32	812840	246	880830	180	932010	426	067990	28
33	812988	246	880722	180	932266	426	067734	27
34	813135	246	880613	180	932522	426	067478	26
35	813283	246	880505	180	932778	426	067222	25
36	813430	245	880397	180	933033	426	066967	24
37	813578	245	880289	181	933289	426	066711	23
38	813725	245	880180	181	933545	426	066455	22
39	813872	245	880072	181	933800	426	066200	21
40	814019	245	879963	181	934056	426	065944	20
41	9.814166	245	9.879855	181	9.934311	426	10.065689	19
42	814313	245	879746	181	934567	426	065433	18
43	814460	244	879637	181	934823	426	065177	17
44	814607	244	879529	181	935078	426	064922	16
45	814753	244	879420	181	935333	426	064667	15
46	814900	244	879311	181	935589	426	064411	14
47	815046	244	879202	182	935844	426	064156	13
48	815193	244	879093	182	936100	426	063900	12
49	815339	244	878984	182	936355	426	063645	11
50	815485	243	878875	182	936610	426	063390	10
51	9.815631	243	9.878766	182	9.936866	425	10.063134	9
52	815778	243	878656	182	937121	425	062879	8
53	815924	243	878547	182	937376	425	062624	7
54	816069	243	878438	182	937632	425	062368	6
55	816215	243	878328	182	937887	425	062113	5
56	816361	243	878219	183	938142	425	061858	4
57	816507	242	878109	183	938398	425	061602	3
58	816652	242	877999	183	938653	425	061347	2
59	816798	242	877890	183	938908	425	061092	1
60	816943	242	877780	183	939163	425	060837	0
	Cosine		Sine		Cotang.		Tang.	M.

SINES AND TANGENTS. (41 Degrees.)

M.	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.816943	242	9.877780	183	9.939163	425	10.060837	60
1	817088	242	877670	183	939418	425	060582	59
2	817233	242	877560	183	939673	425	060327	58
3	817379	242	877450	183	939928	425	060072	57
4	817524	241	877340	183	940183	425	059817	56
5	817668	241	877230	184	940438	425	059562	55
6	817813	241	877120	184	940694	425	059306	54
7	817958	241	877010	184	940949	425	059051	53
8	818103	241	876899	184	941204	425	058796	52
9	818247	241	876789	184	941458	425	058542	51
10	818392	241	876678	184	941714	425	058286	50
11	9.818536	240	9.876568	184	9.941968	425	10.058032	49
12	818681	240	876457	184	942223	425	057777	48
13	818825	240	876347	184	942478	425	057522	47
14	818969	240	876236	185	942733	425	057267	46
15	819113	240	876125	185	942988	425	057012	45
16	819257	240	876014	185	943243	425	056757	44
17	819401	240	875904	185	943498	425	056502	43
18	819545	239	875793	185	943752	425	056248	42
19	819689	239	875682	185	944007	425	055993	41
20	819832	239	875571	185	944262	425	055738	40
21	9.819976	239	9.875459	185	9.944517	425	10.055483	39
22	820120	239	875348	185	944771	424	055229	38
23	820263	239	875237	185	945026	424	054974	37
24	820406	239	875126	186	945281	424	054719	36
25	820550	238	875014	186	945535	424	054465	35
26	820693	238	874903	186	945790	424	054210	34
27	820836	238	874791	186	946045	424	053955	33
28	820979	238	874680	186	946299	424	053701	32
29	821122	238	874568	186	946554	424	053446	31
30	821265	238	874456	186	946808	424	053192	30
31	9.821407	238	9.874344	186	9.947063	424	10.052937	29
32	821550	238	874232	187	947318	424	052682	28
33	821693	237	874121	187	947572	424	052428	27
34	821835	237	874009	187	947826	424	052174	26
35	821977	237	873896	187	948081	424	051919	25
36	822120	237	873784	187	948336	424	051664	24
37	822262	237	873672	187	948590	424	051410	23
38	822404	237	873560	187	948844	424	051156	22
39	822546	237	873448	187	949099	424	050901	21
40	822688	236	873335	187	949353	424	050647	20
41	9.822830	236	9.873223	187	9.949607	424	10.050393	19
42	822972	236	873110	188	949862	424	050138	18
43	823114	236	872998	188	950116	424	049884	17
44	823255	236	872885	188	950370	424	049630	16
45	823397	236	872772	188	950625	424	049375	15
46	823539	236	872659	188	950879	424	049121	14
47	823680	235	872547	188	951133	424	048867	13
48	823821	235	872434	188	951388	424	048612	12
49	823963	235	872321	188	951642	424	048358	11
50	824104	235	872208	188	951896	424	048104	10
51	9.824245	235	9.872095	189	9.952150	424	10.047850	9
52	824386	235	871981	189	952405	424	047595	8
53	824527	235	871868	189	952659	424	047341	7
54	824668	234	871755	189	952913	424	047087	6
55	824808	234	871641	189	953167	423	046833	5
56	824949	234	871528	189	953421	423	046579	4
57	825090	234	871414	189	953675	423	046325	3
58	825230	234	871301	189	953929	423	046071	2
59	825371	234	871187	189	954183	423	045817	1
60	825511	234	871073	190	954437	423	045563	0
	Cosine		Sine		Cotang.		Tang.	M.



M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	M.
0	9.825511	234	9.871073	190	9.954437	423	10.045563	60
1	825651	233	870960	190	954691	423	045309	59
2	825791	233	870846	190	954945	423	045055	58
3	825931	233	870732	190	955200	423	044800	57
4	826071	233	870618	190	955454	423	044546	56
5	826211	233	870504	190	955707	423	044293	55
6	826351	233	870390	190	955961	423	044039	54
7	826491	233	870276	190	956215	423	043785	53
8	826631	233	870161	190	956469	423	043531	52
9	826770	232	870047	191	956723	423	043277	51
10	826910	232	869933	191	956977	423	043023	50
11	9.827049	232	9.869818	191	9.957231	423	10.042769	49
12	827189	232	869704	191	957485	423	042515	48
13	827328	232	869589	191	957739	423	042261	47
14	827467	232	869474	191	957993	423	042007	46
15	827606	232	869360	191	958246	423	041754	45
16	827745	232	869245	191	958500	423	041500	44
17	827884	231	869130	191	958754	423	041246	43
18	828023	231	869015	192	959008	423	040992	42
19	828162	231	868900	192	959262	423	040738	41
20	828301	231	868785	192	959516	423	040484	40
21	9.828439	231	9.868670	192	9.959769	423	10.040231	39
22	828578	231	868555	192	960023	423	039977	38
23	828716	231	868440	192	960277	423	039723	37
24	828855	230	868324	192	960531	423	039469	36
25	828993	230	868209	192	960784	423	039216	35
26	829131	230	868093	192	961038	423	038962	34
27	829269	230	867978	193	961291	423	038709	33
28	829407	230	867862	193	961545	423	038455	32
29	829545	230	867747	193	961799	423	038201	31
30	829683	230	867631	193	962052	423	037948	30
31	9.829821	229	9.867515	193	9.962306	423	10.037694	29
32	829959	229	867399	193	962560	423	037440	28
33	830097	229	867283	193	962813	423	037187	27
34	830234	229	867167	193	963067	423	036933	26
35	830372	229	867051	193	963320	423	036680	25
36	830509	229	866935	194	963574	423	036426	24
37	830646	229	866819	194	963827	423	036173	23
38	830784	229	866703	194	964081	423	035919	22
39	830921	228	866586	194	964335	423	035665	21
40	831058	228	866470	194	964588	422	035412	20
41	9.831195	228	9.866353	194	9.964842	422	10.035158	19
42	831332	228	866237	194	965095	422	034905	18
43	831469	228	866120	194	965349	422	034651	17
44	831606	228	866004	195	965602	422	034398	16
45	831742	228	865887	195	965855	422	034145	15
46	831879	228	865770	195	966109	422	033891	14
47	832015	227	865653	195	966362	422	033638	13
48	832152	227	865536	195	966616	422	033384	12
49	832288	227	865419	195	966869	422	033131	11
50	832425	227	865302	195	967123	422	032877	10
51	9.832561	227	9.865185	195	9.967376	422	10.032624	9
52	832697	227	865068	195	967629	422	032371	8
53	832833	227	864950	195	967883	422	032117	7
54	832969	226	864833	196	968136	422	031864	6
55	833105	226	864716	196	968389	422	031611	5
56	833241	226	864598	196	968643	422	031357	4
57	833377	226	864481	196	968896	422	031104	3
58	833512	226	864363	196	969149	422	030851	2
59	833648	226	864245	196	969403	422	030597	1
60	833783	226	864127	196	969656	422	030344	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Sine.	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.833783	226	9.864127	196	9.969656	422	10.030344	60
1	833919	225	864010	196	969909	422	030091	59
2	834054	225	863892	197	970162	422	029838	58
3	834189	225	863774	197	970416	422	029584	57
4	834325	225	863656	197	970669	422	029331	56
5	834460	225	863538	197	970922	422	029078	55
6	834595	225	863419	197	971175	422	028825	54
7	834730	225	863301	197	971429	422	028571	53
8	834865	225	863183	197	971682	422	028318	52
9	834999	224	863064	197	971935	422	028065	51
10	835134	224	862946	198	972188	422	027812	50
11	9.835269	224	9.862827	198	9.972441	422	10.027559	49
12	835403	224	862709	198	972694	422	027306	48
13	835538	224	862590	198	972948	422	027052	47
14	835672	224	862471	198	973201	422	026799	46
15	835807	224	862353	198	973454	422	026546	45
16	835941	224	862234	198	973707	422	026293	44
17	836075	223	862115	198	973960	422	026040	43
18	836209	223	861996	198	974213	422	025787	42
19	836343	223	861877	198	974466	422	025534	41
20	836477	223	861758	199	974719	422	025281	40
21	9.836611	223	9.861638	199	9.974973	422	10.025027	39
22	836745	223	861519	199	975226	422	024774	38
23	836878	223	861400	199	975479	422	024521	37
24	837012	222	861280	199	975732	422	024268	36
25	837146	222	861161	199	975985	422	024015	35
26	837279	222	861041	199	976238	422	023762	34
27	837412	222	860922	199	976491	422	023509	33
28	837546	222	860802	199	976744	422	023256	32
29	837679	222	860682	200	976997	422	023003	31
30	837812	222	860562	200	977250	422	022750	30
31	9.837945	222	9.860442	200	9.977503	422	10.022497	29
32	838078	221	860322	200	977756	422	022244	28
33	838211	221	860202	200	978009	422	021991	27
34	838344	221	860082	200	978262	422	021738	26
35	838477	221	859962	200	978515	422	021485	25
36	838610	221	859842	200	978768	422	021232	24
37	838742	221	859721	201	979021	422	020979	23
38	838875	221	859601	201	979274	422	020726	22
39	839007	221	859480	201	979527	422	020473	21
40	839140	220	859360	201	979780	422	020220	20
41	9.839272	220	9.859239	201	9.980033	422	10.019967	19
42	839404	220	859119	201	980286	422	019714	18
43	839536	220	858998	201	980538	422	019462	17
44	839668	220	858877	201	980791	421	019209	16
45	839800	220	858756	202	981044	421	018956	15
46	839932	220	858635	202	981297	421	018703	14
47	840064	219	858514	202	981550	421	018450	13
48	840196	219	858393	202	981803	421	018197	12
49	840328	219	858272	202	982056	421	017944	11
50	840459	219	858151	202	982309	421	017691	10
51	9.840591	219	9.858029	202	9.982562	421	10.017438	9
52	840722	219	857908	202	982814	421	017186	8
53	840854	219	857786	202	983067	421	016933	7
54	840985	219	857665	203	983320	421	016680	6
55	841116	218	857543	203	983573	421	016427	5
56	841247	218	857422	203	983826	421	016174	4
57	841378	218	857300	203	984079	421	015921	3
58	841509	218	857178	203	984331	421	015669	2
59	841640	218	857056	203	984584	421	015416	1
60	841771	218	856934	203	984837	421	015163	0
	Cosine		Sine		Cotang.		Tang.	M.

M	Sine	D.	Cosine	D.	Tang.	D.	Cotang.	
0	9.841771	218	9.856934	203	9.984837	421	10.015163	60
1	841902	218	856812	203	985090	421	014910	59
2	842033	218	856690	204	985343	421	014657	58
3	842163	217	856568	204	985596	421	014404	57
4	842294	217	856446	204	985848	421	014152	56
5	842424	217	856323	204	986101	421	013999	55
6	842555	217	856201	204	986354	421	013646	54
7	842685	217	856078	204	986607	421	013393	53
8	842815	217	855956	204	986860	421	013140	52
9	842946	217	855833	204	987112	421	012888	51
10	843076	217	855711	205	987365	421	012635	50
11	9.843206	216	9.855588	205	9.987618	421	10.012382	49
12	843336	216	855465	205	987871	421	012129	48
13	843466	216	855342	205	988123	421	011877	47
14	843595	216	855219	205	988376	421	011624	46
15	843725	216	855096	205	988629	421	011371	45
16	843855	216	854973	205	988882	421	011118	44
17	843984	216	854850	205	989134	421	010866	43
18	844114	215	854727	206	989387	421	010613	42
19	844243	215	854603	206	989640	421	010360	41
20	844372	215	854480	206	989893	421	010107	40
21	9.844502	215	9.854356	206	9.990145	421	10.009855	39
22	844631	215	854233	206	990398	421	009602	38
23	844760	215	854109	206	990651	421	009349	37
24	844889	215	853986	206	990903	421	009097	36
25	845018	215	853862	206	991156	421	008844	35
26	845147	215	853738	206	991409	421	008591	34
27	845276	214	853614	207	991662	421	008338	33
28	845405	214	853490	207	991914	421	008086	32
29	845533	214	853366	207	992167	421	007833	31
30	845662	214	853242	207	992420	421	007580	30
31	9.845790	214	9.853118	207	9.992672	421	10.007328	29
32	845919	214	852994	207	992925	421	007075	28
33	846047	214	852869	207	993178	421	006822	27
34	846175	214	852745	207	993430	421	006570	26
35	846304	214	852620	207	993683	421	006317	25
36	846432	213	852496	208	993936	421	006064	24
37	846560	213	852371	208	994189	421	005811	23
38	846688	213	852247	208	994441	421	005559	22
39	846816	213	852122	208	994694	421	005306	21
40	846944	213	851997	208	994947	421	005053	20
41	9.847071	213	9.851872	208	9.995199	421	10.004801	19
42	847199	213	851747	208	995452	421	004548	18
43	847327	213	851622	208	995705	421	004295	17
44	847454	212	851497	209	995957	421	004043	16
45	8 7582	212	851372	209	996210	421	003790	15
46	7709	212	851246	209	996463	421	003537	14
47	847836	212	851121	209	996715	421	003285	13
48	847964	212	850996	209	996968	421	003032	12
49	848091	212	850870	209	997221	421	002779	11
50	848218	212	850745	209	997473	421	002527	10
51	9.848345	212	9.850619	209	9.997726	421	10.002271	9
52	848472	211	850493	210	997979	421	002021	8
53	848599	211	850368	210	998231	421	001769	7
54	848726	211	850242	210	998484	421	001516	6
55	848852	211	850116	210	998737	421	001263	5
56	848979	211	849990	210	998989	421	001011	4
57	849106	211	849864	210	999242	421	000758	3
58	849232	211	849738	210	999495	421	000505	2
59	849359	211	849611	210	999748	421	000253	1
60	849485	211	849485	210	10.000000	421	000000	0
	Cosine		Sine		Cotang.		Tang.	M.

# A TABLE OF NATURAL SINES.

M	0 Deg.		1 Deg.		2 Deg.		3 Deg.		4 Deg.		M
	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	
0	00000	Unit.	01745	99985	03490	99939	05234	99863	06976	99756	60
1	00029	00000	01774	99984	03519	99938	05263	99861	07005	99754	59
2	00058	00000	01803	99984	03548	99937	05292	99860	07034	99752	58
3	00087	00000	01832	99983	03577	99936	05321	99858	07063	99750	57
4	00116	00000	01862	99983	03606	99935	05350	99857	07092	99748	56
5	00145	00000	01891	99982	03635	99934	05379	99855	07121	99746	55
6	00175	00000	01920	99982	03664	99933	05408	99854	07150	99744	54
7	00204	00000	01949	99981	03693	99932	05437	99852	07179	99742	53
8	00233	00000	01978	99980	03723	99931	05466	99851	07208	99740	52
9	00262	00000	02007	99980	03752	99930	05495	99849	07237	99738	51
10	00291	00000	02036	99979	03781	99929	05524	99847	07266	99736	50
11	00320	99999	02065	99979	03810	99927	05553	99846	07295	99734	49
12	00349	99999	02094	99978	03839	99926	05582	99844	07324	99731	48
13	00378	99999	02123	99977	03868	99925	05611	99842	07353	99729	47
14	00407	99999	02152	99977	03897	99924	05640	99841	07382	99727	46
15	00436	99999	02181	99976	03926	99923	05669	99839	07411	99725	45
16	00465	99999	02211	99976	03955	99922	05698	99838	07440	99723	44
17	00495	99999	02240	99975	03984	99921	05727	99836	07469	99721	43
18	00524	99999	02269	99974	04013	99919	05756	99834	07498	99719	42
19	00553	99998	02298	99974	04042	99918	05785	99833	07527	99716	41
20	00582	99998	02327	99973	04071	99917	05814	99831	07556	99714	40
21	00611	99998	02356	99972	04100	99916	05843	99829	07585	99712	39
22	00640	99998	02385	99972	04129	99915	05873	99827	07614	99710	38
23	00669	99998	02414	99971	04159	99913	05902	99826	07643	99708	37
24	00698	99998	02443	99970	04188	99912	05931	99824	07672	99705	36
25	00727	99997	02472	99969	04217	99911	05960	99822	07701	99703	35
26	00756	99997	02501	99969	04246	99910	05989	99821	07730	99701	34
27	00785	99997	02530	99968	04275	99909	06018	99819	07759	99699	33
28	00814	99997	02560	99967	04304	99907	06047	99817	07788	99696	32
29	00844	99996	02589	99966	04333	99906	06076	99815	07817	99694	31
30	00873	99996	02618	99966	04362	99905	06105	99813	07846	99692	30
31	00902	99996	02647	99965	04391	99904	06134	99812	07875	99689	29
32	00931	99996	02676	99964	04420	99902	06163	99810	07904	99687	28
33	00960	99995	02705	99963	04449	99901	06192	99808	07933	99685	27
34	00989	99995	02734	99963	04478	99900	06221	99806	07962	99683	26
35	01018	99995	02763	99962	04507	99898	06250	99804	07991	99680	25
36	01047	99995	02792	99961	04536	99897	06279	99803	08020	99678	24
37	01076	99994	02821	99960	04565	99896	06308	99801	08049	99676	23
38	01105	99994	02850	99959	04594	99894	06337	99799	08078	99673	22
39	01134	99994	02879	99959	04623	99893	06366	99797	08107	99671	21
40	01164	99993	02908	99958	04653	99892	06395	99795	08136	99668	20
41	01193	99993	02938	99957	04682	99890	06424	99793	08165	99666	19
42	01222	99993	02967	99956	04711	99889	06453	99792	08194	99664	18
43	01251	99992	02996	99955	04740	99888	06482	99790	08223	99661	17
44	01280	99992	03025	99954	04769	99886	06511	99788	08252	99659	16
45	01309	99991	03054	99953	04798	99885	06540	99786	08281	99657	15
46	01338	99991	03083	99952	04827	99883	06569	99784	08310	99654	14
47	01367	99991	03112	99952	04856	99882	06598	99782	08339	99652	13
48	01396	99990	03141	99951	04885	99881	06627	99780	08368	99649	12
49	01425	99990	03170	99950	04914	99879	06656	99778	08397	99647	11
50	01454	99989	03199	99949	04943	99878	06685	99776	08426	99644	10
51	01483	99989	03228	99948	04972	99876	06714	99774	08455	99642	9
52	01513	99989	03257	99947	05001	99875	06743	99772	08484	99639	8
53	01542	99988	03286	99946	05030	99873	06773	99770	08513	99637	7
54	01571	99988	03316	99945	05059	99872	06802	99768	08542	99635	6
55	01600	99987	03345	99944	05088	99870	06831	99766	08571	99632	5
56	01629	99987	03374	99943	05117	99869	06860	99764	08600	99630	4
57	01658	99986	03403	99942	05146	99867	06889	99762	08629	99627	3
58	01687	99986	03432	99941	05175	99866	06918	99760	08658	99625	2
59	01716	99985	03461	99940	05205	99864	06947	99758	08687	99622	1
M	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	N. Co-Sine	Nat. Sine	M
	89 Deg.		88 Deg.		87 Deg.		86 Deg.		85 Deg.		

A TABLE OF NATURAL SINES.

M	5 Deg.		6 Deg.		7 Deg.		8 Deg.		9 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	08716	99619	10453	99452	12187	99255	13917	99027	15643	98769	60
1	08745	99617	10482	99449	12216	99251	13946	99023	15672	98764	59
2	08774	99614	10511	99446	12245	99248	13975	99019	15701	98760	58
3	08803	99612	10540	99443	12274	99244	14004	99015	15730	98755	57
4	08831	99609	10569	99440	12302	99240	14033	99011	15758	98751	56
5	08860	99607	10597	99437	12331	99237	14061	99006	15787	98746	55
6	08889	99604	10626	99434	12360	99233	14090	99002	15816	98741	54
7	08918	99602	10655	99431	12389	99230	14119	98998	15845	98737	53
8	08947	99599	10684	99428	12418	99226	14148	98994	15873	98732	52
9	08976	99596	10713	99424	12447	99222	14177	98990	15902	98728	51
10	09005	99594	10742	99421	12476	99219	14205	98986	15931	98723	50
11	09034	99591	10771	99418	12504	99215	14234	98982	15959	98718	49
12	09063	99588	10800	99415	12533	99211	14263	98978	15988	98714	48
13	09092	99586	10829	99412	12562	99208	14292	98973	16017	98709	47
14	09121	99583	10858	99409	12591	99204	14320	98969	16046	98704	46
15	09150	99580	10887	99406	12620	99200	14349	98965	16074	98700	45
16	09179	99578	10916	99402	12649	99197	14378	98961	16103	98695	44
17	09208	99575	10945	99399	12678	99193	14407	98957	16132	98690	43
18	09237	99572	10973	99396	12706	99189	14436	98953	16160	98686	42
19	09266	99570	11002	99393	12735	99186	14464	98948	16189	98681	41
20	09295	99567	11031	99390	12764	99182	14493	98944	16218	98676	40
21	09324	99564	11060	99386	12793	99178	14522	98940	16246	98671	39
22	09353	99562	11089	99383	12822	99175	14551	98936	16275	98667	38
23	09382	99559	11118	99380	12851	99171	14580	98931	16304	98662	37
24	09411	99556	11147	99377	12880	99167	14608	98927	16333	98657	36
25	09440	99553	11176	99374	12908	99163	14637	98923	16361	98652	35
26	09469	99551	11205	99370	12937	99160	14666	98919	16390	98648	34
27	09498	99548	11234	99367	12966	99156	14695	98914	16419	98643	33
28	09527	99545	11263	99364	12995	99152	14723	98910	16447	98638	32
29	09556	99542	11291	99360	13024	99148	14752	98906	16476	98633	31
30	09585	99540	11320	99357	13053	99144	14781	98902	16505	98629	30
31	09614	99537	11349	99354	13081	99141	14810	98897	16533	98624	29
32	09642	99534	11378	99351	13110	99137	14838	98893	16562	98619	28
33	09671	99531	11407	99347	13139	99133	14867	98889	16591	98614	27
34	09700	99528	11436	99344	13168	99129	14896	98884	16620	98609	26
35	09729	99526	11465	99341	13197	99125	14925	98880	16648	98604	25
36	09758	99523	11494	99337	13226	99122	14954	98876	16677	98600	24
37	09787	99520	11523	99334	13254	99118	14982	98871	16706	98595	23
38	09816	99517	11552	99331	13283	99114	15011	98867	16734	98590	22
39	09845	99514	11580	99327	13312	99110	15040	98863	16763	98585	21
40	09874	99511	11609	99324	13341	99106	15069	98858	16792	98580	20
41	09903	99508	11638	99320	13370	99102	15097	98854	16820	98575	19
42	09932	99506	11667	99317	13399	99098	15126	98849	16849	98570	18
43	09961	99503	11696	99314	13427	99094	15155	98845	16878	98565	17
44	09990	99500	11725	99310	13456	99091	15184	98841	16906	98561	16
45	10019	99497	11754	99307	13485	99087	15212	98836	16935	98556	15
46	10048	99494	11783	99303	13514	99083	15241	98832	16964	98551	14
47	10077	99491	11812	99300	13543	99079	15270	98827	16992	98546	13
48	10106	99488	11840	99297	13572	99075	15298	98823	17021	98541	12
49	10135	99485	11869	99293	13600	99071	15327	98818	17050	98536	11
50	10164	99482	11898	99290	13629	99067	15356	98814	17078	98531	10
51	10192	99479	11927	99286	13658	99063	15385	98809	17107	98526	9
52	10221	99476	11956	99283	13687	99059	15414	98805	17136	98521	8
53	10250	99473	11985	99279	13716	99055	15442	98800	17164	98516	7
54	10279	99470	12014	99276	13744	99051	15471	98796	17193	98511	6
55	10308	99467	12043	99272	13773	99047	15500	98791	17222	98506	5
56	10337	99464	12071	99269	13802	99043	15529	98787	17250	98501	4
57	10366	99461	12100	99265	13831	99039	15557	98782	17279	98496	3
58	10395	99458	12129	99262	13860	99035	15586	98778	17308	98491	2
59	10424	99455	12158	99258	13889	99031	15615	98773	17336	98486	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	84 Deg.		63 Deg.		82 Deg.		81 Deg.		80 Deg.		

A TABLE OF NATURAL SINES.

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M	10 Deg.		11 Deg.		12 Deg.		13 Deg.		14 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	17365	98481	19081	98163	20791	97815	22495	97437	24192	97030	60
1	17393	98476	19109	98157	20820	97809	22523	97430	24220	97023	59
2	17422	98471	19138	98152	20848	97803	22552	97424	24249	97015	58
3	17451	98466	19167	98146	20877	97797	22580	97417	24277	97008	57
4	17479	98461	19195	98140	20905	97791	22608	97411	24305	97001	56
5	17508	98455	19224	98135	20933	97784	22637	97404	24333	96994	55
6	17537	98450	19252	98129	20962	97778	22665	97398	24362	96987	54
7	17565	98445	19281	98124	20990	97772	22693	97391	24390	96980	53
8	17594	98440	19309	98118	21019	97766	22722	97384	24418	96973	52
9	17623	98435	19338	98112	21047	97760	22750	97378	24446	96966	51
10	17651	98430	19366	98107	21076	97754	22778	97371	24474	96959	50
11	17680	98425	19395	98101	21104	97748	22807	97365	24503	96952	49
12	17708	98420	19423	98096	21132	97742	22835	97358	24531	96945	48
13	17737	98414	19452	98090	21161	97735	22863	97351	24559	96937	47
14	17766	98409	19481	98084	21189	97729	22892	97345	24587	96930	46
15	17794	98404	19509	98079	21218	97723	22920	97338	24615	96923	45
16	17823	98399	19538	98073	21246	97717	22948	97331	24644	96916	44
17	17852	98394	19566	98067	21275	97711	22977	97325	24672	96909	43
18	17880	98389	19595	98061	21303	97705	23005	97318	24700	96902	42
19	17909	98383	19623	98056	21331	97698	23033	97311	24728	96894	41
20	17937	98378	19652	98050	21360	97692	23062	97304	24756	96887	40
21	17966	98373	19680	98044	21388	97686	23090	97298	24784	96880	39
22	17995	98368	19709	98039	21417	97680	23118	97291	24813	96873	38
23	18023	98362	19737	98033	21445	97673	23146	97284	24841	96866	37
24	18052	98357	19766	98027	21474	97667	23175	97278	24869	96858	36
25	18081	98352	19794	98021	21502	97661	23203	97271	24897	96851	35
26	18109	98347	19823	98016	21530	97655	23231	97264	24925	96844	34
27	18138	98341	19851	98010	21559	97648	23260	97257	24953	96837	33
28	18166	98336	19880	98004	21587	97642	23288	97251	24982	96829	32
29	18195	98331	19908	97998	21616	97636	23316	97244	25010	96822	31
30	18224	98325	19937	97992	21644	97630	23345	97237	25038	96815	30
31	18252	98320	19965	97987	21672	97623	23373	97230	25066	96807	29
32	18281	98315	19994	97981	21701	97617	23401	97223	25094	96800	28
33	18309	98310	20022	97975	21729	97611	23429	97217	25122	96793	27
34	18338	98304	20051	97969	21758	97604	23458	97210	25151	96786	26
35	18367	98299	20079	97963	21786	97598	23486	97203	25179	96778	25
36	18395	98294	20108	97958	21814	97592	23514	97196	25207	96771	24
37	18424	98288	20136	97952	21843	97585	23542	97189	25235	96764	23
38	18452	98283	20165	97946	21871	97579	23571	97182	25263	96756	22
39	18481	98277	20193	97940	21899	97573	23599	97176	25291	96749	21
40	18509	98272	20222	97934	21928	97566	23627	97169	25320	96742	20
41	18538	98267	20250	97928	21956	97560	23656	97162	25348	96734	19
42	18567	98261	20279	97922	21985	97553	23684	97155	25376	96727	18
43	18595	98256	20307	97916	22013	97547	23712	97148	25404	96719	17
44	18624	98250	20336	97910	22041	97541	23740	97141	25432	96712	16
45	18652	98245	20364	97905	22070	97534	23769	97134	25460	96705	15
46	18681	98240	20393	97899	22098	97528	23797	97127	25488	96697	14
47	18710	98234	20421	97893	22126	97521	23825	97120	25516	96690	13
48	18738	98229	20450	97887	22155	97515	23853	97113	25545	96682	12
49	18767	98223	20478	97881	22183	97508	23882	97106	25573	96675	11
50	18795	98218	20507	97875	22212	97502	23910	97100	25601	96667	10
51	18824	98212	20535	97869	22240	97496	23938	97093	25629	96660	9
52	18852	98207	20563	97863	22268	97489	23966	97086	25657	96653	8
53	18881	98201	20592	97857	22297	97483	23995	97079	25685	96645	7
54	18910	98196	20620	97851	22325	97476	24023	97072	25713	96638	6
55	18938	98190	20649	97845	22353	97470	24051	97065	25741	96630	5
56	18967	98185	20677	97839	22382	97463	24079	97058	25769	96623	4
57	18995	98179	20706	97833	22410	97457	24108	97051	25798	96615	3
58	19024	98174	20734	97827	22438	97450	24136	97044	25826	96608	2
59	19052	98168	20763	97821	22467	97444	24164	97037	25854	96600	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	79 Deg.		78 Deg.		77 Deg.		76 Deg.		75 Deg.		

A TABLE OF NATURAL SINES.

M	15 Deg.		16 Deg.		17 Deg.		18 Deg.		19 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	25882	96593	27564	96126	29237	95630	30902	95106	32557	94552	60
1	25910	96585	27592	96118	29265	95622	30929	95097	32584	94542	59
2	25938	96578	27620	96110	29293	95613	30957	95088	32612	94533	58
3	25966	96570	27648	96102	29321	95605	30985	95079	32639	94523	57
4	25994	96562	27676	96094	29348	95596	31012	95070	32667	94514	56
5	26022	96555	27704	96086	29376	95588	31040	95061	32694	94504	55
6	26050	96547	27731	96078	29404	95579	31068	95052	32722	94495	54
7	26079	96540	27759	96070	29432	95571	31095	95043	32749	94485	53
8	26107	96532	27787	96062	29460	95562	31123	95033	32777	94476	52
9	26135	96524	27815	96054	29487	95554	31151	95024	32804	94466	51
10	26163	96517	27843	96046	29515	95545	31178	95015	32832	94457	50
11	26191	96509	27871	96037	29543	95536	31206	95006	32859	94447	49
12	26219	96502	27899	96029	29571	95528	31233	94997	32887	94438	48
13	26247	96494	27927	96021	29599	95519	31261	94988	32914	94428	47
14	26275	96486	27955	96013	29626	95511	31289	94979	32942	94418	46
15	26303	96479	27983	96005	29654	95502	31316	94970	32969	94409	45
16	26331	96471	28011	95997	29682	95493	31344	94961	32997	94399	44
17	26359	96463	28039	95989	29710	95485	31372	94952	33024	94390	43
18	26387	96456	28067	95981	29737	95476	31399	94943	33051	94380	42
19	26415	96448	28095	95972	29765	95467	31427	94933	33079	94370	41
20	26443	96440	28123	95964	29793	95459	31454	94924	33106	94361	40
21	26471	96433	28150	95956	29821	95450	31482	94915	33134	94351	39
22	26500	96425	28178	95948	29849	95441	31510	94906	33161	94342	38
23	26528	96417	28206	95940	29876	95433	31537	94897	33189	94332	37
24	26556	96410	28234	95931	29904	95424	31565	94888	33216	94322	36
25	26584	96402	28262	95923	29932	95415	31593	94878	33244	94313	35
26	26612	96394	28290	95915	29960	95407	31620	94869	33271	94303	34
27	26640	96386	28318	95907	29987	95398	31648	94860	33298	94293	33
28	26668	96379	28346	95898	30015	95389	31675	94851	33326	94284	32
29	26696	96371	28374	95890	30043	95380	31703	94842	33353	94274	31
30	26724	96363	28402	95882	30071	95372	31730	94832	33381	94264	30
31	26752	96355	28429	95874	30098	95363	31758	94823	33408	94254	29
32	26780	96347	28457	95865	30126	95354	31786	94814	33436	94245	28
33	26808	96340	28485	95857	30154	95345	31813	94805	33463	94235	27
34	26836	96332	28513	95849	30182	95337	31841	94795	33490	94225	26
35	26864	96324	28541	95841	30209	95328	31868	94786	33518	94215	25
36	26892	96316	28569	95832	30237	95319	31896	94777	33545	94206	24
37	26920	96308	28597	95824	30265	95310	31923	94768	33573	94196	23
38	26948	96301	28625	95816	30292	95301	31951	94759	33600	94186	22
39	26976	96293	28652	95807	30320	95293	31979	94750	33627	94176	21
40	27004	96285	28680	95799	30348	95284	32006	94740	33655	94167	20
41	27032	96277	28708	95791	30376	95275	32034	94730	33682	94157	19
42	27060	96269	28736	95782	30403	95266	32061	94721	33710	94147	18
43	27088	96261	28764	95774	30431	95257	32089	94712	33737	94137	17
44	27116	96253	28792	95766	30459	95248	32116	94702	33764	94127	16
45	27144	96246	28820	95757	30486	95240	32144	94693	33792	94118	15
46	27172	96238	28847	95749	30514	95231	32171	94684	33819	94108	14
47	27200	96230	28875	95740	30542	95222	32199	94674	33846	94098	13
48	27228	96222	28903	95732	30570	95213	32227	94665	33874	94088	12
49	27256	96214	28931	95724	30597	95204	32254	94656	33901	94078	11
50	27284	96206	28959	95715	30625	95195	32282	94646	33929	94068	10
51	27312	96198	28987	95707	30653	95186	32309	94637	33956	94058	9
52	27340	96190	29015	95698	30680	95177	32337	94627	33983	94049	8
53	27368	96182	29042	95690	30708	95168	32364	94618	34011	94039	7
54	27396	96174	29070	95681	30736	95159	32392	94609	34038	94029	6
55	27424	96166	29098	95673	30763	95150	32419	94599	34065	94019	5
56	27452	96158	29126	95664	30791	95142	32447	94590	34093	94009	4
57	27480	96150	29154	95656	30819	95133	32474	94580	34120	93999	3
58	27508	96142	29182	95647	30846	95124	32502	94571	34147	93989	2
59	27536	96134	29209	95639	30874	95115	32529	94561	34175	93979	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	74 Deg.		73 Deg.		72 Deg.		71 Deg.		70 Deg.		

M	20 Deg.		21 Deg.		22 Deg.		23 Deg.		24 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	34202	93969	35837	93358	37461	92718	39073	92050	40674	9135-	60
1	34229	93959	35864	93348	37488	92707	39100	92039	40700	91343	59
2	34257	93949	35891	93337	37515	92697	39127	92028	40727	91331	58
3	34284	93939	35918	93327	37542	92686	39153	92016	40753	91319	57
4	34311	93929	35945	93316	37569	92675	39180	92005	40780	91307	56
5	34339	93919	35973	93306	37595	92664	39207	91994	40806	91295	55
6	34366	93909	36000	93295	37622	92653	39234	91982	40833	91283	54
7	34393	93899	36027	93285	37649	92642	39260	91971	40860	91272	53
8	34421	93889	36054	93274	37676	92631	39287	91959	40886	91260	52
9	34448	93879	36081	93264	37703	92620	39314	91948	40913	91248	51
10	34475	93869	36108	93253	37730	92609	39341	91936	40939	91236	50
11	34503	93859	36135	93243	37757	92598	39367	91925	40966	91224	49
12	34530	93849	36162	93232	37784	92587	39394	91914	40992	91212	48
13	34557	93839	36190	93222	37811	92576	39421	91902	41019	91200	47
14	34584	93829	36217	93211	37838	92565	39448	91891	41045	91188	46
15	34612	93819	36244	93201	37865	92554	39474	91879	41072	91176	45
16	34639	93809	36271	93190	37892	92543	39501	91868	41098	91164	44
17	34666	93799	36298	93180	37919	92532	39528	91856	41125	91152	43
18	34694	93789	36325	93169	37946	92521	39555	91845	41151	91140	42
19	34721	93779	36352	93159	37973	92510	39581	91833	41178	91128	41
20	34748	93769	36379	93148	37999	92499	39608	91822	41204	91116	40
21	34775	93759	36406	93137	38026	92488	39635	91810	41231	91104	39
22	34803	93748	36434	93127	38053	92477	39661	91799	41257	91092	38
23	34830	93738	36461	93116	38080	92466	39688	91787	41284	91080	37
24	34857	93728	36488	93106	38107	92455	39715	91775	41310	91068	36
25	34884	93718	36515	93095	38134	92444	39741	91764	41337	91056	35
26	34912	93708	36542	93084	38161	92432	39768	91752	41363	91044	34
27	34939	93698	36569	93074	38188	92421	39795	91741	41390	91032	33
28	34966	93688	36596	93063	38215	92410	39822	91729	41416	91020	32
29	34993	93677	36623	93052	38241	92399	39848	91718	41443	91008	31
30	35021	93667	36650	93042	38268	92388	39875	91706	41469	90996	30
31	35048	93657	36677	93031	38295	92377	39902	91694	41496	90984	29
32	35075	93647	36704	93020	38322	92366	39928	91683	41522	90972	28
33	35102	93637	36731	93010	38349	92355	39955	91671	41549	90960	27
34	35130	93626	36758	92999	38376	92343	39982	91660	41575	90948	26
35	35157	93616	36785	92988	38403	92332	40008	91648	41602	90936	25
36	35183	93606	36812	92978	38430	92321	40035	91636	41628	90924	24
37	35211	93596	36839	92967	38456	92310	40062	91625	41655	90911	23
38	35239	93585	36867	92956	38483	92299	40088	91613	41681	90899	22
39	35266	93575	36894	92945	38510	92287	40115	91601	41707	90887	21
40	35293	93565	36921	92935	38537	92276	40141	91590	41734	90875	20
41	35320	93555	36948	92924	38564	92265	40168	91578	41760	90863	19
42	35347	93544	36975	92913	38591	92254	40195	91566	41787	90851	18
43	35375	93534	37002	92902	38617	92243	40221	91555	41813	90839	17
44	35402	93524	37029	92892	38644	92231	40248	91543	41840	90826	16
45	35429	93514	37056	92881	38671	92220	40275	91531	41866	90814	15
46	35456	93503	37083	92870	38698	92209	40301	91519	41892	90802	14
47	35481	93493	37110	92859	38725	92198	40328	91508	41919	90790	13
48	35511	93483	37137	92849	38752	92186	40355	91496	41945	90778	12
49	35538	93472	37164	92838	38778	92175	40381	91484	41972	90766	11
50	35565	93462	37191	92827	38805	92164	40408	91472	41998	90753	10
51	35592	93452	37218	92816	38832	92152	40434	91461	42024	90741	9
52	35619	93441	37245	92805	38859	92141	40461	91449	42051	90729	8
53	35647	93431	37272	92794	38886	92130	40488	91437	42077	90717	7
54	35674	93420	37299	92784	38912	92119	40514	91425	42104	90704	6
55	35701	93410	37326	92773	38939	92107	40541	91414	42130	90692	5
56	35728	93400	37353	92762	38966	92096	40567	91402	42156	90680	4
57	35755	93389	37380	92751	38993	92085	40594	91390	42183	90668	3
58	35782	93379	37407	92740	39020	92073	40621	91378	42209	90655	2
59	35810	93368	37434	92729	39046	92062	40647	91366	42235	90643	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	69 Deg.		68 Deg.		67 Deg.		66 Deg.		65 Deg.		



M	25 Deg.		26 Deg.		27 Deg.		28 Deg.		29 Deg.		M
	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	
0	42262	90631	43837	89879	45399	89101	46947	88295	48481	87462	60
1	42288	90618	43863	89867	45425	89087	46973	88281	48506	87448	59
2	42315	90606	43889	89854	45451	89074	46999	88267	48532	87434	58
3	42341	90594	43916	89841	45477	89061	47024	88254	48557	87420	57
4	42367	90582	43942	89828	45503	89048	47050	88240	48583	87406	56
5	42394	90569	43968	89816	45529	89035	47076	88226	48608	87391	55
6	42420	90557	43994	89803	45554	89021	47101	88213	48634	87377	54
7	42446	90545	44020	89790	45580	89008	47127	88199	48659	87363	53
8	42473	90532	44046	89777	45606	88995	47153	88185	48684	87349	52
9	42499	90520	44072	89764	45632	88981	47178	88172	48710	87335	51
10	42525	90507	44098	89752	45658	88968	47204	88158	48735	87321	50
11	42552	90495	44124	89739	45684	88955	47229	88144	48761	87306	49
12	42578	90483	44151	89726	45710	88942	47255	88130	48786	87292	48
13	42604	90470	44177	89713	45736	88928	47281	88117	48811	87278	47
14	42631	90458	44203	89700	45762	88915	47306	88103	48837	87264	46
15	42657	90446	44229	89687	45787	88902	47332	88089	48862	87250	45
16	42683	90433	44255	89674	45813	88888	47358	88075	48888	87235	44
17	42709	90421	44281	89662	45839	88875	47383	88062	48913	87221	43
18	42736	90408	44307	89649	45865	88862	47409	88048	48938	87207	42
19	42762	90396	44333	89636	45891	88848	47434	88034	48964	87193	41
20	42788	90383	44359	89623	45917	88835	47460	88020	48989	87178	40
21	42815	90371	44385	89610	45942	88822	47486	88006	49014	87164	39
22	42841	90358	44411	89597	45968	88808	47511	87993	49040	87150	38
23	42867	90346	44437	89584	45994	88795	47537	87979	49065	87136	37
24	42894	90334	44464	89571	46020	88782	47562	87965	49090	87121	36
25	42920	90321	44490	89558	46046	88768	47588	87951	49116	87107	35
26	42946	90309	44516	89545	46072	88755	47614	87937	49141	87093	34
27	42972	90296	44542	89532	46097	88741	47639	87923	49166	87079	33
28	42999	90284	44568	89519	46123	88728	47665	87909	49192	87064	32
29	43025	90271	44594	89506	46149	88715	47690	87896	49217	87050	31
30	43051	90259	44620	89493	46175	88701	47716	87882	49242	87036	30
31	43077	90246	44646	89480	46201	88688	47741	87868	49268	87021	29
32	43104	90233	44672	89467	46226	88674	47767	87854	49293	87007	28
33	43130	90221	44698	89454	46252	88661	47793	87840	49318	86993	27
34	43156	90208	44724	89441	46278	88647	47818	87826	49344	86978	26
35	43182	90196	44750	89428	46304	88634	47844	87812	49369	86964	25
36	43209	90183	44776	89415	46330	88620	47869	87798	49394	86949	24
37	43235	90171	44802	89402	46355	88607	47895	87784	49419	86935	23
38	43261	90158	44828	89389	46381	88593	47920	87770	49445	86921	22
39	43287	90146	44854	89376	46407	88580	47946	87756	49470	86906	21
40	43313	90133	44880	89363	46433	88566	47971	87743	49495	86892	20
41	43340	90120	44906	89350	46458	88553	47997	87729	49521	86878	19
42	43366	90108	44932	89337	46484	88539	48022	87715	49546	86863	18
43	43392	90095	44958	89324	46510	88526	48048	87701	49571	86849	17
44	43418	90082	44984	89311	46536	88512	48073	87687	49596	86834	16
45	43445	90070	45010	89298	46561	88499	48099	87673	49622	86820	15
46	43471	90057	45036	89285	46587	88485	48124	87659	49647	86805	14
47	43497	90045	45062	89272	46613	88472	48150	87645	49672	86791	13
48	43523	90032	45088	89259	46639	88458	48175	87631	49697	86777	12
49	43549	90019	45114	89245	46664	88445	48201	87617	49723	86762	11
50	43575	90007	45140	89232	46690	88431	48226	87603	49748	86748	10
51	43602	89994	45166	89219	46716	88417	48252	87589	49773	86733	9
52	43628	89981	45192	89206	46742	88404	48277	87575	49798	86719	8
53	43654	89968	45218	89193	46767	88390	48303	87561	49824	86704	7
54	43680	89956	45244	89180	46793	88377	48328	87546	49849	86690	6
55	43706	89943	45269	89167	46819	88363	48354	87532	49874	86675	5
56	43733	89930	45295	89153	46844	88349	48379	87518	49899	86661	4
57	43759	89918	45321	89140	46870	88336	48405	87504	49924	86646	3
58	43785	89905	45347	89127	46896	88322	48430	87490	49950	86632	2
59	43811	89892	45373	89114	46921	88308	48456	87476	49975	86617	1
M	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	M
	64 Deg.		63 Deg.		62 Deg.		61 Deg.		60 Deg.		

A TABLE OF NATURAL SINES.

M	30 Deg.		31 Deg.		32 Deg.		33 Deg.		34 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	50000	86603	51504	85717	52992	84905	54464	83867	55919	82904	60
1	50025	86588	51529	85702	53017	84789	54488	83851	55943	82887	59
2	50050	86573	51554	85687	53041	84774	54513	83835	55968	82871	58
3	50076	86559	51579	85672	53066	84759	54537	83819	55992	82855	57
4	50101	86544	51604	85657	53091	84743	54561	83804	56016	82839	56
5	50126	86530	51628	85642	53115	84728	54586	83788	56040	82822	55
6	50151	86515	51653	85627	53140	84712	54610	83772	56064	82806	54
7	50176	86501	51678	85612	53164	84697	54635	83756	56088	82790	53
8	50201	86486	51703	85597	53189	84681	54659	83740	56112	82773	52
9	50227	86471	51728	85582	53214	84666	54683	83724	56136	82757	51
10	50252	86457	51753	85567	53238	84650	54708	83708	56160	82741	50
11	50277	86442	51778	85551	53263	84635	54732	83692	56184	82724	49
12	50302	86427	51803	85536	53288	84619	54756	83676	56208	82708	48
13	50327	86413	51828	85521	53312	84604	54781	83660	56232	82692	47
14	50352	86398	51852	85506	53337	84588	54805	83645	56256	82675	46
15	50377	86384	51877	85491	53361	84573	54829	83629	56280	82659	45
16	50403	86369	51902	85476	53386	84557	54854	83613	56305	82643	44
17	50428	86354	51927	85461	53411	84542	54878	83597	56329	82626	43
18	50453	86340	51952	85446	53435	84526	54902	83581	56353	82610	42
19	50478	86325	51977	85431	53460	84511	54927	83565	56377	82593	41
20	50503	86310	52002	85416	53484	84495	54951	83549	56401	82577	40
21	50528	86295	52026	85401	53509	84480	54975	83533	56425	82561	39
22	50553	86281	52051	85385	53534	84464	54999	83517	56449	82544	38
23	50578	86266	52076	85370	53558	84448	55024	83501	56473	82528	37
24	50603	86251	52101	85355	53583	84433	55048	83485	56497	82511	36
25	50628	86237	52126	85340	53607	84417	55072	83469	56521	82495	35
26	50654	86222	52151	85325	53632	84402	55097	83453	56545	82478	34
27	50679	86207	52175	85310	53656	84386	55121	83437	56569	82462	33
28	50704	86192	52200	85294	53681	84370	55145	83421	56593	82446	32
29	50729	86178	52225	85279	53705	84355	55169	83405	56617	82429	31
30	50754	86163	52250	85264	53730	84339	55194	83389	56641	82413	30
31	50779	86148	52275	85249	53754	84324	55218	83373	56665	82396	29
32	50804	86133	52299	85234	53779	84308	55242	83356	56689	82380	28
33	50829	86119	52324	85218	53804	84292	55266	83340	56713	82363	27
34	50854	86104	52349	85203	53828	84277	55291	83324	56736	82347	26
35	50879	86089	52374	85188	53853	84261	55315	83308	56760	82330	25
36	50904	86074	52399	85173	53877	84245	55339	83292	56784	82314	24
37	50929	86059	52423	85157	53902	84230	55363	83276	56808	82297	23
38	50954	86045	52448	85142	53926	84214	55388	83260	56832	82281	22
39	50979	86030	52473	85127	53951	84198	55412	83244	56856	82264	21
40	51004	86015	52498	85112	53975	84182	55436	83228	56880	82248	20
41	51029	86000	52522	85096	54000	84167	55460	83212	56904	82231	19
42	51054	85985	52547	85081	54024	84151	55484	83195	56928	82214	18
43	51079	85970	52572	85066	54049	84135	55509	83179	56952	82197	17
44	51104	85956	52597	85051	54073	84120	55533	83163	56976	82181	16
45	51129	85941	52621	85035	54097	84104	55557	83147	57000	82165	15
46	51154	85926	52646	85020	54122	84088	55581	83131	57024	82148	14
47	51179	85911	52671	85005	54146	84072	55605	83115	57047	82132	13
48	51204	85896	52696	84989	54171	84057	55630	83098	57071	82115	12
49	51229	85881	52720	84974	54195	84041	55654	83082	57095	82098	11
50	51254	85866	52745	84959	54220	84025	55678	83066	57119	82082	10
51	51279	85851	52770	84943	54244	84009	55702	83050	57143	82065	9
52	51304	85836	52794	84928	54269	83994	55726	83034	57167	82048	8
53	51329	85821	52819	84913	54293	83978	55750	83017	57191	82032	7
54	51354	85806	52844	84897	54317	83962	55774	83001	57215	82015	6
55	51379	85792	52869	84882	54342	83946	55799	82985	57238	81999	5
56	51404	85777	52893	84866	54366	83930	55823	82969	57262	81982	4
57	51429	85762	52918	84851	54391	83915	55847	82953	57286	81965	3
58	51454	85747	52943	84836	54415	83899	55871	82936	57310	81949	2
59	51479	85732	52967	84820	54440	83883	55895	82920	57334	81932	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	59 Deg.		58 Deg.		57 Deg.		56 Deg.		55 Deg.		

A TABLE OF NATURAL SINES.

M	35 Deg.		36 Deg.		37 Deg.		38 Deg.		39 Deg.		M
	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	
0	57358	81915	58779	80902	60182	79864	61566	78801	62932	77715	60
1	57381	81899	58802	80885	60205	79846	61589	78783	62955	77696	59
2	57405	81882	58826	80867	60228	79829	61612	78765	62977	77678	58
3	57429	81865	58849	80850	60251	79811	61635	78747	63000	77660	57
4	57453	81848	58873	80833	60274	79793	61658	78729	63022	77641	56
5	57477	81832	58896	80816	60298	79776	61681	78711	63045	77623	55
6	57501	81815	58920	80799	60321	79758	61704	78694	63068	77605	54
7	57524	81798	58943	80782	60344	79741	61726	78676	63090	77586	53
8	57548	81782	58967	80765	60367	79723	61749	78658	63113	77568	52
9	57572	81765	58990	80748	60390	79706	61772	78640	63135	77550	51
10	57596	81748	59014	80730	60414	79688	61795	78622	63158	77531	50
11	57619	81731	59037	80713	60437	79671	61818	78604	63180	77513	49
12	57643	81714	59061	80696	60460	79653	61841	78586	63203	77494	48
13	57667	81698	59084	80679	60483	79635	61864	78568	63225	77475	47
14	57691	81681	59108	80662	60506	79618	61887	78550	63248	77458	46
15	57715	81664	59131	80644	60529	79600	61909	78532	63271	77439	45
16	57738	81647	59154	80627	60553	79583	61932	78514	63293	77421	44
17	57762	81631	59178	80610	60576	79565	61955	78496	63316	77402	43
18	57786	81614	59201	80593	60599	79547	61978	78478	63338	77384	42
19	57810	81597	59225	80576	60622	79530	62001	78460	63361	77366	41
20	57833	81580	59248	80558	60645	79512	62024	78442	63383	77347	40
21	57857	81563	59272	80541	60668	79494	62046	78424	63406	77329	39
22	57881	81546	59295	80524	60691	79477	62069	78405	63428	77310	38
23	57904	81530	59318	80507	60714	79459	62092	78387	63451	77292	37
24	57928	81513	59342	80489	60738	79441	62115	78369	63473	77273	36
25	57952	81496	59365	80472	60761	79424	62138	78351	63496	77255	35
26	57976	81479	59389	80455	60784	79406	62160	78333	63518	77236	34
27	57999	81462	59412	80438	60807	79388	62183	78315	63540	77218	33
28	58023	81445	59436	80420	60830	79371	62206	78297	63563	77199	32
29	58047	81428	59459	80403	60853	79353	62229	78279	63585	77181	31
30	58070	81412	59482	80386	60876	79335	62251	78261	63608	77162	30
31	58094	81395	59506	80368	60899	79318	62274	78243	63630	77144	29
32	58118	81378	59529	80351	60922	79300	62297	78225	63653	77125	28
33	58141	81361	59552	80334	60945	79282	62320	78206	63675	77107	27
34	58165	81344	59576	80316	60968	79264	62342	78188	63698	77088	26
35	58189	81327	59599	80299	60991	79247	62365	78170	63720	77070	25
36	58212	81310	59622	80282	61015	79229	62388	78152	63742	77051	24
37	58236	81293	59646	80264	61038	79211	62411	78134	63765	77033	23
38	58260	81276	59669	80247	61061	79193	62433	78116	63787	77014	22
39	58283	81259	59693	80230	61084	79176	62456	78098	63810	76996	21
40	58307	81242	59716	80212	61107	79158	62479	78079	63832	76977	20
41	58330	81225	59739	80195	61130	79140	62502	78061	63854	76959	19
42	58354	81208	59763	80178	61153	79122	62524	78043	63877	76940	18
43	58378	81191	59786	80160	61176	79105	62547	78025	63899	76921	17
44	58401	81174	59809	80143	61199	79087	62570	78007	63922	76903	16
45	58425	81157	59832	80125	61222	79069	62592	77988	63944	76884	15
46	58449	81140	59856	80108	61245	79051	62615	77970	63966	76866	14
47	58472	81123	59879	80091	61268	79033	62638	77952	63989	76847	13
48	58496	81106	59902	80073	61291	79015	62660	77934	64011	76828	12
49	58519	81089	59926	80056	61314	78997	62683	77916	64033	76810	11
50	58543	81072	59949	80038	61337	78980	62706	77897	64056	76791	10
51	58567	81055	59972	80021	61360	78962	62728	77879	64078	76772	9
52	58590	81038	59995	80003	61383	78944	62751	77861	64100	76754	8
53	58614	81021	60019	79986	61406	78926	62774	77843	64123	76735	7
54	58637	81004	60042	79968	61429	78908	62796	77824	64145	76717	6
55	58661	80987	60065	79951	61451	78891	62819	77806	64167	76698	5
56	58684	80970	60088	79934	61474	78873	62842	77788	64190	76679	4
57	58708	80953	60112	79916	61497	78855	62864	77769	64212	76661	3
58	58731	80936	60135	79899	61520	78837	62887	77751	64234	76642	2
59	58755	80919	60158	79881	61543	78819	62909	77733	64256	76623	1
M	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	N. CS.	N. S.	M
	54 Deg.		53 Deg.		52 Deg.		51 Deg.		50 Deg.		

A TABLE OF NATURAL SINES

M	40 Deg.		41 Deg.		42 Deg.		43 Deg.		44 Deg.		M
	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	
0	64279	76604	65606	75471	66913	74314	68200	73135	69466	71934	60
1	64301	76586	65628	75452	66935	74295	68221	73116	69487	71914	59
2	64323	76567	65650	75433	66956	74276	68242	73096	69508	71894	58
3	64346	76549	65672	75414	66978	74256	68264	73076	69529	71873	57
4	64368	76530	65694	75395	66999	74237	68285	73056	69549	71853	56
5	64390	76511	65716	75375	67021	74217	68306	73036	69570	71833	55
6	64412	76492	65738	75356	67043	74198	68327	73016	69591	71813	54
7	64435	76473	65759	75337	67064	74178	68349	72996	69612	71792	53
8	64457	76455	65781	75318	67086	74159	68370	72976	69633	71772	52
9	64479	76436	65803	75299	67107	74139	68391	72957	69654	71752	51
10	64501	76417	65825	75280	67129	74120	68412	72937	69675	71732	50
11	64524	76398	65847	75261	67151	74100	68433	72917	69696	71711	49
12	64546	76380	65869	75241	67172	74080	68455	72897	69717	71691	48
13	64568	76361	65891	75222	67194	74061	68476	72877	69737	71671	47
14	64590	76342	65913	75203	67215	74041	68497	72857	69758	71650	46
15	64612	76323	65935	75184	67237	74022	68518	72837	69779	71630	45
16	64635	76304	65956	75165	67258	74002	68539	72817	69800	71610	44
17	64657	76286	65978	75146	67280	73983	68561	72797	69821	71590	43
18	64679	76267	66000	75126	67301	73963	68582	72777	69842	71569	42
19	64701	76248	66022	75107	67323	73944	68603	72757	69862	71549	41
20	64723	76229	66044	75088	67344	73924	68624	72737	69883	71529	40
21	64746	76210	66066	75069	67366	73904	68645	72717	69904	71508	39
22	64768	76192	66088	75050	67387	73885	68666	72697	69925	71488	38
23	64790	76173	66109	75030	67409	73865	68688	72677	69946	71468	37
24	64812	76154	66131	75011	67430	73846	68709	72657	69966	71447	36
25	64834	76135	66153	74992	67452	73826	68730	72637	69987	71427	35
26	64856	76116	66175	74973	67473	73806	68751	72617	70008	71407	34
27	64878	76097	66197	74953	67495	73787	68772	72597	70029	71386	33
28	64901	76078	66218	74934	67516	73767	68793	72577	70049	71366	32
29	64923	76059	66240	74915	67538	73747	68814	72557	70070	71345	31
30	64945	76041	66262	74896	67559	73728	68835	72537	70091	71325	30
31	64967	76022	66284	74876	67580	73708	68857	72517	70112	71305	29
32	64989	76003	66306	74857	67602	73688	68878	72497	70132	71284	28
33	65011	75984	66327	74838	67623	73669	68899	72477	70153	71264	27
34	65033	75965	66349	74818	67645	73649	68920	72457	70174	71243	26
35	65055	75946	66371	74799	67666	73629	68941	72437	70195	71223	25
36	65077	75927	66393	74780	67688	73610	68962	72417	70215	71203	24
37	65099	75908	66414	74760	67709	73590	68983	72397	70236	71182	23
38	65122	75889	66436	74741	67730	73570	69004	72377	70257	71162	22
39	65144	75870	66458	74722	67752	73551	69025	72357	70277	71141	21
40	65166	75851	66480	74703	67773	73531	69046	72337	70298	71121	20
41	65188	75832	66501	74683	67795	73511	69067	72317	70319	71100	19
42	65210	75813	66523	74664	67816	73491	69088	72297	70339	71080	18
43	65232	75794	66545	74644	67837	73472	69109	72277	70360	71059	17
44	65254	75775	66566	74625	67859	73452	69130	72257	70381	71039	16
45	65276	75756	66588	74606	67880	73432	69151	72236	70401	71019	15
46	65298	75738	66610	74586	67901	73412	69172	72216	70422	70998	14
47	65320	75719	66632	74567	67923	73393	69193	72196	70443	70978	13
48	65342	75699	66653	74548	67944	73373	69214	72176	70463	70957	12
49	65364	75680	66675	74528	67965	73353	69235	72156	70484	70937	11
50	65386	75661	66697	74509	67987	73333	69256	72136	70505	70916	10
51	65408	75642	66718	74489	68008	73314	69277	72116	70525	70896	9
52	65430	75623	66740	74470	68029	73294	69298	72095	70546	70875	8
53	65452	75604	66762	74451	68051	73274	69319	72075	70567	70855	7
54	65474	75585	66783	74431	68072	73254	69340	72055	70587	70834	6
55	65496	75566	66805	74412	68093	73234	69361	72035	70608	70813	5
56	65518	75547	66827	74392	68115	73215	69382	72015	70628	70793	4
57	65540	75528	66848	74373	68136	73195	69403	71995	70649	70772	3
58	65562	75509	66870	74353	68157	73175	69424	71974	70670	70752	2
59	65584	75490	66891	74334	68179	73155	69445	71954	70690	70731	1
60	65606	75471	66913	74314	68200	73135	69466	71934	70711	70711	0
M	N. S.	N. S.	N. C.S.	N. S.	N. C.S.	N. S.	N. C.S.	N. C.S.	N. S.	N. C.S.	N. S.
	49 Deg.		48 Deg.		47 Deg.		46 Deg.		45 Deg.		



**A TRAVERSE TABLE,**

**SHOWING THE DIFFERENCE OF**

**LATITUDE AND DEPARTURE**

**FOR DISTANCES BETWEEN 1 AND 100, AND FOR ANGLES  
TO QUARTER DEGREES BETWEEN 1° AND 90°.**

TRAVERSE TABLE.

Distance.	¼ Deg.		½ Deg.		¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.00	1.00	0.01	1.00	0.01	1
2	2.00	0.01	2.00	0.02	2.00	0.03	2
3	3.00	0.01	3.00	0.03	3.00	0.04	3
4	4.00	0.02	4.00	0.03	4.00	0.05	4
5	5.00	0.02	5.00	0.04	5.00	0.07	5
6	6.00	0.03	6.00	0.05	6.00	0.08	6
7	7.00	0.03	7.00	0.06	7.00	0.09	7
8	8.00	0.03	8.00	0.07	8.00	0.10	8
9	9.00	0.04	9.00	0.08	9.00	0.12	9
10	10.00	0.04	10.00	0.09	10.00	0.13	10
11	11.00	0.05	11.00	0.10	11.00	0.14	11
12	12.00	0.05	12.00	0.10	12.00	0.16	12
13	13.00	0.06	13.00	0.11	13.00	0.17	13
14	14.00	0.06	14.00	0.12	14.00	0.18	14
15	15.00	0.07	15.00	0.13	15.00	0.20	15
16	16.00	0.07	16.00	0.14	16.00	0.21	16
17	17.00	0.07	17.00	0.15	17.00	0.22	17
18	18.00	0.08	18.00	0.16	18.00	0.24	18
19	19.00	0.08	19.00	0.17	19.00	0.25	19
20	20.00	0.09	20.00	0.17	20.00	0.26	20
21	21.00	0.09	21.00	0.18	21.00	0.27	21
22	22.00	0.10	22.00	0.19	22.00	0.29	22
23	23.00	0.10	23.00	0.20	23.00	0.30	23
24	24.00	0.10	24.00	0.21	24.00	0.31	24
25	25.00	0.11	25.00	0.22	25.00	0.33	25
26	26.00	0.11	26.00	0.23	26.00	0.34	26
27	27.00	0.12	27.00	0.24	27.00	0.35	27
28	28.00	0.12	28.00	0.24	28.00	0.37	28
29	29.00	0.13	29.00	0.25	29.00	0.38	29
30	30.00	0.13	30.00	0.26	30.00	0.39	30
31	31.00	0.14	31.00	0.27	31.00	0.41	31
32	32.00	0.14	32.00	0.28	32.00	0.42	32
33	33.00	0.14	33.00	0.29	33.00	0.43	33
34	34.00	0.15	34.00	0.30	34.00	0.45	34
35	35.00	0.15	35.00	0.31	35.00	0.46	35
36	36.00	0.16	36.00	0.31	36.00	0.47	36
37	37.00	0.16	37.00	0.32	37.00	0.48	37
38	38.00	0.17	38.00	0.33	38.00	0.50	38
39	39.00	0.17	39.00	0.34	39.00	0.51	39
40	40.00	0.17	40.00	0.35	40.00	0.52	40
41	41.00	0.18	41.00	0.36	41.00	0.54	41
42	42.00	0.18	42.00	0.37	42.00	0.55	42
43	43.00	0.19	43.00	0.38	43.00	0.56	43
44	44.00	0.19	44.00	0.38	44.00	0.58	44
45	45.00	0.20	45.00	0.39	45.00	0.59	45
46	46.00	0.20	46.00	0.40	46.00	0.60	46
47	47.00	0.21	47.00	0.41	47.00	0.62	47
48	48.00	0.21	48.00	0.42	48.00	0.63	48
49	49.00	0.21	49.00	0.43	49.00	0.64	49
50	50.00	0.22	50.00	0.44	50.00	0.65	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	89¼ Deg.		89½ Deg.		89¾ Deg.		

Distance.	$\frac{1}{4}$ Deg.		$\frac{1}{2}$ Deg.		$\frac{3}{4}$ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	51.00	0.22	51.00	0.45	51.00	0.67	51
52	52.00	0.23	52.00	0.45	52.00	0.68	52
53	53.00	0.23	53.00	0.46	53.00	0.69	53
54	54.00	0.24	54.00	0.47	54.00	0.71	54
55	55.00	0.24	55.00	0.48	55.00	0.72	55
56	56.00	0.24	56.00	0.49	56.00	0.73	56
57	57.00	0.25	57.00	0.50	57.00	0.75	57
58	58.00	0.25	58.00	0.51	57.99	0.76	58
59	59.00	0.26	59.00	0.51	58.99	0.77	59
60	60.00	0.26	60.00	0.52	59.99	0.79	60
61	61.00	0.27	61.00	0.53	60.99	0.80	61
62	62.00	0.27	62.00	0.54	61.99	0.81	62
63	63.00	0.27	63.00	0.55	62.99	0.82	63
64	64.00	0.28	64.00	0.56	63.99	0.84	64
65	65.00	0.28	65.00	0.57	64.99	0.85	65
66	66.00	0.29	66.00	0.58	65.99	0.86	66
67	67.00	0.29	67.00	0.58	66.99	0.88	67
68	68.00	0.30	68.00	0.59	67.99	0.89	68
69	69.00	0.30	69.00	0.60	68.99	0.90	69
70	70.00	0.31	70.00	0.61	69.99	0.92	70
71	71.00	0.31	71.00	0.62	70.99	0.93	71
72	72.00	0.31	72.00	0.63	71.99	0.94	72
73	73.00	0.32	73.00	0.64	72.99	0.96	73
74	74.00	0.32	74.00	0.65	73.99	0.97	74
75	75.00	0.33	75.00	0.65	74.99	0.98	75
76	76.00	0.33	76.00	0.66	75.99	0.99	76
77	77.00	0.34	77.00	0.67	76.99	1.01	77
78	78.00	0.34	78.00	0.68	77.99	1.02	78
79	79.00	0.34	79.00	0.69	78.99	1.03	79
80	80.00	0.35	80.00	0.70	79.99	1.05	80
81	81.00	0.35	81.00	0.71	80.99	1.06	81
82	82.00	0.36	82.00	0.72	81.99	1.07	82
83	83.00	0.36	83.00	0.72	82.99	1.09	83
84	84.00	0.37	84.00	0.73	83.99	1.10	84
85	85.00	0.37	85.00	0.74	84.99	1.11	85
86	86.00	0.38	86.00	0.75	85.99	1.13	86
87	87.00	0.38	87.00	0.76	86.99	1.14	87
88	88.00	0.38	88.00	0.77	87.99	1.15	88
89	89.00	0.39	89.00	0.78	88.99	1.16	89
90	90.00	0.39	90.00	0.79	89.99	1.18	90
91	91.00	0.40	91.00	0.79	90.99	1.19	91
92	92.00	0.40	92.00	0.80	91.99	1.20	92
93	93.00	0.41	93.00	0.81	92.99	1.22	93
94	94.00	0.41	94.00	0.82	93.99	1.23	94
95	95.00	0.41	95.00	0.83	94.99	1.24	95
96	96.00	0.42	96.00	0.84	95.99	1.26	96
97	97.00	0.42	97.00	0.85	96.99	1.27	97
98	98.00	0.43	98.00	0.86	97.99	1.28	98
99	99.00	0.43	99.00	0.86	98.99	1.30	99
100	100.00	0.44	100.00	0.87	99.99	1.31	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	$89\frac{1}{4}$ Deg.		$89\frac{1}{2}$ Deg.		$89\frac{3}{4}$ Deg.		



## TRAVERSE TABLE.

Distance.	1 Deg.		1½ Deg.		1½ Deg.		1½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.02	1.00	0.02	1.00	0.03	1.00	0.03	1
2	2.00	0.03	2.00	0.04	2.00	0.05	2.00	0.06	2
3	3.00	0.05	3.00	0.07	3.00	0.08	3.00	0.09	3
4	4.00	0.07	4.00	0.09	4.00	0.10	4.00	0.12	4
5	5.00	0.09	5.00	0.11	5.00	0.13	5.00	0.15	5
6	6.00	0.10	6.00	0.13	6.00	0.16	6.00	0.18	6
7	7.00	0.12	7.00	0.15	7.00	0.18	7.00	0.21	7
8	8.00	0.14	8.00	0.17	8.00	0.21	8.00	0.25	8
9	9.00	0.16	9.00	0.20	9.00	0.24	9.00	0.28	9
10	10.00	0.17	10.00	0.22	10.00	0.26	10.00	0.31	10
11	11.00	0.19	11.00	0.24	11.00	0.28	10.99	0.34	11
12	12.00	0.21	12.00	0.26	12.00	0.31	11.99	0.37	12
13	13.00	0.23	13.00	0.28	13.00	0.34	12.99	0.40	13
14	14.00	0.24	14.00	0.31	14.00	0.37	13.99	0.43	14
15	15.00	0.26	15.00	0.33	14.99	0.39	14.99	0.46	15
16	16.00	0.28	16.00	0.35	15.99	0.42	15.99	0.49	16
17	17.00	0.30	17.00	0.37	16.99	0.45	16.99	0.52	17
18	18.00	0.31	18.00	0.39	17.99	0.47	17.99	0.55	18
19	19.00	0.33	19.00	0.41	18.99	0.50	18.99	0.58	19
20	20.00	0.35	20.00	0.44	19.99	0.52	19.99	0.61	20
21	21.00	0.37	21.00	0.46	20.99	0.55	20.99	0.64	21
22	22.00	0.38	21.99	0.48	21.99	0.58	21.99	0.67	22
23	23.00	0.40	22.99	0.50	22.99	0.60	22.99	0.70	23
24	24.00	0.42	23.99	0.52	23.99	0.62	23.99	0.73	24
25	25.00	0.44	24.99	0.55	24.99	0.65	24.99	0.76	25
26	26.00	0.45	25.99	0.57	25.99	0.68	25.99	0.79	26
27	27.00	0.47	26.99	0.59	26.99	0.71	26.99	0.83	27
28	28.00	0.49	27.99	0.61	27.99	0.73	27.99	0.86	28
29	29.00	0.51	28.99	0.63	28.99	0.76	28.99	0.89	29
30	30.00	0.52	29.99	0.65	29.99	0.79	29.99	0.92	30
31	31.00	0.54	30.99	0.68	30.99	0.81	30.99	0.95	31
32	32.00	0.56	31.99	0.70	31.99	0.84	31.99	0.98	32
33	32.99	0.58	32.99	0.72	32.99	0.86	32.98	1.01	33
34	33.99	0.59	33.99	0.74	33.99	0.89	33.98	1.04	34
35	34.99	0.61	34.99	0.76	34.99	0.92	34.98	1.07	35
36	35.99	0.63	35.99	0.79	35.99	0.94	35.98	1.10	36
37	36.99	0.65	36.99	0.81	36.99	0.97	36.98	1.13	37
38	37.99	0.66	37.99	0.83	37.99	0.99	37.98	1.16	38
39	38.99	0.68	38.99	0.85	38.99	1.02	38.98	1.19	39
40	39.99	0.70	39.99	0.87	39.99	1.05	39.98	1.22	40
41	40.99	0.72	40.99	0.89	40.99	1.07	40.98	1.25	41
42	41.99	0.73	41.99	0.92	41.99	1.10	41.98	1.28	42
43	42.99	0.75	42.99	0.94	42.99	1.13	42.98	1.31	43
44	43.99	0.77	43.99	0.96	43.99	1.15	43.98	1.34	44
45	44.99	0.79	44.99	0.98	44.99	1.18	44.98	1.37	45
46	45.99	0.80	45.99	1.00	45.99	1.20	45.98	1.40	46
47	46.99	0.82	46.99	1.03	46.99	1.23	46.98	1.44	47
48	47.99	0.84	47.99	1.05	47.98	1.26	47.98	1.47	48
49	48.99	0.86	48.99	1.07	48.98	1.28	48.98	1.50	49
50	49.99	0.87	49.99	1.09	49.98	1.31	49.98	1.53	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	89 Deg.		88½ Deg.		88½ Deg.		88½ Deg.		

TRAVERSE TABLE.

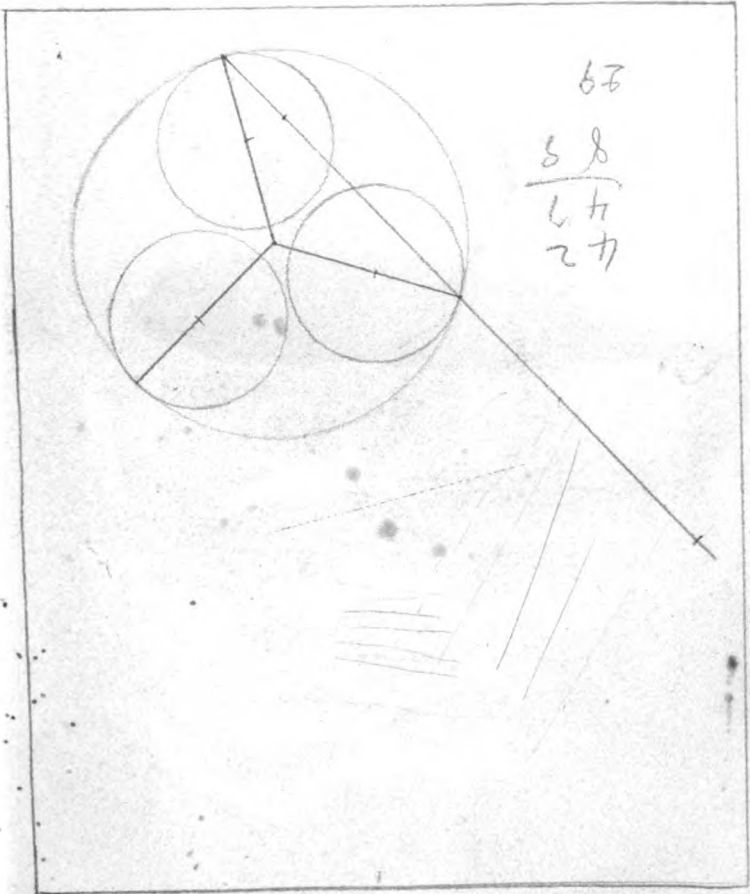
5

Distance.	1 Deg.		1½ Deg.		1½ Deg.		1½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.99	0.89	50.99	1.11	50.98	1.34	50.98	1.56	51
52	51.99	0.91	51.99	1.13	51.98	1.36	51.98	1.59	52
53	52.99	0.92	52.99	1.16	52.98	1.39	52.98	1.62	53
54	53.99	0.94	53.99	1.18	53.98	1.41	53.97	1.65	54
55	54.99	0.96	54.99	1.20	54.98	1.44	54.97	1.68	55
56	55.99	0.98	55.99	1.22	55.98	1.47	55.97	1.71	56
57	56.99	0.99	56.99	1.24	56.98	1.49	56.97	1.74	57
58	57.99	1.01	57.99	1.27	57.98	1.52	57.97	1.77	58
59	58.99	1.03	58.99	1.29	58.98	1.54	58.97	1.80	59
60	59.99	1.05	59.99	1.31	59.98	1.57	59.97	1.83	60
61	60.99	1.06	60.99	1.33	60.98	1.60	60.97	1.86	61
62	61.99	1.08	61.99	1.35	61.98	1.62	61.97	1.89	62
63	62.99	1.10	62.99	1.37	62.98	1.65	62.97	1.92	63
64	63.99	1.12	63.98	1.40	63.98	1.68	63.97	1.95	64
65	64.99	1.13	64.98	1.42	64.98	1.70	64.97	1.99	65
66	65.99	1.15	65.98	1.44	65.98	1.73	65.97	2.02	66
67	66.99	1.17	66.98	1.46	66.98	1.75	66.97	2.05	67
68	67.99	1.19	67.98	1.48	67.98	1.78	67.97	2.08	68
69	68.99	1.20	68.98	1.51	68.98	1.81	68.97	2.11	69
70	69.99	1.22	69.98	1.53	69.98	1.83	69.97	2.14	70
71	70.99	1.24	70.98	1.55	70.98	1.86	70.97	2.17	71
72	71.99	1.26	71.98	1.57	71.98	1.88	71.97	2.20	72
73	72.99	1.27	72.98	1.59	72.97	1.91	72.97	2.23	73
74	73.99	1.29	73.98	1.61	73.97	1.94	73.97	2.26	74
75	74.99	1.31	74.98	1.64	74.97	1.96	74.97	2.29	75
76	75.99	1.33	75.98	1.66	75.97	1.99	75.96	2.32	76
77	76.99	1.34	76.98	1.68	76.97	2.02	76.96	2.35	77
78	77.99	1.36	77.98	1.70	77.97	2.04	77.96	2.38	78
79	78.99	1.38	78.98	1.72	78.97	2.07	78.96	2.41	79
80	79.99	1.40	79.98	1.75	79.97	2.09	79.96	2.44	80
81	80.99	1.41	80.98	1.77	80.97	2.12	80.96	2.47	81
82	81.99	1.43	81.98	1.79	81.97	2.15	81.96	2.50	82
83	82.99	1.45	82.98	1.81	82.97	2.17	82.96	2.53	83
84	83.99	1.47	83.98	1.83	83.97	2.20	83.96	2.57	84
85	84.99	1.48	84.98	1.85	84.97	2.23	84.96	2.60	85
86	85.99	1.50	85.98	1.88	85.97	2.25	85.96	2.63	86
87	86.99	1.52	86.98	1.90	86.97	2.28	86.96	2.66	87
88	87.99	1.54	87.98	1.92	87.97	2.30	87.96	2.69	88
89	88.99	1.55	88.98	1.94	88.97	2.33	88.96	2.72	89
90	89.99	1.57	89.98	1.96	89.97	2.36	89.96	2.75	90
91	90.99	1.59	90.98	1.99	90.97	2.38	90.96	2.78	91
92	91.99	1.61	91.98	2.01	91.97	2.41	91.96	2.81	92
93	92.99	1.62	92.98	2.03	92.97	2.43	92.96	2.84	93
94	93.99	1.64	93.98	2.05	93.97	2.46	93.96	2.87	94
95	94.99	1.66	94.98	2.07	94.97	2.49	94.96	2.90	95
96	95.99	1.68	95.98	2.09	95.97	2.51	95.96	2.94	96
97	96.99	1.69	96.98	2.12	96.97	2.54	96.96	2.96	97
98	97.99	1.71	97.98	2.14	97.97	2.57	97.96	2.99	98
99	98.98	1.73	98.98	2.16	98.97	2.59	98.96	3.02	99
100	99.98	1.75	99.98	2.18	99.97	2.62	99.96	3.05	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	89 Deg.		88½ Deg.		88½ Deg.		88¼ Deg.		

## TRAVERSE TABLE.

Distance.	2 Deg.		2¼ Deg.		2½ Deg.		2¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.03	1.00	0.04	1.00	0.04	1.00	0.05	1
2	2.00	0.07	2.00	0.08	2.00	0.09	2.00	0.10	2
3	3.00	0.10	3.00	0.12	3.00	0.13	3.00	0.14	3
4	4.00	0.14	4.00	0.16	4.00	0.17	4.00	0.19	4
5	5.00	0.17	5.00	0.20	5.00	0.22	4.99	0.24	5
6	6.00	0.21	6.00	0.24	5.99	0.26	5.99	0.29	6
7	7.00	0.24	6.99	0.27	6.99	0.31	6.99	0.34	7
8	7.99	0.28	7.99	0.31	7.99	0.35	7.99	0.38	8
9	8.99	0.31	8.99	0.35	8.99	0.39	8.99	0.43	9
10	9.99	0.35	9.99	0.39	9.99	0.44	9.99	0.48	10
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53	11
12	11.99	0.42	11.99	0.47	11.99	0.52	11.99	0.58	12
13	12.99	0.45	12.99	0.51	12.99	0.57	12.99	0.62	13
14	13.99	0.49	13.99	0.55	13.99	0.61	13.98	0.67	14
15	14.99	0.52	14.99	0.59	14.99	0.65	14.98	0.72	15
16	15.99	0.56	15.99	0.63	15.99	0.70	15.98	0.77	16
17	16.99	0.59	16.99	0.67	16.98	0.74	16.98	0.82	17
18	17.99	0.63	17.99	0.71	17.98	0.79	17.98	0.86	18
19	18.99	0.66	18.99	0.75	18.98	0.83	18.98	0.91	19
20	19.99	0.70	19.98	0.79	19.98	0.87	19.98	0.96	20
21	20.99	0.73	20.98	0.82	20.98	0.92	20.98	1.01	21
22	21.99	0.77	21.98	0.86	21.98	0.96	21.97	1.06	22
23	22.99	0.80	22.98	0.90	22.98	1.00	22.97	1.10	23
24	23.99	0.84	23.98	0.94	23.98	1.05	23.97	1.15	24
25	24.98	0.87	24.98	0.98	24.98	1.09	24.97	1.20	25
26	25.98	0.91	25.98	1.02	25.98	1.13	25.97	1.25	26
27	26.98	0.94	26.98	1.06	26.97	1.18	26.97	1.30	27
28	27.98	0.98	27.98	1.10	27.97	1.22	27.97	1.34	28
29	28.98	1.01	28.98	1.14	28.97	1.26	28.97	1.39	29
30	29.98	1.05	29.98	1.18	29.97	1.31	29.97	1.44	30
31	30.98	1.08	30.98	1.22	30.97	1.35	30.96	1.49	31
32	31.98	1.12	31.98	1.26	31.97	1.40	31.96	1.54	32
33	32.98	1.15	32.97	1.30	32.97	1.44	32.96	1.58	33
34	33.98	1.19	33.97	1.33	33.97	1.48	33.96	1.63	34
35	34.98	1.22	34.97	1.37	34.97	1.53	34.96	1.68	35
36	35.98	1.26	35.97	1.41	35.97	1.57	35.96	1.73	36
37	36.98	1.29	36.97	1.45	36.96	1.61	36.96	1.78	37
38	37.98	1.33	37.97	1.49	37.96	1.66	37.96	1.82	38
39	38.98	1.36	38.97	1.53	38.96	1.70	38.96	1.87	39
40	39.98	1.40	39.97	1.57	39.96	1.75	39.95	1.92	40
41	40.98	1.43	40.97	1.61	40.96	1.77	40.95	1.97	41
42	41.97	1.47	41.97	1.65	41.96	1.83	41.95	2.02	42
43	42.97	1.50	42.97	1.69	42.96	1.88	42.95	2.06	43
44	43.97	1.54	43.97	1.73	43.96	1.92	43.95	2.11	44
45	44.97	1.57	44.97	1.77	44.96	1.96	44.95	2.16	45
46	45.97	1.61	45.96	1.81	45.96	2.01	45.95	2.21	46
47	46.97	1.64	46.96	1.85	46.96	2.05	46.95	2.25	47
48	47.97	1.68	47.96	1.88	47.95	2.09	47.95	2.30	48
49	48.97	1.71	48.96	1.92	48.95	2.14	48.94	2.35	49
50	49.97	1.74	49.96	1.96	49.95	2.18	49.94	2.40	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	88 Deg.		87¼ Deg.		87½ Deg.		87¾ Deg.		

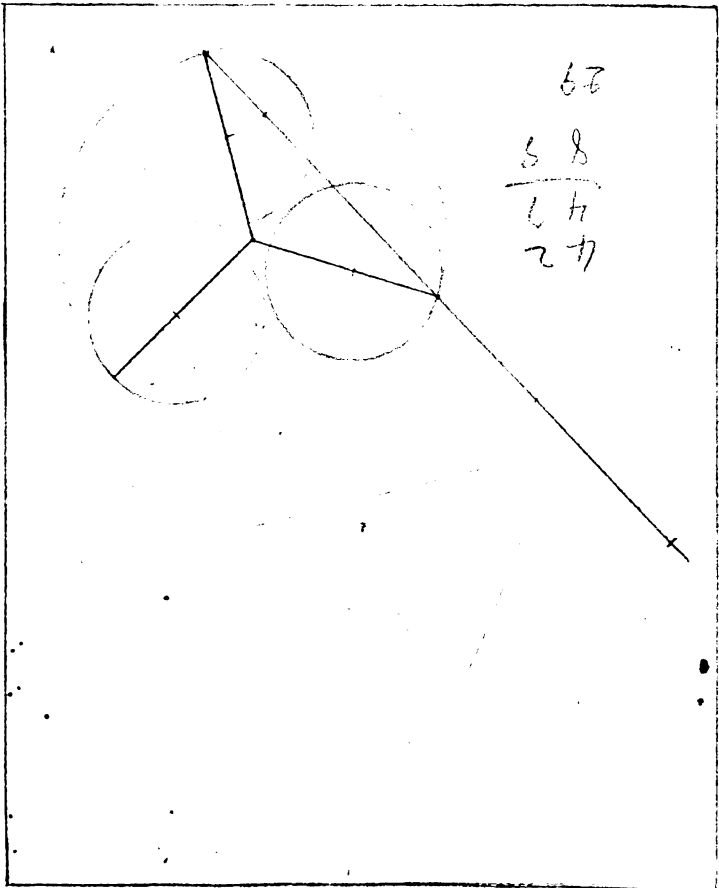
TRAVERSE TABLE.



D	88 Deg.	87 $\frac{1}{2}$ Deg.	87 $\frac{1}{2}$ Deg.	87 $\frac{1}{2}$ Deg.	D
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## TRAVERSE TABLE.

Distance.	2 Deg.		2½ Deg.		2½ Deg.		2½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.03	1.00	0.04	1.00	0.04	1.00	0.05	1
2	2.00	0.07	2.00	0.08	2.00	0.09	2.00	0.10	2
3	3.00	0.10	3.00	0.12	3.00	0.13	3.00	0.14	3
4	4.00	0.14	4.00	0.16	4.00	0.17	4.00	0.19	4
5	5.00	0.17	5.00	0.20	5.00	0.22	4.99	0.24	5
6	6.00	0.21	6.00	0.24	5.99	0.26	5.99	0.29	6
7	7.00	0.24	6.99	0.27	6.99	0.31	6.99	0.34	7
8	7.99	0.28	7.99	0.31	7.99	0.35	7.99	0.38	8
9	8.99	0.31	8.99	0.35	8.99	0.39	8.99	0.43	9
10	9.99	0.35	9.99	0.39	9.99	0.44	9.99	0.48	10
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53	11
12	11.99	0.42	11.99	0.47	11.99	0.52	11.99	0.58	12
13	12.99	0.45	12.99	0.51	12.99	0.57	12.99	0.62	13
14	13.99	0.49	13.99	0.55	13.99	0.61	13.98	0.67	14
15	14.99	0.52	14.99	0.59	14.99	0.65	14.98	0.72	15
16	15.99	0.56	15.99	0.63	15.99	0.70	15.98	0.77	16
17	16.99	0.59	16.99	0.67	16.98	0.74	16.98	0.82	17
18	17.99	0.63	17.99	0.71	17.98	0.79	17.98	0.86	18
19	18.99	0.66	18.99	0.75	18.98	0.83	18.98	0.91	19
20	19.99	0.70	19.98	0.79	19.98	0.87	19.98	0.96	20
21	20.99	0.73	20.98	0.82	20.98	0.92	20.98	1.01	21
22	21.99	0.77	21.98	0.86	21.98	0.96	21.97	1.06	22
23	22.99	0.80	22.98	0.90	22.98	1.00	22.97	1.10	23
24	23.99	0.84	23.98	0.94	23.98	1.05	23.97	1.15	24
25	24.98	0.87	24.98	0.98	24.98	1.09	24.97	1.20	25
26	25.98	0.91	25.98	1.02	25.98	1.13	25.97	1.25	26
27	26.98	0.94	26.98	1.06	26.97	1.18	26.97	1.30	27
28	27.98	0.98	27.98	1.10	27.97	1.22	27.97	1.34	28
29	28.98	1.01	28.98	1.14	28.97	1.26	28.97	1.39	29
30	29.98	1.05	29.98	1.18	29.97	1.31	29.97	1.44	30
31	30.98	1.08	30.98	1.22	30.97	1.35	30.96	1.49	31
32	31.98	1.12	31.98	1.26	31.97	1.40	31.96	1.54	32
33	32.98	1.15	32.97	1.30	32.97	1.44	32.96	1.58	33
34	33.98	1.19	33.97	1.33	33.97	1.48	33.96	1.63	34
35	34.98	1.22	34.97	1.37	34.97	1.53	34.96	1.68	35
36	35.98	1.26	35.97	1.41	35.97	1.57	35.96	1.73	36
37	36.98	1.29	36.97	1.45	36.96	1.61	36.96	1.78	37
38	37.98	1.33	37.97	1.49	37.96	1.66	37.96	1.82	38
39	38.98	1.36	38.97	1.53	38.96	1.70	38.96	1.87	39
40	39.98	1.40	39.97	1.57	39.96	1.75	39.95	1.92	40
41	40.98	1.43	40.97	1.61	40.96	1.77	40.95	1.97	41
42	41.97	1.47	41.97	1.65	41.96	1.83	41.95	2.02	42
43	42.97	1.50	42.97	1.69	42.96	1.88	42.95	2.06	43
44	43.97	1.54	43.97	1.73	43.96	1.92	43.95	2.11	44
45	44.97	1.57	44.97	1.77	44.96	1.96	44.95	2.16	45
46	45.97	1.61	45.96	1.81	45.96	2.01	45.95	2.21	46
47	46.97	1.64	46.96	1.85	46.96	2.05	46.95	2.25	47
48	47.97	1.68	47.96	1.88	47.95	2.09	47.95	2.30	48
49	48.97	1.71	48.96	1.92	48.95	2.14	48.94	2.35	49
50	49.97	1.74	49.96	1.96	49.95	2.18	49.94	2.40	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	88 Deg.		87½ Deg.		87½ Deg.		87½ Deg.		



88 Deg.	87 $\frac{1}{4}$ Deg.	87 $\frac{1}{2}$ Deg.	87 $\frac{1}{4}$ Deg.
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Distance.	3 Deg.		3½ Deg.		3½ Deg.		3¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.05	1.00	0.06	1.00	0.06	1.00	0.06	1
2	2.00	0.10	2.00	0.11	2.00	0.12	2.00	0.13	2
3	3.00	0.16	3.00	0.17	2.99	0.18	2.99	0.20	3
4	3.99	0.21	3.99	0.23	3.99	0.24	3.99	0.26	4
5	4.99	0.26	4.99	0.28	4.99	0.31	4.99	0.33	5
6	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39	6
7	6.99	0.37	6.99	0.40	6.99	0.43	6.99	0.46	7
8	7.99	0.42	7.99	0.45	7.99	0.49	7.98	0.52	8
9	8.99	0.47	8.99	0.51	8.98	0.55	8.98	0.59	9
10	9.99	0.52	9.98	0.57	9.98	0.61	9.98	0.65	10
11	10.98	0.58	10.98	0.62	10.98	0.67	10.98	0.72	11
12	11.98	0.63	11.98	0.68	11.98	0.73	11.97	0.78	12
13	12.98	0.68	12.98	0.73	12.98	0.79	12.97	0.85	13
14	13.98	0.73	13.98	0.79	13.97	0.85	13.97	0.92	14
15	14.98	0.79	14.98	0.85	14.97	0.92	14.97	0.98	15
16	15.98	0.84	15.97	0.91	15.97	0.98	15.97	1.05	16
17	16.98	0.89	16.97	0.96	16.97	1.04	16.96	1.11	17
18	17.98	0.94	17.97	1.02	17.97	1.10	17.96	1.18	18
19	18.98	0.99	18.97	1.08	18.96	1.16	18.96	1.24	19
20	19.97	1.05	19.97	1.13	19.96	1.22	19.96	1.31	20
21	20.97	1.10	20.97	1.19	20.96	1.28	20.96	1.37	21
22	21.97	1.15	21.96	1.25	21.96	1.34	21.95	1.44	22
23	22.97	1.20	22.96	1.30	22.96	1.40	22.95	1.50	23
24	23.97	1.26	23.96	1.36	23.96	1.47	23.95	1.57	24
25	24.97	1.31	24.96	1.42	24.95	1.53	24.95	1.64	25
26	25.96	1.36	25.96	1.47	25.95	1.59	25.94	1.70	26
27	26.96	1.41	26.96	1.53	26.95	1.65	26.94	1.77	27
28	27.96	1.47	27.95	1.59	27.95	1.71	27.94	1.83	28
29	28.96	1.52	28.95	1.64	28.95	1.77	28.94	1.90	29
30	29.96	1.57	29.95	1.70	29.94	1.83	29.94	1.96	30
31	30.96	1.62	30.95	1.76	30.94	1.89	30.93	2.03	31
32	31.96	1.67	31.95	1.81	31.94	1.95	31.93	2.09	32
33	32.95	1.73	32.95	1.87	32.94	2.01	32.93	2.16	33
34	33.95	1.78	33.95	1.93	33.94	2.08	33.93	2.22	34
35	34.95	1.83	34.94	1.98	34.93	2.11	34.92	2.29	35
36	35.95	1.88	35.94	2.04	35.93	2.20	35.92	2.35	36
37	36.95	1.94	36.94	2.10	36.93	2.26	36.92	2.42	37
38	37.95	1.99	37.94	2.15	37.93	2.32	37.92	2.49	38
39	38.95	2.04	38.94	2.21	38.93	2.38	38.92	2.55	39
40	39.95	2.09	39.94	2.27	39.93	2.44	39.91	2.62	40
41	40.94	2.15	40.93	2.32	40.92	2.50	40.91	2.63	41
42	41.94	2.20	41.93	2.38	41.92	2.56	41.91	2.75	42
43	42.94	2.25	42.93	2.44	42.92	2.63	42.91	2.81	43
44	43.94	2.30	43.93	2.49	43.92	2.69	43.91	2.88	44
45	44.94	2.36	44.93	2.55	44.92	2.75	44.90	2.94	45
46	45.94	2.41	45.93	2.61	45.91	2.81	45.90	3.01	46
47	46.94	2.46	46.92	2.66	46.91	2.87	46.90	3.07	47
48	47.93	2.51	47.92	2.72	47.91	2.93	47.90	3.14	48
49	48.93	2.56	48.92	2.78	48.91	2.99	48.90	3.20	49
50	49.93	2.62	49.92	2.83	49.91	3.05	49.89	3.27	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	87 Deg.		86½ Deg.		86½ Deg.		86¼ Deg.		

TRAVERSE TABLE.

Distance.	3 Deg.		3½ Deg.		3¾ Deg.		3 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.93	2.67	50.92	2.89	50.90	3.11	50.89	3.34	51
52	51.93	2.72	51.92	2.95	51.90	3.17	51.89	3.40	52
53	52.93	2.77	52.91	3.00	52.90	3.24	52.89	3.47	53
54	53.93	2.83	53.91	3.06	53.90	3.30	53.88	3.53	54
55	54.92	2.88	54.91	3.12	54.90	3.36	54.88	3.60	55
56	55.92	2.93	55.91	3.17	55.90	3.42	55.88	3.66	56
57	56.92	2.98	56.91	3.23	56.89	3.48	56.88	3.73	57
58	57.92	3.04	57.91	3.29	57.89	3.54	57.88	3.79	58
59	58.92	3.09	58.91	3.34	58.89	3.60	58.87	3.86	59
60	59.92	3.14	59.90	3.40	59.89	3.66	59.87	3.92	60
61	60.92	3.19	60.90	3.46	60.89	3.72	60.87	3.99	61
62	61.92	3.24	61.90	3.51	61.88	3.79	61.87	4.05	62
63	62.91	3.30	62.90	3.57	62.88	3.85	62.87	4.12	63
64	63.91	3.35	63.90	3.63	63.88	3.91	63.86	4.19	64
65	64.91	3.40	64.90	3.69	64.88	3.97	64.86	4.25	65
66	65.91	3.45	65.89	3.74	65.88	4.03	65.86	4.32	66
67	66.91	3.51	66.89	3.80	66.88	4.09	66.86	4.38	67
68	67.91	3.56	67.89	3.86	67.87	4.15	67.85	4.45	68
69	68.91	3.61	68.89	3.91	68.87	4.21	68.85	4.51	69
70	69.90	3.66	69.89	3.97	69.87	4.27	69.85	4.58	70
71	70.90	3.72	70.89	4.03	70.87	4.33	70.85	4.64	71
72	71.90	3.77	71.88	4.08	71.87	4.40	71.85	4.71	72
73	72.90	3.82	72.88	4.14	72.86	4.46	72.84	4.77	73
74	73.90	3.87	73.88	4.20	73.86	4.52	73.84	4.84	74
75	74.90	3.93	74.88	4.25	74.86	4.58	74.84	4.91	75
76	75.90	3.98	75.88	4.31	75.86	4.64	75.84	4.97	76
77	76.89	4.03	76.88	4.37	76.86	4.70	76.84	5.04	77
78	77.89	4.08	77.87	4.42	77.85	4.76	77.83	5.10	78
79	78.89	4.13	78.87	4.48	78.85	4.82	78.83	5.17	79
80	79.89	4.19	79.87	4.54	79.85	4.88	79.83	5.23	80
81	80.89	4.24	80.87	4.59	80.85	4.94	80.83	5.30	81
82	81.89	4.29	81.87	4.65	81.85	5.01	81.82	5.36	82
83	82.89	4.34	82.87	4.71	82.85	5.07	82.82	5.43	83
84	83.88	4.40	83.86	4.76	83.84	5.13	83.82	5.49	84
85	84.88	4.45	84.86	4.82	84.84	5.19	84.82	5.56	85
86	85.88	4.50	85.86	4.88	85.84	5.25	85.82	5.62	86
87	86.88	4.55	86.86	4.93	86.84	5.31	86.81	5.69	87
88	87.88	4.61	87.86	4.99	87.84	5.37	87.81	5.76	88
89	88.88	4.66	88.86	5.05	88.83	5.43	88.81	5.82	89
90	89.88	4.71	89.86	5.10	89.83	5.49	89.81	5.89	90
91	90.88	4.76	90.85	5.16	90.83	5.56	90.81	5.95	91
92	91.87	4.81	91.85	5.22	91.83	5.62	91.80	6.02	92
93	92.87	4.87	92.85	5.27	92.83	5.68	92.80	6.08	93
94	93.87	4.92	93.85	5.33	93.82	5.74	93.80	6.15	94
95	94.87	4.97	94.85	5.39	94.82	5.80	94.80	6.21	95
96	95.87	5.02	95.85	5.44	95.82	5.86	95.79	6.28	96
97	96.87	5.08	96.84	5.50	96.82	5.92	96.79	6.34	97
98	97.87	5.13	97.84	5.56	97.82	5.98	97.79	6.41	98
99	98.86	5.18	98.84	5.61	98.82	6.04	98.79	6.47	99
100	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	87 Deg.		86½ Deg.		85½ Deg.		86¼ Deg.		



TRAVERSE TABLE

Distance.	4 Deg.		4½ Deg.		4¾ Deg.		4¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.07	1.00	0.07	1.00	0.08	1.00	0.08	1
2	2.00	0.14	1.99	0.15	1.99	0.16	1.99	0.17	2
3	2.99	0.21	2.99	0.22	2.99	0.24	2.99	0.25	3
4	3.99	0.28	3.99	0.30	3.99	0.31	3.98	0.33	4
5	4.99	0.35	4.99	0.37	4.98	0.39	4.98	0.41	5
6	5.99	0.42	5.98	0.44	5.98	0.47	5.98	0.50	6
7	6.98	0.49	6.98	0.52	6.98	0.55	6.97	0.58	7
8	7.98	0.56	7.98	0.59	7.98	0.63	7.97	0.66	8
9	8.98	0.63	8.98	0.67	8.97	0.71	8.97	0.75	9
10	9.98	0.70	9.97	0.74	9.97	0.78	9.97	0.83	10
11	10.97	0.77	10.97	0.82	10.97	0.86	10.96	0.91	11
12	11.97	0.84	11.97	0.89	11.96	0.94	11.96	0.99	12
13	12.97	0.91	12.96	0.96	12.96	1.02	12.96	1.08	13
14	13.97	0.98	13.96	1.04	13.96	1.10	13.95	1.16	14
15	14.96	1.05	14.96	1.11	14.95	1.18	14.95	1.24	15
16	15.96	1.12	15.96	1.19	15.95	1.26	15.95	1.32	16
17	16.96	1.19	16.95	1.26	16.95	1.33	16.94	1.41	17
18	17.96	1.26	17.95	1.33	17.94	1.41	17.94	1.49	18
19	18.95	1.33	18.95	1.40	18.94	1.49	18.93	1.57	19
20	19.95	1.40	19.95	1.48	19.94	1.57	19.93	1.66	20
21	20.95	1.46	20.94	1.56	20.94	1.65	20.93	1.74	21
22	21.95	1.53	21.94	1.63	21.93	1.73	21.92	1.82	22
23	22.94	1.60	22.94	1.70	22.93	1.80	22.92	1.90	23
24	23.94	1.67	23.93	1.78	23.93	1.88	23.92	1.99	24
25	24.94	1.74	24.93	1.85	24.92	1.96	24.91	2.07	25
26	25.94	1.81	25.93	1.93	25.92	2.04	25.91	2.15	26
27	26.93	1.88	26.93	2.00	26.92	2.12	26.91	2.24	27
28	27.93	1.95	27.92	2.08	27.91	2.20	27.90	2.32	28
29	28.93	2.02	28.92	2.15	28.91	2.28	28.90	2.40	29
30	29.93	2.09	29.92	2.22	29.91	2.35	29.90	2.48	30
31	30.92	2.16	30.91	2.30	30.90	2.43	30.89	2.57	31
32	31.92	2.23	31.91	2.37	31.90	2.51	31.89	2.65	32
33	32.92	2.30	32.91	2.45	32.90	2.59	32.89	2.73	33
34	33.92	2.37	33.91	2.52	33.90	2.67	33.88	2.82	34
35	34.91	2.44	34.90	2.59	34.89	2.75	34.88	2.90	35
36	35.91	2.51	35.90	2.67	35.89	2.82	35.88	2.98	36
37	36.91	2.58	36.90	2.74	36.89	2.90	36.87	3.06	37
38	37.91	2.65	37.90	2.82	37.88	2.98	37.87	3.15	38
39	38.90	2.72	38.89	2.89	38.88	3.06	38.87	3.23	39
40	39.90	2.79	39.89	2.96	39.88	3.14	39.86	3.31	40
41	40.90	2.86	40.89	3.04	40.87	3.22	40.86	3.40	41
42	41.90	2.93	41.88	3.11	41.87	3.30	41.86	3.48	42
43	42.90	3.00	42.88	3.19	42.87	3.37	42.85	3.56	43
44	43.89	3.07	43.88	3.26	43.86	3.45	43.85	3.64	44
45	44.89	3.14	44.88	3.33	44.86	3.53	44.85	3.73	45
46	45.89	3.21	45.87	3.41	45.86	3.61	45.84	3.81	46
47	46.89	3.28	46.87	3.48	46.86	3.69	46.84	3.89	47
48	47.88	3.35	47.87	3.56	47.85	3.77	47.84	3.97	48
49	48.88	3.42	48.87	3.63	48.85	3.84	48.83	4.06	49
50	49.88	3.49	49.86	3.71	49.85	3.92	49.83	4.14	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	86 Deg.		85½ Deg.		85¼ Deg.		85¼ Deg.		

TRAVERSE TABLE.

Distance.	4 Deg.		4½ Deg.		4½ Deg.		4½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.88	3.56	50.86	3.78	50.84	4.00	50.82	4.22	51
52	51.87	3.63	51.86	3.85	51.84	4.08	51.82	4.31	52
53	52.87	3.70	52.85	3.93	52.84	4.16	52.82	4.39	53
54	53.87	3.77	53.85	4.00	53.83	4.24	53.81	4.47	54
55	54.87	3.84	54.85	4.08	54.83	4.32	54.81	4.55	55
56	55.86	3.91	55.85	4.15	55.83	4.39	55.81	4.64	56
57	56.86	3.98	56.84	4.22	56.82	4.47	56.80	4.72	57
58	57.86	4.05	57.84	4.30	57.82	4.55	57.80	4.80	58
59	58.86	4.12	58.84	4.37	58.82	4.63	58.80	4.89	59
60	59.85	4.19	59.84	4.45	59.82	4.71	59.79	4.97	60
61	60.85	4.26	60.83	4.52	60.81	4.79	60.79	5.05	61
62	61.85	4.32	61.83	4.59	61.81	4.86	61.79	5.13	62
63	62.85	4.39	62.83	4.67	62.81	4.94	62.78	5.22	63
64	63.84	4.46	63.82	4.74	63.80	5.02	63.78	5.30	64
65	64.84	4.53	64.82	4.82	64.80	5.10	64.78	5.38	65
66	65.84	4.60	65.82	4.89	65.80	5.18	65.77	5.47	66
67	66.84	4.67	66.82	4.97	66.79	5.26	66.77	5.55	67
68	67.83	4.74	67.81	5.04	67.79	5.34	67.77	5.63	68
69	68.83	4.81	68.81	5.11	68.79	5.41	68.76	5.71	69
70	69.83	4.88	69.81	5.19	69.78	5.49	69.76	5.80	70
71	70.83	4.95	70.80	5.26	70.78	5.57	70.76	5.88	71
72	71.82	5.02	71.80	5.34	71.78	5.65	71.75	5.96	72
73	72.82	5.09	72.80	5.41	72.77	5.73	72.75	6.04	73
74	73.82	5.16	73.80	5.48	73.77	5.81	73.75	6.13	74
75	74.82	5.23	74.79	5.56	74.77	5.88	74.74	6.21	75
76	75.81	5.30	75.79	5.63	75.77	5.96	75.74	6.29	76
77	76.81	5.37	76.79	5.71	76.76	6.04	76.74	6.38	77
78	77.81	5.44	77.79	5.78	77.76	6.12	77.73	6.46	78
79	78.81	5.51	78.78	5.85	78.76	6.20	78.73	6.54	79
80	79.81	5.58	79.78	5.93	79.75	6.28	79.73	6.62	80
81	80.80	5.65	80.78	6.00	80.75	6.36	80.72	6.71	81
82	81.80	5.72	81.78	6.08	81.75	6.43	81.72	6.79	82
83	82.80	5.79	82.77	6.15	82.74	6.51	82.71	6.87	83
84	83.80	5.86	83.77	6.23	83.74	6.59	83.71	6.96	84
85	84.79	5.93	84.77	6.30	84.74	6.67	84.71	7.04	85
86	85.79	6.00	85.76	6.37	85.73	6.75	85.70	7.12	86
87	86.79	6.07	86.76	6.45	86.73	6.83	86.70	7.20	87
88	87.79	6.14	87.76	6.52	87.73	6.90	87.70	7.29	88
89	88.78	6.21	88.76	6.60	88.73	6.98	88.70	7.37	89
90	89.78	6.28	89.75	6.67	89.72	7.06	89.69	7.45	90
91	90.78	6.35	90.75	6.74	90.72	7.14	90.69	7.54	91
92	91.78	6.42	91.75	6.82	91.72	7.22	91.68	7.62	92
93	92.77	6.49	92.74	6.89	92.71	7.30	92.68	7.70	93
94	93.77	6.56	93.74	6.97	93.71	7.38	93.68	7.78	94
95	94.77	6.63	94.74	7.04	94.71	7.45	94.67	7.87	95
96	95.77	6.70	95.74	7.11	95.70	7.53	95.67	7.95	96
97	96.76	6.77	96.73	7.19	96.70	7.61	96.67	8.03	97
98	97.76	6.84	97.73	7.26	97.70	7.69	97.66	8.12	98
99	98.76	6.91	98.73	7.34	98.69	7.77	98.66	8.20	99
100	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	86 Deg.		85½ Deg.		85½ Deg.		85½ Deg.		

Distance.	5 Deg.		5½ Deg.		5¾ Deg.		5¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	1.00	0.09	1.00	0.09	1.00	0.10	0.99	0.10	1
2	1.99	0.17	1.99	0.18	1.99	0.19	1.99	0.20	2
3	2.99	0.26	2.99	0.27	2.99	0.29	2.98	0.30	3
4	3.98	0.35	3.98	0.37	3.98	0.38	3.98	0.40	4
5	4.98	0.44	4.98	0.46	4.98	0.48	4.97	0.50	5
6	5.98	0.52	5.97	0.55	5.97	0.58	5.97	0.60	6
7	6.97	0.61	6.97	0.64	6.97	0.67	6.96	0.70	7
8	7.97	0.70	7.97	0.73	7.96	0.76	7.96	0.80	8
9	8.97	0.78	8.96	0.82	8.96	0.86	8.95	0.90	9
10	9.96	0.87	9.96	0.92	9.95	0.96	9.95	1.00	10
11	10.96	0.96	10.95	1.01	10.95	1.05	10.94	1.10	11
12	11.95	1.05	11.95	1.10	11.94	1.15	11.94	1.20	12
13	12.95	1.13	12.95	1.19	12.94	1.25	12.93	1.30	13
14	13.95	1.22	13.94	1.28	13.94	1.34	13.93	1.40	14
15	14.94	1.31	14.94	1.37	14.93	1.44	14.92	1.50	15
16	15.94	1.39	15.93	1.46	15.93	1.53	15.92	1.60	16
17	16.94	1.48	16.93	1.56	16.92	1.63	16.91	1.70	17
18	17.93	1.57	17.92	1.65	17.92	1.73	17.91	1.80	18
19	18.93	1.66	18.92	1.74	18.91	1.82	18.90	1.90	19
20	19.92	1.74	19.92	1.83	19.91	1.92	19.90	2.00	20
21	20.92	1.83	20.91	1.92	20.90	2.01	20.89	2.10	21
22	21.92	1.92	21.91	2.01	21.90	2.11	21.89	2.20	22
23	22.91	2.00	22.90	2.10	22.89	2.20	22.88	2.30	23
24	23.91	2.09	23.90	2.20	23.89	2.30	23.88	2.40	24
25	24.90	2.18	24.90	2.29	24.88	2.40	24.87	2.50	25
26	25.90	2.27	25.89	2.38	25.88	2.49	25.87	2.60	26
27	26.90	2.35	26.89	2.47	26.88	2.59	26.86	2.71	27
28	27.89	2.44	27.88	2.56	27.87	2.68	27.86	2.81	28
29	28.89	2.53	28.88	2.65	28.87	2.78	28.85	2.91	29
30	29.89	2.61	29.87	2.75	29.86	2.88	29.85	3.01	30
31	30.88	2.70	30.87	2.84	30.86	2.97	30.84	3.11	31
32	31.88	2.79	31.87	2.93	31.85	3.07	31.84	3.21	32
33	32.87	2.88	32.86	3.02	32.85	3.16	32.83	3.31	33
34	33.87	2.96	33.86	3.11	33.84	3.26	33.83	3.41	34
35	34.87	3.05	34.85	3.20	34.84	3.35	34.82	3.51	35
36	35.86	3.14	35.85	3.29	35.83	3.45	35.82	3.61	36
37	36.86	3.22	36.84	3.39	36.83	3.55	36.81	3.71	37
38	37.86	3.31	37.84	3.48	37.83	3.64	37.81	3.81	38
39	38.85	3.40	38.84	3.57	38.82	3.74	38.80	3.91	39
40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	4.01	40
41	40.84	3.57	40.83	3.75	40.81	3.93	40.79	4.11	41
42	41.84	3.66	41.82	3.84	41.81	4.03	41.79	4.21	42
43	42.84	3.75	42.82	3.93	42.80	4.12	42.78	4.31	43
44	43.83	3.83	43.82	4.03	43.80	4.22	43.78	4.41	44
45	44.83	3.92	44.81	4.12	44.79	4.31	44.77	4.51	45
46	45.82	4.01	45.81	4.21	45.79	4.41	45.77	4.61	46
47	46.82	4.10	46.80	4.30	46.78	4.50	46.76	4.71	47
48	47.82	4.18	47.80	4.39	47.78	4.60	47.76	4.81	48
49	48.81	4.27	48.79	4.48	48.77	4.70	48.75	4.91	49
50	49.81	4.36	49.79	4.58	49.77	4.79	49.75	5.01	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	85 Deg.		84½ Deg.		84¼ Deg.		84¼ Deg.		

Distance.	5 Deg.		5¼ Deg.		5½ Deg.		5¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.81	4.44	50.79	4.67	50.77	4.89	50.74	5.11	51
52	51.80	4.53	51.78	4.76	51.76	4.98	51.74	5.21	52
53	52.80	4.62	52.78	4.85	52.76	5.08	52.73	5.31	53
54	53.79	4.71	53.77	4.94	53.75	5.18	53.73	5.41	54
55	54.79	4.79	54.77	5.03	54.75	5.27	54.72	5.51	55
56	55.79	4.88	55.77	5.12	55.74	5.37	55.72	5.61	56
57	56.78	4.97	56.76	5.22	56.74	5.46	56.71	5.71	57
58	57.78	5.06	57.76	5.31	57.73	5.56	57.71	5.81	58
59	58.78	5.14	58.75	5.40	58.73	5.65	58.70	5.91	59
60	59.77	5.23	59.75	5.49	59.72	5.75	59.70	6.01	60
61	60.77	5.32	60.74	5.58	60.72	5.85	60.69	6.11	61
62	61.76	5.40	61.74	5.67	61.71	5.94	61.69	6.21	62
63	62.76	5.49	62.74	5.76	62.71	6.04	62.68	6.31	63
64	63.76	5.58	63.73	5.86	63.71	6.13	63.68	6.41	64
65	64.75	5.67	64.73	5.95	64.70	6.23	64.67	6.51	65
66	65.75	5.75	65.72	6.04	65.70	6.33	65.67	6.61	66
67	66.75	5.84	66.72	6.13	66.69	6.42	66.66	6.71	67
68	67.74	5.93	67.71	6.22	67.69	6.52	67.66	6.81	68
69	68.74	6.01	68.71	6.31	68.68	6.61	68.65	6.91	69
70	69.73	6.10	69.71	6.41	69.68	6.71	69.65	7.01	70
71	70.73	6.19	70.70	6.50	70.67	6.81	70.64	7.11	71
72	71.73	6.28	71.70	6.59	71.67	6.90	71.64	7.21	72
73	72.72	6.36	72.69	6.68	72.66	7.00	72.63	7.31	73
74	73.72	6.45	73.69	6.77	73.66	7.09	73.63	7.41	74
75	74.71	6.54	74.69	6.86	74.65	7.19	74.62	7.51	75
76	75.71	6.62	75.68	6.95	75.65	7.28	75.62	7.61	76
77	76.71	6.71	76.68	7.05	76.65	7.38	76.61	7.71	77
78	77.70	6.80	77.67	7.14	77.64	7.48	77.61	7.81	78
79	78.70	6.89	78.67	7.23	78.64	7.57	78.60	7.91	79
80	79.70	6.97	79.66	7.32	79.63	7.67	79.60	8.02	80
81	80.69	7.06	80.66	7.41	80.63	7.76	80.59	8.12	81
82	81.69	7.15	81.66	7.50	81.62	7.86	81.59	8.22	82
83	82.68	7.23	82.65	7.59	82.62	7.96	82.58	8.32	83
84	83.68	7.32	83.65	7.69	83.61	8.05	83.58	8.42	84
85	84.68	7.41	84.64	7.78	84.61	8.15	84.57	8.52	85
86	85.67	7.50	85.64	7.87	85.60	8.24	85.57	8.62	86
87	86.67	7.58	86.64	7.96	86.60	8.34	86.56	8.72	87
88	87.67	7.67	87.63	8.05	87.59	8.43	87.56	8.82	88
89	88.66	7.76	88.63	8.14	88.59	8.53	88.55	8.92	89
90	89.66	7.84	89.62	8.24	89.59	8.63	89.55	9.02	90
91	90.65	7.93	90.62	8.33	90.58	8.72	90.54	9.12	91
92	91.65	8.02	91.61	8.42	91.58	8.82	91.54	9.22	92
93	92.65	8.11	92.61	8.51	92.57	8.91	92.53	9.32	93
94	93.64	8.19	93.61	8.60	93.57	9.01	93.53	9.42	94
95	94.64	8.28	94.60	8.69	94.56	9.11	94.52	9.52	95
96	95.63	8.37	95.60	8.78	95.56	9.20	95.52	9.62	96
97	96.63	8.45	96.59	8.88	96.55	9.30	96.51	9.72	97
98	97.63	8.54	97.59	8.97	97.55	9.39	97.51	9.82	98
99	98.62	8.63	98.59	9.06	98.54	9.49	98.50	9.92	99
100	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	85 Deg.		84¼ Deg.		84½ Deg.		84¾ Deg.		

Distance.	6 Deg.		6½ Deg.		6¾ Deg.		6¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.10	0.99	0.11	0.99	0.11	0.99	0.12	1
2	1.99	0.21	1.99	0.22	1.99	0.23	1.99	0.24	2
3	2.98	0.31	2.98	0.33	2.98	0.34	2.98	0.35	3
4	3.98	0.41	3.98	0.44	3.97	0.45	3.97	0.47	4
5	4.97	0.52	4.97	0.54	4.97	0.57	4.97	0.59	5
6	5.96	0.63	5.96	0.65	5.96	0.68	5.96	0.71	6
7	6.95	0.73	6.95	0.76	6.95	0.79	6.95	0.82	7
8	7.95	0.84	7.95	0.87	7.95	0.91	7.94	0.94	8
9	8.95	0.94	8.95	0.98	8.94	1.02	8.94	1.06	9
10	9.94	1.05	9.94	1.09	9.94	1.13	9.93	1.18	10
11	10.94	1.15	10.93	1.20	10.93	1.25	10.92	1.29	11
12	11.93	1.25	11.93	1.31	11.92	1.36	11.92	1.41	12
13	12.93	1.35	12.92	1.42	12.92	1.47	12.91	1.53	13
14	13.92	1.46	13.92	1.52	13.91	1.59	13.90	1.65	14
15	14.92	1.57	14.91	1.63	14.91	1.70	14.90	1.76	15
16	15.91	1.67	15.90	1.74	15.90	1.81	15.89	1.88	16
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00	17
18	17.91	1.88	17.89	1.96	17.88	2.04	17.88	2.12	18
19	18.90	1.99	18.89	2.07	18.88	2.15	18.87	2.23	19
20	19.89	2.09	19.88	2.18	19.87	2.26	19.86	2.35	20
21	20.89	2.20	20.87	2.29	20.87	2.38	20.85	2.47	21
22	21.88	2.30	21.87	2.40	21.86	2.49	21.85	2.59	22
23	22.87	2.40	22.86	2.50	22.85	2.60	22.84	2.70	23
24	23.87	2.51	23.86	2.61	23.85	2.72	23.83	2.82	24
25	24.86	2.61	24.85	2.72	24.84	2.83	24.83	2.94	25
26	25.86	2.72	25.85	2.83	25.83	2.94	25.82	3.06	26
27	26.85	2.82	26.84	2.94	26.83	3.06	26.81	3.17	27
28	27.85	2.93	27.83	3.05	27.82	3.17	27.81	3.29	28
29	28.84	3.03	28.83	3.16	28.81	3.28	28.80	3.41	29
30	29.84	3.14	29.82	3.27	29.81	3.40	29.79	3.53	30
31	30.83	3.24	30.82	3.37	30.80	3.51	30.79	3.64	31
32	31.82	3.34	31.81	3.48	31.79	3.62	31.78	3.76	32
33	32.82	3.45	32.80	3.59	32.79	3.74	32.77	3.88	33
34	33.81	3.55	33.80	3.70	33.78	3.85	33.76	4.00	34
35	34.81	3.66	34.79	3.81	34.78	3.96	34.76	4.11	35
36	35.80	3.76	35.79	3.92	35.77	4.08	35.75	4.23	36
37	36.80	3.87	36.78	4.03	36.76	4.19	36.75	4.35	37
38	37.79	3.97	37.77	4.14	37.76	4.30	37.74	4.47	38
39	38.79	4.08	38.77	4.25	38.75	4.41	38.73	4.58	39
40	39.78	4.18	39.76	4.35	39.74	4.53	39.72	4.70	40
41	40.78	4.29	40.76	4.46	40.74	4.64	40.72	4.82	41
42	41.77	4.39	41.75	4.57	41.73	4.76	41.71	4.94	42
43	42.76	4.49	42.74	4.68	42.72	4.87	42.70	5.05	43
44	43.76	4.60	43.74	4.79	43.72	4.98	43.70	5.17	44
45	44.75	4.70	44.73	4.90	44.71	5.09	44.69	5.29	45
46	45.75	4.81	45.73	5.01	45.70	5.21	45.68	5.41	46
47	46.74	4.91	46.72	5.12	46.70	5.32	46.67	5.52	47
48	47.74	5.02	47.71	5.23	47.69	5.43	47.67	5.64	48
49	48.73	5.12	48.71	5.34	48.69	5.55	48.66	5.76	49
50	49.73	5.23	49.70	5.44	49.68	5.66	49.65	5.88	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	84 Deg.		83½ Deg.		83¼ Deg.		83¼ Deg.		

TRAVERSE TABLE.

Distance.	6 Deg.		6¼ Deg.		6½ Deg.		6¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.72	5.33	50.70	5.55	50.67	5.77	50.65	5.99	51
52	51.72	5.44	51.69	5.66	51.67	5.89	51.64	6.11	52
53	52.71	5.54	52.68	5.77	52.66	6.00	52.63	6.23	53
54	53.70	5.64	53.68	5.88	53.65	6.11	53.63	6.35	54
55	54.70	5.75	54.67	5.99	54.65	6.23	54.62	6.46	55
56	55.69	5.85	55.67	6.10	55.64	6.34	55.61	6.58	56
57	56.69	5.96	56.66	6.21	56.63	6.45	56.60	6.70	57
58	57.68	6.06	57.66	6.31	57.63	6.57	57.60	6.82	58
59	58.68	6.17	58.65	6.42	58.62	6.68	58.59	6.93	59
60	59.67	6.27	59.64	6.53	59.61	6.79	59.58	7.05	60
61	60.67	6.38	60.64	6.64	60.61	6.91	60.58	7.17	61
62	61.66	6.48	61.63	6.75	61.60	7.02	61.57	7.29	62
63	62.65	6.59	62.63	6.86	62.60	7.13	62.56	7.40	63
64	63.65	6.69	63.62	6.97	63.59	7.25	63.56	7.52	64
65	64.64	6.79	64.61	7.08	64.58	7.36	64.55	7.64	65
66	65.64	6.90	65.61	7.19	65.58	7.47	65.54	7.76	66
67	66.63	7.00	66.60	7.29	66.57	7.58	66.54	7.88	67
68	67.63	7.11	67.60	7.40	67.56	7.70	67.53	7.99	68
69	68.62	7.21	68.59	7.51	68.56	7.81	68.52	8.11	69
70	69.62	7.32	69.58	7.62	69.55	7.92	69.51	8.23	70
71	70.61	7.42	70.58	7.73	70.54	8.04	70.51	8.35	71
72	71.61	7.53	71.57	7.84	71.54	8.15	71.50	8.46	72
73	72.60	7.63	72.57	7.95	72.53	8.26	72.49	8.58	73
74	73.59	7.74	73.56	8.06	73.52	8.38	73.49	8.70	74
75	74.59	7.84	74.55	8.17	74.52	8.49	74.48	8.82	75
76	75.58	7.94	75.55	8.27	75.51	8.60	75.47	8.93	76
77	76.58	8.05	76.54	8.38	76.51	8.72	76.47	9.05	77
78	77.57	8.15	77.54	8.49	77.50	8.83	77.46	9.17	78
79	78.57	8.26	78.53	8.60	78.49	8.94	78.45	9.29	79
80	79.56	8.36	79.53	8.71	79.49	9.06	79.45	9.40	80
81	80.56	8.47	80.52	8.82	80.48	9.17	80.44	9.52	81
82	81.55	8.57	81.51	8.93	81.47	9.28	81.43	9.64	82
83	82.55	8.68	82.51	9.04	82.47	9.40	82.42	9.76	83
84	83.54	8.78	83.50	9.14	83.46	9.51	83.42	9.87	84
85	84.53	8.88	84.50	9.25	84.45	9.62	84.41	9.99	85
86	85.53	8.99	85.49	9.36	85.45	9.74	85.40	10.11	86
87	86.52	9.09	86.48	9.47	86.44	9.85	86.40	10.23	87
88	87.52	9.20	87.48	9.58	87.43	9.96	87.39	10.34	88
89	88.51	9.30	88.47	9.69	88.43	10.08	88.38	10.46	89
90	89.51	9.41	89.47	9.80	89.42	10.19	89.38	10.58	90
91	90.50	9.51	90.46	9.91	90.42	10.30	90.37	10.70	91
92	91.50	9.62	91.45	10.02	91.41	10.41	91.36	10.81	92
93	92.49	9.72	92.45	10.12	92.40	10.53	92.36	10.93	93
94	93.49	9.83	93.44	10.23	93.40	10.64	93.35	11.05	94
95	94.48	9.93	94.44	10.34	94.39	10.75	94.34	11.17	95
96	95.47	10.03	95.43	10.45	95.38	10.87	95.33	11.28	96
97	96.47	10.14	96.42	10.56	96.38	10.98	96.33	11.40	97
98	97.46	10.24	97.42	10.67	97.37	11.09	97.32	11.52	98
99	98.46	10.35	98.41	10.78	98.36	11.21	98.31	11.64	99
100	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	84 Deg.		83¾ Deg.		83½ Deg.		83¼ Deg.		

Distance.	7 Deg.		7½ Deg.		7¾ Deg.		7¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.12	0.99	0.13	0.99	0.13	0.99	0.13	1
2	1.99	0.24	1.98	0.25	1.98	0.26	1.98	0.27	2
3	2.98	0.37	2.98	0.38	2.97	0.39	2.97	0.40	3
4	3.97	0.49	3.97	0.50	3.97	0.52	3.96	0.54	4
5	4.96	0.61	4.96	0.63	4.96	0.65	4.95	0.67	5
6	5.96	0.73	5.95	0.76	5.95	0.78	5.95	0.81	6
7	6.95	0.85	6.94	0.88	6.94	0.91	6.94	0.94	7
8	7.94	0.97	7.94	1.01	7.93	1.04	7.93	1.08	8
9	8.93	1.10	8.93	1.14	8.92	1.17	8.92	1.21	9
10	9.93	1.22	9.92	1.26	9.91	1.31	9.91	1.35	10
11	10.92	1.34	10.91	1.39	10.91	1.44	10.90	1.48	11
12	11.91	1.46	11.90	1.51	11.90	1.57	11.89	1.62	12
13	12.90	1.58	12.90	1.64	12.89	1.70	12.88	1.75	13
14	13.90	1.71	13.89	1.77	13.88	1.83	13.87	1.89	14
15	14.89	1.83	14.88	1.89	14.87	1.96	14.86	2.02	15
16	15.88	1.95	15.87	2.02	15.86	2.09	15.85	2.16	16
17	16.87	2.07	16.86	2.15	16.85	2.22	16.84	2.29	17
18	17.87	2.19	17.86	2.27	17.85	2.35	17.84	2.43	18
19	18.86	2.32	18.85	2.40	18.84	2.48	18.83	2.56	19
20	19.85	2.44	19.84	2.52	19.83	2.61	19.82	2.70	20
21	20.84	2.56	20.83	2.65	20.82	2.74	20.81	2.83	21
22	21.84	2.68	21.82	2.78	21.81	2.87	21.80	2.97	22
23	22.83	2.80	22.82	2.90	22.80	3.00	22.79	3.10	23
24	23.82	2.92	23.81	3.03	23.79	3.13	23.78	3.24	24
25	24.81	3.05	24.80	3.15	24.79	3.26	24.77	3.37	25
26	25.81	3.17	25.79	3.28	25.78	3.39	25.76	3.51	26
27	26.80	3.29	26.78	3.41	26.77	3.52	26.75	3.64	27
28	27.79	3.41	27.78	3.53	27.76	3.65	27.74	3.78	28
29	28.78	3.53	28.77	3.66	28.75	3.79	28.74	3.91	29
30	29.78	3.66	29.76	3.79	29.74	3.92	29.73	4.05	30
31	30.77	3.78	30.75	3.91	30.73	4.05	30.72	4.18	31
32	31.76	3.90	31.74	4.04	31.73	4.18	31.71	4.32	32
33	32.75	4.02	32.74	4.16	32.72	4.31	32.70	4.45	33
34	33.75	4.14	33.73	4.29	33.71	4.44	33.69	4.58	34
35	34.74	4.27	34.72	4.42	34.70	4.57	34.68	4.72	35
36	35.73	4.39	35.71	4.54	35.69	4.70	35.67	4.85	36
37	36.72	4.51	36.70	4.67	36.68	4.83	36.66	4.99	37
38	37.72	4.63	37.70	4.80	37.67	4.96	37.65	5.12	38
39	38.71	4.75	38.69	4.92	38.67	5.09	38.64	5.26	39
40	39.70	4.87	39.68	5.05	39.66	5.22	39.63	5.39	40
41	40.70	5.00	40.67	5.17	40.65	5.35	40.63	5.53	41
42	41.69	5.12	41.66	5.30	41.64	5.48	41.62	5.66	42
43	42.68	5.24	42.66	5.43	42.63	5.61	42.61	5.80	43
44	43.67	5.36	43.65	5.55	43.62	5.74	43.60	5.93	44
45	44.67	5.48	44.64	5.68	44.62	5.87	44.59	6.07	45
46	45.66	5.61	45.63	5.81	45.61	6.00	45.58	6.20	46
47	46.65	5.73	46.62	5.93	46.60	6.13	46.57	6.34	47
48	47.64	5.85	47.62	6.06	47.59	6.27	47.56	6.47	48
49	48.63	5.97	48.61	6.18	48.58	6.40	48.55	6.61	49
50	49.63	6.09	49.60	6.31	49.57	6.53	49.54	6.74	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	83 Deg.		82½ Deg.		82¼ Deg.		82¼ Deg.		

TRAVERSE TABLE.

17

Distance.	7 Deg.		7½ Deg.		7½ Deg.		7½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88	51
52	51.61	6.34	51.58	6.56	51.56	6.79	51.53	7.01	52
53	52.60	6.46	52.58	6.69	52.55	6.92	52.52	7.15	53
54	53.60	6.58	53.57	6.81	53.54	7.05	53.51	7.28	54
55	54.59	6.70	54.56	6.94	54.53	7.18	54.50	7.42	55
56	55.58	6.82	55.55	7.07	55.52	7.31	55.49	7.55	56
57	56.58	6.95	56.54	7.19	56.51	7.44	56.48	7.69	57
58	57.57	7.07	57.54	7.32	57.50	7.57	57.47	7.82	58
59	58.56	7.19	58.53	7.45	58.50	7.70	58.46	7.96	59
60	59.55	7.31	59.52	7.57	59.49	7.83	59.45	8.09	60
61	60.55	7.43	60.51	7.70	60.48	7.96	60.44	8.23	61
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43	8.36	62
63	62.53	7.68	62.50	7.95	62.46	8.22	62.42	8.50	63
64	63.52	7.80	63.49	8.08	63.45	8.35	63.42	8.63	64
65	64.52	7.92	64.48	8.20	64.44	8.48	64.41	8.77	65
66	65.51	8.04	65.47	8.33	65.44	8.61	65.40	8.90	66
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39	9.04	67
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17	68
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	9.30	69
70	69.48	8.53	69.44	8.83	69.40	9.14	69.36	9.44	70
71	70.47	8.65	70.43	8.96	70.39	9.27	70.35	9.57	71
72	71.46	8.77	71.42	9.09	71.38	9.40	71.34	9.71	72
73	72.46	8.90	72.42	9.21	72.38	9.53	72.33	9.84	73
74	73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98	74
75	74.44	9.14	74.40	9.46	74.36	9.79	74.31	10.11	75
76	75.43	9.26	75.39	9.59	75.35	9.92	75.31	10.25	76
77	76.43	9.38	76.38	9.72	76.34	10.05	76.30	10.38	77
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29	10.52	78
79	78.41	9.63	78.37	9.97	78.32	10.31	78.28	10.65	79
80	79.40	9.75	79.36	10.10	79.32	10.44	79.27	10.79	80
81	80.40	9.87	80.35	10.22	80.31	10.57	80.26	10.92	81
82	81.39	9.99	81.34	10.35	81.30	10.70	81.25	11.06	82
83	82.38	10.12	82.34	10.47	82.29	10.83	82.24	11.19	83
84	83.37	10.24	83.33	10.60	83.28	10.96	83.23	11.33	84
85	84.37	10.36	84.32	10.73	84.27	11.09	84.22	11.46	85
86	85.36	10.48	85.31	10.85	85.26	11.23	85.21	11.60	86
87	86.35	10.60	86.30	10.98	86.26	11.36	86.21	11.73	87
88	87.34	10.72	87.30	11.11	87.25	11.49	87.20	11.87	88
89	88.34	10.85	88.29	11.23	88.24	11.62	88.19	12.00	89
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14	90
91	90.32	11.09	90.27	11.48	90.22	11.88	90.17	12.27	91
92	91.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41	92
93	92.31	11.33	92.26	11.74	92.20	12.14	92.15	12.54	93
94	93.30	11.46	93.25	11.86	93.20	12.27	93.14	12.68	94
95	94.29	11.58	94.24	11.99	94.19	12.40	94.13	12.81	95
96	95.28	11.70	95.23	12.12	95.18	12.53	95.12	12.95	96
97	96.28	11.82	96.22	12.24	96.17	12.66	96.11	13.08	97
98	97.27	11.94	97.22	12.37	97.16	12.79	97.10	13.22	98
99	98.26	12.07	98.21	12.49	98.15	12.92	98.10	13.35	99
100	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	83 Deg.		82½ Deg.		82½ Deg.		82½ Deg.		



Distance.	8 Deg.		8½ Deg.		8½ Deg.		8½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.14	0.99	0.14	0.99	0.15	0.99	0.15	1
2	1.98	0.28	1.98	0.29	1.98	0.30	1.98	0.30	2
3	2.97	0.42	2.97	0.43	2.97	0.44	2.97	0.46	3
4	3.96	0.56	3.96	0.57	3.96	0.59	3.95	0.61	4
5	4.95	0.70	4.95	0.72	4.95	0.74	4.94	0.76	5
6	5.94	0.84	5.94	0.86	5.93	0.89	5.93	0.91	6
7	6.93	0.97	6.93	1.00	6.92	1.03	6.92	1.06	7
8	7.92	1.11	7.92	1.15	7.91	1.18	7.91	1.22	8
9	8.91	1.25	8.91	1.29	8.90	1.33	8.90	1.37	9
10	9.90	1.39	9.90	1.43	9.89	1.48	9.88	1.52	10
11	10.89	1.53	10.89	1.58	10.88	1.63	10.87	1.67	11
12	11.88	1.67	11.88	1.72	11.87	1.77	11.86	1.83	12
13	12.87	1.81	12.87	1.87	12.86	1.92	12.85	1.98	13
14	13.86	1.95	13.86	2.01	13.85	2.07	13.84	2.13	14
15	14.85	2.09	14.85	2.15	14.84	2.22	14.83	2.28	15
16	15.84	2.23	15.84	2.30	15.82	2.36	15.81	2.43	16
17	16.83	2.37	16.83	2.44	16.81	2.51	16.80	2.59	17
18	17.82	2.51	17.81	2.58	17.80	2.66	17.79	2.74	18
19	18.82	2.64	18.80	2.73	18.79	2.81	18.78	2.89	19
20	19.81	2.78	19.79	2.87	19.78	2.95	19.77	3.04	20
21	20.80	2.92	20.78	3.01	20.77	3.10	20.76	3.19	21
22	21.79	3.06	21.77	3.16	21.76	3.25	21.74	3.35	22
23	22.78	3.20	22.76	3.30	22.75	3.40	22.73	3.50	23
24	23.77	3.34	23.75	3.44	23.74	3.55	23.72	3.65	24
25	24.76	3.48	24.74	3.59	24.73	3.70	24.71	3.80	25
26	25.75	3.62	25.73	3.73	25.71	3.84	25.70	3.96	26
27	26.74	3.76	26.72	3.87	26.70	3.99	26.69	4.11	27
28	27.73	3.90	27.71	4.02	27.69	4.14	27.67	4.26	28
29	28.72	4.04	28.70	4.16	28.68	4.29	28.66	4.41	29
30	29.71	4.18	29.69	4.30	29.67	4.43	29.65	4.56	30
31	30.70	4.31	30.68	4.45	30.66	4.58	30.64	4.72	31
32	31.69	4.45	31.67	4.59	31.65	4.73	31.63	4.87	32
33	32.68	4.59	32.66	4.74	32.64	4.88	32.62	5.02	33
34	33.67	4.73	33.65	4.88	33.63	5.03	33.60	5.17	34
35	34.66	4.87	34.64	5.02	34.62	5.17	34.59	5.32	35
36	35.65	5.01	35.63	5.17	35.60	5.32	35.58	5.48	36
37	36.64	5.15	36.62	5.31	36.59	5.47	36.57	5.63	37
38	37.63	5.29	37.61	5.45	37.58	5.62	37.56	5.78	38
39	38.62	5.43	38.60	5.60	38.57	5.76	38.55	5.93	39
40	39.61	5.57	39.59	5.74	39.56	5.91	39.53	6.08	40
41	40.60	5.71	40.58	5.88	40.55	6.06	40.52	6.24	41
42	41.59	5.85	41.57	6.03	41.54	6.21	41.51	6.39	42
43	42.58	5.98	42.56	6.17	42.53	6.36	42.50	6.54	43
44	43.57	6.12	43.54	6.31	43.52	6.50	43.49	6.69	44
45	44.56	6.26	44.53	6.46	44.51	6.65	44.48	6.85	45
46	45.55	6.40	45.52	6.60	45.49	6.80	45.46	7.00	46
47	46.54	6.54	46.51	6.74	46.48	6.95	46.45	7.15	47
48	47.53	6.68	47.50	6.89	47.47	7.09	47.44	7.30	48
49	48.52	6.82	48.49	7.03	48.46	7.24	48.43	7.45	49
50	49.51	6.96	49.48	7.17	49.45	7.39	49.42	7.61	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	82 Deg.		81½ Deg.		81½ Deg.		81½ Deg.		

TRAVERSE TABLE.

Distance.	8 Deg.		8¼ Deg.		8½ Deg.		8¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.50	7.10	50.47	7.32	50.44	7.54	50.41	7.76	51
52	51.49	7.24	51.46	7.46	51.43	7.69	51.39	7.91	52
53	52.48	7.38	52.45	7.61	52.42	7.83	52.38	8.06	53
54	53.47	7.52	53.44	7.75	53.41	7.98	53.37	8.21	54
55	54.46	7.65	54.43	7.89	54.40	8.13	54.36	8.37	55
56	55.46	7.79	55.42	8.04	55.38	8.28	55.35	8.52	56
57	56.45	7.93	56.41	8.18	56.37	8.43	56.34	8.67	57
58	57.44	8.07	57.40	8.32	57.36	8.57	57.32	8.82	58
59	58.43	8.21	58.39	8.47	58.35	8.72	58.31	8.98	59
60	59.42	8.35	59.38	8.61	59.34	8.87	59.30	9.13	60
61	60.41	8.49	60.37	8.75	60.33	9.02	60.29	9.28	61
62	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43	62
63	62.39	8.77	62.35	9.04	62.31	9.31	62.27	9.58	63
64	63.38	8.91	63.34	9.18	63.30	9.46	63.26	9.74	64
65	64.37	9.05	64.33	9.33	64.29	9.61	64.24	9.89	65
66	65.36	9.19	65.32	9.47	65.28	9.76	65.23	10.04	66
67	66.35	9.32	66.31	9.61	66.26	9.90	66.22	10.19	67
68	67.34	9.46	67.30	9.76	67.25	10.05	67.21	10.34	68
69	68.33	9.60	68.29	9.90	68.24	10.20	68.20	10.50	69
70	69.32	9.74	69.28	10.04	69.23	10.35	69.19	10.65	70
71	70.31	9.88	70.27	10.19	70.22	10.49	70.17	10.80	71
72	71.30	10.02	71.25	10.33	71.21	10.64	71.16	10.95	72
73	72.29	10.16	72.24	10.47	72.20	10.79	72.15	11.10	73
74	73.28	10.30	73.23	10.62	73.19	10.94	73.14	11.26	74
75	74.27	10.44	74.22	10.76	74.18	11.09	74.13	11.41	75
76	75.26	10.58	75.21	10.91	75.17	11.23	75.12	11.56	76
77	76.25	10.72	76.20	11.05	76.15	11.38	76.10	11.71	77
78	77.24	10.86	77.19	11.19	77.14	11.53	77.09	11.87	78
79	78.23	10.99	78.18	11.34	78.13	11.68	78.08	12.02	79
80	79.22	11.13	79.17	11.48	79.12	11.82	79.07	12.17	80
81	80.21	11.27	80.16	11.62	80.11	11.97	80.06	12.32	81
82	81.20	11.41	81.15	11.77	81.10	12.12	81.05	12.47	82
83	82.19	11.55	82.14	11.91	82.09	12.27	82.03	12.63	83
84	83.18	11.69	83.13	12.05	83.08	12.42	83.02	12.78	84
85	84.17	11.83	84.12	12.20	84.07	12.56	84.01	12.93	85
86	85.16	11.97	85.11	12.34	85.06	12.71	85.00	13.08	86
87	86.15	12.11	86.10	12.48	86.04	12.86	85.99	13.23	87
88	87.14	12.25	87.09	12.63	87.03	13.01	86.98	13.39	88
89	88.13	12.39	88.08	12.77	88.02	13.16	87.96	13.54	89
90	89.12	12.53	89.07	12.91	89.01	13.30	88.95	13.69	90
91	90.11	12.66	90.06	13.06	90.00	13.45	89.94	13.84	91
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14.00	92
93	92.09	12.94	92.04	13.34	91.98	13.75	91.92	14.15	93
94	93.08	13.08	93.03	13.49	92.97	13.89	92.91	14.30	94
95	94.08	13.22	94.02	13.63	93.96	14.04	93.89	14.45	95
96	95.07	13.36	95.01	13.78	94.95	14.19	94.88	14.60	96
97	96.06	13.50	96.00	13.92	95.93	14.34	95.87	14.76	97
98	97.05	13.64	96.99	14.06	96.92	14.49	96.86	14.91	98
99	98.04	13.78	97.98	14.21	97.91	14.63	97.85	15.06	99
100	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	82 Deg.		81¾ Deg.		81½ Deg.		81¼ Deg.		

TRAVERSE TABLE.

Distance	9 Deg.		9½ Deg.		9¾ Deg.		9¼ Deg		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.99	0.16	0.99	0.16	0.99	0.17	0.99	0.17	1
2	1.98	0.31	1.97	0.32	1.97	0.33	1.97	0.34	2
3	2.96	0.47	2.96	0.48	2.96	0.50	2.96	0.51	3
4	3.95	0.63	3.95	0.64	3.95	0.66	3.94	0.68	4
5	4.94	0.78	4.93	0.80	4.93	0.83	4.93	0.85	5
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02	6
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90	1.19	7
8	7.90	1.25	7.90	1.29	7.89	1.32	7.88	1.35	8
9	8.89	1.41	8.88	1.45	8.88	1.49	8.87	1.52	9
10	9.88	1.56	9.87	1.61	9.86	1.65	9.86	1.69	10
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84	1.86	11
12	11.85	1.88	11.84	1.93	11.84	1.98	11.83	2.03	12
13	12.84	2.03	12.83	2.09	12.82	2.15	12.81	2.20	13
14	13.83	2.19	13.82	2.25	13.81	2.31	13.80	2.37	14
15	14.82	2.35	14.80	2.41	14.79	2.48	14.78	2.54	15
16	15.80	2.50	15.79	2.57	15.78	2.64	15.77	2.71	16
17	16.79	2.66	16.78	2.73	16.77	2.81	16.75	2.88	17
18	17.78	2.82	17.77	2.89	17.75	2.97	17.74	3.05	18
19	18.77	2.97	18.75	3.05	18.74	3.14	18.73	3.22	19
20	19.75	3.13	19.74	3.21	19.73	3.30	19.71	3.39	20
21	20.74	3.29	20.73	3.38	20.71	3.47	20.70	3.56	21
22	21.73	3.44	21.71	3.54	21.70	3.63	21.68	3.73	22
23	22.72	3.60	22.70	3.70	22.68	3.80	22.67	3.90	23
24	23.70	3.75	23.69	3.86	23.67	3.96	23.65	4.06	24
25	24.69	3.91	24.67	4.02	24.66	4.13	24.64	4.23	25
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40	26
27	26.67	4.22	26.65	4.34	26.63	4.46	26.61	4.57	27
28	27.66	4.38	27.64	4.50	27.62	4.62	27.60	4.74	28
29	28.64	4.54	28.62	4.66	28.60	4.79	28.58	4.91	29
30	29.63	4.69	29.61	4.82	29.59	4.95	29.57	5.08	30
31	30.62	4.85	30.60	4.98	30.57	5.12	30.55	5.25	31
32	31.61	5.01	31.58	5.14	31.56	5.28	31.54	5.42	32
33	32.59	5.16	32.57	5.30	32.55	5.45	32.52	5.59	33
34	33.58	5.32	33.56	5.47	33.53	5.61	33.51	5.76	34
35	34.57	5.48	34.54	5.63	34.52	5.78	34.49	5.93	35
36	35.56	5.63	35.53	5.79	35.51	5.94	35.48	6.10	36
37	36.54	5.79	36.52	5.95	36.49	6.11	36.47	6.27	37
38	37.53	5.94	37.51	6.11	37.48	6.27	37.45	6.44	38
39	38.52	6.10	38.49	6.27	38.47	6.44	38.44	6.60	39
40	39.51	6.26	39.48	6.43	39.45	6.60	39.42	6.77	40
41	40.50	6.41	40.47	6.59	40.44	6.77	40.41	6.94	41
42	41.48	6.57	41.45	6.75	41.42	6.92	41.39	7.11	42
43	42.47	6.73	42.44	6.91	42.41	7.10	42.38	7.28	43
44	43.46	6.88	43.43	7.07	43.40	7.26	43.36	7.45	44
45	44.45	7.04	44.41	7.23	44.38	7.43	44.35	7.62	45
46	45.43	7.20	45.40	7.39	45.37	7.59	45.34	7.79	46
47	46.42	7.35	46.39	7.55	46.36	7.76	46.32	7.96	47
48	47.41	7.51	47.38	7.72	47.34	7.92	47.31	8.13	48
49	48.40	7.67	48.36	7.88	48.33	8.09	48.29	8.30	49
50	49.38	7.82	49.35	8.04	49.32	8.25	49.28	8.47	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	81 Deg.		80½ Deg.		80¼ Deg.		80¼ Deg.		

TRAVERSE TABLE.

Distance.	9 Deg.		9½ Deg.		9¾ Deg.		9¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.37	7.98	50.34	8.20	50.30	8.42	50.26	8.64	51
52	51.36	8.13	51.32	8.36	51.29	8.58	51.25	8.81	52
53	52.35	8.29	52.31	8.52	52.27	8.75	52.23	8.98	53
54	53.34	8.45	53.30	8.68	53.26	8.91	53.22	9.14	54
55	54.32	8.60	54.28	8.84	54.25	9.08	54.21	9.31	55
56	55.31	8.76	55.27	9.00	55.23	9.24	55.19	9.48	56
57	56.30	8.92	56.26	9.16	56.22	9.41	56.18	9.65	57
58	57.29	9.07	57.25	9.32	57.20	9.57	57.16	9.82	58
59	58.27	9.23	58.23	9.48	58.19	9.74	58.15	9.99	59
60	59.26	9.39	59.22	9.64	59.18	9.90	59.13	10.16	60
61	60.25	9.54	60.21	9.81	60.16	10.07	60.12	10.33	61
62	61.24	9.70	61.19	9.97	61.15	10.23	61.10	10.50	62
63	62.22	9.86	62.18	10.13	62.14	10.40	62.09	10.67	63
64	63.21	10.01	63.17	10.29	63.12	10.56	63.08	10.84	64
65	64.20	10.17	64.15	10.45	64.11	10.73	64.06	11.01	65
66	65.19	10.32	65.14	10.61	65.09	10.89	65.05	11.18	66
67	66.18	10.48	66.13	10.77	66.08	11.06	66.03	11.35	67
68	67.16	10.64	67.12	10.93	67.07	11.22	67.02	11.52	68
69	68.15	10.79	68.10	11.09	68.05	11.39	68.00	11.69	69
70	69.14	10.95	69.09	11.25	69.04	11.55	68.99	11.85	70
71	70.13	11.11	70.08	11.41	70.03	11.72	69.97	12.02	71
72	71.11	11.26	71.06	11.57	71.01	11.88	70.96	12.19	72
73	72.10	11.42	72.05	11.73	72.00	12.05	71.95	12.36	73
74	73.09	11.58	73.04	11.89	72.99	12.21	72.93	12.53	74
75	74.08	11.73	74.02	12.06	73.97	12.38	73.92	12.70	75
76	75.06	11.89	75.01	12.22	74.96	12.54	74.90	12.87	76
77	76.05	12.05	76.00	12.38	75.94	12.71	75.89	13.04	77
78	77.04	12.20	76.99	12.54	76.93	12.87	76.87	13.21	78
79	78.03	12.36	77.97	12.70	77.92	13.04	77.86	13.38	79
80	79.02	12.51	78.96	12.86	78.90	13.20	78.84	13.55	80
81	80.00	12.67	79.95	13.02	79.89	13.37	79.83	13.72	81
82	80.99	12.83	80.93	13.18	80.88	13.53	80.82	13.89	82
83	81.98	12.98	81.92	13.34	81.86	13.70	81.80	14.06	83
84	82.97	13.14	82.91	13.50	82.85	13.86	82.79	14.23	84
85	83.95	13.30	83.89	13.66	83.83	14.03	83.77	14.39	85
86	84.94	13.45	84.88	13.82	84.82	14.19	84.76	14.56	86
87	85.93	13.61	85.87	13.98	85.81	14.36	85.74	14.73	87
88	86.92	13.77	86.86	14.15	86.79	14.52	86.73	14.90	88
89	87.90	13.92	87.84	14.31	87.78	14.69	87.71	15.07	89
90	88.89	14.08	88.83	14.47	88.77	14.85	88.70	15.24	90
91	89.88	14.24	89.82	14.63	89.75	15.02	89.69	15.41	91
92	90.87	14.39	90.80	14.79	90.74	15.18	90.67	15.58	92
93	91.86	14.55	91.79	14.95	91.72	15.35	91.66	15.75	93
94	92.84	14.70	92.78	15.11	92.71	15.51	92.64	15.92	94
95	93.83	14.86	93.76	15.27	93.70	15.68	93.63	16.09	95
96	94.82	15.02	94.75	15.43	94.68	15.84	94.61	16.26	96
97	95.81	15.17	95.74	15.59	95.67	16.01	95.60	16.43	97
98	96.79	15.33	96.73	15.75	96.66	16.17	96.58	16.60	98
99	97.78	15.49	97.71	15.91	97.64	16.34	97.57	16.77	99
100	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	81 Deg.		80½ Deg.		80¼ Deg.		80¼ Deg.		

TRAVERSE TABLE.

Distance.	10 Deg.		10½ Deg.		10¾ Deg.		10¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.17	0.98	0.18	0.98	0.18	0.98	0.19	1
2	1.97	0.35	1.97	0.36	1.97	0.36	1.96	0.37	2
3	2.95	0.52	2.95	0.53	2.95	0.55	2.95	0.56	3
4	3.94	0.69	3.94	0.71	3.93	0.73	3.93	0.75	4
5	4.92	0.87	4.92	0.89	4.92	0.91	4.91	0.93	5
6	5.91	1.04	5.90	1.07	5.90	1.09	5.89	1.12	6
7	6.89	1.22	6.89	1.25	6.88	1.28	6.88	1.31	7
8	7.88	1.39	7.87	1.42	7.87	1.46	7.86	1.49	8
9	8.86	1.56	8.86	1.60	8.85	1.64	8.84	1.68	9
10	9.85	1.74	9.84	1.78	9.83	1.82	9.82	1.87	10
11	10.83	1.91	10.82	1.96	10.82	2.00	10.81	2.05	11
12	11.82	2.08	11.81	2.14	11.80	2.19	11.79	2.24	12
13	12.80	2.26	12.79	2.31	12.78	2.37	12.77	2.42	13
14	13.79	2.43	13.78	2.49	13.77	2.55	13.75	2.61	14
15	14.77	2.60	14.76	2.67	14.75	2.73	14.74	2.80	15
16	15.76	2.78	15.74	2.85	15.73	2.92	15.72	2.98	16
17	16.74	2.95	16.73	3.03	16.72	3.10	16.70	3.17	17
18	17.73	3.13	17.71	3.20	17.70	3.28	17.68	3.36	18
19	18.71	3.30	18.70	3.38	18.68	3.46	18.67	3.54	19
20	19.70	3.47	19.68	3.56	19.67	3.64	19.65	3.73	20
21	20.68	3.65	20.66	3.74	20.65	3.83	20.63	3.92	21
22	21.67	3.82	21.65	3.91	21.63	4.01	21.61	4.10	22
23	22.65	3.99	22.63	4.09	22.61	4.19	22.60	4.29	23
24	23.64	4.17	23.62	4.27	23.60	4.37	23.58	4.48	24
25	24.62	4.34	24.60	4.45	24.58	4.56	24.56	4.66	25
26	25.61	4.51	25.59	4.63	25.56	4.74	25.54	4.85	26
27	26.59	4.69	26.57	4.80	26.55	4.92	26.53	5.04	27
28	27.57	4.86	27.55	4.98	27.53	5.10	27.51	5.22	28
29	28.56	5.04	28.54	5.16	28.51	5.28	28.49	5.41	29
30	29.54	5.21	29.52	5.34	29.50	5.47	29.47	5.60	30
31	30.53	5.38	30.51	5.52	30.48	5.65	30.46	5.78	31
32	31.51	5.56	31.49	5.69	31.46	5.83	31.44	5.97	32
33	32.50	5.73	32.47	5.87	32.45	6.01	32.42	6.16	33
34	33.48	5.90	33.46	6.05	33.43	6.20	33.40	6.34	34
35	34.47	6.08	34.44	6.23	34.41	6.38	34.39	6.53	35
36	35.45	6.25	35.43	6.41	35.40	6.56	35.37	6.71	36
37	36.44	6.42	36.41	6.58	36.38	6.74	36.35	6.90	37
38	37.42	6.60	37.39	6.76	37.36	6.92	37.33	7.09	38
39	38.41	6.77	38.38	6.94	38.35	7.11	38.32	7.27	39
40	39.39	6.95	39.36	7.12	39.33	7.29	39.30	7.46	40
41	40.38	7.12	40.35	7.30	40.31	7.47	40.28	7.65	41
42	41.36	7.29	41.33	7.47	41.30	7.65	41.26	7.83	42
43	42.35	7.47	42.31	7.65	42.28	7.84	42.25	8.02	43
44	43.33	7.64	43.30	7.83	43.26	8.02	43.23	8.21	44
45	44.32	7.81	44.28	8.01	44.25	8.20	44.21	8.39	45
46	45.30	7.99	45.27	8.19	45.23	8.38	45.19	8.58	46
47	46.29	8.16	46.25	8.36	46.21	8.57	46.18	8.77	47
48	47.27	8.34	47.23	8.54	47.20	8.75	47.16	8.95	48
49	48.26	8.51	48.22	8.72	48.18	8.93	48.14	9.14	49
50	49.24	8.68	49.20	8.90	49.16	9.11	49.12	9.33	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	80 Deg.		79½ Deg.		79¼ Deg.		79¼ Deg.		

Distance.	10 Deg.		10½ Deg.		10¾ Deg.		10¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.23	8.86	50.19	9.08	50.15	9.29	50.10	9.51	51
52	51.21	9.03	51.17	9.25	51.13	9.48	51.09	9.70	52
53	52.19	9.20	52.15	9.43	52.11	9.66	52.07	9.89	53
54	53.18	9.38	53.14	9.61	53.10	9.84	53.05	10.07	54
55	54.16	9.55	54.12	9.79	54.08	10.02	54.03	10.26	55
56	55.15	9.72	55.11	9.96	55.06	10.21	55.02	10.45	56
57	56.13	9.90	56.09	10.14	56.05	10.39	56.00	10.63	57
58	57.12	10.07	57.07	10.32	57.03	10.57	56.98	10.82	58
59	58.10	10.25	58.06	10.50	58.01	10.75	57.96	11.00	59
60	59.09	10.42	59.04	10.68	59.00	10.93	58.95	11.19	60
61	60.07	10.59	60.03	10.85	59.98	11.12	59.93	11.38	61
62	61.06	10.77	61.01	11.03	60.96	11.30	60.91	11.56	62
63	62.04	10.94	61.99	11.21	61.95	11.48	61.89	11.75	63
64	63.03	11.11	62.98	11.39	62.93	11.66	62.88	11.94	64
65	64.01	11.29	63.96	11.57	63.91	11.85	63.86	12.12	65
66	65.00	11.46	64.95	11.74	64.89	12.03	64.84	12.31	66
67	65.98	11.63	65.93	11.92	65.88	12.21	65.82	12.50	67
68	66.97	11.81	66.91	12.10	66.86	12.39	66.81	12.68	68
69	67.95	11.98	67.90	12.28	67.84	12.57	67.79	12.87	69
70	68.94	12.16	68.88	12.46	68.83	12.76	68.77	13.06	70
71	69.92	12.33	69.87	12.63	69.81	12.94	69.75	13.24	71
72	70.91	12.50	70.85	12.81	70.79	13.12	70.74	13.43	72
73	71.89	12.68	71.83	12.99	71.78	13.30	71.72	13.62	73
74	72.88	12.85	72.82	13.17	72.76	13.49	72.70	13.80	74
75	73.86	13.02	73.80	13.35	73.74	13.67	73.68	13.99	75
76	74.85	13.20	74.79	13.52	74.73	13.85	74.67	14.18	76
77	75.83	13.37	75.77	13.70	75.71	14.03	75.65	14.36	77
78	76.82	13.54	76.76	13.88	76.69	14.21	76.63	14.55	78
79	77.80	13.72	77.74	14.06	77.68	14.40	77.61	14.74	79
80	78.78	13.89	78.72	14.24	78.66	14.58	78.60	14.92	80
81	79.77	14.07	79.71	14.41	79.64	14.76	79.58	15.11	81
82	80.75	14.24	80.69	14.59	80.63	14.94	80.56	15.29	82
83	81.74	14.41	81.68	14.77	81.61	15.13	81.54	15.48	83
84	82.72	14.59	82.66	14.95	82.59	15.31	82.53	15.67	84
85	83.71	14.76	83.64	15.13	83.58	15.49	83.51	15.85	85
86	84.69	14.93	84.63	15.30	84.56	15.67	84.49	16.04	86
87	85.68	15.11	85.61	15.48	85.54	15.85	85.47	16.23	87
88	86.66	15.28	86.60	15.66	86.53	16.04	86.46	16.41	88
89	87.65	15.45	87.58	15.84	87.51	16.22	87.44	16.60	89
90	88.63	15.63	88.56	16.01	88.49	16.40	88.42	16.79	90
91	89.62	15.80	89.55	16.19	89.48	16.58	89.40	16.97	91
92	90.60	15.98	90.53	16.37	90.46	16.77	90.39	17.16	92
93	91.59	16.15	91.52	16.55	91.44	16.95	91.37	17.35	93
94	92.57	16.32	92.50	16.73	92.43	17.13	92.35	17.53	94
95	93.56	16.50	93.48	16.90	93.41	17.31	93.33	17.72	95
96	94.54	16.67	94.47	17.08	94.39	17.49	94.32	17.91	96
97	95.53	16.84	95.45	17.26	95.38	17.68	95.30	18.09	97
98	96.51	17.02	96.44	17.44	96.36	17.86	96.28	18.28	98
99	97.50	17.19	97.42	17.62	97.34	18.04	97.26	18.47	99
100	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	80 Deg.		79½ Deg.		79¼ Deg.		79¼ Deg.		

## TRAVERSE TABLE.

Distance.	11 Deg.		11½ Deg.		11¼ Deg.		11½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.19	0.98	0.20	0.98	0.20	0.98	0.20	1
2	1.96	0.38	1.96	0.39	1.96	0.40	1.96	0.41	2
3	2.94	0.57	2.94	0.59	2.94	0.60	2.94	0.61	3
4	3.93	0.76	3.92	0.78	3.92	0.80	3.92	0.82	4
5	4.91	0.95	4.90	0.98	4.90	1.00	4.90	1.02	5
6	5.89	1.14	5.88	1.17	5.88	1.20	5.87	1.22	6
7	6.87	1.34	6.87	1.37	6.86	1.40	6.85	1.43	7
8	7.85	1.53	7.85	1.56	7.84	1.59	7.83	1.63	8
9	8.83	1.72	8.83	1.76	8.82	1.79	8.81	1.83	9
10	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04	10
11	10.80	2.10	10.79	2.15	10.78	2.19	10.77	2.24	11
12	11.78	2.29	11.77	2.34	11.76	2.39	11.75	2.44	12
13	12.76	2.48	12.75	2.54	12.74	2.59	12.73	2.65	13
14	13.74	2.67	13.73	2.73	13.72	2.79	13.71	2.85	14
15	14.72	2.86	14.71	2.93	14.70	2.99	14.69	3.06	15
16	15.71	3.05	15.69	3.12	15.68	3.19	15.66	3.26	16
17	16.69	3.24	16.67	3.32	16.66	3.39	16.64	3.46	17
18	17.67	3.43	17.65	3.51	17.64	3.59	17.62	3.66	18
19	18.65	3.63	18.63	3.71	18.62	3.79	18.60	3.87	19
20	19.63	3.82	19.62	3.90	19.60	3.99	19.58	4.07	20
21	20.61	4.01	20.60	4.10	20.58	4.19	20.56	4.28	21
22	21.60	4.20	21.58	4.29	21.56	4.39	21.54	4.48	22
23	22.58	4.39	22.56	4.49	22.54	4.59	22.52	4.68	23
24	23.56	4.58	23.54	4.68	23.52	4.78	23.50	4.89	24
25	24.54	4.77	24.52	4.88	24.50	4.98	24.48	5.09	25
26	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5.30	26
27	26.50	5.15	26.48	5.27	26.46	5.38	26.43	5.50	27
28	27.49	5.34	27.46	5.46	27.44	5.58	27.41	5.70	28
29	28.47	5.53	28.44	5.66	28.42	5.78	28.39	5.91	29
30	29.45	5.72	29.42	5.85	29.40	5.98	29.37	6.11	30
31	30.43	5.92	30.40	6.05	30.38	6.18	30.35	6.31	31
32	31.41	6.11	31.39	6.24	31.36	6.38	31.33	6.52	32
33	32.39	6.30	32.37	6.44	32.34	6.58	32.31	6.72	33
34	33.38	6.49	33.35	6.63	33.32	6.78	33.29	6.92	34
35	34.36	6.68	34.33	6.83	34.30	6.98	34.27	7.13	35
36	35.34	6.87	35.31	7.02	35.28	7.18	35.25	7.33	36
37	36.32	7.06	36.29	7.22	36.26	7.38	36.22	7.53	37
38	37.30	7.25	37.27	7.41	37.24	7.58	37.20	7.74	38
39	38.28	7.44	38.25	7.61	38.22	7.78	38.18	7.94	39
40	39.27	7.63	39.23	7.80	39.20	7.97	39.16	8.15	40
41	40.25	7.82	40.21	8.00	40.18	8.17	40.14	8.35	41
42	41.23	8.01	41.19	8.19	41.16	8.37	41.12	8.55	42
43	42.21	8.20	42.17	8.39	42.14	8.57	42.10	8.76	43
44	43.19	8.40	43.15	8.58	43.12	8.77	43.08	8.96	44
45	44.17	8.59	44.14	8.78	44.10	8.97	44.06	9.16	45
46	45.15	8.78	45.12	8.97	45.08	9.17	45.04	9.37	46
47	46.14	8.97	46.10	9.17	46.06	9.37	46.02	9.57	47
48	47.12	9.16	47.08	9.36	47.04	9.57	46.99	9.78	48
49	48.10	9.35	48.06	9.56	48.02	9.77	47.97	9.98	49
50	49.08	9.54	49.04	9.75	49.00	9.97	48.95	10.18	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	79 Deg.		78½ Deg.		78¼ Deg.		78½ Deg.		

TRAVERSE TABLE.

Distance	11 Deg.		11½ Deg.		11¾ Deg.		11¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	50.06	9.73	50.02	9.95	49.98	10.17	49.93	10.39	51
52	51.04	9.92	51.00	10.14	50.96	10.37	50.91	10.59	52
53	52.03	10.11	51.98	10.34	51.94	10.57	51.89	10.79	53
54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00	54
55	53.99	10.49	53.94	10.73	53.90	10.97	53.85	11.20	55
56	54.97	10.69	54.92	10.93	54.88	11.16	54.83	11.40	56
57	55.95	10.88	55.90	11.12	55.86	11.36	55.81	11.61	57
58	56.93	11.07	56.89	11.32	56.84	11.56	56.78	11.81	58
59	57.92	11.26	57.87	11.51	57.82	11.76	57.76	12.01	59
60	58.90	11.45	58.85	11.71	58.80	11.96	58.74	12.22	60
61	59.88	11.64	59.83	11.90	59.78	12.16	59.72	12.42	61
62	60.86	11.83	60.81	12.10	60.76	12.36	60.70	12.63	62
63	61.84	12.02	61.79	12.29	61.74	12.56	61.68	12.83	63
64	62.82	12.21	62.77	12.49	62.72	12.76	62.66	13.03	64
65	63.81	12.40	63.75	12.68	63.70	12.96	63.64	13.24	65
66	64.79	12.59	64.73	12.88	64.68	13.16	64.62	13.44	66
67	65.77	12.78	65.71	13.07	65.66	13.36	65.60	13.64	67
68	66.75	12.98	66.69	13.27	66.63	13.56	66.58	13.85	68
69	67.73	13.17	67.67	13.46	67.61	13.76	67.55	14.05	69
70	68.71	13.36	68.66	13.66	68.59	13.96	68.53	14.25	70
71	69.70	13.55	69.64	13.85	69.57	14.16	69.51	14.46	71
72	70.68	13.74	70.62	14.05	70.55	14.35	70.49	14.66	72
73	71.66	13.93	71.60	14.24	71.53	14.55	71.47	14.87	73
74	72.64	14.12	72.58	14.44	72.51	14.75	72.45	15.07	74
75	73.62	14.31	73.56	14.63	73.49	14.95	73.43	15.27	75
76	74.60	14.50	74.54	14.83	74.47	15.15	74.41	15.48	76
77	75.59	14.69	75.52	15.02	75.45	15.35	75.39	15.68	77
78	76.57	14.88	76.50	15.22	76.43	15.55	76.37	15.88	78
79	77.55	15.07	77.48	15.41	77.41	15.75	77.34	16.09	79
80	78.53	15.26	78.46	15.61	78.39	15.95	78.32	16.29	80
81	79.51	15.46	79.44	15.80	79.37	16.15	79.30	16.49	81
82	80.49	15.65	80.42	16.00	80.35	16.35	80.28	16.70	82
83	81.48	15.84	81.41	16.19	81.33	16.55	81.26	16.90	83
84	82.46	16.03	82.39	16.39	82.31	16.75	82.24	17.11	84
85	83.44	16.22	83.37	16.58	83.29	16.95	83.22	17.31	85
86	84.42	16.41	84.35	16.78	84.27	17.15	84.20	17.51	86
87	85.40	16.60	85.33	16.97	85.25	17.35	85.18	17.72	87
88	86.38	16.79	86.31	17.17	86.23	17.54	86.16	17.92	88
89	87.36	16.98	87.29	17.36	87.21	17.74	87.14	18.12	89
90	88.35	17.17	88.27	17.56	88.19	17.94	88.11	18.33	90
91	89.33	17.36	89.25	17.75	89.17	18.14	89.09	18.53	91
92	90.31	17.55	90.23	17.95	90.15	18.34	90.07	18.74	92
93	91.29	17.75	91.21	18.14	91.13	18.54	91.05	18.94	93
94	92.27	17.94	92.19	18.34	92.11	18.74	92.03	19.14	94
95	93.25	18.13	93.17	18.53	93.09	18.94	93.01	19.35	95
96	94.24	18.32	94.16	18.73	94.07	19.14	93.99	19.55	96
97	95.22	18.51	95.14	18.92	95.05	19.34	94.97	19.75	97
98	96.20	18.70	96.12	19.12	96.03	19.54	95.95	19.96	98
99	97.18	18.89	97.10	19.31	97.01	19.74	96.93	20.16	99
100	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	79 Deg.		78½ Deg.		78¼ Deg.		78¾ Deg.		



## TRAVERSE TABLE.

Distance.	12 Deg		12½ Deg.		12½ Deg.		12¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.98	0.21	0.98	0.21	0.98	0.22	0.98	0.22	1
2	1.96	0.42	1.95	0.42	1.95	0.43	1.95	0.44	2
3	2.93	0.62	2.93	0.64	2.93	0.65	2.93	0.66	3
4	3.91	0.83	3.91	0.85	3.91	0.87	3.90	0.88	4
5	4.89	1.04	4.89	1.06	4.88	1.08	4.88	1.10	5
6	5.87	1.25	5.86	1.27	5.86	1.30	5.85	1.32	6
7	6.85	1.46	6.84	1.49	6.83	1.52	6.83	1.54	7
8	7.83	1.66	7.82	1.70	7.81	1.73	7.80	1.77	8
9	8.80	1.87	8.80	1.91	8.79	1.95	8.78	1.99	9
10	9.78	2.08	9.77	2.12	9.76	2.16	9.75	2.21	10
11	10.76	2.29	10.75	2.33	10.74	2.38	10.73	2.43	11
12	11.74	2.49	11.73	2.55	11.72	2.60	11.70	2.65	12
13	12.72	2.70	12.70	2.76	12.69	2.81	12.68	2.87	13
14	13.69	2.91	13.68	2.97	13.67	3.03	13.65	3.09	14
15	14.67	3.12	14.66	3.18	14.64	3.25	14.63	3.31	15
16	15.65	3.33	15.64	3.39	15.62	3.46	15.61	3.53	16
17	16.63	3.53	16.61	3.61	16.60	3.68	16.58	3.75	17
18	17.61	3.74	17.59	3.82	17.57	3.90	17.56	3.97	18
19	18.58	3.95	18.57	4.03	18.55	4.11	18.53	4.19	19
20	19.56	4.16	19.54	4.24	19.53	4.33	19.51	4.41	20
21	20.54	4.37	20.52	4.46	20.50	4.55	20.48	4.63	21
22	21.52	4.57	21.50	4.67	21.48	4.76	21.46	4.86	22
23	22.50	4.78	22.48	4.88	22.45	4.98	22.43	5.08	23
24	23.48	4.99	23.45	5.09	23.43	5.19	23.41	5.30	24
25	24.45	5.20	24.43	5.30	24.41	5.41	24.38	5.52	25
26	25.43	5.41	25.41	5.52	25.38	5.63	25.36	5.74	26
27	26.41	5.61	26.39	5.73	26.36	5.84	26.33	5.96	27
28	27.39	5.82	27.36	5.94	27.34	6.06	27.31	6.18	28
29	28.37	6.03	28.34	6.15	28.31	6.28	28.28	6.40	29
30	29.34	6.24	29.32	6.37	29.29	6.49	29.26	6.62	30
31	30.32	6.45	30.29	6.58	30.27	6.71	30.24	6.84	31
32	31.30	6.65	31.27	6.79	31.24	6.93	31.21	7.06	32
33	32.28	6.86	32.25	7.00	32.22	7.14	32.19	7.28	33
34	33.26	7.07	33.23	7.21	33.19	7.36	33.16	7.50	34
35	34.24	7.28	34.20	7.43	34.17	7.58	34.14	7.72	35
36	35.21	7.48	35.18	7.64	35.15	7.79	35.11	7.95	36
37	36.19	7.69	36.16	7.85	36.12	8.01	36.09	8.17	37
38	37.17	7.90	37.13	8.06	37.10	8.22	37.06	8.39	38
39	38.15	8.11	38.11	8.27	38.08	8.44	38.04	8.61	39
40	39.13	8.32	39.09	8.49	39.05	8.66	39.01	8.83	40
41	40.10	8.52	40.07	8.70	40.03	8.87	39.99	9.05	41
42	41.08	8.73	41.04	8.91	41.00	9.09	40.96	9.27	42
43	42.06	8.94	42.02	9.12	41.98	9.31	41.94	9.49	43
44	43.04	9.15	43.00	9.34	42.96	9.52	42.92	9.71	44
45	44.02	9.36	43.98	9.55	43.93	9.74	43.89	9.93	45
46	44.99	9.56	44.95	9.76	44.91	9.96	44.87	10.15	46
47	45.97	9.77	45.93	9.97	45.89	10.17	45.84	10.37	47
48	46.95	9.98	46.91	10.18	46.86	10.39	46.82	10.59	48
49	47.93	10.19	47.88	10.40	47.84	10.61	47.79	10.81	49
50	48.91	10.40	48.86	10.61	48.81	10.82	48.77	11.03	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	78 Deg.		77½ Deg.		77½ Deg.		77¼ Deg.		

TRAVERSE TABLE.

Distance.	12 Deg.		12½ Deg.		12¾ Deg.		12¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.89	10.60	49.84	10.82	49.79	11.04	49.74	11.26	51
52	50.86	10.81	50.82	11.03	50.77	11.25	50.72	11.48	52
53	51.84	11.02	51.79	11.25	51.74	11.47	51.69	11.70	53
54	52.82	11.23	52.77	11.46	52.72	11.69	52.67	11.92	54
55	53.80	11.44	53.75	11.67	53.70	11.90	53.64	12.14	55
56	54.78	11.64	54.72	11.88	54.67	12.12	54.62	12.36	56
57	55.75	11.85	55.70	12.09	55.65	12.34	55.59	12.58	57
58	56.73	12.06	56.68	12.31	56.63	12.55	56.57	12.80	58
59	57.71	12.27	57.66	12.52	57.60	12.77	57.55	13.02	59
60	58.69	12.47	58.63	12.73	58.58	12.99	58.52	13.24	60
61	59.67	12.68	59.61	12.94	59.55	13.20	59.50	13.46	61
62	60.65	12.89	60.59	13.16	60.53	13.42	60.47	13.68	62
63	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90	63
64	62.60	13.31	62.54	13.58	62.48	13.85	62.42	14.12	64
65	63.58	13.51	63.52	13.79	63.46	14.07	63.40	14.35	65
66	64.56	13.72	64.50	14.00	64.44	14.29	64.37	14.57	66
67	65.54	13.93	65.47	14.22	65.41	14.50	65.35	14.79	67
68	66.51	14.14	66.45	14.43	66.39	14.72	66.32	15.01	68
69	67.49	14.35	67.43	14.64	67.36	14.93	67.30	15.23	69
70	68.47	14.55	68.41	14.85	68.34	15.15	68.27	15.45	70
71	69.45	14.76	69.38	15.06	69.32	15.37	69.25	15.67	71
72	70.43	14.97	70.36	15.28	70.29	15.58	70.22	15.89	72
73	71.40	15.18	71.34	15.49	71.27	15.80	71.20	16.11	73
74	72.38	15.39	72.32	15.70	72.25	16.02	72.18	16.33	74
75	73.36	15.59	73.29	15.91	73.22	16.23	73.15	16.55	75
76	74.34	15.80	74.27	16.13	74.20	16.45	74.13	16.77	76
77	75.32	16.01	75.25	16.34	75.17	16.67	75.10	16.99	77
78	76.30	16.22	76.22	16.55	76.15	16.88	76.08	17.21	78
79	77.27	16.43	77.20	16.76	77.13	17.10	77.05	17.44	79
80	78.25	16.63	78.18	16.97	78.10	17.32	78.03	17.66	80
81	79.23	16.84	79.16	17.19	79.08	17.53	79.00	17.88	81
82	80.21	17.05	80.13	17.40	80.06	17.75	79.98	18.10	82
83	81.19	17.26	81.11	17.61	81.03	17.96	80.95	18.32	83
84	82.16	17.46	82.09	17.82	82.01	18.18	81.93	18.54	84
85	83.14	17.67	83.06	18.04	82.99	18.40	82.90	18.76	85
86	84.12	17.88	84.04	18.25	83.96	18.61	83.88	18.98	86
87	85.10	18.09	85.02	18.46	84.94	18.83	84.85	19.20	87
88	86.08	18.30	86.00	18.67	85.91	19.05	85.83	19.42	88
89	87.06	18.50	86.97	18.88	86.89	19.26	86.81	19.64	89
90	88.03	18.71	87.95	19.10	87.87	19.48	87.78	19.86	90
91	89.01	18.92	88.93	19.31	88.84	19.70	88.76	20.08	91
92	89.99	19.13	89.91	19.52	89.82	19.91	89.73	20.30	92
93	90.97	19.34	90.88	19.73	90.80	20.13	90.71	20.52	93
94	91.95	19.54	91.86	19.94	91.77	20.35	91.68	20.75	94
95	92.92	19.75	92.84	20.16	92.75	20.56	92.66	20.97	95
96	93.90	19.96	93.81	20.37	93.72	20.78	93.63	21.19	96
97	94.88	20.17	94.79	20.58	94.70	20.99	94.61	21.41	97
98	95.86	20.38	95.77	20.79	95.68	21.21	95.58	21.63	98
99	96.84	20.58	96.75	21.01	96.65	21.43	96.56	21.85	99
100	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	78 Deg.		77½ Deg.		77¼ Deg.		77¼ Deg.		

Distance.	13 Deg.		13¼ Deg.		13½ Deg.		13¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.97	0.23	0.97	0.23	0.97	0.23	0.97	0.24	1
2	1.95	0.45	1.95	0.46	1.95	0.47	1.94	0.48	2
3	2.92	0.67	2.92	0.69	2.92	0.70	2.91	0.71	3
4	3.90	0.90	3.89	0.92	3.89	0.93	3.89	0.95	4
5	4.87	1.12	4.87	1.15	4.86	1.17	4.86	1.19	5
6	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43	6
7	6.82	1.57	6.81	1.60	6.81	1.63	6.80	1.66	7
8	7.80	1.80	7.79	1.83	7.78	1.87	7.77	1.90	8
9	8.77	2.02	8.76	2.06	8.75	2.10	8.74	2.14	9
10	9.74	2.25	9.73	2.29	9.72	2.33	9.71	2.38	10
11	10.72	2.47	10.71	2.52	10.70	2.57	10.68	2.61	11
12	11.69	2.70	11.68	2.75	11.67	2.80	11.66	2.85	12
13	12.67	2.92	12.65	2.98	12.64	3.03	12.63	3.09	13
14	13.64	3.15	13.63	3.21	13.61	3.27	13.60	3.33	14
15	14.62	3.37	14.60	3.44	14.59	3.50	14.57	3.57	15
16	15.59	3.60	15.57	3.67	15.56	3.74	15.54	3.80	16
17	16.57	3.82	16.55	3.90	16.53	3.97	16.51	4.04	17
18	17.54	4.05	17.52	4.13	17.50	4.20	17.48	4.28	18
19	18.51	4.27	18.49	4.35	18.48	4.44	18.46	4.52	19
20	19.49	4.50	19.47	4.58	19.45	4.67	19.43	4.75	20
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99	21
22	21.44	4.95	21.41	5.04	21.39	5.14	21.37	5.23	22
23	22.41	5.17	22.39	5.27	22.36	5.37	22.34	5.47	23
24	23.38	5.40	23.36	5.50	23.34	5.60	23.31	5.70	24
25	24.36	5.62	24.33	5.73	24.31	5.84	24.28	5.94	25
26	25.33	5.85	25.31	5.96	25.28	6.07	25.25	6.18	26
27	26.31	6.07	26.28	6.19	26.25	6.30	26.23	6.42	27
28	27.28	6.30	27.25	6.42	27.23	6.54	27.20	6.66	28
29	28.26	6.52	28.23	6.65	28.20	6.77	28.17	6.89	29
30	29.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13	30
31	30.21	6.97	30.17	7.11	30.14	7.24	30.11	7.37	31
32	31.18	7.20	31.15	7.33	31.12	7.47	31.08	7.61	32
33	32.15	7.42	32.12	7.56	32.09	7.70	32.05	7.84	33
34	33.13	7.65	33.09	7.79	33.06	7.94	33.03	8.08	34
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8.32	35
36	35.08	8.10	35.04	8.25	35.01	8.40	34.97	8.56	36
37	36.05	8.32	36.02	8.48	35.98	8.64	35.94	8.79	37
38	37.03	8.55	36.99	8.71	36.95	8.87	36.91	9.03	38
39	38.00	8.77	37.96	8.94	37.92	9.10	37.88	9.27	39
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51	40
41	39.95	9.22	39.91	9.40	39.87	9.57	39.83	9.75	41
42	40.92	9.45	40.88	9.63	40.84	9.80	40.80	9.98	42
43	41.90	9.67	41.86	9.86	41.81	10.04	41.77	10.22	43
44	42.87	9.90	42.83	10.08	42.78	10.27	42.74	10.46	44
45	43.85	10.12	43.80	10.31	43.76	10.51	43.71	10.70	45
46	44.82	10.35	44.78	10.54	44.73	10.74	44.68	10.93	46
47	45.80	10.57	45.75	10.77	45.70	10.97	45.65	11.17	47
48	46.77	10.80	46.72	11.00	46.67	11.21	46.62	11.41	48
49	47.74	11.02	47.70	11.23	47.65	11.44	47.60	11.65	49
50	48.72	11.25	48.67	11.46	48.62	11.67	48.57	11.88	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	77 Deg.		76¼ Deg.		76½ Deg.		76¼ Deg.		

TRAVERSE TABLE

Distance.	13 Deg.		13½ Deg.		13¾ Deg.		13¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.69	11.47	49.64	11.69	49.59	11.91	49.54	12.12	51
52	50.67	11.70	50.62	11.92	50.56	12.14	50.51	12.36	52
53	51.64	11.92	51.59	12.15	51.54	12.37	51.48	12.60	53
54	52.62	12.15	52.56	12.38	52.51	12.61	52.45	12.84	54
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07	55
56	54.56	12.60	54.51	12.84	54.45	13.07	54.40	13.31	56
57	55.54	12.82	55.48	13.06	55.43	13.31	55.37	13.55	57
58	56.51	13.05	56.46	13.29	56.40	13.54	56.34	13.79	58
59	57.49	13.27	57.43	13.52	57.37	13.77	57.31	14.02	59
60	58.46	13.50	58.40	13.75	58.34	14.01	58.28	14.26	60
61	59.44	13.72	59.38	13.98	59.31	14.24	59.25	14.50	61
62	60.41	13.95	60.35	14.21	60.29	14.47	60.22	14.74	62
63	61.39	14.17	61.32	14.44	61.26	14.71	61.19	14.97	63
64	62.36	14.40	62.30	14.67	62.23	14.94	62.17	15.21	64
65	63.33	14.62	63.27	14.90	63.20	15.17	63.14	15.45	65
66	64.31	14.85	64.24	15.13	64.18	15.41	64.11	15.69	66
67	65.28	15.07	65.22	15.36	65.15	15.64	65.08	15.93	67
68	66.26	15.30	66.19	15.59	66.12	15.87	66.05	16.16	68
69	67.23	15.52	67.16	15.81	67.09	16.11	67.02	16.40	69
70	68.21	15.75	68.14	16.04	68.07	16.34	67.99	16.64	70
71	69.18	15.97	69.11	16.27	69.04	16.57	68.97	16.88	71
72	70.15	16.20	70.08	16.50	70.01	16.81	69.94	17.11	72
73	71.13	16.42	71.06	16.73	70.98	17.04	70.91	17.35	73
74	72.10	16.65	72.03	16.96	71.96	17.28	71.88	17.59	74
75	73.08	16.87	73.00	17.19	72.93	17.50	72.85	17.83	75
76	74.05	17.10	73.98	17.42	73.90	17.74	73.82	18.06	76
77	75.03	17.32	74.95	17.65	74.87	17.98	74.79	18.30	77
78	76.00	17.55	75.92	17.88	75.84	18.21	75.76	18.54	78
79	76.98	17.77	76.90	18.11	76.82	18.44	76.74	18.78	79
80	77.95	18.00	77.87	18.34	77.79	18.68	77.71	19.01	80
81	78.92	18.22	78.84	18.57	78.76	18.91	78.68	19.25	81
82	79.90	18.45	79.82	18.79	79.73	19.14	79.65	19.49	82
83	80.87	18.67	80.79	19.02	80.71	19.38	80.62	19.73	83
84	81.85	18.90	81.76	19.25	81.68	19.61	81.59	19.97	84
85	82.82	19.12	82.74	19.48	82.65	19.84	82.56	20.20	85
86	83.80	19.35	83.71	19.71	83.62	20.08	83.54	20.44	86
87	84.77	19.57	84.68	19.94	84.60	20.31	84.51	20.68	87
88	85.74	19.80	85.66	20.17	85.57	20.54	85.48	20.92	88
89	86.72	20.02	86.63	20.40	86.54	20.78	86.45	21.15	89
90	87.69	20.25	87.60	20.63	87.51	21.01	87.42	21.39	90
91	88.67	20.47	88.58	20.86	88.49	21.24	88.39	21.63	91
92	89.64	20.70	89.55	21.09	89.46	21.48	89.36	21.87	92
93	90.62	20.92	90.52	21.32	90.43	21.71	90.33	22.10	93
94	91.59	21.15	91.50	21.54	91.31	21.94	91.31	22.34	94
95	92.57	21.37	92.47	21.77	92.38	22.18	92.28	22.58	95
96	93.54	21.60	93.44	22.00	93.35	22.41	93.25	22.82	96
97	94.51	21.82	94.42	22.23	94.32	22.64	94.22	23.06	97
98	95.49	22.05	95.39	22.46	95.29	22.88	95.19	23.29	98
99	96.46	22.27	96.36	22.69	96.26	23.11	96.16	23.53	99
100	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	77 Deg.		76½ Deg.		76¼ Deg.		76¼ Deg.		

Distance.	14 Deg.		14½ Deg.		14¾ Deg.		14¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.97	0.24	0.97	0.25	0.97	0.25	0.97	0.25	1
2	1.94	0.48	1.94	0.49	1.94	0.50	1.93	0.51	2
3	2.91	0.73	2.91	0.74	2.90	0.75	2.90	0.76	3
4	3.88	0.97	3.88	0.98	3.87	1.00	3.87	1.02	4
5	4.85	1.21	4.85	1.23	4.84	1.25	4.84	1.27	5
6	5.82	1.45	5.82	1.48	5.81	1.50	5.80	1.53	6
7	6.79	1.69	6.78	1.72	6.78	1.75	6.77	1.78	7
8	7.76	1.94	7.75	1.97	7.75	2.00	7.74	2.04	8
9	8.73	2.18	8.72	2.22	8.71	2.25	8.70	2.29	9
10	9.70	2.42	9.69	2.46	9.68	2.50	9.67	2.55	10
11	10.67	2.66	10.66	2.71	10.65	2.75	10.64	2.80	11
12	11.64	2.90	11.63	2.95	11.62	3.00	11.60	3.06	12
13	12.61	3.15	12.60	3.20	12.59	3.25	12.57	3.31	13
14	13.58	3.39	13.57	3.45	13.55	3.51	13.54	3.56	14
15	14.55	3.63	14.54	3.69	14.52	3.76	14.51	3.82	15
16	15.52	3.87	15.51	3.94	15.49	4.01	15.47	4.07	16
17	16.50	4.11	16.48	4.18	16.46	4.26	16.44	4.33	17
18	17.47	4.35	17.45	4.43	17.43	4.51	17.41	4.58	18
19	18.44	4.60	18.42	4.68	18.39	4.76	18.37	4.84	19
20	19.41	4.84	19.38	4.92	19.36	5.01	19.34	5.09	20
21	20.38	5.08	20.35	5.17	20.33	5.26	20.31	5.35	21
22	21.35	5.32	21.32	5.42	21.30	5.51	21.28	5.60	22
23	22.32	5.56	22.29	5.66	22.27	5.76	22.24	5.86	23
24	23.29	5.81	23.26	5.91	23.24	6.01	23.21	6.11	24
25	24.26	6.05	24.23	6.15	24.20	6.26	24.18	6.37	25
26	25.23	6.29	25.20	6.40	25.17	6.51	25.14	6.62	26
27	26.20	6.53	26.17	6.65	26.14	6.76	26.11	6.87	27
28	27.17	6.77	27.14	6.89	27.11	7.01	27.08	7.13	28
29	28.14	7.02	28.11	7.14	28.08	7.26	28.04	7.38	29
30	29.11	7.26	29.08	7.38	29.04	7.51	29.01	7.64	30
31	30.08	7.50	30.05	7.63	30.01	7.76	29.98	7.89	31
32	31.05	7.74	31.02	7.88	30.98	8.01	30.95	8.15	32
33	32.02	7.98	31.98	8.12	31.95	8.26	31.91	8.40	33
34	32.99	8.23	32.95	8.37	32.92	8.51	32.88	8.66	34
35	33.96	8.47	33.92	8.62	33.89	8.76	33.85	8.91	35
36	34.93	8.71	34.89	8.86	34.85	9.01	34.81	9.17	36
37	35.90	8.95	35.86	9.11	35.82	9.26	35.78	9.42	37
38	36.87	9.19	36.83	9.35	36.79	9.51	36.75	9.67	38
39	37.84	9.44	37.80	9.60	37.76	9.76	37.71	9.93	39
40	38.81	9.68	38.77	9.85	38.73	10.02	38.68	10.18	40
41	39.78	9.92	39.74	10.09	39.69	10.27	39.65	10.44	41
42	40.75	10.16	40.71	10.34	40.66	10.52	40.62	10.69	42
43	41.72	10.40	41.68	10.58	41.63	10.77	41.59	10.95	43
44	42.69	10.64	42.65	10.83	42.60	11.02	42.55	11.20	44
45	43.66	10.89	43.62	11.08	43.57	11.27	43.52	11.46	45
46	44.63	11.13	44.58	11.32	44.53	11.52	44.48	11.71	46
47	45.60	11.37	45.55	11.57	45.50	11.77	45.45	11.97	47
48	46.57	11.61	46.52	11.82	46.47	12.02	46.42	12.22	48
49	47.54	11.85	47.49	12.06	47.44	12.27	47.39	12.48	49
50	48.51	12.10	48.46	12.31	48.41	12.52	48.35	12.73	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	76 Deg.		75½ Deg.		75¼ Deg.		75¼ Deg.		

TRAVERSE TABLE.

Distance.	14 Deg.		14½ Deg.		14¾ Deg.		14¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.49	12.34	49.43	12.55	49.38	12.77	49.32	12.98	51
52	50.46	12.58	50.40	12.80	50.34	13.02	50.29	13.24	52
53	51.43	12.82	51.37	13.05	51.31	13.27	51.25	13.49	53
54	52.40	13.06	52.34	13.29	52.28	13.52	52.22	13.75	54
55	53.37	13.31	53.31	13.54	53.25	13.77	53.19	14.00	55
56	54.34	13.55	54.28	13.78	54.22	14.02	54.15	14.26	56
57	55.31	13.79	55.25	14.03	55.18	14.27	55.12	14.51	57
58	56.28	14.03	56.22	14.28	56.15	14.52	56.09	14.77	58
59	57.25	14.27	57.18	14.52	57.12	14.77	57.06	15.02	59
60	58.22	14.52	58.15	14.77	58.09	15.02	58.02	15.28	60
61	59.19	14.76	59.12	15.02	59.06	15.27	58.99	15.53	61
62	60.16	15.00	60.09	15.26	60.03	15.52	59.96	15.79	62
63	61.13	15.24	61.06	15.51	60.99	15.77	60.92	16.04	63
64	62.10	15.48	62.03	15.75	61.96	16.02	61.89	16.29	64
65	63.07	15.72	63.00	16.00	62.93	16.27	62.86	16.55	65
66	64.04	15.97	63.97	16.25	63.90	16.53	63.83	16.80	66
67	65.01	16.21	64.94	16.49	64.87	16.78	64.79	17.06	67
68	65.98	16.45	65.91	16.74	65.83	17.03	65.76	17.31	68
69	66.95	16.69	66.88	16.98	66.80	17.28	66.73	17.57	69
70	67.92	16.93	67.85	17.23	67.77	17.53	67.69	17.82	70
71	68.89	17.18	68.82	17.48	68.74	17.78	68.66	18.08	71
72	69.86	17.42	69.78	17.72	69.71	18.03	69.63	18.33	72
73	70.83	17.66	70.75	17.97	70.67	18.28	70.59	18.59	73
74	71.80	17.90	71.72	18.22	71.64	18.53	71.56	18.84	74
75	72.77	18.14	72.69	18.46	72.61	18.78	72.53	19.10	75
76	73.74	18.39	73.66	18.71	73.58	19.03	73.50	19.35	76
77	74.71	18.63	74.63	18.95	74.55	19.28	74.46	19.60	77
78	75.68	18.87	75.60	19.20	75.52	19.53	75.43	19.86	78
79	76.65	19.11	76.57	19.45	76.48	19.78	76.40	20.11	79
80	77.62	19.35	77.54	19.69	77.45	20.03	77.36	20.37	80
81	78.59	19.60	78.51	19.94	78.42	20.28	78.33	20.62	81
82	79.56	19.84	79.48	20.18	79.39	20.53	79.30	20.88	82
83	80.53	20.08	80.45	20.43	80.36	20.78	80.26	21.13	83
84	81.50	20.32	81.42	20.68	81.32	21.03	81.23	21.39	84
85	82.48	20.56	82.38	20.92	82.29	21.28	82.20	21.64	85
86	83.45	20.81	83.35	21.17	83.26	21.53	83.17	21.90	86
87	84.42	21.05	84.32	21.42	84.23	21.78	84.13	22.15	87
88	85.39	21.29	85.29	21.66	85.20	22.03	85.10	22.41	88
89	86.36	21.53	86.26	21.91	86.17	22.28	86.07	22.66	89
90	87.33	21.77	87.23	22.15	87.13	22.53	87.03	22.91	90
91	88.30	22.01	88.20	22.40	88.10	22.78	88.00	23.17	91
92	89.27	22.26	89.17	22.65	89.07	23.04	88.97	23.42	92
93	90.24	22.50	90.14	22.89	90.04	23.29	89.94	23.68	93
94	91.21	22.74	91.11	23.14	91.01	23.54	90.90	23.93	94
95	92.18	22.98	92.08	23.38	91.97	23.79	91.87	24.19	95
96	93.15	23.22	93.05	23.63	92.94	24.04	92.84	24.44	96
97	94.12	23.47	94.02	23.88	93.91	24.29	93.80	24.70	97
98	95.09	23.71	94.98	24.12	94.88	24.54	94.77	24.95	98
99	96.06	23.96	95.95	24.37	95.85	24.79	95.74	25.21	99
100	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	76 Deg.		75½ Deg.		75¼ Deg.		75¼ Deg.		

TRAVEL TABLE

Distance	15 Deg.		15½ Deg.		15¾ Deg.		15¾ Deg.		Distance
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.00	0.00	0.00	0.00	0.00	0.27	0.96	0.27	1
2	0.15	0.51	1.03	0.53	1.83	0.53	1.92	0.54	2
3	0.30	1.02	2.06	0.79	2.79	0.80	2.89	0.81	3
4	0.45	1.53	3.05	1.05	3.85	1.07	3.85	1.09	4
5	0.60	2.04	4.02	1.32	4.92	1.34	4.81	1.36	5
6	0.75	2.55	5.79	1.57	5.79	1.60	5.77	1.63	6
7	0.90	3.06	6.75	1.84	6.75	1.87	6.74	1.90	7
8	1.05	3.57	7.72	2.10	7.71	2.14	7.70	2.17	8
9	1.20	4.08	8.69	2.37	8.67	2.41	8.66	2.44	9
10	1.35	4.59	9.65	2.63	9.64	2.67	9.62	2.71	10
11	1.50	5.10	10.61	2.89	10.61	2.94	10.59	2.94	11
12	1.65	5.61	11.58	3.16	11.58	3.21	11.55	3.25	12
13	1.80	6.12	12.54	3.42	12.53	3.47	12.51	3.53	13
14	1.95	6.63	13.51	3.68	13.49	3.74	13.47	3.80	14
15	2.10	7.14	14.47	3.95	14.45	4.01	14.44	4.07	15
16	2.25	7.65	15.44	4.21	15.42	4.28	15.41	4.34	16
17	2.40	8.16	16.40	4.47	16.38	4.54	16.36	4.61	17
18	2.55	8.67	17.37	4.73	17.35	4.81	17.32	4.88	18
19	2.70	9.18	18.33	5.00	18.31	5.08	18.29	5.15	19
20	2.85	9.69	19.30	5.25	19.27	5.34	19.25	5.42	20
21	3.00	10.20	20.26	5.52	20.24	5.61	20.21	5.70	21
22	3.15	10.71	21.23	5.79	21.20	5.88	21.17	5.97	22
23	3.30	11.22	22.19	6.05	22.16	6.15	22.14	6.24	23
24	3.45	11.73	23.15	6.31	23.13	6.41	23.10	6.51	24
25	3.60	12.24	24.12	6.58	24.09	6.68	24.06	6.79	25
26	3.75	12.75	25.08	6.84	25.05	6.95	25.02	7.07	26
27	3.90	13.26	26.05	7.10	26.02	7.22	25.99	7.33	27
28	4.05	13.77	27.01	7.36	27.00	7.49	26.96	7.50	28
29	4.20	14.28	27.98	7.63	27.95	7.75	27.91	7.87	29
30	4.35	14.79	28.94	7.89	28.91	8.02	28.87	8.14	30
31	4.50	15.30	29.91	8.15	29.87	8.29	29.84	8.41	31
32	4.65	15.81	30.87	8.42	30.84	8.55	30.81	8.69	32
33	4.80	16.32	31.84	8.69	31.80	8.82	31.76	8.96	33
34	4.95	16.83	32.80	8.94	32.76	9.09	32.72	9.23	34
35	5.10	17.34	33.77	9.21	33.73	9.35	33.69	9.51	35
36	5.25	17.85	34.73	9.47	34.69	9.62	34.65	9.77	36
37	5.40	18.36	35.70	9.73	35.65	9.89	35.61	10.04	37
38	5.55	18.87	36.66	10.00	36.62	10.16	36.57	10.31	38
39	5.70	19.38	37.63	10.26	37.58	10.42	37.54	10.59	39
40	5.85	19.89	38.59	10.52	38.55	10.69	38.50	10.86	40
41	6.00	20.40	39.56	10.78	39.51	10.96	39.46	11.13	41
42	6.15	20.91	40.52	11.05	40.47	11.22	40.42	11.40	42
43	6.30	21.42	41.49	11.31	41.44	11.49	41.39	11.67	43
44	6.45	21.93	42.45	11.57	42.40	11.76	42.35	11.94	44
45	6.60	22.44	43.42	11.84	43.36	12.03	43.31	12.21	45
46	6.75	22.95	44.38	12.10	44.33	12.29	44.27	12.49	46
47	6.90	23.46	45.35	12.36	45.29	12.56	45.24	12.76	47
48	7.05	23.97	46.31	12.63	46.25	12.83	46.20	13.03	48
49	7.20	24.48	47.27	12.89	47.22	13.09	47.16	13.30	49
50	7.35	24.99	48.24	13.15	48.18	13.36	48.12	13.57	50
Distance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
	75 Deg.		74½ Deg.		74¼ Deg.		74¼ Deg.		

TRAVERSE TABLE.

Distance.	15 Deg.		15½ Deg.		15¾ Deg.		15¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.26	13.20	49.20	13.41	49.15	13.63	49.09	13.84	51
52	50.23	13.46	50.17	13.68	50.11	13.90	50.05	14.11	52
53	51.19	13.72	51.13	13.94	51.07	14.16	51.01	14.39	53
54	52.16	13.98	52.10	14.20	52.04	14.43	51.97	14.66	54
55	53.13	14.24	53.06	14.47	53.00	14.70	52.94	14.93	55
56	54.09	14.49	54.03	14.73	53.96	14.97	53.90	15.20	56
57	55.06	14.75	54.99	14.99	54.93	15.23	54.86	15.47	57
58	56.02	15.01	55.96	15.26	55.89	15.50	55.82	15.74	58
59	56.99	15.27	56.92	15.52	56.85	15.77	56.78	16.01	59
60	57.96	15.53	57.89	15.78	57.82	16.03	57.75	16.29	60
61	58.92	15.79	58.85	16.04	58.78	16.30	58.71	16.56	61
62	59.89	16.05	59.82	16.31	59.75	16.57	59.67	16.83	62
63	60.85	16.31	60.78	16.57	60.71	16.84	60.63	17.10	63
64	61.82	16.56	61.75	16.83	61.67	17.10	61.60	17.37	64
65	62.79	16.82	62.71	17.10	62.64	17.37	62.56	17.64	65
66	63.75	17.08	63.68	17.35	63.60	17.64	63.52	17.92	66
67	64.72	17.34	64.64	17.62	64.56	17.90	64.48	18.19	67
68	65.68	17.60	65.61	17.89	65.53	18.17	65.45	18.46	68
69	66.65	17.86	66.57	18.15	66.49	18.44	66.41	18.73	69
70	67.61	18.12	67.54	18.41	67.45	18.71	67.37	19.00	70
71	68.58	18.38	68.50	18.68	68.42	18.97	68.33	19.27	71
72	69.55	18.63	69.46	18.94	69.38	19.24	69.30	19.54	72
73	70.51	18.89	70.43	19.20	70.35	19.51	70.26	19.82	73
74	71.48	19.15	71.39	19.46	71.31	19.78	71.22	20.09	74
75	72.44	19.41	72.36	19.73	72.27	20.04	72.18	20.36	75
76	73.41	19.67	73.32	19.99	73.24	20.31	73.15	20.63	76
77	74.38	19.93	74.29	20.25	74.20	20.58	74.11	20.90	77
78	75.34	20.19	75.25	20.52	75.16	20.84	75.07	21.17	78
79	76.31	20.45	76.22	20.78	76.13	21.11	76.03	21.44	79
80	77.27	20.71	77.18	21.04	77.09	21.38	77.00	21.72	80
81	78.24	20.96	78.15	21.31	78.05	21.65	77.96	21.99	81
82	79.21	21.22	79.11	21.57	79.02	21.91	78.92	22.26	82
83	80.17	21.48	80.08	21.83	79.98	22.18	79.88	22.53	83
84	81.14	21.74	81.04	22.09	80.94	22.45	80.85	22.80	84
85	82.10	22.00	82.01	22.36	81.91	22.72	81.81	23.07	85
86	83.07	22.26	82.97	22.62	82.87	22.98	82.77	23.34	86
87	84.04	22.52	83.94	22.88	83.84	23.25	83.73	23.62	87
88	85.00	22.78	84.90	23.15	84.80	23.52	84.70	23.89	88
89	85.97	23.03	85.87	23.41	85.76	23.78	85.66	24.16	89
90	86.93	23.29	86.83	23.67	86.73	24.05	86.62	24.43	90
91	87.90	23.55	87.80	23.94	87.69	24.32	87.58	24.70	91
92	88.87	23.81	88.76	24.20	88.65	24.59	88.55	24.97	92
93	89.83	24.07	89.73	24.46	89.62	24.85	89.51	25.24	93
94	90.80	24.33	90.69	24.72	90.58	25.12	90.47	25.52	94
95	91.76	24.59	91.65	24.99	91.54	25.39	91.43	25.79	95
96	92.73	24.85	92.62	25.25	92.51	25.65	92.40	26.06	96
97	93.69	25.11	93.58	25.51	93.47	25.92	93.36	26.33	97
98	94.66	25.36	94.55	25.78	94.44	26.19	94.32	26.60	98
99	95.63	25.62	95.51	26.04	95.40	26.46	95.28	26.87	99
100	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	75 Deg.		74½ Deg.		74½ Deg.		74½ Deg.		



TRAVERSE TABLE.

Distance.	16 Deg.		16½ Deg.		16¾ Deg.		16¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29	1
2	1.92	0.55	1.92	0.56	1.92	0.57	1.92	0.59	2
3	2.88	0.83	2.88	0.84	2.88	0.85	2.87	0.86	3
4	3.85	1.10	3.84	1.12	3.84	1.14	3.83	1.15	4
5	4.81	1.38	4.80	1.40	4.79	1.42	4.79	1.44	5
6	5.77	1.65	5.76	1.68	5.75	1.70	5.75	1.73	6
7	6.73	1.93	6.72	1.96	6.71	1.99	6.70	2.02	7
8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31	8
9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59	9
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88	10
11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17	11
12	11.54	3.31	11.52	3.36	11.51	3.41	11.49	3.46	12
13	12.50	3.58	12.48	3.64	12.46	3.69	12.45	3.75	13
14	13.46	3.86	13.44	3.92	13.42	3.98	13.41	4.03	14
15	14.42	4.13	14.40	4.20	14.38	4.26	14.36	4.32	15
16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4.61	16
17	16.34	4.69	16.32	4.76	16.30	4.83	16.28	4.90	17
18	17.30	4.96	17.28	5.04	17.26	5.11	17.24	5.19	18
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19	5.48	19
20	19.23	5.51	19.20	5.60	19.18	5.68	19.15	5.76	20
21	20.19	5.79	20.16	5.88	20.14	5.96	20.11	6.05	21
22	21.15	6.06	21.12	6.16	21.09	6.25	21.07	6.34	22
23	22.11	6.34	22.08	6.44	22.05	6.53	22.02	6.63	23
24	23.07	6.62	23.04	6.72	23.01	6.82	22.98	6.92	24
25	24.03	6.89	24.00	7.00	23.97	7.10	23.94	7.20	25
26	24.99	7.17	24.96	7.28	24.93	7.38	24.90	7.49	26
27	25.95	7.44	25.92	7.56	25.89	7.67	25.85	7.78	27
28	26.92	7.72	26.88	7.84	26.85	7.95	26.81	8.07	28
29	27.88	7.99	27.84	8.11	27.81	8.24	27.77	8.36	29
30	28.84	8.27	28.80	8.39	28.76	8.52	28.73	8.65	30
31	29.80	8.54	29.76	8.67	29.72	8.80	29.68	8.93	31
32	30.76	8.82	30.72	8.95	30.68	9.09	30.64	9.22	32
33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51	33
34	32.68	9.37	32.64	9.51	32.60	9.66	32.56	9.80	34
35	33.64	9.65	33.60	9.79	33.56	9.94	33.51	10.09	35
36	34.61	9.92	34.56	10.07	34.52	10.22	34.47	10.38	36
37	35.57	10.20	35.52	10.35	35.48	10.51	35.43	10.66	37
38	36.53	10.47	36.48	10.63	36.44	10.79	36.39	10.95	38
39	37.49	10.75	37.44	10.91	37.39	11.08	37.35	11.24	39
40	38.45	11.03	38.40	11.19	38.35	11.36	38.30	11.53	40
41	39.41	11.30	39.36	11.47	39.31	11.64	39.26	11.82	41
42	40.37	11.58	40.32	11.75	40.27	11.93	40.22	12.10	42
43	41.33	11.85	41.28	12.03	41.23	12.21	41.18	12.39	43
44	42.30	12.13	42.24	12.31	42.19	12.50	42.13	12.68	44
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97	45
46	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26	46
47	45.18	12.95	45.12	13.15	45.06	13.35	45.01	13.55	47
48	46.14	13.23	46.08	13.43	46.02	13.63	45.96	13.83	48
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12	49
50	48.06	13.78	48.00	13.99	47.94	14.20	47.88	14.41	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73½ Deg.		73¼ Deg.		73¼ Deg.		

Distance.	16 Deg.		16½ Deg.		16¾ Deg.		16¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70	51
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99	52
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27	53
54	51.91	14.89	51.84	15.11	51.78	15.34	51.71	15.56	54
55	52.87	15.16	52.80	15.39	52.74	15.62	52.67	15.85	55
56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14	56
57	54.79	15.71	54.72	15.95	54.65	16.19	54.58	16.43	57
58	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72	58
59	56.71	16.26	56.64	16.51	56.57	16.76	56.50	17.00	59
60	57.68	16.54	57.60	16.79	57.53	17.04	57.45	17.29	60
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58	61
62	59.60	17.09	59.52	17.35	59.45	17.61	59.37	17.87	62
63	60.56	17.37	60.48	17.63	60.41	17.89	60.33	18.16	63
64	61.52	17.64	61.44	17.91	61.36	18.18	61.28	18.44	64
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	65
66	63.44	18.19	63.36	18.47	63.28	18.74	63.20	19.02	66
67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31	67
68	65.37	18.74	65.28	19.03	65.20	19.31	65.11	19.60	68
69	66.33	19.02	66.24	19.31	66.16	19.60	66.07	19.89	69
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	70
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46	71
72	69.21	19.85	69.12	20.15	69.03	20.45	68.95	20.75	72
73	70.17	20.12	70.08	20.43	69.99	20.73	69.90	21.04	73
74	71.13	20.40	71.04	20.71	70.95	21.02	70.86	21.33	74
75	72.09	20.67	72.00	20.99	71.91	21.30	71.82	21.61	75
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	76
77	74.02	21.22	73.92	21.55	73.83	21.87	73.73	22.19	77
78	74.98	21.50	74.88	21.83	74.79	22.15	74.69	22.48	78
79	75.94	21.78	75.84	22.11	75.75	22.44	75.65	22.77	79
80	76.90	22.05	76.80	22.39	76.71	22.72	76.61	23.06	80
81	77.86	22.33	77.76	22.67	77.66	23.01	77.56	23.34	81
82	78.82	22.60	78.72	22.95	78.62	23.29	78.52	23.63	82
83	79.78	22.88	79.68	23.23	79.58	23.57	79.48	23.92	83
84	80.75	23.15	80.64	23.51	80.54	23.86	80.44	24.21	84
85	81.71	23.43	81.60	23.79	81.50	24.14	81.39	24.50	85
86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.78	86
87	83.63	23.98	83.52	24.35	83.42	24.71	83.31	25.07	87
88	84.59	24.26	84.48	24.62	84.38	24.99	84.27	25.36	88
89	85.55	24.53	85.44	24.90	85.33	25.28	85.22	25.65	89
90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94	90
91	87.47	25.08	87.36	25.46	87.25	25.85	87.14	26.23	91
92	88.44	25.36	88.32	25.74	88.21	26.13	88.10	26.51	92
93	89.40	25.63	89.28	26.02	89.17	26.41	89.05	26.80	93
94	90.36	25.91	90.24	26.30	90.13	26.70	90.01	27.09	94
95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38	95
96	92.28	26.46	92.16	26.86	92.05	27.27	91.93	27.67	96
97	93.24	26.74	93.12	27.14	93.01	27.55	92.88	27.95	97
98	94.20	27.01	94.08	27.42	93.96	27.83	93.84	28.24	98
99	95.16	27.29	95.04	27.70	94.92	28.12	94.80	28.53	99
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73½ Deg.		73¼ Deg.		73¼ Deg.		

Distance.	17 Deg.		17¼ Deg.		17½ Deg.		17¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.29	0.95	0.30	0.95	0.30	0.95	0.30	1
2	1.91	0.58	1.91	0.59	1.91	0.60	1.90	0.61	2
3	2.87	0.88	2.87	0.89	2.86	0.90	2.86	0.91	3
4	3.83	1.17	3.82	1.19	3.81	1.20	3.81	1.22	4
5	4.78	1.46	4.78	1.48	4.77	1.50	4.76	1.52	5
6	5.74	1.75	5.73	1.78	5.72	1.80	5.71	1.83	6
7	6.69	2.05	6.69	2.08	6.68	2.10	6.67	2.13	7
8	7.65	2.34	7.64	2.37	7.63	2.41	7.62	2.44	8
9	8.61	2.63	8.60	2.67	8.58	2.71	8.57	2.74	9
10	9.56	2.92	9.55	2.97	9.54	3.01	9.52	3.05	10
11	10.52	3.22	10.51	3.26	10.49	3.31	10.48	3.35	11
12	11.48	3.51	11.46	3.56	11.44	3.61	11.43	3.66	12
13	12.43	3.80	12.42	3.85	12.40	3.91	12.38	3.96	13
14	13.39	4.09	13.37	4.15	13.35	4.21	13.33	4.27	14
15	14.34	4.39	14.33	4.45	14.31	4.51	14.29	4.57	15
16	15.30	4.68	15.28	4.74	15.26	4.81	15.24	4.88	16
17	16.26	4.97	16.24	5.04	16.21	5.11	16.19	5.18	17
18	17.21	5.26	17.19	5.34	17.17	5.41	17.14	5.49	18
19	18.17	5.56	18.15	5.63	18.12	5.71	18.10	5.79	19
20	19.13	5.85	19.10	5.93	19.07	6.01	19.05	6.10	20
21	20.08	6.14	20.06	6.23	20.03	6.31	20.00	6.40	21
22	21.04	6.43	21.01	6.52	20.98	6.62	20.95	6.71	22
23	21.99	6.72	21.97	6.82	21.94	6.92	21.91	7.01	23
24	22.95	7.02	22.92	7.12	22.89	7.22	22.86	7.32	24
25	23.91	7.31	23.88	7.41	23.84	7.52	23.81	7.62	25
26	24.86	7.60	24.83	7.71	24.80	7.82	24.76	7.93	26
27	25.82	7.89	25.79	8.01	25.75	8.12	25.71	8.23	27
28	26.78	8.19	26.74	8.30	26.70	8.42	26.67	8.54	28
29	27.73	8.48	27.70	8.60	27.66	8.72	27.62	8.84	29
30	28.69	8.77	28.65	8.90	28.61	9.02	28.57	9.15	30
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52	9.45	31
32	30.60	9.36	30.56	9.49	30.52	9.62	30.48	9.76	32
33	31.56	9.65	31.52	9.79	31.47	9.92	31.43	10.06	33
34	32.51	9.94	32.47	10.08	32.43	10.22	32.38	10.37	34
35	33.47	10.23	33.43	10.38	33.38	10.52	33.33	10.67	35
36	34.43	10.53	34.38	10.68	34.33	10.83	34.29	10.98	36
37	35.38	10.82	35.34	10.97	35.29	11.13	35.24	11.28	37
38	36.34	11.11	36.29	11.27	36.24	11.43	36.19	11.58	38
39	37.30	11.40	37.25	11.57	37.19	11.73	37.14	11.89	39
40	38.25	11.69	38.20	11.86	38.15	12.03	38.10	12.19	40
41	39.21	11.99	39.16	12.16	39.10	12.33	39.05	12.50	41
42	40.16	12.28	40.11	12.45	40.06	12.63	40.00	12.80	42
43	41.12	12.57	41.07	12.75	41.01	12.93	40.95	13.11	43
44	42.08	12.86	42.02	13.05	41.96	13.23	41.91	13.41	44
45	43.03	13.16	42.98	13.34	42.92	13.53	42.86	13.72	45
46	43.99	13.45	43.93	13.64	43.87	13.83	43.81	14.02	46
47	44.95	13.74	44.89	13.94	44.82	14.13	44.76	14.33	47
48	45.90	14.03	45.84	14.23	45.78	14.43	45.71	14.63	48
49	46.86	14.33	46.80	14.53	46.73	14.73	46.67	14.94	49
50	47.82	14.62	47.75	14.83	47.69	15.04	47.62	15.24	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	73 Deg.		72¼ Deg.		72½ Deg.		72¾ Deg.		

TRAVERSE TABLE.

Distance.	17 Deg.		17½ Deg.		17¾ Deg.		17½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	48.77	14.91	48.71	15.12	48.64	15.34	48.57	15.55	51
52	49.73	15.20	49.66	15.42	49.59	15.64	49.52	15.85	52
53	50.68	15.50	50.62	15.72	50.55	15.94	50.48	16.16	53
54	51.64	15.79	51.57	16.01	51.50	16.24	51.43	16.46	54
55	52.60	16.08	52.53	16.31	52.45	16.54	52.38	16.77	55
56	53.55	16.37	53.48	16.61	53.41	16.84	53.33	17.07	56
57	54.51	16.67	54.44	16.90	54.36	17.14	54.29	17.38	57
58	55.47	16.96	55.39	17.20	55.32	17.44	55.24	17.68	58
59	56.42	17.25	56.35	17.50	56.27	17.74	56.10	17.99	59
60	57.38	17.54	57.30	17.79	57.22	18.04	57.14	18.29	60
61	58.33	17.83	58.26	18.09	58.18	18.34	58.10	18.60	61
62	59.29	18.13	59.21	18.39	59.13	18.64	59.05	18.90	62
63	60.25	18.42	60.17	18.68	60.08	18.94	60.00	19.21	63
64	61.20	18.71	61.12	18.98	61.04	19.25	60.95	19.51	64
65	62.16	19.00	62.08	19.28	61.99	19.55	61.91	19.82	65
66	63.12	19.30	63.03	19.57	62.95	19.85	62.86	20.12	66
67	64.07	19.59	63.99	19.87	63.90	20.15	63.81	20.43	67
68	65.03	19.88	64.94	20.16	64.85	20.45	64.76	20.73	68
69	65.99	20.17	65.90	20.46	65.81	20.75	65.72	21.04	69
70	66.94	20.47	66.85	20.75	66.76	21.05	66.67	21.34	70
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65	71
72	68.85	21.05	68.76	21.35	68.67	21.65	68.57	21.95	72
73	69.81	21.34	69.72	21.65	69.62	21.95	69.52	22.26	73
74	70.77	21.64	70.67	21.94	70.58	22.25	70.48	22.56	74
75	71.72	21.93	71.63	22.24	71.53	22.55	71.43	22.86	75
76	72.68	22.22	72.58	22.54	72.48	22.85	72.38	23.17	76
77	73.64	22.51	73.54	22.83	73.44	23.15	73.33	23.47	77
78	74.59	22.80	74.49	23.13	74.39	23.46	74.29	23.78	78
79	75.55	23.10	75.45	23.43	75.34	23.76	75.24	24.08	79
80	76.50	23.39	76.40	23.72	76.30	24.05	76.19	24.39	80
81	77.46	23.68	77.36	24.02	77.25	24.36	77.14	24.69	81
82	78.42	23.97	78.31	24.32	78.20	24.66	78.10	25.00	82
83	79.37	24.27	79.27	24.61	79.16	25.96	79.05	25.30	83
84	80.33	24.56	80.22	24.91	80.11	25.26	80.09	25.61	84
85	81.29	24.85	81.18	25.21	81.07	25.56	80.95	25.91	85
86	82.24	25.14	82.13	25.50	82.02	25.86	81.91	26.22	86
87	83.20	25.44	83.09	25.80	82.97	26.16	82.86	26.52	87
88	84.15	25.73	84.04	26.10	83.93	26.46	83.81	26.83	88
89	85.11	26.02	85.00	26.39	84.88	26.76	84.76	27.13	89
90	86.07	26.31	85.95	26.69	85.83	27.06	85.72	27.44	90
91	87.02	26.61	86.91	26.99	86.79	27.36	86.67	27.74	91
92	87.98	26.90	87.86	27.28	87.74	27.66	87.62	28.05	92
93	88.94	27.19	88.82	27.58	88.70	27.97	88.57	28.35	93
94	89.89	27.48	89.77	27.87	89.65	28.27	89.53	28.66	94
95	90.85	27.78	90.73	28.17	90.60	28.57	90.48	28.96	95
96	91.81	28.07	91.68	28.47	91.56	28.87	91.43	29.27	96
97	92.76	28.36	92.64	28.76	92.51	29.17	92.38	29.57	97
98	93.72	28.65	93.59	29.06	93.46	29.47	93.33	29.88	98
99	94.67	28.94	94.55	29.36	94.42	29.77	94.29	30.18	99
100	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	100

Distance.	73 Deg.		72½ Deg.		72¼ Deg.		72¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
73									73
74									74
75									75
76									76
77									77
78									78
79									79
80									80
81									81
82									82
83									83
84									84
85									85
86									86
87									87
88									88
89									89
90									90
91									91
92									92
93									93
94									94
95									95
96									96
97									97
98									98
99									99
100									100

Distance.	18 Deg.		18½ Deg.		18¾ Deg.		18¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.95	0.31	0.95	0.31	0.95	0.32	0.95	0.32	1
2	1.90	0.62	1.90	0.63	1.90	0.63	1.89	0.64	2
3	2.85	0.94	2.85	0.94	2.84	0.95	2.84	0.96	3
4	3.80	1.24	3.80	1.25	3.79	1.27	3.79	1.29	4
5	4.76	1.55	4.75	1.57	4.74	1.59	4.73	1.61	5
6	5.71	1.85	5.70	1.88	5.69	1.90	5.68	1.93	6
7	6.66	2.16	6.65	2.19	6.64	2.22	6.63	2.25	7
8	7.61	2.47	7.60	2.51	7.59	2.54	7.58	2.57	8
9	8.56	2.78	8.55	2.82	8.53	2.86	8.52	2.89	9
10	9.51	3.09	9.50	3.13	9.48	3.17	9.47	3.21	10
11	10.46	3.40	10.45	3.44	10.43	3.49	10.42	3.54	11
12	11.41	3.71	11.40	3.76	11.38	3.81	11.36	3.86	12
13	12.36	4.02	12.35	4.07	12.33	4.12	12.31	4.18	13
14	13.31	4.33	13.30	4.38	13.28	4.44	13.26	4.50	14
15	14.26	4.64	14.25	4.70	14.22	4.77	14.20	4.82	15
16	15.21	4.94	15.20	5.01	15.17	5.08	15.15	5.14	16
17	16.16	5.25	16.14	5.32	16.12	5.39	16.10	5.46	17
18	17.11	5.56	17.09	5.64	17.07	5.71	17.04	5.79	18
19	18.06	5.87	18.04	5.95	18.02	6.03	17.99	6.11	19
20	19.02	6.18	18.99	6.26	18.97	6.35	18.94	6.43	20
21	19.97	6.49	19.94	6.58	19.91	6.66	19.89	6.75	21
22	20.92	6.80	20.89	6.89	20.86	6.98	20.83	7.07	22
23	21.87	7.11	21.84	7.20	21.81	7.30	21.78	7.39	23
24	22.83	7.42	22.79	7.52	22.76	7.62	22.73	7.71	24
25	23.78	7.73	23.74	7.83	23.71	7.93	23.67	8.04	25
26	24.74	8.03	24.69	8.14	24.66	8.25	24.62	8.36	26
27	25.69	8.34	25.64	8.46	25.60	8.57	25.57	8.68	27
28	26.64	8.65	26.59	8.77	26.55	8.88	26.51	9.00	28
29	27.60	8.96	27.54	9.08	27.50	9.20	27.46	9.32	29
30	28.55	9.27	28.49	9.39	28.45	9.52	28.41	9.64	30
31	29.51	9.58	29.44	9.71	29.40	9.84	29.35	9.96	31
32	30.46	9.89	30.39	10.02	30.35	10.15	30.30	10.29	32
33	31.41	10.20	31.34	10.33	31.29	10.47	31.25	10.61	33
34	32.36	10.51	32.29	10.65	32.24	10.79	32.20	10.93	34
35	33.31	10.82	33.24	10.96	33.19	11.11	33.14	11.25	35
36	34.26	11.13	34.19	11.27	34.14	11.42	34.09	11.57	36
37	35.21	11.43	35.14	11.59	35.09	11.74	35.04	11.89	37
38	36.16	11.74	36.09	11.90	36.04	12.06	35.98	12.21	38
39	37.11	12.05	37.04	12.21	36.98	12.37	36.93	12.54	39
40	38.06	12.36	37.99	12.53	37.93	12.69	37.88	12.86	40
41	38.99	12.67	38.94	12.84	38.88	13.01	38.82	13.18	41
42	39.94	12.98	39.89	13.15	39.83	13.33	39.77	13.50	42
43	40.89	13.29	40.84	13.47	40.78	13.64	40.72	13.82	43
44	41.85	13.60	41.79	13.78	41.73	13.96	41.66	14.14	44
45	42.80	13.91	42.74	14.09	42.67	14.28	42.61	14.46	45
46	43.75	14.21	43.69	14.41	43.62	14.60	43.56	14.79	46
47	44.70	14.52	44.64	14.72	44.57	14.91	44.51	15.11	47
48	45.65	14.83	45.59	15.03	45.52	15.23	45.45	15.43	48
49	46.60	15.14	46.54	15.35	46.47	15.55	46.40	15.75	49
50	47.55	15.45	47.48	15.66	47.42	15.87	47.35	16.07	50

Distance.	72 Deg.		71½ Deg.		71¼ Deg.		71¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
1									1
2									2
3									3
4									4
5									5
6									6
7									7
8									8
9									9
10									10
11									11
12									12
13									13
14									14
15									15
16									16
17									17
18									18
19									19
20									20
21									21
22									22
23									23
24									24
25									25
26									26
27									27
28									28
29									29
30									30
31									31
32									32
33									33
34									34
35									35
36									36
37									37
38									38
39									39
40									40
41									41
42									42
43									43
44									44
45									45
46									46
47									47
48									48
49									49
50									50

TRAVERSE TABLE.

Distance.	18 Deg.		18½ Deg.		18¾ Deg.		18¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	18.50	15.76	48.43	15.97	48.36	16.18	48.29	16.39	51
52	49.45	16.07	49.38	16.28	49.31	16.50	49.24	16.71	52
53	50.41	16.38	50.33	16.60	50.26	16.82	50.19	17.04	53
54	51.36	16.69	51.28	16.91	51.21	17.13	51.13	17.36	54
55	52.31	17.00	52.23	17.22	52.16	17.45	52.08	17.68	55
56	53.26	17.30	53.18	17.54	53.11	17.77	53.03	18.00	56
57	54.21	17.61	54.13	17.85	54.05	18.09	53.98	18.32	57
58	55.16	17.92	55.08	18.16	55.00	18.40	54.92	18.64	58
59	56.11	18.23	56.03	18.48	55.95	18.72	55.87	18.96	59
60	57.06	18.54	56.98	18.79	56.90	19.04	56.82	19.29	60
61	58.01	18.85	57.93	19.10	57.85	19.36	57.76	19.61	61
62	58.97	19.16	58.88	19.42	58.80	19.67	58.71	19.93	62
63	59.92	19.47	59.83	19.73	59.74	19.99	59.66	20.25	63
64	60.87	19.78	60.78	20.04	60.69	20.31	60.60	20.57	64
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.89	65
66	62.77	20.40	62.68	20.67	62.59	20.94	62.50	21.22	66
67	63.72	20.70	63.63	20.98	63.54	21.26	63.44	21.54	67
68	64.67	21.01	64.58	21.30	64.49	21.58	64.39	21.86	68
69	65.62	21.32	65.53	21.61	65.43	21.89	65.34	22.18	69
70	66.57	21.63	66.48	21.92	66.38	22.21	66.29	22.50	70
71	67.53	21.94	67.43	22.23	67.33	22.53	67.23	22.82	71
72	68.48	22.25	68.38	22.55	68.28	22.85	68.18	23.14	72
73	69.43	22.56	69.33	22.86	69.23	23.16	69.13	23.47	73
74	70.38	22.87	70.28	23.17	70.18	23.48	70.07	23.79	74
75	71.33	23.18	71.23	23.49	71.12	23.80	71.02	24.11	75
76	72.28	23.49	72.18	23.80	72.07	24.12	71.97	24.43	76
77	73.23	23.79	73.13	24.11	73.02	24.43	72.91	24.75	77
78	74.18	24.10	74.08	24.43	73.97	24.75	73.86	25.07	78
79	75.13	24.41	75.03	24.74	74.92	25.07	74.81	25.39	79
80	76.08	24.72	75.98	25.05	75.87	25.38	75.75	25.72	80
81	77.04	25.03	76.93	25.37	76.81	25.70	76.70	26.04	81
82	77.99	25.34	77.88	25.68	77.76	26.02	77.65	26.36	82
83	78.94	25.65	78.83	25.99	78.71	26.34	78.60	26.68	83
84	79.89	25.96	79.77	26.31	79.66	26.65	79.54	27.00	84
85	80.84	26.27	80.72	26.62	80.61	26.97	80.49	27.32	85
86	81.79	26.58	81.67	26.93	81.56	27.29	81.44	27.64	86
87	82.74	26.88	82.62	27.25	82.50	27.61	82.38	27.97	87
88	83.69	27.19	83.57	27.56	83.45	27.92	83.33	28.29	88
89	84.64	27.50	84.52	27.87	84.40	28.24	84.28	28.61	89
90	85.60	27.81	85.47	28.18	85.35	28.56	85.22	28.93	90
91	86.55	28.12	86.42	28.50	86.30	28.87	86.17	29.25	91
92	87.50	28.43	87.37	28.81	87.25	29.19	87.12	29.57	92
93	88.45	28.74	88.32	29.12	88.19	29.51	88.06	29.89	93
94	89.40	29.05	89.27	29.44	89.14	29.83	89.01	30.22	94
95	90.35	29.36	90.22	29.75	90.09	30.14	89.96	30.54	95
96	91.30	29.67	91.17	30.06	91.04	30.46	90.91	30.86	96
97	92.25	29.97	92.12	30.38	91.99	30.78	91.85	31.18	97
98	93.20	30.28	93.07	30.69	92.94	31.10	92.80	31.50	98
99	94.15	30.59	94.02	31.00	93.88	31.41	93.75	31.82	99
100	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	72 Deg.		71½ Deg.		71½ Deg.		71½ Deg.		

Distance.	19 Deg.		19½ Deg.		19¾ Deg.		19½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.95	0.33	0.91	0.33	0.94	0.33	0.94	0.34	1
2	1.89	0.65	1.89	0.66	1.89	0.67	1.88	0.68	2
3	2.84	0.98	2.83	0.99	2.83	1.00	2.82	1.01	3
4	3.78	1.30	3.78	1.32	3.77	1.34	3.76	1.35	4
5	4.73	1.63	4.72	1.65	4.71	1.67	4.71	1.69	5
6	5.67	1.95	5.66	1.98	5.66	2.00	5.65	2.03	6
7	6.62	2.28	6.61	2.31	6.60	2.34	6.59	2.37	7
8	7.56	2.60	7.55	2.64	7.54	2.67	7.53	2.70	8
9	8.51	2.93	8.50	2.97	8.48	3.00	8.47	3.04	9
10	9.46	3.26	9.44	3.30	9.43	3.34	9.41	3.38	10
11	10.40	3.58	10.38	3.63	10.37	3.67	10.35	3.72	11
12	11.35	3.91	11.33	3.96	11.31	4.01	11.29	4.06	12
13	12.29	4.23	12.27	4.29	12.25	4.34	12.24	4.39	13
14	13.24	4.56	13.22	4.62	13.20	4.67	13.18	4.73	14
15	14.18	4.88	14.16	4.95	14.14	5.01	14.12	5.07	15
16	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5.41	16
17	16.07	5.53	16.05	5.60	16.02	5.67	16.00	5.74	17
18	17.02	5.86	16.99	5.93	16.97	6.01	16.94	6.08	18
19	17.96	6.19	17.94	6.26	17.91	6.34	17.88	6.42	19
20	18.91	6.51	18.88	6.59	18.85	6.68	18.82	6.76	20
21	19.86	6.84	19.83	6.92	19.80	7.01	19.76	7.10	21
22	20.80	7.16	20.77	7.25	20.74	7.34	20.71	7.43	22
23	21.75	7.49	21.71	7.58	21.68	7.68	21.65	7.77	23
24	22.69	7.81	22.66	7.91	22.62	8.01	22.59	8.11	24
25	23.64	8.14	23.60	8.24	23.57	8.35	23.53	8.45	25
26	24.58	8.46	24.55	8.57	24.51	8.68	24.47	8.79	26
27	25.53	8.79	25.49	8.90	25.45	9.01	25.41	9.12	27
28	26.47	9.12	26.43	9.23	26.39	9.35	26.35	9.46	28
29	27.42	9.44	27.38	9.56	27.34	9.68	27.29	9.80	29
30	28.37	9.77	28.32	9.89	28.28	10.01	28.24	10.14	30
31	29.31	10.09	29.27	10.22	29.22	10.35	29.18	10.48	31
32	30.26	10.42	30.21	10.55	30.16	10.68	30.12	10.81	32
33	31.20	10.74	31.15	10.88	31.11	11.02	31.06	11.15	33
34	32.15	11.07	32.10	11.21	32.05	11.35	32.00	11.49	34
35	33.09	11.39	33.04	11.54	32.99	11.68	32.94	11.83	35
36	34.04	11.72	33.99	11.87	33.94	12.02	33.88	12.17	36
37	34.98	12.05	34.93	12.20	34.88	12.35	34.82	12.50	37
38	35.93	12.37	35.88	12.53	35.82	12.68	35.76	12.84	38
39	36.88	12.70	36.82	12.86	36.76	13.02	36.71	13.18	39
40	37.82	13.02	37.76	13.19	37.71	13.35	37.65	13.52	40
41	38.77	13.35	38.71	13.52	38.65	13.69	38.59	13.85	41
42	39.71	13.67	39.65	13.85	39.59	14.02	39.53	14.19	42
43	40.66	14.00	40.60	14.18	40.53	14.35	40.47	14.53	43
44	41.60	14.32	41.54	14.51	41.48	14.69	41.41	14.87	44
45	42.55	14.65	42.48	14.84	42.42	15.02	42.35	15.21	45
46	43.49	14.98	43.43	15.17	43.36	15.36	43.29	15.54	46
47	44.44	15.30	44.37	15.50	44.30	15.69	44.24	15.88	47
48	45.38	15.63	45.32	15.83	45.25	16.02	45.18	16.22	48
49	46.33	15.95	46.26	16.15	46.19	16.36	46.12	16.56	49
50	47.28	16.28	47.20	16.48	47.13	16.69	47.06	16.90	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	71 Deg.		70½ Deg.		70¼ Deg.		70¼ Deg.		

TRAVERSE TABLE.

41

Distance.	19 Deg.		19½ Deg.		19¾ Deg.		19¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	48.22	16.60	48.15	16.81	48.07	17.02	48.00	17.23	51
52	49.17	16.93	49.09	17.14	49.02	17.36	48.94	17.57	52
53	50.11	17.26	50.04	17.47	49.96	17.69	49.88	17.91	53
54	51.06	17.58	50.98	17.80	50.90	18.03	50.82	18.25	54
55	52.00	17.91	51.92	18.13	51.85	18.36	51.76	18.59	55
56	52.95	18.23	52.87	18.46	52.79	18.69	52.71	18.92	56
57	53.89	18.56	53.81	18.79	53.73	19.03	53.65	19.26	57
58	54.84	18.88	54.76	19.12	54.67	19.36	54.59	19.60	58
59	55.79	19.21	55.70	19.45	55.62	19.69	55.53	19.94	59
60	56.73	19.53	56.65	19.78	56.56	20.03	56.47	20.27	60
61	57.68	19.86	57.59	20.11	57.50	20.36	57.41	20.61	61
62	58.62	20.19	58.53	20.44	58.44	20.70	58.35	20.95	62
63	59.57	20.51	59.48	20.77	59.39	21.03	59.29	21.29	63
64	60.51	20.84	60.42	21.10	60.33	21.36	60.24	21.63	64
65	61.46	21.16	61.37	21.43	61.27	21.70	61.18	21.96	65
66	62.40	21.49	62.31	21.76	62.21	22.03	62.12	22.30	66
67	63.35	21.81	63.25	22.09	63.16	22.37	63.06	22.64	67
68	64.30	22.14	64.20	22.42	64.10	22.70	64.00	22.98	68
69	65.24	22.46	65.14	22.75	65.04	23.03	64.94	23.32	69
70	66.19	22.79	66.09	23.08	65.98	23.37	65.88	23.65	70
71	67.13	23.12	67.03	23.41	66.93	23.70	66.82	23.99	71
72	68.08	23.44	67.97	23.74	67.87	24.03	67.76	24.33	72
73	69.02	23.77	68.92	24.07	68.81	24.37	68.71	24.67	73
74	69.97	24.09	69.86	24.40	69.76	24.70	69.65	25.01	74
75	70.91	24.42	70.81	24.73	70.70	25.04	70.59	25.34	75
76	71.86	24.74	71.75	25.06	71.64	25.37	71.53	25.68	76
77	72.80	25.07	72.69	25.39	72.58	25.70	72.47	26.02	77
78	73.75	25.39	73.64	25.72	73.53	26.04	73.41	26.36	78
79	74.70	25.72	74.58	26.05	74.47	26.37	74.35	26.70	79
80	75.64	26.05	75.53	26.38	75.41	26.70	75.29	27.03	80
81	76.59	26.37	76.47	26.70	76.35	27.04	76.24	27.37	81
82	77.53	26.70	77.42	27.03	77.30	27.37	77.18	27.71	82
83	78.48	27.02	78.36	27.36	78.24	27.71	78.12	28.05	83
84	79.42	27.35	79.30	27.69	79.18	28.04	79.06	28.39	84
85	80.37	27.67	80.25	28.02	80.12	28.37	80.00	28.72	85
86	81.31	28.00	81.19	28.35	81.07	28.71	80.94	29.06	86
87	82.26	28.32	82.14	28.68	82.01	29.04	81.88	29.40	87
88	83.21	28.65	83.08	29.01	92.95	29.37	82.82	29.74	88
89	84.15	28.98	84.02	29.34	83.90	29.71	83.76	30.07	89
90	85.10	29.30	84.97	29.67	84.84	30.04	84.71	30.41	90
91	86.04	29.63	85.91	30.00	85.78	30.38	85.65	30.75	91
92	86.99	29.95	86.86	30.33	86.72	30.71	86.59	31.09	92
93	87.93	30.28	87.80	30.66	87.67	31.04	87.53	31.43	93
94	88.88	30.60	88.74	30.99	88.61	31.38	88.47	31.76	94
95	89.82	30.93	89.69	31.32	89.55	31.71	89.41	32.10	95
96	90.77	31.25	90.63	31.65	90.49	32.05	90.35	32.44	96
97	91.72	31.58	91.58	31.98	91.44	32.38	91.29	32.78	97
98	92.66	31.91	92.52	32.31	92.38	32.71	92.24	33.12	98
99	93.61	32.23	93.46	32.64	93.32	33.05	93.18	33.45	99
100	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	71 Deg.		70½ Deg.		70¼ Deg.		70¼ Deg.		



TRAVERSE TABLE.

Distance.	16 Deg.		16½ Deg.		16¾ Deg.		16¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29	1
2	1.92	0.55	1.92	0.56	1.92	0.57	1.92	0.58	2
3	2.88	0.83	2.88	0.84	2.88	0.85	2.87	0.86	3
4	3.85	1.10	3.84	1.12	3.84	1.14	3.83	1.15	4
5	4.81	1.38	4.80	1.40	4.79	1.42	4.79	1.44	5
6	5.77	1.65	5.76	1.68	5.75	1.70	5.75	1.73	6
7	6.73	1.93	6.72	1.96	6.71	1.99	6.70	2.02	7
8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31	8
9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59	9
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88	10
11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17	11
12	11.54	3.31	11.52	3.36	11.51	3.41	11.49	3.46	12
13	12.50	3.58	12.48	3.64	12.46	3.69	12.45	3.75	13
14	13.46	3.86	13.44	3.92	13.42	3.93	13.41	4.03	14
15	14.42	4.13	14.40	4.20	14.38	4.26	14.36	4.32	15
16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4.61	16
17	16.34	4.69	16.32	4.76	16.30	4.83	16.28	4.90	17
18	17.30	4.96	17.28	5.04	17.26	5.11	17.24	5.19	18
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19	5.48	19
20	19.23	5.51	19.20	5.60	19.18	5.68	19.15	5.76	20
21	20.19	5.79	20.16	5.88	20.14	5.96	20.11	6.05	21
22	21.15	6.06	21.12	6.16	21.09	6.25	21.07	6.34	22
23	22.11	6.34	22.08	6.44	22.05	6.53	22.02	6.63	23
24	23.07	6.62	23.04	6.72	23.01	6.82	22.99	6.92	24
25	24.03	6.89	24.00	7.00	23.97	7.10	23.94	7.20	25
26	24.99	7.17	24.96	7.28	24.93	7.38	24.90	7.49	26
27	25.95	7.44	25.92	7.56	25.89	7.67	25.85	7.78	27
28	26.92	7.72	26.88	7.84	26.85	7.95	26.81	8.07	28
29	27.88	7.99	27.84	8.11	27.81	8.24	27.77	8.35	29
30	28.84	8.27	28.80	8.39	28.76	8.52	28.73	8.65	30
31	29.80	8.54	29.76	8.67	29.72	8.80	29.68	8.93	31
32	30.76	8.82	30.72	8.95	30.68	9.09	30.64	9.22	32
33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51	33
34	32.68	9.37	32.64	9.51	32.60	9.66	32.56	9.80	34
35	33.64	9.65	33.60	9.79	33.56	9.94	33.51	10.09	35
36	34.61	9.92	34.56	10.07	34.52	10.22	34.47	10.38	36
37	35.57	10.20	35.52	10.35	35.48	10.51	35.43	10.66	37
38	36.53	10.47	36.48	10.63	36.44	10.79	36.39	10.95	38
39	37.49	10.75	37.44	10.91	37.39	11.08	37.35	11.24	39
40	38.45	11.03	38.40	11.19	38.35	11.36	38.30	11.53	40
41	39.41	11.30	39.36	11.47	39.31	11.64	39.26	11.82	41
42	40.37	11.58	40.32	11.75	40.27	11.93	40.22	12.10	42
43	41.33	11.85	41.28	12.03	41.23	12.21	41.18	12.39	43
44	42.30	12.13	42.24	12.31	42.19	12.50	42.13	12.68	44
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97	45
46	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26	46
47	45.18	12.95	45.12	13.15	45.06	13.35	45.01	13.55	47
48	46.14	13.23	46.08	13.43	46.02	13.63	45.96	13.83	48
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12	49
50	48.06	13.78	48.00	13.99	47.94	14.20	47.88	14.41	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73½ Deg.		73¼ Deg.		73¼ Deg.		

TRAVERSE TABLE.

Distance.	16 Deg.		16½ Deg.		16¾ Deg.		16¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70	51
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99	52
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27	53
54	51.91	14.88	51.84	15.11	51.78	15.34	51.71	15.56	54
55	52.87	15.16	52.80	15.39	52.74	15.62	52.67	15.85	55
56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14	56
57	54.79	15.71	54.72	15.95	54.65	16.19	54.58	16.43	57
58	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72	58
59	56.71	16.26	56.64	16.51	56.57	16.76	56.50	17.00	59
60	57.68	16.54	57.60	16.79	57.53	17.04	57.45	17.29	60
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58	61
62	59.60	17.09	59.52	17.35	59.45	17.61	59.37	17.87	62
63	60.56	17.37	60.48	17.63	60.41	17.89	60.33	18.16	63
64	61.52	17.64	61.44	17.91	61.36	18.18	61.28	18.44	64
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	65
66	63.44	18.19	63.36	18.47	63.25	18.74	63.20	19.02	66
67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31	67
68	65.37	18.74	65.28	19.03	65.20	19.31	65.11	19.60	68
69	66.33	19.02	66.24	19.31	66.16	19.60	66.07	19.89	69
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	70
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46	71
72	69.21	19.85	69.12	20.15	69.03	20.45	68.95	20.75	72
73	70.17	20.12	70.08	20.43	69.99	20.73	69.90	21.04	73
74	71.13	20.40	71.04	20.71	70.95	21.02	70.86	21.33	74
75	72.09	20.67	72.00	20.99	71.91	21.30	71.82	21.61	75
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	76
77	74.02	21.22	73.92	21.55	73.83	21.87	73.73	22.19	77
78	74.98	21.50	74.88	21.83	74.79	22.15	74.69	22.48	78
79	75.94	21.78	75.84	22.11	75.75	22.44	75.65	22.77	79
80	76.90	22.05	76.80	22.39	76.71	22.72	76.61	23.06	80
81	77.86	22.33	77.76	22.67	77.66	23.01	77.56	23.34	81
82	78.82	22.60	78.72	22.95	78.62	23.29	78.52	23.63	82
83	79.78	22.88	79.68	23.23	79.58	23.57	79.48	23.92	83
84	80.75	23.15	80.64	23.51	80.54	23.86	80.44	24.21	84
85	81.71	23.43	81.60	23.79	81.50	24.14	81.39	24.50	85
86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.78	86
87	83.63	23.98	83.52	24.35	83.42	24.71	83.31	25.07	87
88	84.59	24.26	84.48	24.62	84.38	24.99	84.27	25.36	88
89	85.55	24.53	85.44	24.90	85.33	25.28	85.22	25.65	89
90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94	90
91	87.47	25.08	87.36	25.46	87.25	25.85	87.14	26.23	91
92	88.44	25.36	88.32	25.74	88.21	26.13	88.10	26.51	92
93	89.40	25.63	89.28	26.02	89.17	26.41	89.05	26.80	93
94	90.36	25.91	90.24	26.30	90.13	26.70	90.01	27.09	94
95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38	95
96	92.28	26.46	92.16	26.86	92.05	27.27	91.93	27.67	96
97	93.24	26.74	93.12	27.14	93.01	27.55	92.88	27.95	97
98	94.20	27.01	94.08	27.42	93.96	27.83	93.84	28.24	98
99	95.16	27.29	95.04	27.70	94.92	28.12	94.80	28.53	99
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73½ Deg.		73¼ Deg.		73¼ Deg.		

## TRAVERSE TABLE.

Distance.	16 Deg.		16½ Deg.		16¾ Deg.		16⅞ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29	1
2	1.92	0.55	1.92	0.56	1.92	0.57	1.92	0.59	2
3	2.88	0.83	2.88	0.84	2.88	0.85	2.87	0.86	3
4	3.85	1.10	3.84	1.12	3.84	1.14	3.83	1.15	4
5	4.81	1.38	4.80	1.40	4.79	1.42	4.79	1.44	5
6	5.77	1.65	5.76	1.68	5.75	1.70	5.75	1.73	6
7	6.73	1.93	6.72	1.96	6.71	1.99	6.70	2.02	7
8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31	8
9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59	9
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88	10
11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17	11
12	11.54	3.31	11.52	3.36	11.51	3.41	11.49	3.46	12
13	12.50	3.58	12.48	3.64	12.46	3.69	12.45	3.75	13
14	13.46	3.86	13.44	3.92	13.42	3.98	13.41	4.03	14
15	14.42	4.13	14.40	4.20	14.38	4.26	14.36	4.32	15
16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4.61	16
17	16.34	4.69	16.32	4.76	16.30	4.83	16.28	4.90	17
18	17.30	4.96	17.28	5.04	17.26	5.11	17.24	5.19	18
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19	5.48	19
20	19.23	5.51	19.20	5.60	19.18	5.68	19.15	5.76	20
21	20.19	5.79	20.16	5.88	20.14	5.96	20.11	6.05	21
22	21.15	6.06	21.12	6.16	21.09	6.25	21.07	6.34	22
23	22.11	6.34	22.08	6.44	22.05	6.53	22.02	6.63	23
24	23.07	6.62	23.04	6.72	23.01	6.82	22.98	6.92	24
25	24.03	6.89	24.00	7.00	23.97	7.10	23.94	7.20	25
26	24.99	7.17	24.96	7.28	24.93	7.38	24.90	7.49	26
27	25.95	7.44	25.92	7.56	25.89	7.67	25.85	7.78	27
28	26.92	7.72	26.88	7.84	26.85	7.95	26.81	8.07	28
29	27.88	7.99	27.84	8.11	27.81	8.24	27.77	8.36	29
30	28.84	8.27	28.80	8.39	28.76	8.52	28.73	8.65	30
31	29.80	8.54	29.76	8.67	29.72	8.80	29.68	8.93	31
32	30.76	8.82	30.72	8.95	30.68	9.09	30.64	9.22	32
33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51	33
34	32.68	9.37	32.64	9.51	32.60	9.66	32.56	9.80	34
35	33.64	9.65	33.60	9.79	33.56	9.94	33.51	10.09	35
36	34.61	9.92	34.56	10.07	34.52	10.22	34.47	10.38	36
37	35.57	10.20	35.52	10.35	35.48	10.51	35.43	10.66	37
38	36.53	10.47	36.48	10.63	36.44	10.79	36.39	10.95	38
39	37.49	10.75	37.44	10.91	37.39	11.08	37.35	11.24	39
40	38.45	11.03	38.40	11.19	38.35	11.36	38.30	11.53	40
41	39.41	11.30	39.36	11.47	39.31	11.64	39.26	11.82	41
42	40.37	11.58	40.32	11.75	40.27	11.93	40.22	12.10	42
43	41.33	11.85	41.28	12.03	41.23	12.21	41.18	12.39	43
44	42.30	12.13	42.24	12.31	42.19	12.50	42.13	12.68	44
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97	45
46	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26	46
47	45.18	12.95	45.12	13.15	45.06	13.35	45.01	13.55	47
48	46.14	13.23	46.08	13.43	46.02	13.63	45.96	13.83	48
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12	49
50	48.06	13.78	48.00	13.99	47.94	14.20	47.88	14.41	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73¾ Deg.		73½ Deg.		73¼ Deg.		

TRAVERSE TABLE.

Distance.	16 Deg.		16½ Deg.		16½ Deg.		16½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70	51
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99	52
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27	53
54	51.91	14.88	51.84	15.11	51.78	15.34	51.71	15.56	54
55	52.87	15.16	52.80	15.39	52.74	15.62	52.67	15.85	55
56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14	56
57	54.79	15.71	54.72	15.95	54.65	16.19	54.58	16.43	57
58	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72	58
59	56.71	16.26	56.64	16.51	56.57	16.76	56.50	17.00	59
60	57.68	16.54	57.60	16.79	57.53	17.04	57.45	17.29	60
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58	61
62	59.60	17.09	59.52	17.35	59.45	17.61	59.37	17.87	62
63	60.56	17.37	60.48	17.63	60.41	17.89	60.33	18.16	63
64	61.52	17.64	61.44	17.91	61.36	18.18	61.28	18.44	64
65	62.48	17.92	62.40	18.19	62.32	18.46	62.24	18.73	65
66	63.44	18.19	63.36	18.47	63.28	18.74	63.20	19.02	66
67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31	67
68	65.37	18.74	65.28	19.03	65.20	19.31	65.11	19.60	68
69	66.33	19.02	66.24	19.31	66.16	19.60	66.07	19.89	69
70	67.29	19.29	67.20	19.59	67.12	19.88	67.03	20.17	70
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46	71
72	69.21	19.85	69.12	20.15	69.03	20.45	68.95	20.75	72
73	70.17	20.12	70.08	20.43	69.99	20.73	69.90	21.04	73
74	71.13	20.40	71.04	20.71	70.95	21.02	70.86	21.33	74
75	72.09	20.67	72.00	20.99	71.91	21.30	71.82	21.61	75
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90	76
77	74.02	21.22	73.92	21.55	73.83	21.87	73.73	22.19	77
78	74.98	21.50	74.88	21.83	74.79	22.15	74.69	22.48	78
79	75.94	21.78	75.84	22.11	75.75	22.44	75.65	22.77	79
80	76.90	22.05	76.80	22.39	76.71	22.72	76.61	23.06	80
81	77.86	22.33	77.76	22.67	77.66	23.01	77.56	23.34	81
82	78.82	22.60	78.72	22.95	78.62	23.29	78.52	23.63	82
83	79.78	22.88	79.68	23.23	79.58	23.57	79.48	23.92	83
84	80.75	23.15	80.64	23.51	80.54	23.86	80.44	24.21	84
85	81.71	23.43	81.60	23.79	81.50	24.14	81.39	24.50	85
86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.78	86
87	83.63	23.98	83.52	24.35	83.42	24.71	83.31	25.07	87
88	84.59	24.26	84.48	24.62	84.38	24.99	84.27	25.36	88
89	85.55	24.53	85.44	24.90	85.33	25.28	85.22	25.65	89
90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94	90
91	87.47	25.08	87.36	25.46	87.25	25.85	87.14	26.23	91
92	88.44	25.36	88.32	25.74	88.21	26.13	88.10	26.51	92
93	89.40	25.63	89.28	26.02	89.17	26.41	89.05	26.80	93
94	90.36	25.91	90.24	26.30	90.13	26.70	90.01	27.09	94
95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38	95
96	92.28	26.46	92.16	26.86	92.05	27.27	91.93	27.67	96
97	93.24	26.74	93.12	27.14	93.01	27.55	92.88	27.95	97
98	94.20	27.01	94.08	27.42	93.96	27.83	93.84	28.24	98
99	95.16	27.29	95.04	27.70	94.92	28.12	94.80	28.53	99
100	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	74 Deg.		73½ Deg.		73½ Deg.		73½ Deg.		



Distance.	20 Deg.		20½ Deg.		20¾ Deg.		20¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.92	17.44	47.35	17.65	47.77	17.86	47.69	18.07	51
52	48.86	17.79	48.79	18.00	48.71	18.21	48.63	18.42	52
53	49.80	18.13	49.72	18.34	49.64	18.56	49.56	18.78	53
54	50.74	18.47	50.66	18.69	50.58	18.91	50.50	19.13	54
55	51.68	18.81	51.60	19.04	51.52	19.26	51.43	19.49	55
56	52.62	19.15	52.54	19.38	52.45	19.61	52.37	19.84	56
57	53.56	19.50	53.48	19.73	53.39	19.96	53.30	20.19	57
58	54.50	19.84	54.42	20.07	54.33	20.31	54.24	20.55	58
59	55.44	20.18	55.35	20.42	55.26	20.66	55.17	20.90	59
60	56.38	20.52	56.29	20.77	56.20	21.01	56.11	21.26	60
61	57.32	20.86	57.23	21.11	57.14	21.36	57.04	21.61	61
62	58.26	21.21	58.17	21.46	58.07	21.71	57.98	21.97	62
63	59.20	21.55	59.11	21.81	59.01	22.06	58.91	22.32	63
64	60.14	21.89	60.04	22.15	59.95	22.41	59.85	22.67	64
65	61.08	22.23	60.98	22.50	60.88	22.76	60.78	23.03	65
66	62.02	22.57	61.92	22.84	61.82	23.11	61.72	23.38	66
67	62.96	22.92	62.86	23.19	62.76	23.46	62.65	23.74	67
68	63.90	23.26	63.80	23.54	63.69	23.81	63.59	24.09	68
69	64.84	23.60	64.74	23.88	64.63	24.16	64.52	24.45	69
70	65.78	23.94	65.67	24.23	65.57	24.51	65.46	24.80	70
71	66.72	24.28	66.61	24.57	66.50	24.86	66.39	25.15	71
72	67.66	24.63	67.55	24.92	67.44	25.21	67.33	25.51	72
73	68.60	24.97	68.49	25.27	68.38	25.57	68.26	25.86	73
74	69.54	25.31	69.43	25.61	69.31	25.92	69.20	26.22	74
75	70.48	25.65	70.36	25.96	70.25	26.27	70.14	26.57	75
76	71.42	25.99	71.30	26.30	71.19	26.62	71.07	26.93	76
77	72.36	26.34	72.24	26.65	72.12	26.97	72.01	27.28	77
78	73.30	26.68	73.18	27.00	73.06	27.32	72.94	27.63	78
79	74.24	27.02	74.12	27.34	74.00	27.67	73.88	27.99	79
80	75.18	27.36	75.06	27.69	74.93	28.02	74.81	28.34	80
81	76.12	27.70	75.99	28.04	75.87	28.37	75.75	28.70	81
82	77.05	28.05	76.93	28.38	76.81	28.72	76.68	29.05	82
83	77.99	28.39	77.87	28.73	77.74	29.07	77.62	29.41	83
84	78.93	28.73	78.81	29.07	78.68	29.42	78.55	29.76	84
85	79.87	29.07	79.75	29.42	79.62	29.77	79.49	30.11	85
86	80.81	29.41	80.68	29.77	80.55	30.12	80.42	30.47	86
87	81.75	29.76	81.62	30.11	81.49	30.47	81.36	30.82	87
88	82.69	30.10	82.56	30.46	82.43	30.82	82.29	31.18	88
89	83.63	30.44	83.50	30.80	83.36	31.17	83.23	31.53	89
90	84.57	30.78	84.44	31.15	84.30	31.52	84.16	31.89	90
91	85.51	31.12	85.38	31.50	85.24	31.87	85.10	32.24	91
92	86.45	31.47	86.31	31.84	86.17	32.22	86.03	32.59	92
93	87.39	31.81	87.25	32.19	87.11	32.57	86.97	32.95	93
94	88.33	32.15	88.19	32.54	88.05	32.92	87.90	33.30	94
95	89.27	32.49	89.13	32.88	88.98	33.27	88.84	33.66	95
96	90.21	32.83	90.07	33.23	89.92	33.62	89.77	34.01	96
97	91.15	33.18	91.00	33.57	90.86	33.97	90.71	34.37	97
98	92.09	33.52	91.94	33.92	91.79	34.32	91.64	34.72	98
99	93.03	33.86	92.88	34.27	92.73	34.67	92.58	35.07	99
100	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	100

Distance.	70 Deg.		69½ Deg.		69¼ Deg.		69¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

## TRAVERSE TABLE.

Distance.	21 Deg.		21½ Deg.		21¾ Deg.		21½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.93	0.36	0.93	0.36	0.93	0.37	0.93	0.37	1
2	1.87	0.72	1.86	0.72	1.86	0.73	1.86	0.74	2
3	2.80	1.08	2.80	1.09	2.79	1.10	2.79	1.11	3
4	3.73	1.43	3.73	1.45	3.72	1.47	3.72	1.48	4
5	4.67	1.79	4.66	1.81	4.65	1.83	4.64	1.85	5
6	5.60	2.15	5.59	2.17	5.58	2.20	5.57	2.22	6
7	6.54	2.51	6.52	2.54	6.51	2.57	6.50	2.59	7
8	7.47	2.87	7.46	2.90	7.44	2.93	7.43	2.96	8
9	8.40	3.23	8.39	3.26	8.37	3.30	8.36	3.34	9
10	9.34	3.58	9.32	3.62	9.30	3.67	9.29	3.71	10
11	10.27	3.94	10.25	3.99	10.23	4.03	10.22	4.08	11
12	11.20	4.30	11.18	4.35	11.17	4.40	11.15	4.45	12
13	12.14	4.66	12.12	4.71	12.10	4.76	12.07	4.82	13
14	13.07	5.02	13.05	5.07	13.03	5.13	13.00	5.19	14
15	14.00	5.38	13.98	5.44	13.96	5.50	13.93	5.56	15
16	14.94	5.73	14.91	5.80	14.89	5.86	14.86	5.93	16
17	15.87	6.09	15.84	6.16	15.82	6.23	15.79	6.30	17
18	16.80	6.45	16.78	6.52	16.75	6.60	16.72	6.67	18
19	17.74	6.81	17.71	6.89	17.68	6.96	17.65	7.04	19
20	18.67	7.17	18.64	7.25	18.61	7.33	18.58	7.41	20
21	19.61	7.53	19.57	7.61	19.54	7.70	19.50	7.78	21
22	20.54	7.88	20.50	7.97	20.47	8.06	20.43	8.15	22
23	21.47	8.24	21.44	8.34	21.40	8.43	21.36	8.52	23
24	22.41	8.60	22.37	8.70	22.33	8.80	22.29	8.89	24
25	23.34	8.96	23.30	9.06	23.26	9.16	23.22	9.26	25
26	24.27	9.32	24.23	9.42	24.19	9.53	24.15	9.63	26
27	25.21	9.68	25.16	9.79	25.12	9.90	25.08	10.01	27
28	26.14	10.03	26.10	10.15	26.05	10.26	26.01	10.38	28
29	27.07	10.39	27.03	10.51	26.98	10.63	26.94	10.75	29
30	28.01	10.75	27.96	10.87	27.91	11.00	27.86	11.12	30
31	28.94	11.11	28.89	11.24	28.84	11.36	28.79	11.49	31
32	29.87	11.47	29.82	11.60	29.77	11.73	29.72	11.86	32
33	30.81	11.83	30.76	11.96	30.70	12.09	30.65	12.23	33
34	31.74	12.18	31.69	12.32	31.63	12.46	31.58	12.60	34
35	32.68	12.54	32.62	12.69	32.56	12.83	32.51	12.97	35
36	33.61	12.90	33.55	13.05	33.50	13.19	33.44	13.34	36
37	34.54	13.26	34.48	13.41	34.43	13.56	34.37	13.71	37
38	35.48	13.62	35.42	13.77	35.36	13.93	35.29	14.08	38
39	36.41	13.98	36.35	14.14	36.29	14.29	36.22	14.45	39
40	37.34	14.33	37.28	14.50	37.22	14.66	37.15	14.82	40
41	38.28	14.69	38.21	14.86	38.15	15.03	38.08	15.19	41
42	39.21	15.05	39.14	15.22	39.08	15.39	39.01	15.56	42
43	40.14	15.41	40.08	15.58	40.01	15.76	39.94	15.93	43
44	41.08	15.77	41.01	15.95	40.94	16.13	40.87	16.30	44
45	42.01	16.13	41.94	16.31	41.87	16.49	41.80	16.68	45
46	42.94	16.48	42.87	16.67	42.80	16.86	42.73	17.05	46
47	43.88	16.84	43.80	17.03	43.73	17.23	43.65	17.42	47
48	44.81	17.20	44.74	17.40	44.66	17.59	44.58	17.79	48
49	45.75	17.56	45.67	17.76	45.59	17.96	45.51	18.16	49
50	46.68	17.92	46.60	18.12	46.52	18.33	46.44	18.53	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	69 Deg.		68½ Deg.		68½ Deg.		68½ Deg.		

TRAVERSE TABLE.

Distance.	21 Deg.		21¼ Deg.		21½ Deg.		21¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.61	18.28	47.53	18.48	47.45	18.69	47.37	18.90	51
52	48.55	18.64	48.46	18.85	48.38	19.06	48.30	19.27	52
53	49.48	18.99	49.40	19.21	49.31	19.42	49.23	19.64	53
54	50.41	19.35	50.33	19.57	50.24	19.79	50.16	20.01	54
55	51.35	19.71	51.26	19.93	51.17	20.16	51.08	20.38	55
56	52.28	20.07	52.19	20.30	52.10	20.52	52.01	20.75	56
57	53.21	20.43	53.12	20.66	53.03	20.89	52.94	21.12	57
58	54.15	20.79	54.06	21.02	53.96	21.26	53.87	21.49	58
59	55.08	21.14	54.99	21.38	54.89	21.62	54.80	21.86	59
60	56.01	21.50	55.92	21.75	55.83	21.99	55.73	22.23	60
61	56.95	21.86	56.85	22.11	56.76	22.36	56.66	22.60	61
62	57.88	22.22	57.78	22.47	57.69	22.72	57.59	22.97	62
63	58.82	22.58	58.72	22.83	58.62	23.09	58.52	23.35	63
64	59.75	22.94	59.65	23.20	59.55	23.46	59.44	23.72	64
65	60.68	23.29	60.58	23.56	60.48	23.82	60.37	24.09	65
66	61.62	23.65	61.51	23.92	61.41	24.19	61.30	24.46	66
67	62.55	24.01	62.44	24.28	62.34	24.56	62.23	24.83	67
68	63.48	24.37	63.38	24.65	63.27	24.92	63.16	25.20	68
69	64.42	24.73	64.31	25.01	64.20	25.29	64.09	25.57	69
70	65.35	25.09	65.24	25.37	65.13	25.66	65.02	25.94	70
71	66.28	25.44	66.17	25.73	66.06	26.02	65.95	26.31	71
72	67.22	25.80	67.10	26.10	66.99	26.39	66.87	26.68	72
73	68.15	26.16	68.04	26.46	67.92	26.75	67.80	27.05	73
74	69.08	26.52	68.97	26.82	68.85	27.12	68.73	27.42	74
75	70.02	26.88	69.90	27.18	69.78	27.49	69.66	27.79	75
76	70.95	27.24	70.83	27.55	70.71	27.85	70.59	28.16	76
77	71.89	27.59	71.76	27.91	71.64	28.22	71.52	28.53	77
78	72.82	27.95	72.70	28.27	72.57	28.59	72.45	28.90	78
79	73.75	28.31	73.63	28.63	73.50	28.95	73.38	29.27	79
80	74.69	28.67	74.56	29.00	74.43	29.32	74.30	29.64	80
81	75.62	29.03	75.49	29.36	75.36	29.69	75.23	30.02	81
82	76.55	29.39	76.42	29.72	76.29	30.05	76.16	30.39	82
83	77.49	29.74	77.36	30.08	77.22	30.42	77.09	30.76	83
84	78.42	30.10	78.29	30.44	78.16	30.79	78.02	31.13	84
85	79.35	30.46	79.22	30.81	79.09	31.15	78.95	31.50	85
86	80.29	30.82	80.15	31.17	80.02	31.52	79.88	31.87	86
87	81.22	31.18	81.08	31.53	80.95	31.89	80.81	32.24	87
88	82.16	31.54	82.02	31.89	81.88	32.25	81.74	32.61	88
89	83.09	31.89	82.95	32.26	82.81	32.62	82.66	32.98	89
90	84.02	32.25	83.88	32.62	83.74	32.99	83.59	33.35	90
91	84.96	32.61	84.81	32.98	84.67	33.35	84.52	33.72	91
92	85.89	32.97	85.74	33.34	85.60	33.72	85.45	34.09	92
93	86.82	33.33	86.68	33.71	86.53	34.08	86.38	34.46	93
94	87.76	33.69	87.61	34.07	87.46	34.45	87.31	34.83	94
95	88.69	34.04	88.54	34.43	88.39	34.82	88.24	35.20	95
96	89.62	34.40	89.47	34.79	89.32	35.18	89.17	35.57	96
97	90.56	34.76	90.40	35.16	90.25	35.55	90.09	35.94	97
98	91.49	35.12	91.34	35.52	91.18	35.92	91.02	36.31	98
99	92.42	35.48	92.27	35.88	92.11	36.28	91.95	36.69	99
100	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	69 Deg.		68¼ Deg.		68½ Deg.		68¾ Deg.		



TRAVERSE TABLE.

Distance.	22 Deg.		22½ Deg.		22½ Deg.		22½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.93	0.37	0.93	0.38	0.92	0.38	0.92	0.39	1
2	1.85	0.75	1.85	0.76	1.85	0.77	1.84	0.77	2
3	2.78	1.12	2.78	1.14	2.77	1.15	2.77	1.16	3
4	3.71	1.50	3.70	1.51	3.70	1.53	3.69	1.55	4
5	4.64	1.87	4.63	1.89	4.62	1.91	4.61	1.93	5
6	5.56	2.25	5.55	2.27	5.54	2.30	5.53	2.32	6
7	6.49	2.62	6.48	2.65	6.47	2.68	6.46	2.71	7
8	7.42	3.00	7.40	3.03	7.39	3.06	7.38	3.09	8
9	8.34	3.37	8.33	3.41	8.31	3.44	8.30	3.48	9
10	9.27	3.75	9.26	3.79	9.24	3.83	9.22	3.87	10
11	10.20	4.12	10.18	4.17	10.16	4.21	10.14	4.25	11
12	11.13	4.50	11.11	4.54	11.09	4.59	11.07	4.64	12
13	12.05	4.87	12.03	4.92	12.01	4.97	11.99	5.03	13
14	12.98	5.24	12.96	5.30	12.93	5.36	12.91	5.41	14
15	13.91	5.62	13.88	5.68	13.86	5.74	13.83	5.80	15
16	14.83	5.99	14.81	6.06	14.78	6.12	14.76	6.19	16
17	15.76	6.37	15.73	6.44	15.71	6.51	15.68	6.57	17
18	16.69	6.74	16.66	6.82	16.63	6.89	16.60	6.96	18
19	17.62	7.12	17.59	7.19	17.55	7.27	17.52	7.35	19
20	18.54	7.49	18.51	7.57	18.48	7.65	18.44	7.73	20
21	19.47	7.87	19.44	7.95	19.40	8.04	19.37	8.12	21
22	20.40	8.24	20.36	8.33	20.33	8.42	20.29	8.51	22
23	21.33	8.62	21.29	8.71	21.25	8.80	21.21	8.89	23
24	22.25	8.99	22.21	9.09	22.17	9.18	22.13	9.28	24
25	23.18	9.37	23.14	9.47	23.10	9.57	23.05	9.67	25
26	24.11	9.74	24.06	9.84	24.02	9.95	23.98	10.05	26
27	25.03	10.11	24.99	10.22	24.94	10.33	24.90	10.44	27
28	25.96	10.49	25.92	10.60	25.87	10.72	25.82	10.83	28
29	26.89	10.86	26.84	10.98	26.79	11.10	26.74	11.21	29
30	27.82	11.24	27.77	11.36	27.72	11.48	27.67	11.60	30
31	28.74	11.61	28.69	11.74	28.64	11.86	28.59	11.99	31
32	29.67	11.99	29.62	12.12	29.56	12.25	29.51	12.37	32
33	30.60	12.36	30.54	12.50	30.49	12.63	30.43	12.76	33
34	31.52	12.74	31.47	12.87	31.41	13.01	31.35	13.15	34
35	32.45	13.11	32.39	13.25	32.34	13.39	32.28	13.53	35
36	33.38	13.49	33.32	13.63	33.26	13.78	33.20	13.92	36
37	34.31	13.86	34.24	14.01	34.18	14.16	34.12	14.31	37
38	35.23	14.24	35.17	14.39	35.11	14.54	35.04	14.70	38
39	36.16	14.61	36.10	14.77	36.03	14.92	35.97	15.08	39
40	37.09	14.98	37.02	15.15	36.96	15.31	36.89	15.47	40
41	38.01	15.36	37.95	15.52	37.88	15.69	37.81	15.86	41
42	38.94	15.73	38.87	15.90	38.80	16.07	38.73	16.24	42
43	39.87	16.11	39.80	16.28	39.73	16.46	39.65	16.63	43
44	40.80	16.48	40.72	16.66	40.65	16.84	40.58	17.02	44
45	41.72	16.86	41.65	17.04	41.57	17.22	41.50	17.40	45
46	42.65	17.23	42.57	17.42	42.50	17.60	42.42	17.79	46
47	43.58	17.61	43.50	17.80	43.42	17.99	43.34	18.18	47
48	44.50	17.98	44.43	18.18	44.35	18.37	44.27	18.56	48
49	45.43	18.36	45.35	18.55	45.27	18.75	45.19	18.95	49
50	46.36	18.73	46.28	18.93	46.19	19.13	46.11	19.34	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	68 Deg.		67½ Deg.		67½ Deg.		67½ Deg.		

TRAVERSE TABLE.

Distance.	22 Deg.		22½ Deg.		22½ Deg.		22½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	47.29	19.10	47.20	19.51	47.12	19.52	47.03	19.72	51
52	48.21	19.48	48.13	19.69	48.04	19.90	47.95	20.11	52
53	49.14	19.85	49.05	20.07	48.97	20.28	48.88	20.59	53
54	50.07	20.23	49.98	20.45	49.89	20.66	49.80	20.88	54
55	51.00	20.60	50.90	20.83	50.81	21.05	50.72	21.27	55
56	51.92	20.98	51.83	21.20	51.74	21.43	51.64	21.66	56
57	52.85	21.35	52.76	21.58	52.66	21.81	52.57	22.04	57
58	53.78	21.73	53.68	21.96	53.59	22.20	53.49	22.43	58
59	54.70	22.10	54.61	22.34	54.51	22.58	54.41	22.82	59
60	55.63	22.48	55.53	22.72	55.43	22.96	55.33	23.20	60
61	56.56	22.85	56.47	23.10	56.36	23.34	56.25	23.59	61
62	57.49	23.23	57.38	23.48	57.28	23.73	57.18	23.98	62
63	58.41	23.60	58.31	23.85	58.20	24.11	58.10	24.38	63
64	59.34	23.97	59.23	24.23	59.13	24.49	59.02	24.75	64
65	60.27	24.35	60.16	24.61	60.05	24.87	59.94	25.14	65
66	61.19	24.72	61.09	24.99	60.98	25.26	60.87	25.52	66
67	62.12	25.10	62.01	25.37	61.90	25.64	61.79	25.91	67
68	63.05	25.47	62.94	25.75	62.82	26.02	62.71	26.30	68
69	63.98	25.85	63.86	26.13	63.75	26.41	63.63	26.68	69
70	64.90	26.22	64.79	26.51	64.67	26.79	64.55	27.07	70
71	65.83	26.60	65.71	26.88	65.60	27.17	65.48	27.46	71
72	66.76	26.97	66.64	27.26	66.52	27.55	66.40	27.84	72
73	67.68	27.35	67.56	27.64	67.44	27.94	67.32	28.23	73
74	68.61	27.72	68.49	28.02	68.37	28.32	68.24	28.62	74
75	69.54	28.10	69.42	28.40	69.29	28.70	69.17	29.00	75
76	70.47	28.47	70.34	28.78	70.21	29.08	70.09	29.39	76
77	71.39	28.84	71.27	29.16	71.14	29.47	71.01	29.78	77
78	72.32	29.22	72.19	29.53	72.06	29.85	71.93	30.16	78
79	73.25	29.59	73.12	29.91	72.99	30.23	72.85	30.55	79
80	74.17	29.97	74.04	30.29	73.91	30.61	73.78	30.94	80
81	75.10	30.34	74.97	30.67	74.83	31.00	74.70	31.32	81
82	76.03	30.72	75.89	31.05	75.76	31.38	75.62	31.71	82
83	76.96	31.09	76.82	31.43	76.68	31.76	76.54	32.10	83
84	77.88	31.47	77.75	31.81	77.61	32.15	77.46	32.48	84
85	78.81	31.84	78.67	32.19	78.53	32.53	78.39	32.87	85
86	79.74	32.22	79.60	32.56	79.45	32.91	79.31	33.26	86
87	80.66	32.59	80.52	32.94	80.38	33.29	80.23	33.64	87
88	81.59	32.97	81.45	33.32	81.30	33.68	81.15	34.03	88
89	82.52	33.34	82.37	33.70	82.23	34.06	82.08	34.42	89
90	83.45	33.71	83.30	34.08	83.15	34.44	83.00	34.80	90
91	84.37	34.09	84.22	34.46	84.07	34.82	83.92	35.19	91
92	85.30	34.46	85.15	34.84	85.00	35.21	84.84	35.58	92
93	86.23	34.84	86.08	35.21	85.92	35.59	85.76	35.96	93
94	87.16	35.21	87.00	35.59	86.84	35.97	86.69	36.35	94
95	88.08	35.59	87.93	35.97	87.77	36.35	87.61	36.74	95
96	89.01	35.96	88.85	36.35	88.69	36.74	88.53	37.12	96
97	89.94	36.34	89.78	36.73	89.62	37.12	89.45	37.51	97
98	90.86	36.71	90.70	37.11	90.54	37.50	90.38	37.90	98
99	91.79	37.09	91.63	37.49	91.46	37.89	91.30	38.28	99
100	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	68 Deg.		67½ Deg.		67½ Deg.		67½ Deg.		

Distance.	23 Deg.		23½ Deg.		23¾ Deg.		23¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.92	0.39	0.92	0.39	0.92	0.40	0.92	0.40	1
2	1.84	0.78	1.84	0.79	1.83	0.80	1.83	0.81	2
3	2.76	1.17	2.76	1.18	2.75	1.20	2.75	1.21	3
4	3.68	1.56	3.68	1.58	3.67	1.59	3.66	1.61	4
5	4.60	1.95	4.59	1.97	4.59	1.99	4.58	2.01	5
6	5.52	2.34	5.51	2.37	5.50	2.39	5.49	2.42	6
7	6.44	2.74	6.43	2.76	6.42	2.79	6.41	2.82	7
8	7.36	3.13	7.35	3.16	7.34	3.19	7.32	3.22	8
9	8.28	3.52	8.27	3.55	8.25	3.59	8.24	3.62	9
10	9.20	3.91	9.19	3.95	9.17	3.99	9.15	4.03	10
11	10.13	4.30	10.11	4.34	10.09	4.39	10.07	4.43	11
12	11.05	4.69	11.03	4.74	11.00	4.78	10.98	4.83	12
13	11.97	5.08	11.94	5.13	11.92	5.18	11.90	5.24	13
14	12.89	5.47	12.86	5.53	12.84	5.58	12.81	5.64	14
15	13.81	5.86	13.78	5.92	13.76	5.98	13.73	6.04	15
16	14.73	6.25	14.70	6.32	14.67	6.38	14.64	6.44	16
17	15.65	6.64	15.62	6.71	15.59	6.78	15.56	6.85	17
18	16.57	7.03	16.54	7.11	16.51	7.18	16.48	7.25	18
19	17.49	7.42	17.46	7.50	17.42	7.58	17.39	7.65	19
20	18.41	7.81	18.38	7.89	18.34	7.97	18.31	8.05	20
21	19.33	8.21	19.29	8.29	19.26	8.37	19.22	8.46	21
22	20.25	8.60	20.21	8.68	20.18	8.77	20.14	8.86	22
23	21.17	8.99	21.13	9.08	21.09	9.17	21.05	9.26	23
24	22.09	9.28	22.05	9.47	22.01	9.57	21.97	9.67	24
25	23.01	9.77	22.97	9.87	22.93	9.97	22.88	10.07	25
26	23.93	10.16	23.89	10.26	23.84	10.37	23.80	10.47	26
27	24.85	10.55	24.81	10.66	24.76	10.77	24.71	10.87	27
28	25.77	10.94	25.73	11.05	25.68	11.16	25.63	11.28	28
29	26.69	11.33	26.64	11.45	26.59	11.56	26.54	11.68	29
30	27.62	11.72	27.56	11.84	27.51	11.96	27.46	12.08	30
31	28.54	12.11	28.48	12.24	28.43	12.36	28.37	12.49	31
32	29.46	12.50	29.40	12.63	29.35	12.76	29.29	12.89	32
33	30.38	12.89	30.32	13.03	30.26	13.16	30.21	13.29	33
34	31.30	13.28	31.24	13.42	31.18	13.56	31.12	13.69	34
35	32.22	13.68	32.16	13.82	32.10	13.96	32.04	14.10	35
36	33.14	14.07	33.08	14.21	33.01	14.35	32.95	14.50	36
37	34.06	14.46	34.00	14.61	33.93	14.75	33.87	14.90	37
38	34.98	14.85	34.91	15.00	34.85	15.15	34.78	15.30	38
39	35.90	15.24	35.83	15.39	35.77	15.55	35.70	15.71	39
40	36.82	15.63	36.75	15.79	36.68	15.95	36.61	16.11	40
41	37.74	16.02	37.67	16.18	37.60	16.35	37.53	16.51	41
42	38.66	16.41	38.59	16.58	38.52	16.75	38.44	16.92	42
43	39.58	16.80	39.51	16.97	39.43	17.15	39.36	17.32	43
44	40.50	17.19	40.43	17.37	40.35	17.54	40.27	17.72	44
45	41.42	17.58	41.35	17.76	41.27	17.94	41.19	18.12	45
46	42.34	17.97	42.26	18.16	42.18	18.34	42.10	18.53	46
47	43.26	18.36	43.18	18.55	43.10	18.74	43.02	18.93	47
48	44.18	18.76	44.10	18.95	44.02	19.14	43.93	19.33	48
49	45.10	19.15	45.02	19.34	44.94	19.54	44.85	19.73	49
50	46.03	19.54	45.94	19.74	45.85	19.94	45.77	20.14	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	67 Deg		66½ Deg.		66¼ Deg.		66¼ Deg.		

Distance.	23 Deg.		23¼ Deg.		23½ Deg.		23¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.95	19.93	46.86	20.13	46.77	20.34	46.68	20.54	51
52	47.87	20.32	47.78	20.53	47.69	20.73	47.60	20.94	52
53	48.79	20.71	48.70	20.92	48.60	21.13	48.51	21.35	53
54	49.71	21.10	49.61	21.32	49.52	21.53	49.43	21.75	54
55	50.63	21.49	50.53	21.71	50.44	21.93	50.34	22.15	55
56	51.55	21.88	51.45	22.11	51.36	22.33	51.26	22.55	56
57	52.47	22.27	52.37	22.50	52.27	22.73	52.17	22.96	57
58	53.39	22.66	53.29	22.90	53.19	23.13	53.09	23.36	58
59	54.31	23.05	54.21	23.29	54.11	23.53	54.00	23.76	59
60	55.23	23.44	55.13	23.68	55.02	23.92	54.92	24.16	60
61	56.15	23.83	56.05	24.08	55.91	24.32	55.83	24.57	61
62	57.07	24.23	56.97	24.47	56.86	24.72	56.75	24.97	62
63	57.99	24.62	57.88	24.87	57.77	25.12	57.66	25.37	63
64	58.91	25.01	58.80	25.26	58.69	25.52	58.58	25.78	64
65	59.83	25.40	59.72	25.66	59.61	25.92	59.50	26.18	65
66	60.75	25.79	60.64	26.05	60.53	26.32	60.41	26.58	66
67	61.67	26.18	61.56	26.45	61.41	26.72	61.33	26.98	67
68	62.59	26.57	62.48	26.84	62.36	27.11	62.24	27.39	68
69	63.51	26.96	63.40	27.24	63.28	27.51	63.16	27.79	69
70	64.44	27.35	64.32	27.63	64.19	27.91	64.07	28.19	70
71	65.36	27.74	65.23	28.03	65.11	28.31	64.99	28.59	71
72	66.28	28.13	66.15	28.42	66.03	28.71	65.90	29.00	72
73	67.20	28.52	67.07	28.82	66.95	29.11	66.82	29.40	73
74	68.12	28.91	67.99	29.21	67.86	29.51	67.73	29.80	74
75	69.04	29.30	68.91	29.61	68.78	29.91	68.65	30.21	75
76	69.96	29.70	69.83	30.00	69.70	30.30	69.56	30.61	76
77	70.88	30.09	70.75	30.40	70.61	30.70	70.48	31.01	77
78	71.80	30.48	71.67	30.79	71.53	31.10	71.39	31.41	78
79	72.72	30.87	72.58	31.18	72.45	31.50	72.31	31.82	79
80	73.64	31.26	73.50	31.58	73.36	31.90	73.22	32.22	80
81	74.56	31.65	74.42	31.97	74.28	32.30	74.14	32.62	81
82	75.48	32.04	75.34	32.37	75.20	32.70	75.06	33.03	82
83	76.40	32.43	76.26	32.76	76.12	33.10	75.97	33.43	83
84	77.32	32.82	77.18	33.16	77.03	33.49	76.89	33.83	84
85	78.24	33.21	78.10	33.55	77.95	33.89	77.80	34.23	85
86	79.16	33.60	79.02	33.95	78.87	34.29	78.72	34.64	86
87	80.08	33.99	79.93	34.34	79.78	34.69	79.63	35.04	87
88	81.00	34.38	80.85	34.74	80.70	35.09	80.55	35.44	88
89	81.92	34.78	81.77	35.13	81.62	35.49	81.46	35.84	89
90	82.85	35.17	82.69	35.53	82.54	35.89	82.38	36.25	90
91	83.77	35.56	83.61	35.92	83.45	36.29	83.29	36.65	91
92	84.69	35.95	84.53	36.32	84.37	36.68	84.21	37.05	92
93	85.61	36.34	85.45	36.71	85.29	37.08	85.12	37.46	93
94	86.53	36.73	86.37	37.11	86.20	37.48	86.04	37.86	94
95	87.45	37.12	87.29	37.50	87.12	37.88	86.95	38.26	95
96	88.37	37.51	88.20	37.90	88.04	38.28	87.87	38.66	96
97	89.29	37.90	89.12	38.29	88.95	38.68	88.79	39.07	97
98	90.21	38.29	90.04	38.68	89.87	39.08	89.70	39.47	98
99	91.13	38.68	90.96	39.08	90.79	39.48	90.62	39.87	99
100	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	67 Deg.		66¾ Deg.		66½ Deg.		66¼ Deg.		

Distance.	24 Deg.		24½ Deg.		24½ Deg.		24½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.91	0.41	0.91	0.41	0.91	0.41	0.91	0.42	1
2	1.83	0.81	1.82	0.82	1.82	0.83	1.82	0.84	2
3	2.74	1.22	2.74	1.23	2.73	1.24	2.72	1.26	3
4	3.65	1.63	3.65	1.64	3.64	1.66	3.63	1.67	4
5	4.57	2.03	4.56	2.05	4.55	2.07	4.54	2.09	5
6	5.48	2.44	5.47	2.46	5.46	2.49	5.45	2.51	6
7	6.39	2.85	6.38	2.87	6.37	2.90	6.36	2.93	7
8	7.31	3.25	7.29	3.29	7.28	3.32	7.27	3.35	8
9	8.22	3.66	8.21	3.70	8.19	3.73	8.17	3.77	9
10	9.14	4.07	9.12	4.11	9.10	4.15	9.08	4.19	10
11	10.05	4.47	10.03	4.52	10.01	4.56	9.99	4.61	11
12	10.96	4.88	10.94	4.93	10.92	4.98	10.90	5.02	12
13	11.88	5.29	11.85	5.34	11.83	5.39	11.81	5.44	13
14	12.79	5.69	12.76	5.75	12.74	5.81	12.71	5.86	14
15	13.70	6.10	13.68	6.16	13.65	6.22	13.62	6.28	15
16	14.62	6.51	14.59	6.57	14.56	6.64	14.53	6.70	16
17	15.53	6.92	15.50	6.98	15.47	7.05	15.44	7.12	17
18	16.44	7.32	16.41	7.39	16.38	7.46	16.35	7.54	18
19	17.36	7.73	17.32	7.80	17.29	7.88	17.25	7.95	19
20	18.27	8.13	18.24	8.21	18.20	8.29	18.16	8.37	20
21	19.18	8.54	19.15	8.63	19.11	8.71	19.07	8.79	21
22	20.10	8.95	20.06	9.04	20.02	9.12	19.98	9.21	22
23	21.01	9.35	20.97	9.45	20.93	9.54	20.89	9.63	23
24	21.93	9.76	21.88	9.86	21.84	9.95	21.80	10.05	24
25	22.84	10.17	22.79	10.27	22.75	10.37	22.70	10.47	25
26	23.75	10.58	23.71	10.68	23.66	10.78	23.61	10.89	26
27	24.67	10.98	24.62	11.09	24.57	11.20	24.52	11.30	27
28	25.58	11.39	25.53	11.50	25.48	11.61	25.43	11.72	28
29	26.49	11.80	26.44	11.91	26.39	12.03	26.34	12.14	29
30	27.41	12.20	27.35	12.32	27.30	12.44	27.24	12.56	30
31	28.32	12.61	28.26	12.73	28.21	12.86	28.15	12.98	31
32	29.23	13.02	29.18	13.14	29.12	13.27	29.06	13.40	32
33	30.15	13.42	30.09	13.55	30.03	13.68	29.97	13.82	33
34	31.06	13.83	31.00	13.96	30.94	14.10	30.88	14.23	34
35	31.97	14.24	31.91	14.38	31.85	14.51	31.78	14.65	35
36	32.89	14.64	32.82	14.79	32.76	14.93	32.69	15.07	36
37	33.80	15.05	33.74	15.20	33.67	15.34	33.60	15.49	37
38	34.71	15.46	34.65	15.61	34.58	15.76	34.51	15.91	38
39	35.63	15.86	35.56	16.02	35.49	16.17	35.42	16.33	39
40	36.54	16.27	36.47	16.43	36.40	16.59	36.33	16.75	40
41	37.46	16.68	37.38	16.84	37.31	17.00	37.23	17.16	41
42	38.37	17.08	38.29	17.25	38.22	17.42	38.14	17.58	42
43	39.28	17.49	39.21	17.66	39.13	17.83	39.05	18.00	43
44	40.20	17.90	40.12	18.07	40.04	18.25	39.96	18.42	44
45	41.11	18.30	41.03	18.48	40.95	18.66	40.87	18.84	45
46	42.02	18.71	41.94	18.89	41.86	19.08	41.77	19.26	46
47	42.94	19.12	42.85	19.30	42.77	19.49	42.68	19.68	47
48	43.85	19.52	43.76	19.71	43.68	19.91	43.59	20.10	48
49	44.76	19.93	44.68	20.13	44.59	20.32	44.50	20.51	49
50	45.68	20.34	45.59	20.54	45.50	20.73	45.41	20.93	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	66 Deg.		65½ Deg.		65½ Deg.		65½ Deg.		

TRAVERSE TABLE.

Distance.	24 Deg.		24½ Deg.		24¾ Deg.		24¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.59	20.74	46.50	20.95	46.41	21.15	46.32	21.35	51
52	47.50	21.15	47.41	21.36	47.32	21.56	47.22	21.77	52
53	48.42	21.56	48.32	21.77	48.23	21.98	48.13	22.19	53
54	49.33	21.98	49.24	22.18	49.14	22.39	49.04	22.61	54
55	50.24	22.37	50.15	22.59	50.05	22.81	49.95	23.03	55
56	51.16	22.78	51.06	23.00	50.96	23.22	50.86	23.44	56
57	52.07	23.18	51.97	23.41	51.87	23.64	51.76	23.86	57
58	52.99	23.59	52.88	23.82	52.78	24.05	52.67	24.28	58
59	53.90	24.00	53.79	24.23	53.69	24.47	53.58	24.70	59
60	54.81	24.40	54.71	24.64	54.60	24.88	54.49	25.12	60
61	55.73	24.81	55.62	25.05	55.51	25.30	55.40	25.54	61
62	56.64	25.22	56.53	25.46	56.42	25.71	56.30	25.96	62
63	57.55	25.62	57.44	25.88	57.33	26.13	57.21	26.38	63
64	58.47	26.03	58.35	26.29	58.24	26.54	58.12	26.79	64
65	59.38	26.44	59.26	26.70	59.15	26.96	59.03	27.21	65
66	60.29	26.84	60.18	27.11	60.06	27.37	59.94	27.63	66
67	61.21	27.25	61.09	27.52	60.97	27.78	60.85	28.05	67
68	62.12	27.66	62.00	27.93	61.88	28.20	61.75	28.47	68
69	63.03	28.06	62.91	28.34	62.79	28.61	62.66	28.89	69
70	63.95	28.47	63.82	28.75	63.70	29.03	63.57	29.31	70
71	64.86	28.88	64.74	29.16	64.61	29.44	64.48	29.72	71
72	65.78	29.28	65.65	29.57	65.52	29.86	65.39	30.14	72
73	66.69	29.69	66.56	29.98	66.43	30.27	66.29	30.56	73
74	67.60	30.10	67.47	30.39	67.34	30.69	67.20	30.98	74
75	68.52	30.51	68.38	30.80	68.25	31.10	68.11	31.40	75
76	69.43	30.91	69.29	31.21	69.16	31.52	69.02	31.82	76
77	70.34	31.32	70.21	31.63	70.07	31.93	69.93	32.24	77
78	71.26	31.73	71.12	32.04	70.98	32.35	70.84	32.66	78
79	72.17	32.13	72.03	32.45	71.89	32.76	71.74	33.07	79
80	73.08	32.54	72.94	32.86	72.80	33.18	72.65	33.49	80
81	74.00	32.95	73.85	33.27	73.71	33.59	73.56	33.91	81
82	74.91	33.35	74.76	33.68	74.62	34.00	74.47	34.33	82
83	75.82	33.76	75.68	34.09	75.53	34.42	75.38	34.75	83
84	76.74	34.17	76.59	34.50	76.44	34.83	76.28	35.17	84
85	77.65	34.57	77.50	34.91	77.35	35.25	77.19	35.59	85
86	78.56	34.98	78.41	35.32	78.26	35.66	78.10	36.00	86
87	79.48	35.39	79.32	35.73	79.17	36.08	79.01	36.42	87
88	80.39	35.79	80.24	36.14	80.08	36.49	79.92	36.84	88
89	81.31	36.20	81.15	36.55	80.99	36.91	80.82	37.26	89
90	82.22	36.61	82.06	36.96	81.90	37.32	81.73	37.68	90
91	83.13	37.01	82.97	37.38	82.81	37.74	82.64	38.10	91
92	84.05	37.42	83.88	37.79	83.72	38.15	83.55	38.52	92
93	84.96	37.83	84.79	38.20	84.63	38.57	84.46	38.94	93
94	85.87	38.23	85.71	38.61	85.54	38.98	85.37	39.35	94
95	86.79	38.64	86.62	39.02	86.45	39.40	86.27	39.77	95
96	87.70	39.05	87.53	39.43	87.36	39.81	87.18	40.19	96
97	88.61	39.45	88.44	39.84	88.27	40.23	88.09	40.61	97
98	89.53	39.86	89.35	40.25	89.18	40.64	89.00	41.03	98
99	90.44	40.27	90.26	40.66	90.09	41.05	89.91	41.45	99
100	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	66 Deg.		65½ Deg.		65¾ Deg.		65¾ Deg.		

TRAVERSE TABLE.

Distance.	25 Deg.		25½ Deg.		25¾ Deg.		25¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.91	0.42	0.90	0.43	0.90	0.43	0.90	0.43	1
2	1.81	0.85	1.81	0.85	1.81	0.86	1.80	0.87	2
3	2.72	1.27	2.71	1.28	2.71	1.29	2.70	1.30	3
4	3.63	1.69	3.62	1.71	3.61	1.72	3.60	1.74	4
5	4.53	2.11	4.52	2.13	4.51	2.15	4.50	2.17	5
6	5.44	2.54	5.43	2.56	5.42	2.58	5.40	2.61	6
7	6.34	2.96	6.33	2.99	6.32	3.01	6.30	3.04	7
8	7.25	3.38	7.24	3.41	7.22	3.44	7.21	3.48	8
9	8.16	3.80	8.14	3.84	8.12	3.87	8.11	3.91	9
10	9.06	4.23	9.04	4.27	9.03	4.31	9.01	4.34	10
11	9.97	4.65	9.95	4.69	9.93	4.74	9.91	4.78	11
12	10.88	5.07	10.85	5.12	10.83	5.17	10.81	5.21	12
13	11.78	5.49	11.76	5.55	11.73	5.60	11.71	5.65	13
14	12.69	5.92	12.66	5.97	12.64	6.03	12.61	6.08	14
15	13.59	6.34	13.57	6.40	13.54	6.46	13.51	6.52	15
16	14.50	6.76	14.47	6.83	14.44	6.89	14.41	6.95	16
17	15.41	7.18	15.38	7.25	15.34	7.32	15.31	7.39	17
18	16.31	7.61	16.28	7.68	16.25	7.75	16.21	7.82	18
19	17.22	8.03	17.18	8.10	17.15	8.18	17.11	8.25	19
20	18.13	8.45	18.09	8.53	18.05	8.61	18.01	8.69	20
21	19.03	8.87	18.99	8.96	18.95	9.04	18.91	9.12	21
22	19.94	9.30	19.90	9.38	19.86	9.47	19.82	9.56	22
23	20.85	9.72	20.80	9.81	20.76	9.90	20.72	9.99	23
24	21.75	10.14	21.71	10.24	21.66	10.33	21.62	10.43	24
25	22.66	10.57	22.61	10.66	22.56	10.76	22.52	10.86	25
26	23.56	10.99	23.52	11.09	23.47	11.19	23.42	11.30	26
27	24.47	11.41	24.42	11.52	24.37	11.62	24.32	11.73	27
28	25.38	11.83	25.32	11.94	25.27	12.05	25.22	12.16	28
29	26.28	12.26	26.23	12.37	26.17	12.48	26.12	12.60	29
30	27.19	12.68	27.13	12.80	27.08	12.92	27.02	13.03	30
31	28.10	13.10	28.04	13.22	27.98	13.35	27.92	13.47	31
32	29.00	13.52	28.94	13.65	28.88	13.78	28.82	13.90	32
33	29.91	13.95	29.85	14.08	29.79	14.21	29.72	14.34	33
34	30.81	14.37	30.75	14.50	30.69	14.64	30.62	14.77	34
35	31.72	14.79	31.66	14.93	31.59	15.07	31.52	15.21	35
36	32.63	15.21	32.56	15.36	32.49	15.50	32.43	15.64	36
37	33.53	15.64	33.46	15.78	33.40	15.93	33.33	16.07	37
38	34.44	16.06	34.37	16.21	34.30	16.36	34.23	16.51	38
39	35.35	16.48	35.27	16.64	35.20	16.79	35.13	16.94	39
40	36.25	16.90	36.18	17.06	36.10	17.22	36.03	17.38	40
41	37.16	17.33	37.08	17.49	37.01	17.65	36.93	17.81	41
42	38.06	17.75	37.99	17.92	37.91	18.08	37.83	18.25	42
43	38.97	18.17	38.89	18.34	38.81	18.51	38.73	18.68	43
44	39.88	18.60	39.80	18.77	39.71	18.94	39.63	19.12	44
45	40.78	19.02	40.70	19.20	40.62	19.37	40.53	19.55	45
46	41.69	19.44	41.60	19.62	41.52	19.80	41.43	19.98	46
47	42.60	19.86	42.51	20.05	42.42	20.23	42.33	20.42	47
48	43.50	20.29	43.41	20.48	43.32	20.66	43.23	20.85	48
49	44.41	20.71	44.32	20.90	44.23	21.10	44.13	21.29	49
50	45.32	21.13	45.22	21.33	45.13	21.53	45.03	21.72	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	65 Deg.		64½ Deg.		64¼ Deg.		64¼ Deg.		

TRAVERSE TABLE.

53

Distance.	25 Deg.		25½ Deg.		25¾ Deg.		25¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	46.22	21.55	46.13	21.75	46.03	21.96	45.94	22.16	51
52	47.13	21.98	47.03	22.18	46.93	22.39	46.84	22.59	52
53	48.03	22.40	47.94	22.61	47.84	22.82	47.74	23.03	53
54	48.94	22.82	48.84	23.03	48.74	23.25	48.64	23.46	54
55	49.85	23.24	49.74	23.46	49.64	23.68	49.54	23.89	55
56	50.75	23.67	50.65	23.89	50.54	24.11	50.44	24.33	56
57	51.66	24.09	51.55	24.31	51.45	24.54	51.34	24.76	57
58	52.57	24.51	52.46	24.74	52.35	24.97	52.24	25.20	58
59	53.47	24.93	53.36	25.17	53.25	25.40	53.14	25.63	59
60	54.38	25.36	54.27	25.59	54.16	25.83	54.04	26.07	60
61	55.28	25.78	55.17	26.02	55.06	26.26	54.94	26.50	61
62	56.19	26.20	56.08	26.45	55.96	26.69	55.84	26.94	62
63	57.10	26.62	56.98	26.87	56.86	27.12	56.74	27.37	63
64	58.00	27.05	57.89	27.30	57.77	27.55	57.64	27.80	64
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.24	65
66	59.82	27.89	59.69	28.15	59.57	28.41	59.45	28.67	66
67	60.72	28.32	60.60	28.58	60.47	28.84	60.35	29.11	67
68	61.63	28.74	61.50	29.01	61.38	29.27	61.25	29.54	68
69	62.54	29.16	62.41	29.43	62.28	29.71	62.15	29.98	69
70	63.44	29.58	63.31	29.86	63.18	30.14	63.05	30.41	70
71	64.35	30.01	64.22	30.29	64.08	30.57	63.95	30.85	71
72	65.25	30.43	65.12	30.71	64.99	31.00	64.85	31.28	72
73	66.16	30.85	66.03	31.14	65.89	31.43	65.75	31.71	73
74	67.07	31.27	66.93	31.57	66.79	31.86	66.65	32.15	74
75	67.97	31.70	67.83	31.99	67.69	32.29	67.55	32.58	75
76	68.88	32.12	68.74	32.42	68.60	32.72	68.45	33.02	76
77	69.79	32.54	69.64	32.85	69.50	33.15	69.35	33.45	77
78	70.69	32.96	70.55	33.27	70.40	33.58	70.25	33.89	78
79	71.60	33.39	71.45	33.70	71.30	34.01	71.16	34.32	79
80	72.50	33.81	72.36	34.13	72.21	34.44	72.06	34.76	80
81	73.41	34.23	73.26	34.55	73.11	34.87	72.96	35.19	81
82	74.32	34.65	74.17	34.98	74.01	35.30	73.86	35.62	82
83	75.22	35.08	75.07	35.41	74.91	35.73	74.76	36.06	83
84	76.13	35.50	75.97	35.83	75.82	36.16	75.66	36.49	84
85	77.04	35.92	76.88	36.26	76.72	36.59	76.56	36.93	85
86	77.94	36.35	77.78	36.68	77.62	37.02	77.46	37.36	86
87	78.85	36.77	78.69	37.11	78.52	37.45	78.36	37.80	87
88	79.76	37.19	79.59	37.54	79.43	37.88	79.26	38.23	88
89	80.66	37.61	80.50	37.96	80.33	38.32	80.16	38.67	89
90	81.57	38.04	81.40	38.39	81.23	38.75	81.06	39.10	90
91	82.47	38.46	82.31	38.82	82.14	39.18	81.96	39.53	91
92	83.38	38.88	83.21	39.24	83.04	39.61	82.86	39.97	92
93	84.29	39.30	84.11	39.67	83.94	40.04	83.76	40.40	93
94	85.19	39.73	85.02	40.10	84.84	40.47	84.67	40.84	94
95	86.10	40.15	85.92	40.52	85.75	40.90	85.57	41.27	95
96	87.01	40.57	86.83	40.95	86.65	41.33	86.47	41.71	96
97	87.91	40.99	87.73	41.38	87.55	41.76	87.37	42.14	97
98	88.82	41.42	88.64	41.80	88.45	42.19	88.27	42.58	98
99	89.72	41.84	89.54	42.23	89.36	42.62	89.17	43.01	99
100	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	65 Deg.		64½ Deg.		64½ Deg.		64½ Deg.		



TRAVERSE TABLE.

Distance.	26 Deg.		26½ Deg.		26¾ Deg.		26¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.90	0.44	0.90	0.44	0.89	0.45	0.89	0.45	1
2	1.80	0.88	1.79	0.88	1.79	0.89	1.79	0.90	2
3	2.70	1.32	2.69	1.33	2.68	1.34	2.68	1.35	3
4	3.60	1.75	3.59	1.77	3.58	1.78	3.57	1.80	4
5	4.49	2.19	4.48	2.21	4.47	2.23	4.46	2.25	5
6	5.39	2.63	5.38	2.65	5.37	2.68	5.36	2.70	6
7	6.29	3.07	6.28	3.10	6.26	3.12	6.25	3.15	7
8	7.19	3.51	7.17	3.54	7.16	3.57	7.14	3.60	8
9	8.09	3.95	8.07	3.98	8.05	4.02	8.04	4.05	9
10	8.99	4.38	8.97	4.42	8.95	4.46	8.93	4.50	10
11	9.89	4.82	9.87	4.87	9.84	4.91	9.82	4.95	11
12	10.79	5.26	10.76	5.31	10.74	5.35	10.72	5.40	12
13	11.68	5.70	11.66	5.75	11.63	5.80	11.61	5.85	13
14	12.58	6.14	12.56	6.19	12.53	6.25	12.50	6.30	14
15	13.48	6.58	13.45	6.63	13.42	6.69	13.39	6.75	15
16	14.38	7.01	14.35	7.08	14.32	7.14	14.29	7.20	16
17	15.28	7.45	15.25	7.52	15.21	7.59	15.18	7.65	17
18	16.18	7.89	16.14	7.96	16.11	8.03	16.07	8.10	18
19	17.08	8.33	17.04	8.40	17.00	8.48	16.97	8.55	19
20	17.98	8.77	17.94	8.85	17.90	8.92	17.86	9.00	20
21	18.87	9.21	18.83	9.29	18.79	9.37	18.75	9.45	21
22	19.77	9.64	19.73	9.73	19.69	9.82	19.65	9.90	22
23	20.67	10.08	20.63	10.17	20.58	10.26	20.54	10.35	23
24	21.57	10.52	21.52	10.61	21.48	10.71	21.43	10.80	24
25	22.47	10.96	22.42	11.06	22.37	11.15	22.32	11.25	25
26	23.37	11.40	23.32	11.50	23.27	11.60	23.22	11.70	26
27	24.27	11.84	24.22	11.94	24.16	12.05	24.11	12.15	27
28	25.17	12.27	25.11	12.38	25.06	12.49	25.00	12.60	28
29	26.06	12.71	26.01	12.83	25.95	12.94	25.90	13.05	29
30	26.96	13.15	26.91	13.27	26.85	13.39	26.79	13.50	30
31	27.86	13.59	27.80	13.71	27.74	13.83	27.68	13.95	31
32	28.76	14.03	28.70	14.15	28.64	14.28	28.58	14.40	32
33	29.66	14.47	29.60	14.60	29.53	14.72	29.47	14.85	33
34	30.56	14.90	30.49	15.04	30.43	15.17	30.36	15.30	34
35	31.46	15.34	31.39	15.48	31.32	15.62	31.25	15.75	35
36	32.36	15.78	32.29	15.92	32.22	16.06	32.15	16.20	36
37	33.26	16.22	33.18	16.36	33.11	16.51	33.04	16.65	37
38	34.15	16.66	34.08	16.81	34.01	16.96	33.93	17.10	38
39	35.05	17.10	34.98	17.25	34.90	17.40	34.83	17.55	39
40	35.95	17.53	35.87	17.69	35.80	17.85	35.72	18.00	40
41	36.85	17.97	36.77	18.13	36.69	18.29	36.61	18.45	41
42	37.75	18.41	37.67	18.58	37.59	18.74	37.51	18.90	42
43	38.65	18.85	38.57	19.02	38.48	19.19	38.40	19.35	43
44	39.55	19.29	39.46	19.46	39.38	19.63	39.29	19.80	44
45	40.45	19.73	40.36	19.90	40.27	20.08	40.18	20.25	45
46	41.34	20.17	41.26	20.35	41.17	20.53	41.08	20.70	46
47	42.24	20.60	42.15	20.79	42.06	20.97	41.97	21.15	47
48	43.14	21.04	43.05	21.23	42.96	21.42	42.86	21.60	48
49	44.04	21.48	43.95	21.67	43.85	21.86	43.76	22.05	49
50	44.94	21.92	44.84	22.11	44.75	22.31	44.65	22.50	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	64 Deg.		63½ Deg.		63¼ Deg.		63¼ Deg.		

TRAVERSE TABLE.

Distance.	26 Deg.		26¼ Deg.		26½ Deg.		26¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.84	22.36	45.74	22.56	45.64	22.76	45.54	22.96	51
52	46.74	22.80	46.64	23.00	46.54	23.20	46.43	23.41	52
53	47.64	23.23	47.53	23.44	47.43	23.65	47.33	23.86	53
54	48.53	23.67	48.43	23.88	48.33	24.09	48.22	24.31	54
55	49.43	24.11	49.33	24.33	49.22	24.54	49.11	24.76	55
56	50.33	24.55	50.22	24.77	50.12	24.99	50.01	25.21	56
57	51.23	24.99	51.12	25.21	51.01	25.43	50.90	25.66	57
58	52.13	25.43	52.02	25.65	51.91	25.88	51.79	26.11	58
59	53.03	25.86	52.92	26.09	52.80	26.33	52.69	26.56	59
60	53.93	26.30	53.81	26.54	53.70	26.77	53.58	27.01	60
61	54.83	26.74	54.71	26.98	54.59	27.22	54.47	27.46	61
62	55.73	27.18	55.61	27.42	55.49	27.66	55.36	27.91	62
63	56.62	27.62	56.50	27.86	56.38	28.11	56.26	28.36	63
64	57.52	28.06	57.40	28.31	57.28	28.56	57.15	28.81	64
65	58.42	28.49	58.30	28.75	58.17	29.00	58.04	29.26	65
66	59.32	28.93	59.19	29.19	59.07	29.45	58.94	29.71	66
67	60.22	29.37	60.09	29.63	59.96	29.90	59.83	30.16	67
68	61.12	29.81	60.99	30.08	60.86	30.34	60.72	30.61	68
69	62.02	30.25	61.88	30.52	61.75	30.79	61.62	31.06	69
70	62.92	30.69	62.78	30.96	62.65	31.23	62.51	31.51	70
71	63.81	31.12	63.68	31.40	63.54	31.68	63.40	31.96	71
72	64.71	31.56	64.57	31.84	64.44	32.13	64.29	32.41	72
73	65.61	32.00	65.47	32.29	65.33	32.57	65.19	32.86	73
74	66.51	32.44	66.37	32.73	66.23	33.02	66.08	33.31	74
75	67.41	32.88	67.27	33.17	67.12	33.46	66.97	33.76	75
76	68.31	33.32	68.16	33.61	68.01	33.91	67.87	34.21	76
77	69.21	33.75	69.06	34.06	68.91	34.36	68.76	34.66	77
78	70.11	34.19	69.96	34.50	69.80	34.80	69.65	35.11	78
79	71.00	34.63	70.85	34.94	70.70	35.25	70.55	35.56	79
80	71.90	35.07	71.75	35.38	71.59	35.70	71.44	36.01	80
81	72.80	35.51	72.65	35.83	72.49	36.14	72.33	36.46	81
82	73.70	35.95	73.54	36.27	73.38	36.59	73.22	36.91	82
83	74.60	36.38	74.44	36.71	74.28	37.03	74.12	37.36	83
84	75.50	36.82	75.34	37.15	75.17	37.48	75.01	37.81	84
85	76.40	37.26	76.23	37.59	76.07	37.93	75.90	38.26	85
86	77.30	37.70	77.13	38.04	76.96	38.37	76.80	38.71	86
87	78.20	38.14	78.03	38.48	77.86	38.82	77.69	39.16	87
88	79.09	38.58	78.92	38.92	78.75	39.27	78.58	39.61	88
89	79.99	39.01	79.82	39.36	79.65	39.71	79.48	40.06	89
90	80.89	39.45	80.72	39.81	80.54	40.16	80.37	40.51	90
91	81.79	39.89	81.62	40.25	81.44	40.60	81.26	40.96	91
92	82.69	40.33	82.51	40.69	82.33	41.05	82.15	41.41	92
93	83.59	40.77	83.41	41.13	83.23	41.50	83.05	41.86	93
94	84.49	41.21	84.31	41.58	84.12	41.94	83.94	42.31	94
95	85.39	41.65	85.20	42.02	85.02	42.39	84.83	42.76	95
96	86.28	42.08	86.10	42.46	85.91	42.83	85.73	43.21	96
97	87.18	42.52	87.00	42.90	86.81	43.28	86.62	43.66	97
98	88.08	42.96	87.89	43.34	87.70	43.73	87.51	44.11	98
99	88.98	43.40	88.79	43.79	88.60	44.17	88.40	44.56	99
100	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	100
Distance.	64 Deg.		63¾ Deg.		63½ Deg.		63¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

TRAVERSE TABLE

Distance.	27 Deg.		27½ Deg.		27½ Deg.		27½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.89	0.45	0.89	0.46	0.89	0.46	0.88	0.47	1
2	1.78	0.91	1.78	0.92	1.77	0.92	1.77	0.93	2
3	2.67	1.36	2.67	1.37	2.66	1.39	2.65	1.40	3
4	3.56	1.82	3.56	1.83	3.55	1.85	3.54	1.86	4
5	4.45	2.27	4.45	2.29	4.44	2.31	4.42	2.33	5
6	5.35	2.72	5.33	2.75	5.32	2.77	5.31	2.79	6
7	6.24	3.18	6.22	3.21	6.21	3.23	6.19	3.26	7
8	7.13	3.63	7.11	3.66	7.10	3.69	7.08	3.72	8
9	8.02	4.09	8.00	4.12	7.98	4.16	7.96	4.19	9
10	8.91	4.54	8.89	4.58	8.87	4.62	8.85	4.66	10
11	9.80	4.99	9.78	5.04	9.76	5.08	9.73	5.12	11
12	10.69	5.45	10.67	5.49	10.64	5.54	10.62	5.59	12
13	11.58	5.90	11.56	5.95	11.53	6.00	11.50	6.05	13
14	12.47	6.36	12.45	6.41	12.42	6.46	12.39	6.52	14
15	13.37	6.81	13.34	6.87	13.31	6.93	13.27	6.98	15
16	14.26	7.26	14.22	7.33	14.19	7.39	14.16	7.45	16
17	15.15	7.72	15.11	7.78	15.08	7.85	15.04	7.92	17
18	16.04	8.17	16.00	8.24	15.97	8.31	15.93	8.38	18
19	16.93	8.63	16.89	8.70	16.85	8.77	16.81	8.85	19
20	17.82	9.08	17.78	9.16	17.74	9.23	17.70	9.31	20
21	18.71	9.53	18.67	9.62	18.63	9.70	18.58	9.78	21
22	19.60	9.99	19.56	10.07	19.51	10.16	19.47	10.24	22
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10.71	23
24	21.38	10.90	21.34	10.99	21.29	11.08	21.24	11.17	24
25	22.28	11.35	22.23	11.45	22.18	11.54	22.12	11.64	25
26	23.17	11.80	23.11	11.90	23.06	12.01	23.01	12.11	26
27	24.06	12.26	24.00	12.36	23.95	12.47	23.89	12.57	27
28	24.95	12.71	24.89	12.82	24.84	12.93	24.78	13.04	28
29	25.84	13.17	25.78	13.28	25.72	13.39	25.66	13.50	29
30	26.73	13.62	26.67	13.74	26.61	13.85	26.55	13.97	30
31	27.62	14.07	27.56	14.19	27.50	14.31	27.43	14.43	31
32	28.51	14.53	28.45	14.65	28.38	14.78	28.32	14.90	32
33	29.40	14.98	29.34	15.11	29.27	15.24	29.20	15.37	33
34	30.29	15.44	30.23	15.57	30.16	15.70	30.09	15.83	34
35	31.19	15.89	31.12	16.03	31.05	16.16	30.97	16.30	35
36	32.08	16.34	32.00	16.48	31.93	16.62	31.86	16.76	36
37	32.97	16.80	32.89	16.94	32.82	17.08	32.74	17.23	37
38	33.86	17.25	33.78	17.40	33.71	17.55	33.63	17.69	38
39	34.75	17.71	34.67	17.86	34.59	18.01	34.51	18.16	39
40	35.64	18.16	35.56	18.31	35.48	18.47	35.40	18.62	40
41	36.53	18.61	36.45	18.77	36.37	18.93	36.28	19.09	41
42	37.42	19.07	37.34	19.23	37.25	19.39	37.17	19.56	42
43	38.31	19.52	38.23	19.69	38.14	19.86	38.05	20.02	43
44	39.20	19.98	39.12	20.15	39.03	20.32	38.94	20.49	44
45	40.10	20.43	40.01	20.60	39.92	20.78	39.82	20.95	45
46	40.99	20.88	40.89	21.06	40.80	21.24	40.71	21.42	46
47	41.88	21.34	41.78	21.52	41.69	21.70	41.59	21.88	47
48	42.77	21.79	42.67	21.98	42.58	22.16	42.48	22.35	48
49	43.66	22.25	43.56	22.44	43.46	22.63	43.36	22.82	49
50	44.55	22.70	44.45	22.89	44.35	23.09	44.25	23.28	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	63 Deg.		62½ Deg.		62½ Deg.		62½ Deg.		

TRAVERSE TABLE.

Distance.	27 Deg.		27½ Deg.		27½ Deg.		27½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.44	23.15	45.34	23.35	45.24	23.55	45.13	23.75	51
52	46.33	23.61	46.23	23.81	46.12	24.01	46.02	24.21	52
53	47.22	24.06	47.12	24.27	47.01	24.47	46.90	24.68	53
54	48.11	24.52	48.01	24.73	47.90	24.93	47.79	25.14	54
55	49.01	24.97	48.90	25.18	48.79	25.40	48.67	25.61	55
56	49.90	25.42	49.78	25.64	49.67	25.86	49.56	26.07	56
57	50.79	25.88	50.67	26.10	50.56	26.32	50.44	26.54	57
58	51.68	26.33	51.56	26.56	51.45	26.78	51.33	27.01	58
59	52.57	26.79	52.45	27.01	52.33	27.24	52.21	27.47	59
60	53.46	27.24	53.34	27.47	53.22	27.70	53.10	27.94	60
61	54.35	27.69	54.23	27.93	54.11	28.17	53.98	28.40	61
62	55.24	28.15	55.12	28.39	54.99	28.63	54.87	28.87	62
63	56.13	28.60	56.01	28.85	55.88	29.09	55.75	29.33	63
64	57.02	29.06	56.90	29.30	56.77	29.55	56.64	29.80	64
65	57.92	29.51	57.79	29.76	57.66	30.01	57.52	30.26	65
66	58.81	29.96	58.68	30.22	58.54	30.48	58.41	30.73	66
67	59.70	30.42	59.56	30.68	59.43	30.94	59.29	31.20	67
68	60.59	30.87	60.45	31.14	60.32	31.40	60.18	31.66	68
69	61.48	31.33	61.34	31.59	61.20	31.86	61.06	32.13	69
70	62.37	31.78	62.23	32.05	62.09	32.32	61.95	32.59	70
71	63.26	32.23	63.12	32.51	62.98	32.78	62.83	33.06	71
72	64.15	32.69	64.01	32.97	63.86	33.25	63.72	33.52	72
73	65.04	33.14	64.90	33.42	64.75	33.71	64.60	33.99	73
74	65.93	33.60	65.79	33.88	65.64	34.17	65.49	34.46	74
75	66.83	34.05	66.68	34.34	66.53	34.63	66.37	34.92	75
76	67.72	34.50	67.57	34.80	67.41	35.09	67.26	35.39	76
77	68.61	34.96	68.45	35.26	68.30	35.55	68.14	35.85	77
78	69.50	35.41	69.34	35.71	69.19	36.02	69.03	36.32	78
79	70.39	35.87	70.23	36.17	70.07	36.48	69.91	36.78	79
80	71.28	36.32	71.12	36.63	70.96	36.94	70.80	37.25	80
81	72.17	36.77	72.01	37.09	71.85	37.40	71.68	37.71	81
82	73.06	37.23	72.90	37.55	72.73	37.86	72.57	38.18	82
83	73.95	37.68	73.79	38.00	73.62	38.33	73.45	38.65	83
84	74.84	38.14	74.68	38.46	74.51	38.79	74.34	39.11	84
85	75.74	38.59	75.57	38.92	75.40	39.25	75.22	39.58	85
86	76.63	39.04	76.46	39.38	76.28	39.71	76.11	40.04	86
87	77.52	39.50	77.34	39.83	77.17	40.17	76.99	40.51	87
88	78.41	39.95	78.23	40.29	78.06	40.63	77.88	40.97	88
89	79.30	40.41	79.12	40.75	78.94	41.10	78.76	41.44	89
90	80.19	40.86	80.01	41.21	79.83	41.56	79.65	41.91	90
91	81.08	41.31	80.90	41.67	80.72	42.02	80.53	42.37	91
92	81.97	41.77	81.79	42.12	81.60	42.48	81.42	42.84	92
93	82.86	42.22	82.68	42.58	82.49	42.94	82.30	43.30	93
94	83.75	42.68	83.57	43.04	83.38	43.40	83.19	43.77	94
95	84.65	43.13	84.46	43.50	84.27	43.87	84.07	44.23	95
96	85.54	43.58	85.35	43.96	85.15	44.33	84.96	44.70	96
97	86.43	44.04	86.23	44.41	86.04	44.79	85.84	45.16	97
98	87.32	44.49	87.12	44.87	86.93	45.25	86.73	45.63	98
99	88.21	44.95	88.01	45.33	87.81	45.71	87.61	46.10	99
100	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	100
Distance.	63 Deg.		62½ Deg.		62½ Deg.		62½ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	28 Deg.		28½ Deg.		29 Deg.		29½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.88	0.47	0.88	0.47	0.88	0.48	0.88	0.48	1
2	1.77	0.94	1.76	0.95	1.76	0.95	1.75	0.96	2
3	2.65	1.41	2.64	1.42	2.64	1.43	2.63	1.44	3
4	3.53	1.88	3.52	1.89	3.52	1.91	3.51	1.92	4
5	4.41	2.35	4.40	2.37	4.39	2.39	4.38	2.40	5
6	5.30	2.82	5.29	2.84	5.27	2.86	5.26	2.89	6
7	6.18	3.29	6.17	3.31	6.15	3.34	6.14	3.37	7
8	7.06	3.76	7.05	3.79	7.03	3.82	7.01	3.85	8
9	7.95	4.23	7.93	4.26	7.91	4.29	7.89	4.33	9
10	8.83	4.69	8.81	4.73	8.79	4.77	8.77	4.81	10
11	9.71	5.16	9.69	5.21	9.67	5.25	9.64	5.29	11
12	10.60	5.63	10.57	5.68	10.55	5.73	10.52	5.77	12
13	11.48	6.10	11.45	6.15	11.42	6.20	11.40	6.25	13
14	12.36	6.57	12.33	6.63	12.30	6.68	12.27	6.73	14
15	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.21	15
16	14.13	7.51	14.09	7.57	14.06	7.63	14.03	7.70	16
17	15.01	7.98	14.98	8.05	14.94	8.11	14.90	8.18	17
18	15.89	8.45	15.86	8.52	15.82	8.59	15.78	8.66	18
19	16.78	8.92	16.74	8.99	16.70	9.07	16.66	9.14	19
20	17.66	9.39	17.62	9.47	17.58	9.54	17.53	9.62	20
21	18.54	9.86	18.50	9.94	18.46	10.02	18.41	10.10	21
22	19.42	10.33	19.38	10.41	19.33	10.50	19.29	10.58	22
23	20.31	10.80	20.26	10.89	20.21	10.97	20.16	11.06	23
24	21.19	11.27	21.14	11.36	21.09	11.45	21.04	11.54	24
25	22.07	11.74	22.02	11.83	21.97	11.93	21.92	12.02	25
26	22.96	12.21	22.90	12.31	22.85	12.41	22.79	12.51	26
27	23.84	12.68	23.78	12.78	23.73	12.88	23.67	12.99	27
28	24.72	13.15	24.66	13.25	24.61	13.36	24.55	13.47	28
29	25.61	13.61	25.55	13.73	25.49	13.84	25.43	13.95	29
30	26.49	14.08	26.43	14.20	26.36	14.31	26.30	14.43	30
31	27.37	14.55	27.31	14.67	27.24	14.79	27.18	14.91	31
32	28.25	15.02	28.19	15.15	28.12	15.27	28.06	15.39	32
33	29.14	15.49	29.07	15.62	29.00	15.75	28.93	15.87	33
34	30.02	15.96	29.95	16.09	29.88	16.22	29.81	16.35	34
35	30.90	16.43	30.83	16.57	30.76	16.70	30.69	16.83	35
36	31.79	16.90	31.71	17.04	31.64	17.18	31.56	17.32	36
37	32.67	17.37	32.59	17.51	32.52	17.65	32.44	17.80	37
38	33.55	17.84	33.47	17.99	33.39	18.13	33.32	18.28	38
39	34.43	18.31	34.35	18.46	34.27	18.61	34.19	18.76	39
40	35.32	18.78	35.24	18.93	35.15	19.09	35.07	19.24	40
41	36.20	19.25	36.12	19.41	36.03	19.56	35.95	19.72	41
42	37.08	19.72	37.00	19.88	36.91	20.04	36.82	20.20	42
43	37.97	20.19	37.88	20.35	37.79	20.52	37.70	20.68	43
44	38.85	20.66	38.76	20.83	38.67	20.99	38.58	21.16	44
45	39.73	21.13	39.64	21.30	39.55	21.47	33.45	21.64	45
46	40.62	21.60	40.52	21.77	40.43	21.95	40.33	22.13	46
47	41.50	22.07	41.40	22.25	41.30	22.43	41.21	22.61	47
48	42.38	22.53	42.28	22.72	42.18	22.90	42.08	23.09	48
49	43.26	23.00	43.16	23.19	43.06	23.38	42.96	23.57	49
50	44.15	23.47	44.04	23.67	43.94	23.86	43.84	24.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	62 Deg.		61½ Deg.		61½ Deg.		61½ Deg.		

Distance.	28 Deg.		28½ Deg.		28¾ Deg.		29 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	45.03	23.94	44.93	24.14	44.82	24.34	44.71	24.53	51
52	45.91	24.41	45.81	24.61	45.70	24.81	45.59	25.01	52
53	46.80	24.88	46.69	25.09	46.58	25.29	46.47	25.49	53
54	47.68	25.35	47.57	25.56	47.46	25.77	47.34	25.97	54
55	48.56	25.82	48.45	26.03	48.33	26.24	48.22	26.45	55
56	49.45	26.29	49.33	26.51	49.21	26.72	49.10	26.94	56
57	50.33	26.76	50.21	26.98	50.09	27.20	49.97	27.42	57
58	51.21	27.23	51.09	27.45	50.97	27.68	50.85	27.90	58
59	52.09	27.70	51.97	27.93	51.85	28.15	51.73	28.38	59
60	52.98	28.17	52.85	28.40	52.73	28.63	52.60	28.86	60
61	53.86	28.64	53.73	28.87	53.61	29.11	53.48	29.34	61
62	54.74	29.11	54.62	29.35	54.49	29.58	54.36	29.82	62
63	55.63	29.58	55.50	29.82	55.37	30.06	55.23	30.30	63
64	56.51	30.05	56.38	30.29	56.24	30.54	56.11	30.78	64
65	57.39	30.52	57.26	30.77	57.12	31.02	56.99	31.26	65
66	58.27	30.99	58.14	31.24	58.00	31.49	57.86	31.75	66
67	59.16	31.45	59.02	31.71	58.88	31.97	58.74	32.23	67
68	60.04	31.92	59.90	32.19	59.76	32.45	59.62	32.71	68
69	60.92	32.39	60.78	32.66	60.64	32.92	60.49	33.19	69
70	61.81	32.86	61.66	33.13	61.52	33.40	61.37	33.67	70
71	62.69	33.33	62.54	33.61	62.40	33.88	62.25	34.15	71
72	63.57	33.80	63.42	34.08	63.27	34.36	63.12	34.63	72
73	64.46	34.27	64.30	34.55	64.15	34.83	64.00	35.11	73
74	65.34	34.74	65.19	35.03	65.03	35.31	64.88	35.59	74
75	66.22	35.21	66.07	35.50	65.91	35.79	65.75	36.07	75
76	67.10	35.68	66.95	35.97	66.79	36.26	66.63	36.56	76
77	67.99	36.15	67.83	36.45	67.67	36.74	67.51	37.04	77
78	68.87	36.62	68.71	36.92	68.55	37.22	68.38	37.52	78
79	69.75	37.09	69.59	37.39	69.43	37.70	69.26	38.00	79
80	70.64	37.56	70.47	37.87	70.31	38.17	70.14	38.48	80
81	71.52	38.03	71.35	38.34	71.18	38.65	71.01	38.96	81
82	72.40	38.50	72.23	38.81	72.06	39.13	71.89	39.44	82
83	73.28	38.97	73.11	39.29	72.94	39.60	72.77	39.92	83
84	74.17	39.44	73.99	39.76	73.82	40.08	73.64	40.40	84
85	75.05	39.91	74.88	40.23	74.70	40.56	74.52	40.88	85
86	75.93	40.37	75.76	40.71	75.58	41.04	75.40	41.36	86
87	76.82	40.84	76.64	41.18	76.46	41.51	76.28	41.85	87
88	77.70	41.31	77.52	41.65	77.34	41.99	77.15	42.33	88
89	78.58	41.78	78.40	42.13	78.21	42.47	78.03	42.81	89
90	79.47	42.25	79.28	42.60	79.09	42.94	78.91	43.29	90
91	80.35	42.72	80.16	43.07	79.97	43.42	79.78	43.77	91
92	81.23	43.19	81.04	43.55	80.85	43.90	80.66	44.25	92
93	82.11	43.66	81.92	44.02	81.73	44.38	81.54	44.73	93
94	83.00	44.13	82.80	44.49	82.61	44.85	82.41	45.21	94
95	83.88	44.60	83.68	44.97	83.49	45.33	83.29	45.69	95
96	84.76	45.07	84.57	45.44	84.37	45.81	84.17	46.17	96
97	85.65	45.54	85.45	45.91	85.25	46.28	85.04	46.66	97
98	86.53	46.01	86.33	46.39	86.12	46.76	85.92	47.14	98
99	87.41	46.48	87.21	46.86	87.00	47.24	86.80	47.62	99
100	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	62 Deg.		61½ Deg.		61¼ Deg.		61 Deg.		

Distance.	29 Deg.		29½ Deg.		29½ Deg.		29½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.87	0.48	0.87	0.49	0.87	0.49	0.87	0.50	1
2	1.75	0.67	1.74	0.98	1.74	0.98	1.74	0.99	2
3	2.62	1.45	2.62	1.47	2.61	1.48	2.60	1.49	3
4	3.50	1.94	3.49	1.95	3.48	1.97	3.47	1.98	4
5	4.37	2.42	4.36	2.44	4.35	2.46	4.34	2.48	5
6	5.25	2.91	5.23	2.93	5.22	2.95	5.21	2.98	6
7	6.12	3.39	6.11	3.42	6.09	3.45	6.08	3.47	7
8	7.00	3.88	6.98	3.91	6.96	3.94	6.95	3.97	8
9	7.87	4.36	7.85	4.40	7.83	4.43	7.81	4.47	9
10	8.75	4.85	8.72	4.89	8.70	4.92	8.68	4.96	10
11	9.62	5.33	9.60	5.37	9.57	5.42	9.55	5.46	11
12	10.50	5.82	10.47	5.86	10.44	5.91	10.42	5.95	12
13	11.37	6.30	11.34	6.35	11.31	6.40	11.29	6.45	13
14	12.24	6.79	12.21	6.84	12.18	6.89	12.15	6.95	14
15	13.12	7.27	13.09	7.33	13.06	7.39	13.02	7.44	15
16	13.99	7.76	13.96	7.82	13.93	7.88	13.89	7.94	16
17	14.87	8.24	14.83	8.31	14.80	8.37	14.76	8.44	17
18	15.74	8.73	15.70	8.80	15.67	8.86	15.63	8.93	18
19	16.62	9.21	16.58	9.28	16.54	9.36	16.50	9.43	19
20	17.49	9.70	17.45	9.77	17.41	9.85	17.36	9.92	20
21	18.37	10.18	18.32	10.26	18.28	10.34	18.23	10.42	21
22	19.24	10.67	19.19	10.75	19.15	10.83	19.10	10.92	22
23	20.12	11.15	20.07	11.24	20.02	11.33	19.97	11.41	23
24	20.99	11.64	20.94	11.73	20.89	11.82	20.84	11.91	24
25	21.87	12.12	21.81	12.22	21.76	12.31	21.70	12.41	25
26	22.74	12.60	22.68	12.70	22.63	12.80	22.57	12.90	26
27	23.61	13.09	23.56	13.19	23.50	13.30	23.44	13.40	27
28	24.49	13.57	24.43	13.68	24.37	13.79	24.31	13.89	28
29	25.36	14.06	25.30	14.17	25.24	14.28	25.18	14.39	29
30	26.24	14.54	26.17	14.66	26.11	14.77	26.05	14.89	30
31	27.11	15.03	27.05	15.15	26.98	15.27	26.91	15.38	31
32	27.99	15.51	27.92	15.64	27.85	15.76	27.78	15.88	32
33	28.86	16.00	28.79	16.12	28.72	16.25	28.65	16.38	33
34	29.74	16.48	29.66	16.61	29.59	16.74	29.52	16.87	34
35	30.61	16.97	30.54	17.10	30.46	17.23	30.39	17.37	35
36	31.49	17.45	31.41	17.59	31.33	17.73	31.26	17.86	36
37	32.36	17.94	32.28	18.08	32.20	18.22	32.12	18.36	37
38	33.24	18.42	33.15	18.57	33.07	18.71	32.99	18.86	38
39	34.11	18.91	34.03	19.06	33.94	19.20	33.86	19.35	39
40	34.98	19.39	34.90	19.54	34.81	19.70	34.73	19.85	40
41	35.86	19.88	35.77	20.03	35.68	20.19	35.60	20.34	41
42	36.73	20.36	36.64	20.52	36.55	20.68	36.46	20.84	42
43	37.61	20.85	37.52	21.01	37.43	21.17	37.33	21.34	43
44	38.48	21.33	38.39	21.50	38.30	21.67	38.20	21.83	44
45	39.36	21.82	39.26	21.99	39.17	22.16	39.07	22.33	45
46	40.23	22.30	40.13	22.48	40.04	22.65	39.94	22.83	46
47	41.11	22.79	41.01	22.97	40.91	23.14	40.81	23.32	47
48	41.98	23.27	41.88	23.45	41.78	23.68	41.67	23.82	48
49	42.86	23.76	42.75	23.94	42.65	24.13	42.54	24.31	49
50	43.73	24.24	43.62	24.43	43.52	24.62	43.41	24.81	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	61 Deg.		60½ Deg.		60½ Deg.		60½ Deg.		

TRAVERSE TABLE.

Distance.	29 Deg.		29¼ Deg.		29½ Deg.		29¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	44.61	24.73	44.50	24.92	44.39	25.11	44.28	25.31	51
52	45.48	25.21	45.37	25.41	45.26	25.61	45.15	25.80	52
53	46.35	25.69	46.24	25.90	46.13	26.10	46.01	26.30	53
54	47.23	26.18	47.11	26.39	47.00	26.59	46.88	26.80	54
55	48.10	26.66	47.99	26.87	47.87	27.08	47.75	27.29	55
56	48.98	27.15	48.86	27.36	48.74	27.58	48.62	27.79	56
57	49.85	27.63	49.73	27.85	49.61	28.07	49.49	28.28	57
58	50.73	28.12	50.60	28.34	50.48	28.56	50.36	28.78	58
59	51.60	28.60	51.48	28.83	51.35	29.05	51.22	29.28	59
60	52.48	29.09	52.35	29.32	52.22	29.55	52.09	29.77	60
61	53.35	29.57	53.22	29.81	53.09	30.04	52.96	30.27	61
62	54.23	30.06	54.09	30.29	53.96	30.53	53.83	30.77	62
63	55.10	30.54	54.97	30.78	54.83	31.02	54.70	31.26	63
64	55.98	31.03	55.84	31.27	55.70	31.52	55.56	31.76	64
65	56.85	31.51	56.71	31.76	56.57	32.01	56.43	32.25	65
66	57.72	32.00	57.58	32.25	57.44	32.50	57.30	32.75	66
67	58.60	32.48	58.46	32.74	58.31	32.99	58.17	33.25	67
68	59.47	32.97	59.33	33.23	59.18	33.48	59.04	33.74	68
69	60.35	33.45	60.20	33.71	60.05	33.98	59.91	34.24	69
70	61.22	33.94	61.07	34.20	60.92	34.47	60.77	34.74	70
71	62.10	34.42	61.95	34.69	61.80	34.96	61.64	35.23	71
72	62.97	34.91	62.82	35.18	62.67	35.45	62.51	35.73	72
73	63.85	35.39	63.69	35.67	63.54	35.95	63.38	36.22	73
74	64.72	35.88	64.56	36.16	64.41	36.44	64.25	36.72	74
75	65.60	36.36	65.44	36.65	65.28	36.93	65.11	37.22	75
76	66.47	36.85	66.31	37.14	66.15	37.42	65.98	37.71	76
77	67.35	37.33	67.18	37.62	67.02	37.92	66.85	38.21	77
78	68.22	37.82	68.05	38.11	67.89	38.41	67.72	38.70	78
79	69.09	38.30	68.93	38.60	68.76	38.90	68.59	39.20	79
80	69.97	38.78	69.80	39.09	69.63	39.39	69.46	39.70	80
81	70.84	39.27	70.57	39.58	70.50	39.89	70.32	40.19	81
82	71.72	39.75	71.54	40.07	71.37	40.38	71.19	40.69	82
83	72.59	40.24	72.42	40.56	72.24	40.87	72.06	41.19	83
84	73.47	40.72	73.29	41.04	73.11	41.36	72.93	41.68	84
85	74.34	41.21	74.16	41.53	73.98	41.86	73.80	42.18	85
86	75.22	41.69	75.03	42.02	74.85	42.35	74.67	42.67	86
87	76.09	42.18	75.91	42.51	75.72	42.84	75.53	43.17	87
88	76.97	42.65	76.78	43.00	76.59	43.33	76.40	43.67	88
89	77.84	43.15	77.65	43.49	77.46	43.83	77.27	44.16	89
90	78.72	43.63	78.52	43.98	78.33	44.32	78.14	44.66	90
91	79.59	44.12	79.40	44.46	79.20	44.81	79.01	45.16	91
92	80.46	44.60	80.27	44.95	80.07	45.30	79.87	45.65	92
93	81.34	45.09	81.14	45.44	80.94	45.80	80.74	46.15	93
94	82.21	45.57	82.01	45.93	81.81	46.29	81.61	46.64	94
95	83.09	46.06	82.89	46.42	82.68	46.78	82.48	47.14	95
96	83.96	46.54	83.76	46.91	83.55	47.27	83.35	47.64	96
97	84.84	47.03	84.63	47.40	84.42	47.77	84.22	48.13	97
98	85.71	47.51	85.50	47.88	85.29	48.26	85.08	48.63	98
99	86.59	48.00	86.38	48.37	86.17	48.75	85.95	49.13	99
100	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	61 Deg.		60¼ Deg.		60½ Deg.		60¾ Deg.		



Distance.	30 Deg.		30½ Deg.		30¾ Deg.		30¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.87	0.50	0.86	0.50	0.86	0.51	0.86	0.51	1
2	1.73	1.00	1.73	1.01	1.72	1.02	1.72	1.02	2
3	2.60	1.50	2.59	1.51	2.58	1.52	2.58	1.53	3
4	3.46	2.00	3.46	2.02	3.45	2.03	3.44	2.05	4
5	4.33	2.50	4.32	2.52	4.31	2.54	4.30	2.56	5
6	5.20	3.00	5.18	3.02	5.17	3.05	5.16	3.07	6
7	6.06	3.50	6.05	3.53	6.03	3.55	6.02	3.58	7
8	6.93	4.00	6.91	4.03	6.89	4.06	6.88	4.09	8
9	7.79	4.50	7.77	4.53	7.75	4.57	7.73	4.60	9
10	8.66	5.00	8.64	5.04	8.62	5.08	8.59	5.11	10
11	9.53	5.50	9.50	5.54	9.48	5.58	9.45	5.62	11
12	10.39	6.00	10.37	6.05	10.34	6.09	10.31	6.14	12
13	11.26	6.50	11.23	6.55	11.20	6.60	11.17	6.65	13
14	12.12	7.00	12.09	7.05	12.06	7.11	12.03	7.16	14
15	12.99	7.50	12.96	7.56	12.92	7.61	12.89	7.67	15
16	13.86	8.00	13.82	8.06	13.79	8.12	13.75	8.18	16
17	14.72	8.50	14.69	8.56	14.65	8.63	14.61	8.69	17
18	15.59	9.00	15.55	9.07	15.51	9.14	15.47	9.20	18
19	16.45	9.50	16.41	9.57	16.37	9.64	16.33	9.71	19
20	17.32	10.00	17.28	10.03	17.23	10.15	17.19	10.23	20
21	18.19	10.50	18.14	10.58	18.09	10.66	18.05	10.74	21
22	19.05	11.00	19.00	11.08	18.96	11.17	18.91	11.25	22
23	19.92	11.50	19.87	11.59	19.82	11.67	19.77	11.76	23
24	20.78	12.00	20.73	12.09	20.68	12.18	20.63	12.27	24
25	21.65	12.50	21.60	12.59	21.54	12.69	21.49	12.78	25
26	22.52	13.00	22.46	13.10	22.40	13.20	22.34	13.29	26
27	23.38	13.50	23.32	13.60	23.26	13.70	23.20	13.80	27
28	24.25	14.00	24.19	14.11	24.13	14.21	24.06	14.32	28
29	25.11	14.50	25.05	14.61	24.99	14.72	24.92	14.83	29
30	25.98	15.00	25.92	15.11	25.85	15.23	25.78	15.31	30
31	26.85	15.50	26.78	15.62	26.71	15.73	26.64	15.85	31
32	27.71	16.00	27.64	16.12	27.57	16.24	27.50	16.36	32
33	28.58	16.50	28.51	16.62	28.43	16.75	28.36	16.87	33
34	29.44	17.00	29.37	17.13	29.30	17.26	29.22	17.38	34
35	30.31	17.50	30.23	17.63	30.16	17.76	30.08	17.90	35
36	31.18	18.00	31.10	18.14	31.02	18.27	30.94	18.41	36
37	32.04	18.50	31.96	18.64	31.88	18.78	31.80	18.92	37
38	32.91	19.00	32.83	19.14	32.74	19.29	32.66	19.43	38
39	33.77	19.50	33.69	19.65	33.60	19.79	33.52	19.94	39
40	34.64	20.00	34.55	20.15	34.47	20.30	34.38	20.45	40
41	35.51	20.50	35.42	20.65	35.33	20.81	35.24	20.96	41
42	36.37	21.00	36.28	21.16	36.19	21.32	36.10	21.47	42
43	37.24	21.50	37.14	21.66	37.05	21.82	36.95	21.99	43
44	38.11	22.00	38.01	22.17	37.91	22.33	37.81	22.50	44
45	38.97	22.50	38.87	22.67	38.77	22.84	38.67	23.01	45
46	39.84	23.00	39.74	23.17	39.63	23.35	39.53	23.52	46
47	40.70	23.50	40.60	23.68	40.50	23.85	40.39	24.03	47
48	41.57	24.00	41.46	24.18	41.36	24.35	41.25	24.54	48
49	42.44	24.50	42.33	24.68	42.22	24.87	42.11	25.05	49
50	43.30	25.00	43.19	25.19	43.08	25.38	42.97	25.56	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	60 Deg.		59½ Deg.		59¼ Deg.		59¼ Deg.		

TRAVERSE TABLE.

Distance.	30 Deg.		30½ Deg.		30¾ Deg.		30¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	44.17	25.50	44.06	25.69	43.94	25.88	43.83	26.08	51
52	45.03	26.00	44.92	26.20	44.80	26.39	44.69	26.59	52
53	45.90	26.50	45.78	26.70	45.67	26.90	45.55	27.10	53
54	46.77	27.00	46.65	27.20	46.53	27.41	46.41	27.61	54
55	47.63	27.50	47.51	27.71	47.39	27.91	47.27	28.12	55
56	48.50	28.00	48.37	28.21	48.25	28.42	48.13	28.63	56
57	49.36	28.50	49.24	28.72	49.11	28.93	48.99	29.14	57
58	50.23	29.00	50.10	29.22	49.97	29.44	49.85	29.65	58
59	51.10	29.50	50.97	29.72	50.84	29.94	50.70	30.17	59
60	51.96	30.00	51.83	30.23	51.70	30.45	51.56	30.68	60
61	52.83	30.50	52.69	30.73	52.56	30.96	52.42	31.19	61
62	53.69	31.00	53.56	31.23	53.42	31.47	53.28	31.70	62
63	54.56	31.50	54.42	31.74	54.28	31.97	54.14	32.21	63
64	55.43	32.00	55.29	32.24	55.14	32.48	55.00	32.72	64
65	56.29	32.50	56.15	32.75	56.01	32.99	55.86	33.23	65
66	57.16	33.00	57.01	33.25	56.87	33.50	56.72	33.75	66
67	58.02	33.50	57.88	33.75	57.73	34.01	57.58	34.26	67
68	58.89	34.00	58.74	34.26	58.59	34.51	58.44	34.77	68
69	59.76	34.50	59.60	34.76	59.45	35.02	59.30	35.28	69
70	60.62	35.00	60.47	35.26	60.31	35.53	60.16	35.79	70
71	61.49	35.50	61.33	35.77	61.18	36.04	61.02	36.30	71
72	62.35	36.00	62.20	36.27	62.04	36.54	61.88	36.81	72
73	63.22	36.50	63.06	36.78	62.90	37.05	62.74	37.32	73
74	64.09	37.00	63.92	37.28	63.76	37.56	63.60	37.84	74
75	64.95	37.50	64.79	37.78	64.62	38.07	64.46	38.35	75
76	65.82	38.00	65.65	38.29	65.48	38.57	65.31	38.86	76
77	66.68	38.50	66.52	38.79	66.35	39.08	66.17	39.37	77
78	67.55	39.00	67.38	39.29	67.21	39.59	67.03	39.88	78
79	68.42	39.50	68.24	39.80	68.07	40.10	67.89	40.39	79
80	69.28	40.00	69.11	40.30	68.93	40.60	68.75	40.90	80
81	70.15	40.50	69.97	40.81	69.79	41.11	69.61	41.41	81
82	71.01	41.00	70.83	41.31	70.65	41.62	70.47	41.93	82
83	71.88	41.50	71.70	41.81	71.52	42.13	71.33	42.44	83
84	72.75	42.00	72.56	42.32	72.38	42.63	72.19	42.95	84
85	73.61	42.50	73.43	42.82	73.24	43.14	73.05	43.46	85
86	74.48	43.00	74.29	43.32	74.10	43.65	73.91	43.97	86
87	75.34	43.50	75.15	43.83	74.96	44.16	74.77	44.48	87
88	76.21	44.00	76.02	44.33	75.82	44.66	75.63	44.99	88
89	77.08	44.50	76.88	44.84	76.68	45.17	76.49	45.51	89
90	77.94	45.00	77.75	45.34	77.55	45.68	77.35	46.02	90
91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53	91
92	79.67	46.00	79.47	46.35	79.27	46.69	79.07	47.04	92
93	80.54	46.50	80.34	46.85	80.13	47.20	79.92	47.55	93
94	81.41	47.00	81.20	47.35	80.99	47.71	80.78	48.06	94
95	82.27	47.50	82.06	47.86	81.85	48.22	81.64	48.57	95
96	83.14	48.00	82.93	48.36	82.72	48.72	82.50	49.08	96
97	84.00	48.50	83.79	48.87	83.58	49.23	83.36	49.60	97
98	84.87	49.00	84.66	49.37	84.44	49.74	84.22	50.11	98
99	85.74	49.50	85.52	49.87	85.30	50.25	85.08	50.62	99
100	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	60 Deg.		59½ Deg.		59¼ Deg.		59¼ Deg.		

TRAVERSE TABLE.

Distance.	31 Deg.		31½ Deg.		31¾ Deg.		31¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53	1
2	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05	2
3	2.57	1.55	2.56	1.56	2.56	1.57	2.55	1.58	3
4	3.43	2.06	3.42	2.08	3.41	2.09	3.40	2.10	4
5	4.29	2.58	4.27	2.59	4.26	2.61	4.25	2.63	5
6	5.14	3.09	5.13	3.11	5.12	3.13	5.10	3.16	6
7	6.00	3.61	5.98	3.63	5.97	3.66	5.95	3.68	7
8	6.86	4.12	6.84	4.15	6.82	4.18	6.80	4.21	8
9	7.71	4.64	7.69	4.67	7.67	4.70	7.65	4.74	9
10	8.57	5.15	8.55	5.19	8.53	5.22	8.50	5.26	10
11	9.43	5.67	9.40	5.71	9.38	5.75	9.35	5.79	11
12	10.29	6.18	10.26	6.23	10.23	6.27	10.20	6.31	12
13	11.14	6.70	11.11	6.74	11.08	6.79	11.05	6.84	13
14	12.00	7.21	11.97	7.26	11.94	7.31	11.90	7.37	14
15	12.86	7.73	12.82	7.78	12.79	7.84	12.76	7.89	15
16	13.71	8.24	13.68	8.30	13.64	8.36	13.61	8.42	16
17	14.57	8.76	14.53	8.82	14.49	8.88	14.46	8.95	17
18	15.43	9.27	15.39	9.34	15.35	9.40	15.31	9.47	18
19	16.29	9.79	16.24	9.86	16.20	9.93	16.16	10.00	19
20	17.14	10.30	17.10	10.38	17.05	10.45	17.01	10.52	20
21	18.00	10.82	17.95	10.89	17.91	10.97	17.86	11.05	21
22	18.86	11.33	18.81	11.41	18.76	11.49	18.71	11.58	22
23	19.71	11.85	19.66	11.93	19.61	12.02	19.56	12.10	23
24	20.57	12.36	20.52	12.45	20.46	12.54	20.41	12.63	24
25	21.43	12.88	21.37	12.97	21.32	13.06	21.26	13.16	25
26	22.29	13.39	22.23	13.49	22.17	13.58	22.11	13.68	26
27	23.14	13.91	23.08	14.01	23.02	14.11	22.96	14.21	27
28	24.00	14.42	23.91	14.53	23.87	14.63	23.81	14.73	28
29	24.86	14.94	24.79	15.04	24.73	15.15	24.66	15.26	29
30	25.71	15.45	25.65	15.56	25.58	15.67	25.51	15.79	30
31	26.57	15.97	26.50	16.08	26.43	16.20	26.36	16.31	31
32	27.43	16.48	27.36	16.60	27.28	16.72	27.21	16.84	32
33	28.29	17.00	28.21	17.12	28.14	17.24	28.06	17.37	33
34	29.14	17.51	29.07	17.64	28.99	17.76	28.91	17.89	34
35	30.00	18.03	29.92	18.16	29.84	18.29	29.76	18.42	35
36	30.86	18.54	30.78	18.68	30.70	18.81	30.61	18.94	36
37	31.72	19.06	31.63	19.19	31.55	19.33	31.46	19.47	37
38	32.57	19.57	32.45	19.71	32.40	19.85	32.31	20.00	38
39	33.43	20.09	33.34	20.23	33.25	20.38	33.16	20.52	39
40	34.29	20.60	34.20	20.75	34.11	20.90	34.01	21.05	40
41	35.14	21.12	35.05	21.27	34.96	21.42	34.86	21.57	41
42	36.00	21.63	35.91	21.79	35.81	21.94	35.71	22.10	42
43	36.86	22.15	36.76	22.31	36.66	22.47	36.57	22.63	43
44	37.72	22.66	37.62	22.83	37.52	22.99	37.42	23.15	44
45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68	45
46	39.43	23.69	39.33	23.86	39.22	24.03	39.12	24.21	46
47	40.29	24.21	40.18	24.38	40.07	24.56	39.97	24.73	47
48	41.14	24.72	41.04	24.90	40.93	25.08	40.82	25.26	48
49	42.00	25.24	41.89	25.42	41.78	25.60	41.67	25.78	49
50	42.86	25.76	42.75	25.94	42.63	26.12	42.52	26.31	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	59 Deg.		58½ Deg.		58¾ Deg.		58¼ Deg.		

TRAVERSE TABLE.

65

Distance.	31 Deg.		31½ Deg.		31¾ Deg.		31¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.72	26.27	43.60	26.46	43.48	26.65	43.37	26.84	51
52	44.57	26.78	44.46	26.98	44.34	27.17	44.22	27.36	52
53	45.43	27.30	45.31	27.49	45.19	27.69	45.07	27.89	53
54	46.29	27.81	46.17	28.01	46.04	28.21	45.92	28.42	54
55	47.14	28.33	47.02	28.53	46.90	28.74	46.77	28.94	55
56	48.00	28.84	47.88	29.05	47.75	29.26	47.62	29.47	56
57	48.86	29.36	48.73	29.57	48.60	29.78	48.47	29.99	57
58	49.72	29.87	49.58	30.09	49.45	30.30	49.32	30.52	58
59	50.57	30.39	50.44	30.61	50.31	30.83	50.17	31.05	59
60	51.43	30.90	51.29	31.13	51.16	31.35	51.02	31.57	60
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10	61
62	53.14	31.93	53.00	32.16	52.86	32.39	52.72	32.63	62
63	54.00	32.45	53.86	32.68	53.72	32.92	53.57	33.15	63
64	54.86	32.96	54.71	33.20	54.57	33.44	54.42	33.68	64
65	55.72	33.48	55.57	33.72	55.42	33.96	55.27	34.20	65
66	56.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73	66
67	57.43	34.51	57.28	34.76	57.13	35.01	56.98	35.26	67
68	58.29	35.02	58.13	35.28	57.98	35.53	57.82	35.78	68
69	59.14	35.54	58.99	35.80	58.83	36.05	58.67	36.31	69
70	60.00	36.05	59.84	36.31	59.68	36.57	59.52	36.83	70
71	60.86	36.57	60.70	36.83	60.54	37.10	60.37	37.36	71
72	61.72	37.08	61.55	37.35	61.39	37.62	61.23	37.89	72
73	62.57	37.60	62.41	37.87	62.24	38.14	62.08	38.41	73
74	63.43	38.11	63.26	38.39	63.10	38.66	62.93	38.94	74
75	64.29	38.63	64.12	38.91	63.95	39.19	63.78	39.47	75
76	65.14	39.14	64.97	39.43	64.80	39.71	64.63	39.99	76
77	66.00	39.66	65.83	39.95	65.65	40.23	65.48	40.52	77
78	66.86	40.17	66.68	40.46	66.51	40.75	66.33	41.04	78
79	67.72	40.69	67.54	40.98	67.36	41.28	67.18	41.57	79
80	68.57	41.20	68.39	41.50	68.21	41.80	68.03	42.10	80
81	69.43	41.72	69.25	42.02	69.06	42.32	68.88	42.62	81
82	70.29	42.23	70.10	42.54	69.92	42.84	69.73	43.15	82
83	71.14	42.75	70.96	43.06	70.77	43.37	70.58	43.68	83
84	72.00	43.26	71.81	43.58	71.62	43.89	71.43	44.20	84
85	72.86	43.78	72.67	44.10	72.47	44.41	72.28	44.73	85
86	73.72	44.29	73.52	44.61	73.33	44.93	73.13	45.25	86
87	74.57	44.81	74.38	45.13	74.18	45.46	73.98	45.78	87
88	75.43	45.32	75.23	45.65	75.03	45.98	74.83	46.31	88
89	76.29	45.84	76.09	46.17	75.88	46.50	75.68	46.83	89
90	77.15	46.35	76.94	46.69	76.74	47.02	76.52	47.36	90
91	78.00	46.87	77.80	47.21	77.59	47.55	77.38	47.89	91
92	78.86	47.38	78.65	47.73	78.44	48.07	78.23	48.41	92
93	79.72	47.90	79.51	48.25	79.30	48.59	79.08	48.94	93
94	80.57	48.41	80.36	48.76	80.15	49.11	79.93	49.47	94
95	81.43	48.93	81.22	49.28	81.00	49.64	80.78	49.99	95
96	82.29	49.44	82.07	49.80	81.85	50.16	81.63	50.52	96
97	83.15	49.96	82.93	50.32	82.71	50.68	82.48	51.04	97
98	84.00	50.47	83.78	50.84	83.56	51.20	83.33	51.57	98
99	84.86	50.99	84.64	51.36	84.41	51.73	84.18	52.10	99
100	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	59 Deg.		58½ Deg.		58½ Deg.		58½ Deg.		

TRAVERSE TABLE.

Distance.	32 Deg.		32½ Deg.		33½ Deg.		32¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54	1
2	1.70	1.06	1.69	1.07	1.69	1.07	1.68	1.08	2
3	2.54	1.59	2.54	1.60	2.53	1.61	2.52	1.62	3
4	3.39	2.12	3.38	2.13	3.37	2.15	3.36	2.16	4
5	4.21	2.65	4.23	2.67	4.22	2.69	4.21	2.70	5
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3.25	6
7	5.94	3.71	5.92	3.74	5.90	3.76	5.89	3.79	7
8	6.78	4.24	6.77	4.27	6.75	4.30	6.73	4.33	8
9	7.63	4.77	7.61	4.80	7.59	4.84	7.57	4.87	9
10	8.48	5.30	8.46	5.34	8.43	5.37	8.41	5.41	10
11	9.33	5.83	9.30	5.87	9.28	5.91	9.25	5.95	11
12	10.18	6.36	10.15	6.40	10.12	6.45	10.09	6.49	12
13	11.02	6.89	10.99	6.94	10.96	6.98	10.93	7.03	13
14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57	14
15	12.72	7.95	12.69	8.00	12.65	8.06	12.62	8.11	15
16	13.57	8.48	13.53	8.54	13.49	8.60	13.46	8.66	16
17	14.42	9.01	14.38	9.07	14.34	9.13	14.30	9.20	17
18	15.26	9.54	15.22	9.61	15.18	9.67	15.14	9.74	18
19	16.11	10.07	16.07	10.14	16.02	10.21	15.98	10.28	19
20	16.96	10.60	16.91	10.67	16.87	10.75	16.82	10.82	20
21	17.81	11.13	17.76	11.21	17.71	11.28	17.66	11.36	21
22	18.66	11.66	18.61	11.74	18.55	11.82	18.50	11.90	22
23	19.51	12.19	19.45	12.27	19.40	12.36	19.34	12.44	23
24	20.35	12.72	20.30	12.81	20.24	12.90	20.18	12.98	24
25	21.20	13.25	21.14	13.34	21.08	13.43	21.03	13.52	25
26	22.05	13.78	21.99	13.87	21.93	13.97	21.87	14.07	26
27	22.90	14.31	22.83	14.41	22.77	14.51	22.71	14.61	27
28	23.75	14.84	23.68	14.94	23.61	15.04	23.55	15.15	28
29	24.59	15.37	24.53	15.47	24.46	15.58	24.39	15.69	29
30	25.44	15.90	25.37	16.01	25.30	16.12	25.23	16.23	30
31	26.29	16.43	26.22	16.54	26.15	16.66	26.07	16.77	31
32	27.14	16.96	27.06	17.08	26.99	17.19	26.91	17.31	32
33	27.99	17.49	27.91	17.61	27.83	17.73	27.75	17.85	33
34	28.83	18.02	28.75	18.14	28.68	18.27	28.60	18.39	34
35	29.68	18.55	29.60	18.68	29.52	18.81	29.44	18.93	35
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48	36
37	31.38	19.61	31.29	19.74	31.21	19.88	31.12	20.02	37
38	32.23	20.14	32.14	20.28	32.05	20.42	31.96	20.56	38
39	33.07	20.67	32.98	20.81	32.89	20.95	32.80	21.10	39
40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	21.64	40
41	34.77	21.73	34.67	21.88	34.58	22.03	34.48	22.18	41
42	35.62	22.26	35.52	22.41	35.42	22.57	35.32	22.72	42
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26	43
44	37.31	23.32	37.21	23.48	37.11	23.64	37.01	23.80	44
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34	45
46	39.01	24.38	38.90	24.55	38.80	24.72	38.69	24.88	46
47	39.86	24.91	39.75	25.08	39.64	25.25	39.53	25.43	47
48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97	48
49	41.55	25.97	41.44	26.15	41.33	26.33	41.21	26.51	49
50	42.40	26.50	42.29	26.68	42.17	26.86	42.05	27.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57½ Deg.		57¼ Deg.		

TRAVERSE TABLE.

Distance.	32 Deg.		32½ Deg.		33 Deg.		33½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59	51
52	44.10	27.56	43.98	27.75	43.86	27.94	43.73	28.13	52
53	44.95	28.09	44.82	28.28	44.70	28.48	44.58	28.67	53
54	45.79	28.62	45.67	28.82	45.54	29.01	45.42	29.21	54
55	46.64	29.15	46.51	29.35	46.39	29.55	46.26	29.75	55
56	47.49	29.68	47.36	29.88	47.23	30.09	47.10	30.29	56
57	48.34	30.21	48.21	30.42	48.07	30.63	47.94	30.84	57
58	49.19	30.74	49.05	30.95	48.92	31.16	48.78	31.38	58
59	50.03	31.27	49.90	31.48	49.76	31.70	49.62	31.92	59
60	50.88	31.80	50.74	32.02	50.60	32.24	50.46	32.46	60
61	51.73	32.33	51.59	32.55	51.45	32.78	51.30	33.00	61
62	52.58	32.85	52.44	33.08	52.29	33.31	52.14	33.54	62
63	53.43	33.38	53.28	33.62	53.13	33.85	52.99	34.08	63
64	54.28	33.91	54.13	34.15	53.98	34.39	53.83	34.62	64
65	55.12	34.44	54.97	34.68	54.82	34.92	54.67	35.16	65
66	55.97	34.97	55.82	35.22	55.66	35.46	55.51	35.70	66
67	56.82	35.50	56.66	35.75	56.51	36.00	56.35	36.25	67
68	57.67	36.03	57.51	36.29	57.35	36.54	57.19	36.79	68
69	58.52	36.56	58.36	36.82	58.19	37.07	58.03	37.33	69
70	59.36	37.09	59.20	37.35	59.04	37.61	58.87	37.87	70
71	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	71
72	61.06	38.15	60.89	38.42	60.72	38.69	60.55	38.95	72
73	61.91	38.68	61.74	38.95	61.57	39.22	61.40	39.49	73
74	62.76	39.21	62.58	39.49	62.41	39.76	62.24	40.03	74
75	63.60	39.74	63.43	40.02	63.25	40.30	63.08	40.57	75
76	64.45	40.27	64.28	40.55	64.10	40.83	63.92	41.11	76
77	65.30	40.80	65.12	41.09	64.94	41.37	64.76	41.65	77
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60	42.20	78
79	67.00	41.86	66.81	42.16	66.63	42.45	66.44	42.74	79
80	67.84	42.39	67.66	42.69	67.47	42.98	67.28	43.28	80
81	68.69	42.92	68.50	43.22	68.31	43.52	68.12	43.82	81
82	69.54	43.45	69.35	43.76	69.16	44.06	68.97	44.36	82
83	70.39	43.98	70.20	44.29	70.00	44.60	69.81	44.90	83
84	71.24	44.51	71.04	44.82	70.84	45.13	70.65	45.44	84
85	72.08	45.04	71.89	45.36	71.69	45.67	71.49	45.98	85
86	72.93	45.57	72.73	45.89	72.53	46.21	72.33	46.52	86
87	73.78	46.10	73.58	46.42	73.38	46.75	73.17	47.06	87
88	74.63	46.63	74.42	46.96	74.22	47.28	74.01	47.61	88
89	75.48	47.16	75.27	47.49	75.06	47.82	74.85	48.15	89
90	76.32	47.69	76.12	48.03	75.91	48.36	75.69	48.69	90
91	77.17	48.22	76.96	48.56	76.75	48.89	76.53	49.23	91
92	78.02	48.75	77.81	49.09	77.59	49.43	77.38	49.77	92
93	78.87	49.28	78.65	49.63	78.44	49.97	78.22	50.31	93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
95	80.56	50.34	80.34	50.69	80.12	51.04	79.90	51.39	95
96	81.41	50.87	81.19	51.23	80.97	51.58	80.74	51.93	96
97	82.26	51.40	82.04	51.76	81.81	52.12	81.58	52.47	97
98	83.11	51.93	82.88	52.29	82.65	52.66	82.42	53.02	98
99	83.96	52.46	83.73	52.83	83.50	53.19	83.26	53.56	99
100	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57½ Deg.		57½ Deg.		

TRAVERSE TABLE.

Distance.	32 Deg.		32½ Deg.		32¾ Deg.		33 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54	1
2	1.70	1.06	1.69	1.07	1.69	1.07	1.68	1.08	2
3	2.54	1.59	2.54	1.60	2.53	1.61	2.52	1.62	3
4	3.39	2.12	3.38	2.13	3.37	2.15	3.36	2.16	4
5	4.24	2.65	4.23	2.67	4.22	2.69	4.21	2.70	5
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3.25	6
7	5.94	3.71	5.92	3.74	5.90	3.76	5.89	3.79	7
8	6.78	4.24	6.77	4.27	6.75	4.30	6.73	4.33	8
9	7.63	4.77	7.61	4.80	7.59	4.84	7.57	4.87	9
10	8.48	5.30	8.46	5.34	8.43	5.37	8.41	5.41	10
11	9.33	5.83	9.30	5.87	9.28	5.91	9.25	5.95	11
12	10.18	6.36	10.15	6.40	10.12	6.45	10.09	6.49	12
13	11.02	6.89	10.99	6.94	10.96	6.98	10.93	7.03	13
14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57	14
15	12.72	7.95	12.69	8.00	12.65	8.06	12.62	8.11	15
16	13.57	8.48	13.53	8.54	13.49	8.60	13.46	8.66	16
17	14.42	9.01	14.38	9.07	14.34	9.13	14.30	9.20	17
18	15.26	9.54	15.22	9.61	15.18	9.67	15.14	9.74	18
19	16.11	10.07	16.07	10.14	16.02	10.21	15.98	10.28	19
20	16.96	10.60	16.91	10.67	16.87	10.75	16.82	10.82	20
21	17.81	11.13	17.76	11.21	17.71	11.28	17.66	11.36	21
22	18.66	11.66	18.61	11.74	18.55	11.82	18.50	11.90	22
23	19.51	12.19	19.45	12.27	19.40	12.36	19.34	12.44	23
24	20.35	12.72	20.30	12.81	20.24	12.90	20.18	12.98	24
25	21.20	13.25	21.14	13.34	21.08	13.43	21.03	13.52	25
26	22.05	13.78	21.99	13.87	21.93	13.97	21.87	14.07	26
27	22.90	14.31	22.83	14.41	22.77	14.51	22.71	14.61	27
28	23.75	14.84	23.68	14.94	23.61	15.04	23.55	15.15	28
29	24.59	15.37	24.53	15.47	24.46	15.58	24.39	15.69	29
30	25.44	15.90	25.37	16.01	25.30	16.12	25.23	16.23	30
31	26.29	16.43	26.22	16.54	26.15	16.66	26.07	16.77	31
32	27.14	16.96	27.06	17.08	26.99	17.19	26.91	17.31	32
33	27.99	17.49	27.91	17.61	27.83	17.73	27.75	17.85	33
34	28.83	18.02	28.75	18.14	28.68	18.27	28.60	18.39	34
35	29.68	18.55	29.60	18.68	29.52	18.81	29.44	18.93	35
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48	36
37	31.38	19.61	31.29	19.74	31.21	19.88	31.12	20.02	37
38	32.23	20.14	32.14	20.28	32.05	20.42	31.96	20.56	38
39	33.07	20.67	32.98	20.81	32.89	20.95	32.80	21.10	39
40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	21.64	40
41	34.77	21.73	34.67	21.88	34.58	22.03	34.48	22.18	41
42	35.62	22.26	35.52	22.41	35.42	22.57	35.32	22.72	42
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26	43
44	37.31	23.32	37.21	23.48	37.11	23.64	37.01	23.80	44
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34	45
46	39.01	24.38	38.90	24.55	38.80	24.72	38.69	24.88	46
47	39.86	24.91	39.75	25.08	39.64	25.25	39.53	25.43	47
48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97	48
49	41.55	25.97	41.44	26.15	41.33	26.33	41.21	26.51	49
50	42.40	26.50	42.29	26.68	42.17	26.86	42.05	27.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57¼ Deg.		57¼ Deg.		

TRAVERSE TABLE.

Distance.	32 Deg.		32½ Deg.		32¾ Deg.		33¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59	51
52	44.10	27.56	43.98	27.75	43.86	27.94	43.73	28.13	52
53	44.95	28.09	44.82	28.28	44.70	28.48	44.58	28.67	53
54	45.79	28.62	45.67	28.82	45.54	29.01	45.42	29.21	54
55	46.64	29.15	46.51	29.35	46.39	29.55	46.26	29.75	55
56	47.49	29.68	47.36	29.88	47.23	30.09	47.10	30.29	56
57	48.34	30.21	48.21	30.42	48.07	30.63	47.94	30.84	57
58	49.19	30.74	49.05	30.95	48.92	31.16	48.78	31.38	58
59	50.03	31.27	49.90	31.48	49.76	31.70	49.62	31.92	59
60	50.88	31.80	50.74	32.02	50.60	32.24	50.46	32.46	60
61	51.73	32.33	51.59	32.55	51.45	32.78	51.30	33.00	61
62	52.58	32.85	52.44	33.08	52.29	33.31	52.14	33.54	62
63	53.43	33.38	53.28	33.62	53.13	33.85	52.99	34.08	63
64	54.28	33.91	54.13	34.15	53.98	34.39	53.83	34.62	64
65	55.12	34.44	54.97	34.68	54.82	34.92	54.67	35.16	65
66	55.97	34.97	55.82	35.22	55.66	35.46	55.51	35.70	66
67	56.82	35.50	56.66	35.75	56.51	36.00	56.35	36.25	67
68	57.67	36.03	57.51	36.29	57.35	36.54	57.19	36.79	68
69	58.52	36.56	58.36	36.82	58.19	37.07	58.03	37.33	69
70	59.36	37.09	59.20	37.35	59.04	37.61	58.87	37.87	70
71	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	71
72	61.06	38.15	60.89	38.42	60.72	38.69	60.55	38.95	72
73	61.91	38.68	61.74	38.95	61.57	39.22	61.40	39.49	73
74	62.76	39.21	62.58	39.49	62.41	39.76	62.24	40.03	74
75	63.60	39.74	63.43	40.02	63.25	40.30	63.08	40.57	75
76	64.45	40.27	64.28	40.55	64.10	40.83	63.92	41.11	76
77	65.30	40.80	65.12	41.09	64.94	41.37	64.76	41.65	77
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60	42.20	78
79	67.00	41.86	66.81	42.16	66.63	42.45	66.44	42.74	79
80	67.84	42.39	67.66	42.69	67.47	42.98	67.28	43.28	80
81	68.69	42.92	68.50	43.22	68.31	43.52	68.12	43.82	81
82	69.54	43.45	69.35	43.76	69.16	44.06	68.97	44.36	82
83	70.39	43.98	70.20	44.29	70.00	44.60	69.81	44.90	83
84	71.24	44.51	71.04	44.82	70.84	45.13	70.65	45.44	84
85	72.08	45.04	71.89	45.36	71.69	45.67	71.49	45.98	85
86	72.93	45.57	72.73	45.89	72.53	46.21	72.33	46.52	86
87	73.78	46.10	73.58	46.42	73.38	46.75	73.17	47.06	87
88	74.63	46.63	74.42	46.96	74.22	47.28	74.01	47.61	88
89	75.48	47.16	75.27	47.49	75.06	47.82	74.85	48.15	89
90	76.32	47.69	76.12	48.03	75.91	48.36	75.69	48.69	90
91	77.17	48.22	76.96	48.56	76.75	48.89	76.53	49.23	91
92	78.02	48.75	77.81	49.09	77.59	49.43	77.38	49.77	92
93	78.87	49.28	78.65	49.63	78.44	49.97	78.22	50.31	93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
95	80.56	50.34	80.34	50.69	80.12	51.04	79.90	51.39	95
96	81.41	50.87	81.19	51.23	80.97	51.58	80.74	51.93	96
97	82.26	51.40	82.04	51.76	81.81	52.12	81.58	52.47	97
98	83.11	51.93	82.88	52.29	82.65	52.66	82.42	53.02	98
99	83.96	52.46	83.73	52.83	83.50	53.19	83.26	53.56	99
100	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57¼ Deg.		57¼ Deg.		



Distance.	32 Deg.		32½ Deg.		32¾ Deg.		32¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54	1
2	1.70	1.06	1.69	1.07	1.69	1.07	1.68	1.08	2
3	2.54	1.59	2.54	1.60	2.53	1.61	2.52	1.62	3
4	3.39	2.12	3.38	2.13	3.37	2.15	3.36	2.16	4
5	4.24	2.65	4.23	2.67	4.22	2.69	4.21	2.70	5
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3.25	6
7	5.94	3.71	5.92	3.74	5.90	3.76	5.89	3.79	7
8	6.78	4.24	6.77	4.27	6.75	4.30	6.73	4.33	8
9	7.63	4.77	7.61	4.80	7.59	4.84	7.57	4.87	9
10	8.48	5.30	8.46	5.34	8.43	5.37	8.41	5.41	10
11	9.33	5.83	9.30	5.87	9.28	5.91	9.25	5.95	11
12	10.18	6.36	10.15	6.40	10.12	6.45	10.09	6.49	12
13	11.02	6.89	10.99	6.94	10.96	6.98	10.93	7.03	13
14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57	14
15	12.72	7.95	12.69	8.00	12.65	8.06	12.62	8.11	15
16	13.57	8.48	13.53	8.54	13.49	8.60	13.46	8.66	16
17	14.42	9.01	14.38	9.07	14.34	9.13	14.30	9.20	17
18	15.26	9.54	15.22	9.61	15.18	9.67	15.14	9.74	18
19	16.11	10.07	16.07	10.14	16.02	10.21	15.98	10.28	19
20	16.96	10.60	16.91	10.67	16.87	10.75	16.82	10.82	20
21	17.81	11.13	17.76	11.21	17.71	11.28	17.66	11.36	21
22	18.66	11.66	18.61	11.74	18.55	11.82	18.50	11.90	22
23	19.51	12.19	19.45	12.27	19.40	12.36	19.34	12.44	23
24	20.35	12.72	20.30	12.81	20.24	12.90	20.18	12.98	24
25	21.20	13.25	21.14	13.34	21.08	13.43	21.03	13.52	25
26	22.05	13.78	21.99	13.87	21.93	13.97	21.87	14.07	26
27	22.90	14.31	22.83	14.41	22.77	14.51	22.71	14.61	27
28	23.75	14.84	23.68	14.94	23.61	15.04	23.55	15.15	28
29	24.59	15.37	24.53	15.47	24.46	15.58	24.39	15.69	29
30	25.44	15.90	25.37	16.01	25.30	16.12	25.23	16.23	30
31	26.29	16.43	26.22	16.54	26.15	16.66	26.07	16.77	31
32	27.14	16.96	27.06	17.08	26.99	17.19	26.91	17.31	32
33	27.99	17.49	27.91	17.61	27.83	17.73	27.75	17.85	33
34	28.83	18.02	28.75	18.14	28.68	18.27	28.60	18.39	34
35	29.68	18.55	29.60	18.68	29.52	18.81	29.44	18.93	35
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48	36
37	31.38	19.61	31.29	19.74	31.21	19.88	31.12	20.02	37
38	32.23	20.14	32.14	20.28	32.05	20.42	31.96	20.56	38
39	33.07	20.67	32.98	20.81	32.89	20.95	32.80	21.10	39
40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	21.64	40
41	34.77	21.73	34.67	21.88	34.58	22.03	34.48	22.18	41
42	35.62	22.26	35.52	22.41	35.42	22.57	35.32	22.72	42
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26	43
44	37.31	23.32	37.21	23.48	37.11	23.64	37.01	23.80	44
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34	45
46	39.01	24.38	38.90	24.55	38.80	24.72	38.69	24.88	46
47	39.86	24.91	39.75	25.08	39.64	25.25	39.53	25.43	47
48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97	48
49	41.55	25.97	41.44	26.15	41.33	26.33	41.21	26.51	49
50	42.40	26.50	42.29	26.68	42.17	26.86	42.05	27.05	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57¼ Deg.		57¼ Deg.		

Distance.	32 Deg.		32½ Deg.		32¾ Deg.		32¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59	51
52	44.10	27.56	43.98	27.75	43.86	27.94	43.73	28.13	52
53	44.95	28.09	44.82	28.28	44.70	28.48	44.58	28.67	53
54	45.79	28.62	45.67	28.82	45.54	29.01	45.42	29.21	54
55	46.64	29.15	46.51	29.35	46.39	29.55	46.26	29.75	55
56	47.49	29.68	47.36	29.88	47.23	30.09	47.10	30.29	56
57	48.34	30.21	48.21	30.42	48.07	30.63	47.94	30.84	57
58	49.19	30.74	49.05	30.95	48.92	31.16	48.78	31.38	58
59	50.03	31.27	49.90	31.48	49.76	31.70	49.62	31.92	59
60	50.88	31.80	50.74	32.02	50.60	32.24	50.46	32.46	60
61	51.73	32.33	51.59	32.55	51.45	32.78	51.30	33.00	61
62	52.58	32.85	52.44	33.08	52.29	33.31	52.14	33.54	62
63	53.43	33.38	53.28	33.62	53.13	33.85	52.99	34.08	63
64	54.28	33.91	54.13	34.15	53.98	34.39	53.83	34.62	64
65	55.12	34.44	54.97	34.68	54.82	34.92	54.67	35.16	65
66	55.97	34.97	55.82	35.22	55.66	35.46	55.51	35.70	66
67	56.82	35.50	56.66	35.75	56.51	36.00	56.35	36.25	67
68	57.67	36.03	57.51	36.29	57.35	36.54	57.19	36.79	68
69	58.52	36.56	58.36	36.82	58.19	37.07	58.03	37.33	69
70	59.36	37.09	59.20	37.35	59.04	37.61	58.87	37.87	70
71	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	71
72	61.06	38.15	60.89	38.42	60.72	38.69	60.55	38.95	72
73	61.91	38.68	61.74	38.95	61.57	39.22	61.40	39.49	73
74	62.76	39.21	62.58	39.49	62.41	39.76	62.24	40.03	74
75	63.60	39.74	63.43	40.02	63.25	40.30	63.08	40.57	75
76	64.45	40.27	64.28	40.55	64.10	40.83	63.92	41.11	76
77	65.30	40.80	65.12	41.09	64.94	41.37	64.76	41.65	77
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60	42.20	78
79	67.00	41.86	66.81	42.16	66.63	42.45	66.44	42.74	79
80	67.84	42.39	67.66	42.69	67.47	42.98	67.28	43.28	80
81	68.69	42.92	68.50	43.22	68.31	43.52	68.12	43.82	81
82	69.54	43.45	69.35	43.76	69.16	44.06	68.97	44.36	82
83	70.39	43.98	70.20	44.29	70.00	44.60	69.81	44.90	83
84	71.24	44.51	71.04	44.82	70.84	45.13	70.65	45.44	84
85	72.08	45.04	71.89	45.36	71.69	45.67	71.49	45.98	85
86	72.93	45.57	72.73	45.89	72.53	46.21	72.33	46.52	86
87	73.78	46.10	73.58	46.42	73.38	46.75	73.17	47.06	87
88	74.63	46.63	74.42	46.96	74.22	47.28	74.01	47.61	88
89	75.48	47.16	75.27	47.49	75.06	47.82	74.85	48.15	89
90	76.32	47.69	76.12	48.03	75.91	48.36	75.69	48.69	90
91	77.17	48.22	76.96	48.56	76.75	48.89	76.53	49.23	91
92	78.02	48.75	77.81	49.09	77.59	49.43	77.38	49.77	92
93	78.87	49.28	78.65	49.63	78.44	49.97	78.22	50.31	93
94	79.72	49.81	79.50	50.16	79.28	50.51	79.06	50.85	94
95	80.56	50.34	80.34	50.69	80.12	51.04	79.90	51.39	95
96	81.41	50.87	81.19	51.23	80.97	51.58	80.74	51.93	96
97	82.26	51.40	82.04	51.76	81.81	52.12	81.58	52.47	97
98	83.11	51.93	82.88	52.29	82.65	52.66	82.42	53.02	98
99	83.96	52.46	83.73	52.83	83.50	53.19	83.26	53.56	99
100	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	58 Deg.		57½ Deg.		57½ Deg.		57½ Deg.		

## TRAVERSE TABLE.

Distance.	33 Deg.		33½ Deg.		33½ Deg.		33½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.84	0.54	0.84	0.55	0.83	0.55	0.83	0.56	1
2	1.68	1.09	1.67	1.10	1.67	1.10	1.66	1.11	2
3	2.52	1.63	2.51	1.64	2.50	1.66	2.49	1.67	3
4	3.35	2.18	3.35	2.19	3.34	2.21	3.33	2.22	4
5	4.19	2.72	4.18	2.74	4.17	2.76	4.16	2.78	5
6	5.03	3.27	5.02	3.29	5.00	3.31	4.99	3.33	6
7	5.87	3.81	5.85	3.84	5.84	3.86	5.82	3.89	7
8	6.71	4.36	6.69	4.39	6.67	4.42	6.65	4.44	8
9	7.55	4.90	7.53	4.93	7.50	4.97	7.48	5.00	9
10	8.39	5.45	8.36	5.48	8.34	5.52	8.31	5.56	10
11	9.23	5.99	9.20	6.03	9.17	6.07	9.15	6.11	11
12	10.06	6.54	10.04	6.58	10.01	6.62	9.98	6.67	12
13	10.90	7.08	10.87	7.13	10.84	7.18	10.81	7.22	13
14	11.74	7.62	11.71	7.68	11.67	7.73	11.64	7.78	14
15	12.58	8.17	12.54	8.22	12.51	8.28	12.47	8.33	15
16	13.42	8.71	13.38	8.77	13.34	8.83	13.30	8.89	16
17	14.26	9.26	14.22	9.32	14.18	9.38	14.13	9.44	17
18	15.10	9.80	15.05	9.87	15.01	9.93	14.97	10.00	18
19	15.93	10.35	15.89	10.42	15.84	10.49	15.80	10.56	19
20	16.77	10.89	16.73	10.97	16.68	11.04	16.63	11.11	20
21	17.61	11.44	17.56	11.51	17.51	11.59	17.46	11.67	21
22	18.45	11.98	18.40	12.06	18.35	12.14	18.29	12.22	22
23	19.29	12.53	19.23	12.61	19.18	12.69	19.12	12.78	23
24	20.13	13.07	20.07	13.16	20.01	13.25	19.96	13.33	24
25	20.97	13.62	20.91	13.71	20.85	13.80	20.79	13.89	25
26	21.81	14.16	21.74	14.26	21.68	14.35	21.62	14.44	26
27	22.64	14.71	22.58	14.80	22.51	14.90	22.45	15.00	27
28	23.48	15.25	23.42	15.35	23.35	15.45	23.28	15.56	28
29	24.32	15.79	24.25	15.90	24.18	16.01	24.11	16.11	29
30	25.16	16.34	25.09	16.45	25.02	16.56	24.94	16.67	30
31	26.00	16.88	25.92	17.00	25.85	17.11	25.78	17.22	31
32	26.84	17.43	26.76	17.55	26.68	17.66	26.61	17.78	32
33	27.68	17.97	27.60	18.09	27.52	18.21	27.44	18.33	33
34	28.51	18.52	28.43	18.64	28.35	18.77	28.27	18.89	34
35	29.35	19.06	29.27	19.19	29.19	19.32	29.10	19.44	35
36	30.19	19.61	30.11	19.74	30.02	19.87	29.93	20.00	36
37	31.03	20.15	30.94	20.29	30.85	20.42	30.76	20.56	37
38	31.87	20.70	31.78	20.84	31.69	20.97	31.60	21.11	38
39	32.71	21.24	32.62	21.38	32.52	21.53	32.43	21.67	39
40	33.55	21.79	33.45	21.93	33.36	22.08	33.26	22.22	40
41	34.39	22.33	34.29	22.48	34.19	22.63	34.09	22.78	41
42	35.22	22.87	35.12	23.03	35.02	23.18	34.92	23.33	42
43	36.06	23.42	35.96	23.58	35.86	23.73	35.75	23.89	43
44	36.90	23.96	36.80	24.12	36.69	24.29	36.58	24.45	44
45	37.74	24.51	37.63	24.67	37.52	24.84	37.42	25.00	45
46	38.58	25.05	38.47	25.22	38.36	25.39	38.25	25.56	46
47	39.42	25.60	39.31	25.77	39.19	25.94	39.08	26.11	47
48	40.26	26.14	40.14	26.32	40.03	26.49	39.91	26.67	48
49	41.09	26.69	40.98	26.87	40.86	27.04	40.74	27.22	49
50	41.93	27.23	41.81	27.41	41.69	27.60	41.57	27.78	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	57 Deg.		56½ Deg.		56½ Deg.		56½ Deg.		

TRAVERSE TABLE

Distance.	33 Deg.		33½ Deg.		33¾ Deg.		33¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	42.77	27.78	42.65	27.96	42.53	28.14	42.40	28.33	51
52	43.61	28.32	43.49	28.51	43.36	28.70	43.24	28.89	52
53	44.45	28.87	44.32	29.06	44.20	29.25	44.07	29.45	53
54	45.29	29.41	45.16	29.61	45.03	29.80	44.90	30.00	54
55	46.13	29.96	46.00	30.16	45.86	30.36	45.73	30.56	55
56	46.97	30.50	46.83	30.70	46.70	30.91	46.56	31.11	56
57	47.80	31.04	47.67	31.25	47.53	31.46	47.39	31.67	57
58	48.64	31.59	48.50	31.80	48.37	32.01	48.23	32.22	58
59	49.48	32.13	49.34	32.35	49.20	32.56	49.06	32.78	59
60	50.32	32.68	50.18	32.90	50.03	33.12	49.89	33.33	60
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89	61
62	52.00	33.77	51.85	33.99	51.70	34.22	51.55	34.45	62
63	52.84	34.31	52.69	34.54	52.53	34.77	52.38	35.00	63
64	53.67	34.86	53.52	35.09	53.37	35.32	53.21	35.56	64
65	54.51	35.40	54.36	35.64	54.20	35.88	54.05	36.11	65
66	55.35	35.95	55.19	36.19	55.04	36.43	54.88	36.67	66
67	56.19	36.49	56.03	36.74	55.87	36.98	55.71	37.22	67
68	57.03	37.04	56.87	37.28	56.70	37.53	56.54	37.78	68
69	57.87	37.58	57.70	37.83	57.54	38.08	57.37	38.33	69
70	58.71	38.12	58.54	38.38	58.37	38.64	58.20	38.89	70
71	59.55	38.67	59.38	38.93	59.21	39.19	59.03	39.45	71
72	60.38	39.21	60.21	39.48	60.04	39.74	59.87	40.00	72
73	61.22	39.76	61.05	40.03	60.87	40.29	60.70	40.56	73
74	62.06	40.30	61.89	40.57	61.71	40.84	61.53	41.11	74
75	62.90	40.85	62.72	41.12	62.54	41.40	62.36	41.67	75
76	63.74	41.39	63.56	41.67	63.38	41.95	63.19	42.22	76
77	64.58	41.94	64.39	42.22	64.21	42.50	64.02	42.78	77
78	65.42	42.48	65.23	42.77	65.04	43.05	64.85	43.33	78
79	66.25	43.03	66.07	43.32	65.88	43.60	65.69	43.89	79
80	67.09	43.57	66.90	43.86	66.71	44.15	66.52	44.45	80
81	67.93	44.12	67.74	44.41	67.54	44.71	67.35	45.00	81
82	68.77	44.66	68.58	44.96	68.38	45.26	68.18	45.56	82
83	69.61	45.20	69.41	45.51	69.21	45.81	69.01	46.11	83
84	70.45	45.75	70.25	46.05	70.05	46.36	69.84	46.67	84
85	71.29	46.29	71.08	46.60	70.88	46.91	70.67	47.22	85
86	72.13	46.84	71.92	47.15	71.71	47.47	71.51	47.78	86
87	72.96	47.38	72.76	47.70	72.55	48.02	72.34	48.33	87
88	73.80	47.93	73.59	48.25	73.38	48.57	73.17	48.89	88
89	74.64	48.47	74.43	48.80	74.22	49.12	74.00	49.45	89
90	75.48	49.02	75.27	49.35	75.05	49.67	74.83	50.00	90
91	76.32	49.56	76.10	49.89	75.88	50.23	75.66	50.56	91
92	77.16	50.11	76.94	50.44	76.72	50.78	76.50	51.11	92
93	78.00	50.65	77.77	50.99	77.55	51.33	77.33	51.67	93
94	78.83	51.20	78.61	51.54	78.39	51.88	78.16	52.22	94
95	79.67	51.74	79.45	52.09	79.22	52.43	78.99	52.78	95
96	80.51	52.29	80.28	52.64	80.05	52.99	79.82	53.33	96
97	81.35	52.83	81.12	53.18	80.89	53.54	80.65	53.89	97
98	82.19	53.37	81.96	53.73	81.72	54.09	81.48	54.45	98
99	83.03	53.92	82.79	54.28	82.55	54.64	82.32	55.00	99
100	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	57 Deg.		56½ Deg.		56¼ Deg.		56¼ Deg.		

Distance.	34 Deg.		34½ Deg.		34¾ Deg.		34¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.83	0.56	0.83	0.56	0.82	0.57	0.82	0.57	1
2	1.66	1.12	1.65	1.13	1.65	1.13	1.64	1.14	2
3	2.49	1.68	2.48	1.69	2.47	1.70	2.46	1.71	3
4	3.32	2.24	3.31	2.25	3.30	2.27	3.29	2.28	4
5	4.15	2.80	4.13	2.81	4.12	2.83	4.11	2.85	5
6	4.97	3.36	4.96	3.38	4.94	3.40	4.93	3.42	6
7	5.80	3.91	5.79	3.94	5.77	3.96	5.75	3.99	7
8	6.63	4.47	6.61	4.50	6.59	4.53	6.57	4.56	8
9	7.46	5.03	7.44	5.07	7.42	5.10	7.39	5.13	9
10	8.29	5.59	8.27	5.63	8.24	5.66	8.22	5.70	10
11	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27	11
12	9.95	6.71	9.92	6.75	9.89	6.80	9.86	6.84	12
13	10.78	7.27	10.75	7.32	10.71	7.36	10.69	7.41	13
14	11.61	7.83	11.57	7.88	11.54	7.93	11.50	7.98	14
15	12.44	8.39	12.40	8.44	12.36	8.50	12.32	8.55	15
16	13.26	8.95	13.23	9.00	13.19	9.06	13.15	9.12	16
17	14.09	9.51	14.05	9.57	14.01	9.63	13.97	9.69	17
18	14.92	10.07	14.88	10.13	14.83	10.20	14.79	10.26	18
19	15.75	10.62	15.71	10.69	15.66	10.76	15.61	10.83	19
20	16.58	11.18	16.53	11.26	16.48	11.33	16.43	11.40	20
21	17.41	11.74	17.36	11.82	17.31	11.89	17.25	11.97	21
22	18.24	12.30	18.18	12.38	18.13	12.46	18.08	12.54	22
23	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13.11	23
24	19.90	13.42	19.84	13.51	19.78	13.10	19.72	13.18	24
25	20.73	13.98	20.66	14.07	20.60	14.16	20.54	14.25	25
26	21.55	14.54	21.49	14.63	21.43	14.73	21.36	14.82	26
27	22.38	15.10	22.32	15.20	22.25	15.29	22.18	15.39	27
28	23.21	15.66	23.14	15.76	23.08	15.86	23.01	15.96	28
29	24.04	16.22	23.97	16.32	23.90	16.43	23.83	16.53	29
30	24.87	16.78	24.80	16.88	24.72	16.99	24.65	17.10	30
31	25.70	17.33	25.62	17.45	25.55	17.56	25.47	17.67	31
32	26.53	17.89	26.45	18.01	26.37	18.12	26.29	18.24	32
33	27.36	18.45	27.28	18.57	27.20	18.69	27.11	18.81	33
34	28.19	19.01	28.10	19.14	28.02	19.26	27.94	19.38	34
35	29.02	19.57	28.93	19.70	28.84	19.82	28.76	19.95	35
36	29.85	20.13	29.76	20.26	29.67	20.39	29.58	20.52	36
37	30.67	20.69	30.58	20.82	30.49	20.96	30.40	21.09	37
38	31.50	21.25	31.41	21.39	31.32	21.52	31.22	21.66	38
39	32.33	21.81	32.24	21.95	32.14	22.09	32.04	22.23	39
40	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80	40
41	33.99	22.93	33.89	23.07	33.79	23.22	33.69	23.37	41
42	34.82	23.49	34.72	23.64	34.61	23.79	34.51	23.94	42
43	35.65	24.05	35.54	24.20	35.44	24.36	35.33	24.51	43
44	36.48	24.60	36.37	24.76	36.26	24.92	36.15	25.08	44
45	37.31	25.16	37.20	25.33	37.09	25.49	36.97	25.65	45
46	38.14	25.72	38.02	25.89	37.91	26.05	37.80	26.22	46
47	38.96	26.28	38.85	26.45	38.73	26.62	38.62	26.79	47
48	39.79	26.84	39.68	27.01	39.56	27.19	39.44	27.36	48
49	40.62	27.40	40.50	27.58	40.38	27.75	40.26	27.93	49
50	41.45	27.96	41.33	28.14	41.21	28.32	41.08	28.50	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	56 Deg.		55½ Deg.		55½ Deg.		55½ Deg.		

TRAVERSE TABLE.

Distance.	34 Deg.		34½ Deg.		34¾ Deg.		34¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	42.28	28.52	42.16	28.70	42.03	28.89	41.90	29.07	51
52	43.11	29.08	42.98	29.27	42.85	29.45	42.73	29.64	52
53	43.94	29.64	43.81	29.83	43.68	30.02	43.55	30.21	53
54	44.77	30.20	44.64	30.39	44.50	30.59	44.37	30.78	54
55	45.60	30.76	45.46	30.95	45.33	31.15	45.19	31.35	55
56	46.43	31.31	46.29	31.52	46.15	31.72	46.01	31.92	56
57	47.26	31.87	47.12	32.08	46.98	32.29	46.83	32.49	57
58	48.08	32.43	47.94	32.64	47.80	32.85	47.66	33.06	58
59	48.91	32.99	48.77	33.21	48.62	33.42	48.48	33.63	59
60	49.74	33.55	49.60	33.77	49.45	33.98	49.30	34.20	60
61	50.57	34.11	50.42	34.33	50.27	34.55	50.12	34.77	61
62	51.40	34.67	51.25	34.89	51.10	35.12	50.94	35.34	62
63	52.23	35.23	52.08	35.46	51.92	35.68	51.76	35.91	63
64	53.06	35.79	52.90	36.02	52.74	36.25	52.59	36.48	64
65	53.89	36.35	53.73	36.58	53.57	36.82	53.41	37.05	65
66	54.72	36.91	54.55	37.15	54.39	37.38	54.23	37.62	66
67	55.55	37.46	55.38	37.71	55.22	37.95	55.05	38.19	67
68	56.37	38.03	56.21	38.27	56.04	38.52	55.87	38.76	68
69	57.20	38.58	57.03	38.83	56.86	39.08	56.69	39.33	69
70	58.03	39.14	57.86	39.40	57.69	39.65	57.52	39.90	70
71	58.86	39.70	58.69	39.96	58.51	40.21	58.34	40.47	71
72	59.69	40.26	59.51	40.52	59.34	40.78	59.16	41.04	72
73	60.52	40.82	60.34	41.08	60.16	41.35	59.98	41.61	73
74	61.35	41.38	61.17	41.65	60.99	41.91	60.80	42.18	74
75	62.18	41.94	61.99	42.21	61.81	42.48	61.62	42.75	75
76	63.01	42.50	62.82	42.77	62.63	43.05	62.45	43.32	76
77	63.84	43.06	63.65	43.34	63.46	43.61	63.27	43.89	77
78	64.66	43.62	64.47	43.90	64.28	44.18	64.09	44.46	78
79	65.49	44.18	65.30	44.46	65.11	44.75	64.91	45.03	79
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60	80
81	67.15	45.29	66.95	45.59	66.75	45.88	66.55	46.17	81
82	67.98	45.85	67.78	46.15	67.58	46.45	67.37	46.74	82
83	68.81	46.41	68.61	46.71	68.40	47.01	68.20	47.31	83
84	69.64	46.97	69.43	47.28	69.23	47.58	69.02	47.88	84
85	70.47	47.53	70.26	47.84	70.05	48.14	69.84	48.45	85
86	71.30	48.09	71.09	48.40	70.87	48.71	70.66	49.02	86
87	72.13	48.65	71.91	48.96	71.70	49.28	71.48	49.59	87
88	72.96	49.21	72.74	49.53	72.52	49.84	72.30	50.16	88
89	73.78	49.77	73.57	50.09	73.35	50.41	73.13	50.73	89
90	74.61	50.33	74.39	50.65	74.17	50.98	73.95	51.30	90
91	75.44	50.89	75.22	51.22	75.00	51.54	74.77	51.87	91
92	76.27	51.45	76.05	51.78	75.82	52.11	75.59	52.44	92
93	77.10	52.00	76.87	52.34	76.64	52.68	76.41	53.01	93
94	77.93	52.56	77.70	52.90	77.47	53.24	77.23	53.58	94
95	78.76	53.12	78.53	53.47	78.29	53.81	78.06	54.15	95
96	79.59	53.68	79.35	54.03	79.12	54.37	78.88	54.72	96
97	80.42	54.24	80.18	54.59	79.94	54.94	79.70	55.29	97
98	81.25	54.80	81.01	55.15	80.76	55.51	80.52	55.86	98
99	82.07	55.36	81.83	55.72	81.59	56.07	81.34	56.43	99
100	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	56 Deg.		55½ Deg.		55½ Deg.		55½ Deg.		

TRAVERSE TABLE.

Distance.	35 Deg.		35½ Deg.		35¾ Deg.		35¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.82	0.57	0.82	0.58	0.81	0.58	0.81	0.58	1
2	1.64	1.15	1.63	1.15	1.63	1.16	1.62	1.17	2
3	2.46	1.72	2.45	1.73	2.44	1.74	2.43	1.75	3
4	3.28	2.29	3.27	2.31	3.26	2.32	3.25	2.34	4
5	4.10	2.87	4.08	2.89	4.07	2.90	4.06	2.92	5
6	4.91	3.44	4.90	3.46	4.88	3.48	4.87	3.51	6
7	5.73	4.01	5.72	4.04	5.70	4.06	5.68	4.09	7
8	6.55	4.59	6.53	4.62	6.51	4.65	6.49	4.67	8
9	7.37	5.16	7.35	5.19	7.33	5.23	7.30	5.26	9
10	8.19	5.74	8.17	5.77	8.14	5.81	8.12	5.84	10
11	9.01	6.31	8.98	6.35	8.96	6.39	8.93	6.43	11
12	9.83	6.88	9.80	6.93	9.77	6.97	9.74	7.01	12
13	10.65	7.46	10.62	7.50	10.58	7.55	10.55	7.60	13
14	11.47	8.03	11.43	8.08	11.40	8.13	11.36	8.18	14
15	12.29	8.60	12.25	8.66	12.21	8.71	12.17	8.76	15
16	13.11	9.18	13.07	9.23	13.03	9.29	12.99	9.35	16
17	13.93	9.75	13.88	9.81	13.84	9.87	13.80	9.93	17
18	14.74	10.32	14.70	10.39	14.65	10.45	14.61	10.52	18
19	15.56	10.90	15.52	10.97	15.47	11.03	15.42	11.10	19
20	16.38	11.47	16.33	11.54	16.28	11.61	16.23	11.68	20
21	17.20	12.05	17.15	12.12	17.10	12.19	17.04	12.27	21
22	18.02	12.62	17.97	12.70	17.91	12.78	17.85	12.85	22
23	18.84	13.19	18.78	13.27	18.72	13.36	18.67	13.44	23
24	19.66	13.77	19.60	13.85	19.54	13.94	19.48	14.02	24
25	20.48	14.34	20.42	14.43	20.35	14.52	20.29	14.61	25
26	21.30	14.91	21.23	15.01	21.17	15.10	21.10	15.19	26
27	22.12	15.49	22.05	15.58	21.98	15.68	21.91	15.77	27
28	22.94	16.06	22.87	16.15	22.80	16.26	22.72	16.36	28
29	23.76	16.63	23.68	16.74	23.61	16.84	23.54	16.94	29
30	24.57	17.21	24.50	17.31	24.42	17.42	24.35	17.53	30
31	25.39	17.78	25.32	17.89	25.24	18.00	25.16	18.11	31
32	26.21	18.35	26.13	18.47	26.05	18.58	25.97	18.70	32
33	27.03	18.93	26.95	19.05	26.87	19.16	26.78	19.28	33
34	27.85	19.50	27.77	19.62	27.68	19.74	27.59	19.86	34
35	28.67	20.08	28.58	20.20	28.49	20.32	28.41	20.45	35
36	29.49	20.65	29.40	20.78	29.31	20.91	29.22	21.03	36
37	30.31	21.22	30.22	21.35	30.12	21.49	30.03	21.62	37
38	31.13	21.80	31.03	21.93	30.94	22.07	30.84	22.20	38
39	31.95	22.37	31.85	22.51	31.75	22.65	31.65	22.79	39
40	32.77	22.94	32.67	23.09	32.56	23.23	32.46	23.37	40
41	33.59	23.52	33.48	23.66	33.38	23.81	33.27	23.95	41
42	34.40	24.09	34.30	24.24	34.19	24.39	34.09	24.54	42
43	35.22	24.66	35.12	24.82	35.01	24.97	34.90	25.12	43
44	36.04	25.24	35.93	25.39	35.82	25.55	35.71	25.71	44
45	36.86	25.81	36.75	25.97	36.64	26.13	36.52	26.29	45
46	37.68	26.38	37.57	26.55	37.45	26.71	37.33	26.88	46
47	38.50	26.96	38.38	27.13	38.26	27.29	38.14	27.46	47
48	39.32	27.53	39.20	27.70	39.08	27.87	38.96	28.04	48
49	40.14	28.11	40.02	28.28	39.89	28.45	39.77	28.63	49
50	40.96	28.68	40.83	28.86	40.71	29.04	40.58	29.21	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	55 Deg.		54½ Deg.		54½ Deg.		54½ Deg.		

Distance.	35 Deg.		35½ Deg.		35¾ Deg.		35¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41.78	29.25	41.65	29.43	41.52	29.62	41.39	29.80	51
52	42.60	29.83	42.47	30.01	42.33	30.20	42.20	30.38	52
53	43.42	30.40	43.28	30.59	43.15	30.78	43.01	30.97	53
54	44.23	30.97	44.10	31.17	43.96	31.36	43.82	31.55	54
55	45.05	31.55	44.92	31.74	44.78	31.94	44.64	32.13	55
56	45.87	32.12	45.73	32.32	45.59	32.52	45.45	32.72	56
57	46.69	32.69	46.55	32.90	46.40	33.10	46.26	33.30	57
58	47.51	33.27	47.37	33.47	47.22	33.68	47.07	33.89	58
59	48.33	33.84	48.18	34.05	48.03	34.26	47.88	34.47	59
60	49.15	34.41	49.00	34.63	48.85	34.84	48.69	35.05	60
61	49.97	34.99	49.82	35.21	49.66	35.42	49.51	35.64	61
62	50.79	35.56	50.63	35.78	50.48	36.00	50.32	36.22	62
63	51.61	36.14	51.45	36.36	51.29	36.58	51.13	36.81	63
64	52.43	36.71	52.27	36.94	52.10	37.16	51.94	37.39	64
65	53.24	37.28	53.08	37.51	52.92	37.75	52.75	37.98	65
66	54.06	37.86	53.90	38.09	53.73	38.33	53.56	38.56	66
67	54.88	38.43	54.71	38.67	54.55	38.91	54.38	39.14	67
68	55.70	39.00	55.53	39.25	55.36	39.49	55.19	39.73	68
69	56.52	39.58	56.35	39.82	56.17	40.07	56.00	40.31	69
70	57.34	40.15	57.16	40.40	56.99	40.65	56.81	40.90	70
71	58.16	40.72	57.98	40.98	57.80	41.23	57.62	41.48	71
72	58.98	41.30	58.80	41.55	58.62	41.81	58.43	42.07	72
73	59.80	41.87	59.61	42.13	59.43	42.39	59.24	42.65	73
74	60.62	42.44	60.43	42.71	60.24	42.97	60.06	43.23	74
75	61.44	43.02	61.25	43.29	61.06	43.55	60.87	43.82	75
76	62.26	43.59	62.06	43.86	61.87	44.13	61.68	44.40	76
77	63.07	44.17	62.88	44.44	62.69	44.71	62.49	44.99	77
78	63.89	44.74	63.70	45.02	63.50	45.29	63.30	45.57	78
79	64.71	45.31	64.51	45.59	64.32	45.88	64.11	46.16	79
80	65.53	45.89	65.33	46.17	65.13	46.46	64.93	46.74	80
81	66.35	46.46	66.15	46.75	65.94	47.04	65.74	47.32	81
82	67.17	47.03	66.96	47.33	66.76	47.62	66.55	47.91	82
83	67.99	47.61	67.78	47.90	67.57	48.20	67.36	48.49	83
84	68.81	48.18	68.60	48.48	68.39	48.78	68.17	49.08	84
85	69.63	48.75	69.41	49.06	69.20	49.36	68.98	49.66	85
86	70.45	49.33	70.23	49.63	70.01	49.94	69.80	50.25	86
87	71.27	49.90	71.05	50.21	70.83	50.52	70.61	50.83	87
88	72.09	50.47	71.86	50.79	71.64	51.10	71.42	51.41	88
89	72.90	51.05	72.68	51.37	72.46	51.68	72.23	52.00	89
90	73.72	51.62	73.50	51.94	73.27	52.26	73.04	52.58	90
91	74.54	52.20	74.31	52.52	74.08	52.84	73.85	53.17	91
92	75.36	52.77	75.13	53.10	74.90	53.42	74.66	53.75	92
93	76.18	53.34	75.95	53.67	75.71	54.01	75.48	54.34	93
94	77.00	53.92	76.76	54.25	76.53	54.59	76.29	54.92	94
95	77.82	54.49	77.58	54.83	77.34	55.17	77.10	55.50	95
96	78.64	55.06	78.40	55.41	78.16	55.75	77.91	56.09	96
97	79.46	55.64	79.21	55.98	79.97	56.33	78.72	56.67	97
98	80.28	56.21	80.03	56.56	79.78	56.91	79.53	57.26	98
99	81.10	56.78	80.85	57.14	80.60	57.49	80.35	57.84	99
100	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	55 Deg.		54½ Deg.		54¼ Deg.		54¼ Deg.		



Distance.	36 Deg.		36½ Deg.		36¾ Deg.		36¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.81	0.59	0.81	0.59	0.80	0.59	0.80	0.60	1
2	1.62	1.18	1.61	1.18	1.61	1.19	1.60	1.20	2
3	2.43	1.76	2.42	1.77	2.41	1.78	2.40	1.79	3
4	3.24	2.35	3.23	2.37	3.22	2.38	3.20	2.39	4
5	4.05	2.94	4.03	2.96	4.02	2.97	4.01	2.99	5
6	4.85	3.53	4.84	3.55	4.82	3.57	4.81	3.59	6
7	5.66	4.11	5.65	4.14	5.63	4.16	5.61	4.19	7
8	6.47	4.70	6.45	4.73	6.43	4.76	6.41	4.79	8
9	7.28	5.29	7.26	5.32	7.23	5.35	7.21	5.38	9
10	8.09	5.88	8.06	5.91	8.03	5.95	8.01	5.98	10
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81	6.58	11
12	9.71	7.05	9.68	7.10	9.65	7.14	9.61	7.18	12
13	10.52	7.64	10.48	7.69	10.45	7.73	10.42	7.78	13
14	11.33	8.23	11.29	8.28	11.25	8.33	11.22	8.38	14
15	12.14	8.82	12.10	8.87	12.06	8.92	12.02	8.97	15
16	12.94	9.40	12.90	9.46	12.86	9.52	12.82	9.57	16
17	13.75	9.99	13.71	10.05	13.67	10.11	13.62	10.17	17
18	14.56	10.58	14.52	10.64	14.47	10.71	14.42	10.77	18
19	15.37	11.17	15.32	11.23	15.27	11.30	15.22	11.37	19
20	16.18	11.76	16.13	11.83	16.08	11.90	16.03	11.97	20
21	16.99	12.34	16.94	12.42	16.88	12.49	16.83	12.56	21
22	17.80	12.93	17.74	13.01	17.68	13.09	17.63	13.16	22
23	18.61	13.52	18.55	13.60	18.49	13.68	18.43	13.76	23
24	19.42	14.11	19.35	14.19	19.29	14.28	19.23	14.36	24
25	20.23	14.69	20.16	14.78	20.10	14.87	20.03	14.96	25
26	21.03	15.28	20.97	15.37	20.90	15.47	20.83	15.56	26
27	21.84	15.87	21.77	15.97	21.70	16.06	21.63	16.15	27
28	22.65	16.46	22.58	16.56	22.51	16.65	22.44	16.75	28
29	23.46	17.05	23.39	17.15	23.31	17.25	23.24	17.35	29
30	24.27	17.63	24.19	17.74	24.12	17.84	24.04	17.95	30
31	25.08	18.22	25.00	18.33	24.92	18.44	24.84	18.55	31
32	25.89	18.81	25.81	18.92	25.72	19.03	25.64	19.15	32
33	26.70	19.40	26.61	19.51	26.53	19.63	26.44	19.74	33
34	27.51	19.98	27.42	20.10	27.33	20.22	27.24	20.34	34
35	28.32	20.57	28.23	20.70	28.13	20.82	28.04	20.94	35
36	29.12	21.16	29.03	21.29	28.94	21.41	28.85	21.54	36
37	29.93	21.75	29.84	21.88	29.74	22.01	29.65	22.14	37
38	30.74	22.34	30.64	22.47	30.55	22.60	30.45	22.74	38
39	31.55	22.92	31.45	23.06	31.35	23.20	31.25	23.33	39
40	32.36	23.51	32.26	23.65	32.15	23.79	32.05	23.93	40
41	33.17	24.10	33.06	24.24	32.96	24.39	32.85	24.53	41
42	33.98	24.69	33.87	24.83	33.76	24.98	33.65	25.13	42
43	34.79	25.27	34.68	25.43	34.57	25.58	34.45	25.73	43
44	35.60	25.86	35.48	26.02	35.37	26.17	35.26	26.33	44
45	36.41	26.45	36.29	26.61	36.17	26.77	36.06	26.92	45
46	37.21	27.04	37.10	27.20	36.98	27.36	36.86	27.52	46
47	38.02	27.63	37.90	27.79	37.78	27.96	37.66	28.12	47
48	38.83	28.21	38.71	28.38	38.59	28.55	38.46	28.72	48
49	39.64	28.80	39.52	28.97	39.39	29.15	39.26	29.32	49
50	40.45	29.39	40.32	29.57	40.19	29.74	40.06	29.92	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	54 Deg.		53½ Deg.		53¼ Deg.		53¼ Deg.		

TRAVERSE TABLE.

Distance.	36 Deg.		36½ Deg.		36¾ Deg.		36¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	41.26	29.98	41.13	30.16	41.00	30.34	40.86	30.51	51
52	42.07	30.56	41.94	30.75	41.80	30.93	41.67	31.11	52
53	42.88	31.15	42.74	31.34	42.60	31.53	42.47	31.71	53
54	43.69	31.74	43.55	31.93	43.41	32.12	43.27	32.31	54
55	44.50	32.33	44.35	32.52	44.21	32.72	44.07	32.91	55
56	45.30	32.92	45.16	33.11	45.02	33.31	44.87	33.51	56
57	46.11	33.50	45.97	33.70	45.82	33.90	45.67	34.10	57
58	46.92	34.09	46.77	34.30	46.62	34.50	46.47	34.70	58
59	47.73	34.68	47.58	34.89	47.43	35.09	47.27	35.30	59
60	48.54	35.27	48.39	35.48	48.23	35.69	48.08	35.90	60
61	49.35	35.85	49.19	36.07	49.04	36.28	48.88	36.50	61
62	50.16	36.44	50.00	36.66	49.84	36.88	49.68	37.10	62
63	50.97	37.03	50.81	37.25	50.64	37.47	50.48	37.69	63
64	51.78	37.62	51.61	37.84	51.45	38.07	51.28	38.29	64
65	52.59	38.21	52.42	38.44	52.25	38.66	52.08	38.89	65
66	53.40	38.79	53.23	39.03	53.05	39.26	52.88	39.49	66
67	54.20	39.38	54.03	39.62	53.86	39.85	53.68	40.09	67
68	55.01	39.97	54.84	40.21	54.66	40.45	54.49	40.69	68
69	55.82	40.56	55.64	40.80	55.47	41.04	55.29	41.28	69
70	56.63	41.14	56.45	41.39	56.27	41.64	56.09	41.88	70
71	57.44	41.73	57.26	41.98	57.07	42.23	56.89	42.48	71
72	58.25	42.32	58.06	42.57	57.88	42.83	57.69	43.08	72
73	59.06	42.91	58.87	43.17	58.68	43.42	58.49	43.68	73
74	59.87	43.50	59.68	43.76	59.49	44.02	59.29	44.28	74
75	60.68	44.08	60.48	44.35	60.29	44.61	60.09	44.87	75
76	61.49	44.67	61.29	44.94	61.09	45.21	60.90	45.47	76
77	62.29	45.26	62.10	45.53	61.90	45.80	61.70	46.07	77
78	63.10	45.85	62.90	46.12	62.70	46.40	62.50	46.67	78
79	63.91	46.43	63.71	46.71	63.50	46.99	63.30	47.27	79
80	64.72	47.02	64.52	47.30	64.31	47.59	64.10	47.87	80
81	65.53	47.61	65.32	47.90	65.11	48.18	64.90	48.46	81
82	66.34	48.20	66.13	48.49	65.92	48.78	65.70	49.06	82
83	67.15	48.79	66.93	49.08	66.72	49.37	66.50	49.66	83
84	67.96	49.37	67.74	49.67	67.52	49.97	67.31	50.26	84
85	68.77	49.96	68.55	50.26	68.33	50.56	68.11	50.86	85
86	69.58	50.55	69.35	50.85	69.13	51.15	68.91	51.46	86
87	70.38	51.14	70.16	51.44	69.94	51.75	69.71	52.05	87
88	71.19	51.73	70.97	52.04	70.74	52.34	70.51	52.65	88
89	72.00	52.31	71.77	52.63	71.54	52.94	71.31	53.25	89
90	72.81	52.90	72.58	53.22	72.35	53.53	72.11	53.85	90
91	73.62	53.49	73.39	53.81	73.15	54.13	72.91	54.45	91
92	74.43	54.08	74.19	54.40	73.95	54.72	73.72	55.05	92
93	75.24	54.66	75.00	54.99	74.76	55.32	74.52	55.64	93
94	76.05	55.25	75.81	55.58	75.56	55.91	75.32	56.24	94
95	76.86	55.84	76.61	56.17	76.37	56.51	76.12	56.84	95
96	77.67	56.43	77.42	56.77	77.17	57.10	76.92	57.44	96
97	78.47	57.02	78.23	57.36	77.97	57.70	77.72	58.04	97
98	79.28	57.60	79.03	57.95	78.78	58.29	78.52	58.64	98
99	80.09	58.19	79.84	58.54	79.58	58.89	79.32	59.23	99
100	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	54 Deg.		53½ Deg.		53¼ Deg.		53¼ Deg.		

TRAVERSE TABLE.

Distance	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61	1
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22	2
3	2.40	1.80	2.39	1.82	2.38	1.83	2.37	1.84	3
4	3.20	2.40	3.18	2.42	3.17	2.43	3.16	2.45	4
5	3.99	3.00	3.98	3.03	3.97	3.04	3.95	3.06	5
6	4.79	3.60	4.78	3.63	4.76	3.65	4.74	3.67	6
7	5.59	4.20	5.57	4.24	5.55	4.26	5.53	4.29	7
8	6.38	4.80	6.37	4.84	6.35	4.87	6.33	4.90	8
9	7.18	5.40	7.16	5.45	7.14	5.48	7.12	5.51	9
10	7.97	6.00	7.96	6.05	7.93	6.09	7.91	6.12	10
11	8.77	6.60	8.75	6.66	8.73	6.70	8.70	6.73	11
12	9.56	7.20	9.55	7.25	9.52	7.31	9.49	7.35	12
13	10.36	7.80	10.35	7.87	10.31	7.91	10.28	7.96	13
14	11.15	8.40	11.14	8.47	11.11	8.52	11.07	8.57	14
15	11.95	9.00	11.94	9.08	11.90	9.13	11.86	9.18	15
16	12.74	9.60	12.74	9.68	12.69	9.74	12.65	9.80	16
17	13.54	10.20	13.53	10.29	13.49	10.35	13.44	10.41	17
18	14.33	10.80	14.33	10.90	14.28	10.96	14.23	11.02	18
19	15.13	11.40	15.12	11.50	15.07	11.57	15.02	11.63	19
20	15.92	12.00	15.92	12.11	15.87	12.18	15.81	12.24	20
21	16.72	12.60	16.71	12.71	16.66	12.78	16.60	12.86	21
22	17.51	13.20	17.51	13.32	17.45	13.39	17.40	13.47	22
23	18.31	13.80	18.31	13.92	18.25	14.00	18.19	14.08	23
24	19.10	14.40	19.10	14.53	19.04	14.61	18.98	14.69	24
25	19.90	15.00	19.89	15.13	19.83	15.22	19.77	15.31	25
26	20.69	15.60	20.69	15.74	20.63	15.83	20.56	15.92	26
27	21.49	16.20	21.48	16.34	21.42	16.44	21.35	16.53	27
28	22.28	16.80	22.28	16.95	22.21	17.05	22.14	17.14	28
29	23.08	17.40	23.07	17.55	23.01	17.65	22.93	17.75	29
30	23.87	18.00	23.87	18.16	23.80	18.26	23.72	18.37	30
31	24.67	18.60	24.66	18.77	24.59	18.87	24.51	18.98	31
32	25.46	19.20	25.46	19.37	25.39	19.48	25.30	19.59	32
33	26.26	19.80	26.25	19.97	26.18	20.09	26.09	20.20	33
34	27.05	20.40	27.05	20.58	26.97	20.70	26.88	20.82	34
35	27.85	21.00	27.84	21.19	27.77	21.31	27.67	21.43	35
36	28.64	21.60	28.64	21.79	28.56	21.92	28.46	22.04	36
37	29.44	22.20	29.43	22.40	29.35	22.52	29.26	22.65	37
38	30.23	22.80	30.23	23.00	30.15	23.13	30.05	23.26	38
39	31.03	23.40	31.02	23.61	30.94	23.74	30.84	23.88	39
40	31.82	24.00	31.82	24.21	31.73	24.35	31.63	24.49	40
41	32.62	24.60	32.61	24.82	32.53	24.96	32.42	25.10	41
42	33.41	25.20	33.41	25.42	33.32	25.57	33.21	25.71	42
43	34.21	25.80	34.20	26.03	34.11	26.18	34.00	26.33	43
44	35.00	26.40	34.99	26.63	34.91	26.79	34.79	26.94	44
45	35.80	27.00	35.79	27.24	35.70	27.39	35.58	27.55	45
46	36.59	27.60	36.58	27.84	36.49	28.00	36.37	28.16	46
47	37.39	28.20	37.38	28.45	37.29	28.61	37.16	28.77	47
48	38.18	28.80	38.17	29.05	38.08	29.22	37.95	29.39	48
49	38.98	29.40	38.97	29.66	38.87	29.83	38.74	30.00	49
50	39.77	30.00	39.76	30.26	39.67	30.44	39.53	30.61	50
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance
	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		

TRAVERSE TABLE.

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Distance.	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.73	30.69	40.60	30.87	40.46	31.05	40.33	31.22	51
52	41.53	31.29	41.39	31.48	41.25	31.66	41.12	31.84	52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06	54
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30	45.37	34.50	45.22	34.70	45.07	34.90	57
58	46.32	34.91	46.17	35.11	46.01	35.31	45.86	35.51	58
59	47.12	35.51	46.96	35.71	46.81	35.92	46.65	36.12	59
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73	60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62	49.52	37.31	49.35	37.53	49.19	37.74	49.02	37.96	62
63	50.31	37.91	50.15	38.13	49.98	38.35	49.81	38.57	63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79	65
66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41	66
67	53.51	40.32	53.33	40.55	53.15	40.79	52.98	41.02	67
68	54.31	40.92	54.13	41.16	53.95	41.40	53.77	41.63	68
69	55.11	41.53	54.92	41.77	54.74	42.00	54.56	42.24	69
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86	70
71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43.47	71
72	57.50	43.33	57.31	43.58	57.12	43.83	56.93	44.08	72
73	58.30	43.93	58.11	44.19	57.91	44.44	57.72	44.69	73
74	59.10	44.53	58.90	44.79	58.71	45.05	58.51	45.30	74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53	76
77	61.49	46.34	61.29	46.61	61.09	46.87	60.88	47.14	77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47.75	78
79	63.09	47.54	62.89	47.82	62.67	48.09	62.46	48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82	65.49	49.35	65.27	49.63	65.05	49.92	64.84	50.20	82
83	66.29	49.95	66.07	50.24	65.85	50.53	65.63	50.81	83
84	67.09	50.55	66.86	50.84	66.64	51.14	66.42	51.43	84
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04	85
86	68.68	51.76	68.46	52.06	68.23	52.35	68.00	52.65	86
87	69.48	52.36	69.25	52.66	69.02	52.96	68.79	53.26	87
88	70.28	52.96	70.05	53.27	69.82	53.57	69.58	53.88	88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10	90
91	72.68	54.77	72.44	55.08	72.20	55.40	71.95	55.71	91
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93	74.27	55.97	74.03	56.29	73.78	56.61	73.53	56.94	93
94	75.07	56.57	74.82	56.90	74.58	57.22	74.32	57.55	94
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16	95
96	76.67	57.77	76.42	58.11	76.16	58.44	75.91	58.77	96
97	77.47	58.38	77.21	58.71	76.96	59.05	76.70	59.39	97
98	78.27	58.98	78.01	59.32	77.75	59.66	77.49	60.00	98
99	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		

Distance.	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61	1
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22	2
3	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84	3
4	3.19	2.41	3.18	2.42	3.17	2.43	3.16	2.45	4
5	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06	5
6	4.79	3.61	4.78	3.63	4.76	3.65	4.74	3.67	6
7	5.59	4.21	5.57	4.24	5.55	4.26	5.53	4.29	7
8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90	8
9	7.19	5.42	7.16	5.45	7.14	5.48	7.12	5.51	9
10	7.99	6.02	7.96	6.05	7.93	6.09	7.91	6.12	10
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73	11
12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35	12
13	10.38	7.82	10.35	7.87	10.31	7.91	10.28	7.96	13
14	11.18	8.43	11.14	8.47	11.11	8.52	11.07	8.57	14
15	11.98	9.03	11.94	9.08	11.90	9.13	11.86	9.18	15
16	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80	16
17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41	17
18	14.38	10.83	14.33	10.90	14.28	10.96	14.23	11.02	18
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63	19
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24	20
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86	21
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	13.47	22
23	18.37	13.84	18.31	13.92	18.25	14.00	18.19	14.08	23
24	19.17	14.44	19.10	14.53	19.04	14.61	18.98	14.69	24
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31	25
26	20.76	15.65	20.70	15.74	20.63	15.83	20.56	15.92	26
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53	27
28	22.35	16.85	22.29	16.95	22.21	17.05	22.14	17.14	28
29	23.16	17.45	23.08	17.55	23.01	17.65	22.93	17.75	29
30	23.96	18.05	23.88	18.16	23.80	18.26	23.72	18.37	30
31	24.76	18.66	24.68	18.76	24.59	18.87	24.51	18.98	31
32	25.56	19.26	25.47	19.37	25.39	19.48	25.30	19.59	32
33	26.35	19.86	26.27	19.97	26.18	20.09	26.09	20.20	33
34	27.15	20.46	27.06	20.58	26.97	20.70	26.88	20.82	34
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43	35
36	28.75	21.67	28.66	21.79	28.56	21.92	28.46	22.04	36
37	29.55	22.27	29.45	22.40	29.35	22.52	29.26	22.65	37
38	30.35	22.87	30.25	23.00	30.15	23.13	30.05	23.26	38
39	31.15	23.47	31.04	23.61	30.94	23.74	30.84	23.88	39
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49	40
41	32.74	24.67	32.64	24.82	32.53	24.96	32.42	25.10	41
42	33.54	25.28	33.43	25.42	33.32	25.57	33.21	25.71	42
43	34.34	25.88	34.23	26.03	34.11	26.18	34.00	26.33	43
44	35.14	26.48	35.02	26.63	34.91	26.79	34.79	26.94	44
45	35.94	27.08	35.82	27.24	35.70	27.39	35.58	27.55	45
46	36.74	27.68	36.62	27.84	36.49	28.00	36.37	28.16	46
47	37.54	28.29	37.41	28.45	37.29	28.61	37.16	28.77	47
48	38.33	28.89	38.21	29.05	38.08	29.22	37.95	29.39	48
49	39.13	29.49	39.00	29.66	38.87	29.83	38.74	30.00	49
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		

TRAVERSE TABLE.

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Distance.	37 Deg.		37½ Deg.		37¾ Deg.		37¾ Deg.		Distance.
	Lat.	Dep.	I.at.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.73	30.69	40.60	30.87	40.46	31.05	40.33	31.22	51
52	41.53	31.29	41.39	31.48	41.25	31.66	41.12	31.84	52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06	54
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30	45.37	34.50	45.22	34.70	45.07	34.90	57
58	46.32	34.91	46.17	35.11	46.01	35.31	45.86	35.51	58
59	47.12	35.51	46.96	35.71	46.81	35.92	46.65	36.12	59
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73	60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62	49.52	37.31	49.35	37.53	49.19	37.74	49.02	37.96	62
63	50.31	37.91	50.15	38.13	49.98	38.35	49.81	38.57	63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79	65
66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41	66
67	53.51	40.32	53.33	40.55	53.15	40.79	52.98	41.02	67
68	54.31	40.92	54.13	41.16	53.95	41.40	53.77	41.63	68
69	55.11	41.53	54.92	41.77	54.74	42.00	54.56	42.24	69
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86	70
71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43.47	71
72	57.50	43.33	57.31	43.58	57.12	43.83	56.93	44.08	72
73	58.30	43.93	58.11	44.19	57.91	44.44	57.72	44.69	73
74	59.10	44.53	58.90	44.79	58.71	45.05	58.51	45.30	74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53	76
77	61.49	46.34	61.29	46.61	61.09	46.87	60.88	47.14	77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47.75	78
79	63.09	47.54	62.88	47.82	62.67	48.09	62.46	48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82	65.49	49.35	65.27	49.63	65.05	49.92	64.84	50.20	82
83	66.29	49.95	66.07	50.24	65.85	50.53	65.63	50.81	83
84	67.09	50.55	66.86	50.84	66.64	51.14	66.42	51.43	84
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04	85
86	68.68	51.76	68.46	52.06	68.23	52.35	68.00	52.65	86
87	69.48	52.36	69.25	52.66	69.02	52.96	68.79	53.26	87
88	70.28	52.96	70.05	53.27	69.82	53.57	69.58	53.88	88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10	90
91	72.68	54.77	72.44	55.08	72.20	55.40	71.95	55.71	91
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93	74.27	55.97	74.03	56.29	73.78	56.61	73.53	56.94	93
94	75.07	56.57	74.82	56.90	74.58	57.22	74.32	57.55	94
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16	95
96	76.67	57.77	76.42	58.11	76.16	58.44	75.91	58.77	96
97	77.47	58.38	77.21	58.71	76.96	59.05	76.70	59.39	97
98	78.27	58.98	78.01	59.32	77.75	59.66	77.49	60.00	98
99	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
Distance.	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61	1
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22	2
3	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84	3
4	3.19	2.41	3.18	2.42	3.17	2.43	3.16	2.45	4
5	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06	5
6	4.79	3.61	4.78	3.63	4.76	3.65	4.74	3.67	6
7	5.59	4.21	5.57	4.24	5.55	4.26	5.53	4.29	7
8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90	8
9	7.19	5.42	7.16	5.45	7.14	5.48	7.12	5.51	9
10	7.99	6.02	7.96	6.05	7.93	6.09	7.91	6.12	10
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73	11
12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35	12
13	10.38	7.82	10.35	7.87	10.31	7.91	10.28	7.96	13
14	11.18	8.43	11.14	8.47	11.11	8.52	11.07	8.57	14
15	11.98	9.03	11.94	9.08	11.90	9.13	11.86	9.18	15
16	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80	16
17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41	17
18	14.38	10.83	14.33	10.90	14.28	10.96	14.23	11.02	18
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63	19
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24	20
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86	21
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	13.47	22
23	18.37	13.84	18.31	13.92	18.25	14.00	18.19	14.08	23
24	19.17	14.44	19.10	14.53	19.04	14.61	18.98	14.69	24
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31	25
26	20.76	15.65	20.70	15.74	20.63	15.83	20.56	15.92	26
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53	27
28	22.35	16.85	22.29	16.95	22.21	17.05	22.14	17.14	28
29	23.16	17.45	23.08	17.55	23.01	17.65	22.93	17.75	29
30	23.96	18.05	23.88	18.16	23.80	18.26	23.72	18.37	30
31	24.76	18.66	24.68	18.76	24.59	18.87	24.51	18.98	31
32	25.56	19.26	25.47	19.37	25.39	19.48	25.30	19.59	32
33	26.35	19.86	26.27	19.97	26.18	20.09	26.09	20.20	33
34	27.15	20.46	27.06	20.58	26.97	20.70	26.88	20.82	34
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43	35
36	28.75	21.67	28.66	21.79	28.56	21.92	28.46	22.04	36
37	29.55	22.27	29.45	22.40	29.35	22.52	29.26	22.65	37
38	30.35	22.87	30.25	23.00	30.15	23.13	30.05	23.26	38
39	31.15	23.47	31.04	23.61	30.94	23.74	30.84	23.88	39
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49	40
41	32.74	24.67	32.64	24.82	32.53	24.96	32.42	25.10	41
42	33.54	25.28	33.43	25.42	33.32	25.57	33.21	25.71	42
43	34.34	25.88	34.23	26.03	34.11	26.18	34.00	26.33	43
44	35.14	26.48	35.02	26.63	34.91	26.79	34.79	26.94	44
45	35.94	27.08	35.82	27.24	35.70	27.39	35.58	27.55	45
46	36.74	27.68	36.62	27.84	36.49	28.00	36.37	28.16	46
47	37.54	28.29	37.41	28.45	37.29	28.61	37.16	28.77	47
48	38.33	28.89	38.21	29.05	38.08	29.22	37.95	29.39	48
49	39.13	29.49	39.00	29.66	38.87	29.83	38.74	30.00	49
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		

TRAVERSE TABLE.

77

Distance.	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.73	30.69	40.60	30.87	40.46	31.05	40.33	31.22	51
52	41.53	31.29	41.39	31.48	41.25	31.66	41.12	31.84	52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06	54
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30	45.37	34.50	45.22	34.70	45.07	34.90	57
58	46.32	34.91	46.17	35.11	46.01	35.31	45.86	35.51	58
59	47.12	35.51	46.96	35.71	46.81	35.92	46.65	36.12	59
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73	60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62	49.52	37.31	49.35	37.53	49.19	37.74	49.02	37.96	62
63	50.31	37.91	50.15	38.13	49.98	38.35	49.81	38.57	63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79	65
66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41	66
67	53.51	40.32	53.33	40.55	53.15	40.79	52.98	41.02	67
68	54.31	40.92	54.13	41.16	53.95	41.40	53.77	41.63	68
69	55.11	41.53	54.92	41.77	54.74	42.00	54.56	42.24	69
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86	70
71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43.47	71
72	57.50	43.33	57.31	43.58	57.12	43.83	56.93	44.08	72
73	58.30	43.93	58.11	44.19	57.91	44.44	57.72	44.69	73
74	59.10	44.53	58.90	44.79	58.71	45.05	58.51	45.30	74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53	76
77	61.49	46.34	61.29	46.61	61.09	46.87	60.88	47.14	77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47.75	78
79	63.09	47.54	62.88	47.82	62.67	48.09	62.46	48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82	65.49	49.35	65.27	49.63	65.05	49.92	64.84	50.20	82
83	66.29	49.95	66.07	50.24	65.85	50.53	65.63	50.81	83
84	67.09	50.55	66.86	50.84	66.64	51.14	66.42	51.43	84
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04	85
86	68.68	51.76	68.46	52.06	68.23	52.35	68.00	52.65	86
87	69.48	52.36	69.25	52.66	69.02	52.96	68.79	53.26	87
88	70.28	52.96	70.05	53.27	69.82	53.57	69.58	53.88	88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10	90
91	72.68	54.77	72.44	55.08	72.20	55.40	71.95	55.71	91
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93	74.27	55.97	74.03	56.29	73.78	56.61	73.53	56.94	93
94	75.07	56.57	74.82	56.90	74.58	57.22	74.32	57.55	94
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16	95
96	76.67	57.77	76.42	58.11	76.16	58.44	75.91	58.77	96
97	77.47	58.38	77.21	58.71	76.96	59.05	76.70	59.39	97
98	78.27	58.98	78.01	59.32	77.75	59.66	77.49	60.00	98
99	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		



Distance.	37 Deg.		37½ Deg.		37½ Deg.		37½ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61	1
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22	2
3	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84	3
4	3.19	2.41	3.18	2.42	3.17	2.43	3.16	2.45	4
5	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06	5
6	4.79	3.61	4.78	3.63	4.76	3.65	4.74	3.67	6
7	5.59	4.21	5.57	4.24	5.55	4.26	5.53	4.29	7
8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90	8
9	7.19	5.42	7.16	5.45	7.14	5.48	7.12	5.51	9
10	7.99	6.02	7.96	6.05	7.93	6.09	7.91	6.12	10
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73	11
12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35	12
13	10.38	7.82	10.35	7.87	10.31	7.91	10.28	7.96	13
14	11.18	8.43	11.14	8.47	11.11	8.52	11.07	8.57	14
15	11.98	9.03	11.94	9.08	11.90	9.13	11.86	9.18	15
16	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80	16
17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41	17
18	14.38	10.83	14.33	10.90	14.28	10.96	14.23	11.02	18
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63	19
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24	20
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86	21
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	13.47	22
23	18.37	13.84	18.31	13.92	18.25	14.00	18.19	14.08	23
24	19.17	14.44	19.10	14.53	19.04	14.61	18.98	14.69	24
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31	25
26	20.76	15.65	20.70	15.74	20.63	15.83	20.56	15.92	26
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53	27
28	22.36	16.85	22.29	16.95	22.21	17.05	22.14	17.14	28
29	23.16	17.45	23.08	17.55	23.01	17.65	22.93	17.75	29
30	23.96	18.05	23.88	18.16	23.80	18.26	23.72	18.37	30
31	24.76	18.66	24.68	18.76	24.59	18.87	24.51	18.98	31
32	25.56	19.26	25.47	19.37	25.39	19.48	25.30	19.59	32
33	26.35	19.86	26.27	19.97	26.18	20.09	26.09	20.20	33
34	27.15	20.46	27.06	20.58	26.97	20.70	26.88	20.82	34
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43	35
36	28.75	21.67	28.66	21.79	28.56	21.92	28.46	22.04	36
37	29.55	22.27	29.45	22.40	29.35	22.52	29.26	22.65	37
38	30.35	22.87	30.25	23.00	30.15	23.13	30.05	23.26	38
39	31.15	23.47	31.04	23.61	30.94	23.74	30.84	23.88	39
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49	40
41	32.74	24.67	32.64	24.82	32.53	24.96	32.42	25.10	41
42	33.54	25.28	33.43	25.42	33.32	25.57	33.21	25.71	42
43	34.34	25.88	34.23	26.03	34.11	26.18	34.00	26.33	43
44	35.14	26.48	35.02	26.63	34.91	26.79	34.79	26.94	44
45	35.94	27.08	35.82	27.24	35.70	27.39	35.58	27.55	45
46	36.74	27.68	36.62	27.84	36.49	28.00	36.37	28.16	46
47	37.54	28.29	37.41	28.45	37.29	28.61	37.16	28.77	47
48	38.33	28.89	38.21	29.05	38.08	29.22	37.95	29.39	48
49	39.13	29.49	39.00	29.66	38.87	29.83	38.74	30.00	49
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52½ Deg.		52½ Deg.		

TRAVERSE TABLE.

77

Distance.	37 Deg.		37½ Deg.		37¾ Deg.		37¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	40.73	30.69	40.60	30.87	40.46	31.05	40.33	31.22	51
52	41.53	31.29	41.39	31.48	41.25	31.66	41.12	31.84	52
53	42.33	31.90	42.19	32.08	42.05	32.26	41.91	32.45	53
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06	54
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67	55
56	44.72	33.70	44.58	33.90	44.43	34.09	44.28	34.28	56
57	45.52	34.30	45.37	34.50	45.22	34.70	45.07	34.90	57
58	46.32	34.91	46.17	35.11	46.01	35.31	45.86	35.51	58
59	47.12	35.51	46.96	35.71	46.81	35.92	46.65	36.12	59
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73	60
61	48.72	36.71	48.56	36.92	48.39	37.13	48.23	37.35	61
62	49.52	37.31	49.35	37.53	49.19	37.74	49.02	37.96	62
63	50.31	37.91	50.15	38.13	49.98	38.35	49.81	38.57	63
64	51.11	38.52	50.94	38.74	50.77	38.96	50.60	39.18	64
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79	65
66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41	66
67	53.51	40.32	53.33	40.55	53.15	40.79	52.98	41.02	67
68	54.31	40.92	54.13	41.16	53.95	41.40	53.77	41.63	68
69	55.11	41.53	54.92	41.77	54.74	42.00	54.56	42.24	69
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86	70
71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43.47	71
72	57.50	43.33	57.31	43.58	57.12	43.83	56.93	44.08	72
73	58.30	43.93	58.11	44.19	57.91	44.44	57.72	44.69	73
74	59.10	44.53	58.90	44.79	58.71	45.05	58.51	45.30	74
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92	75
76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53	76
77	61.49	46.34	61.29	46.61	61.09	46.87	60.88	47.14	77
78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47.75	78
79	63.09	47.54	62.88	47.82	62.67	48.09	62.46	48.37	79
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98	80
81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	49.59	81
82	65.49	49.35	65.27	49.63	65.05	49.92	64.84	50.20	82
83	66.29	49.95	66.07	50.24	65.85	50.53	65.63	50.81	83
84	67.09	50.55	66.86	50.84	66.64	51.14	66.42	51.43	84
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04	85
86	68.68	51.76	68.46	52.06	68.23	52.35	68.00	52.65	86
87	69.48	52.36	69.25	52.66	69.02	52.96	68.79	53.26	87
88	70.28	52.96	70.05	53.27	69.82	53.57	69.58	53.88	88
89	71.08	53.56	70.84	53.87	70.61	54.18	70.37	54.49	89
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10	90
91	72.68	54.77	72.44	55.08	72.20	55.40	71.95	55.71	91
92	73.47	55.37	73.23	55.69	72.99	56.01	72.74	56.32	92
93	74.27	55.97	74.03	56.29	73.78	56.61	73.53	56.94	93
94	75.07	56.57	74.82	56.90	74.58	57.22	74.32	57.55	94
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16	95
96	76.67	57.77	76.42	58.11	76.16	58.44	75.91	58.77	96
97	77.47	58.38	77.21	58.71	76.96	59.05	76.70	59.39	97
98	78.27	58.98	78.01	59.32	77.75	59.66	77.49	60.00	98
99	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	99
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	53 Deg.		52½ Deg.		52¼ Deg.		52¼ Deg.		

## TRAVERSE TABLE.

Distance.	38 Deg.		38½ Deg.		38¾ Deg.		39 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.79	0.62	0.79	0.62	0.78	0.62	0.78	0.63	1
2	1.58	1.23	1.57	1.24	1.57	1.24	1.56	1.25	2
3	2.36	1.85	2.36	1.86	2.35	1.87	2.34	1.88	3
4	3.15	2.46	3.14	2.48	3.13	2.49	3.12	2.50	4
5	3.94	3.08	3.93	3.10	3.91	3.11	3.90	3.13	5
6	4.73	3.69	4.71	3.71	4.70	3.74	4.68	3.76	6
7	5.52	4.31	5.50	4.33	5.48	4.36	5.46	4.38	7
8	6.30	4.93	6.28	4.95	6.26	4.98	6.24	5.01	8
9	7.09	5.54	7.07	5.57	7.04	5.60	7.02	5.63	9
10	7.88	6.16	7.85	6.19	7.83	6.23	7.80	6.26	10
11	8.67	6.77	8.64	6.81	8.61	6.85	8.58	6.89	11
12	9.46	7.39	9.42	7.43	9.39	7.47	9.36	7.51	12
13	10.24	8.00	10.21	8.05	10.17	8.09	10.14	8.14	13
14	11.03	8.62	10.99	8.67	10.96	8.72	10.92	8.76	14
15	11.82	9.23	11.78	9.29	11.74	9.34	11.70	9.39	15
16	12.61	9.85	12.57	9.91	12.52	9.96	12.48	10.01	16
17	13.40	10.47	13.35	10.52	13.30	10.58	13.26	10.64	17
18	14.18	11.08	14.14	11.14	14.09	11.21	14.04	11.27	18
19	14.97	11.70	14.92	11.76	14.87	11.83	14.82	11.89	19
20	15.76	12.31	15.71	12.38	15.65	12.45	15.60	12.52	20
21	16.55	12.93	16.49	13.00	16.43	13.07	16.38	13.14	21
22	17.34	13.54	17.28	13.62	17.22	13.70	17.16	13.77	22
23	18.12	14.16	18.06	14.24	18.00	14.32	17.94	14.40	23
24	18.91	14.78	18.85	14.86	18.78	14.94	18.72	15.02	24
25	19.70	15.39	19.63	15.48	19.57	15.56	19.50	15.65	25
26	20.49	16.01	20.42	16.10	20.35	16.19	20.28	16.27	26
27	21.28	16.62	21.20	16.72	21.13	16.81	21.06	16.90	27
28	22.06	17.24	21.99	17.33	21.91	17.43	21.84	17.53	28
29	22.85	17.85	22.77	17.95	22.70	18.05	22.62	18.15	29
30	23.64	18.47	23.56	18.57	23.48	18.68	23.40	18.78	30
31	24.43	19.09	24.34	19.19	24.26	19.30	24.18	19.40	31
32	25.22	19.70	25.13	19.81	25.04	19.92	24.96	20.03	32
33	26.00	20.32	25.92	20.43	25.83	20.54	25.74	20.66	33
34	26.79	20.93	26.70	21.05	26.61	21.17	26.52	21.28	34
35	27.58	21.55	27.49	21.67	27.39	21.79	27.30	21.91	35
36	28.37	22.16	28.27	22.29	28.17	22.41	28.08	22.53	36
37	29.16	22.78	29.06	22.91	28.96	23.03	28.86	23.16	37
38	29.94	23.40	29.84	23.53	29.74	23.66	29.64	23.79	38
39	30.73	24.01	30.63	24.14	30.52	24.28	30.42	24.41	39
40	31.52	24.63	31.41	24.76	31.30	24.90	31.20	25.04	40
41	32.31	25.24	32.20	25.38	32.09	25.52	31.98	25.66	41
42	33.10	25.86	32.98	26.00	32.87	26.15	32.76	26.29	42
43	33.88	26.47	33.77	26.62	33.65	26.77	33.53	26.91	43
44	34.67	27.09	34.55	27.24	34.43	27.39	34.31	27.54	44
45	35.46	27.70	35.34	27.86	35.22	28.01	35.09	28.17	45
46	36.25	28.32	36.12	28.48	36.00	28.64	35.87	28.79	46
47	37.04	28.94	36.91	29.10	36.78	29.26	36.65	29.42	47
48	37.82	29.55	37.70	29.72	37.57	29.88	37.43	30.04	48
49	38.61	30.17	38.48	30.34	38.35	30.50	38.21	30.67	49
50	39.40	30.78	39.27	30.95	39.13	31.13	38.99	31.30	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	52 Deg		51½ Deg.		51½ Deg.		51½ Deg.		



Distance.	39 Deg.		39¼ Deg.		39½ Deg.		39¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64	1
2	1.55	1.26	1.55	1.27	1.54	1.27	1.54	1.28	2
3	2.33	1.89	2.32	1.90	2.31	1.91	2.31	1.92	3
4	3.11	2.52	3.10	2.53	3.09	2.54	3.08	2.56	4
5	3.89	3.15	3.87	3.16	3.86	3.18	3.84	3.20	5
6	4.66	3.78	4.65	3.80	4.63	3.82	4.61	3.84	6
7	5.44	4.41	5.42	4.43	5.40	4.45	5.38	4.48	7
8	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12	8
9	6.99	5.66	6.97	5.69	6.94	5.72	6.92	5.75	9
10	7.77	6.29	7.74	6.33	7.72	6.36	7.69	6.39	10
11	8.55	6.92	8.52	6.96	8.49	7.00	8.46	7.03	11
12	9.33	7.55	9.29	7.59	9.26	7.63	9.23	7.67	12
13	10.10	8.18	10.07	8.23	10.03	8.27	9.99	8.31	13
14	10.88	8.81	10.84	8.86	10.80	8.91	10.76	8.95	14
15	11.66	9.44	11.62	9.49	11.57	9.54	11.53	9.59	15
16	12.43	10.07	12.39	10.12	12.35	10.18	12.30	10.23	16
17	13.21	10.70	13.16	10.76	13.12	10.81	13.07	10.87	17
18	13.99	11.33	13.94	11.39	13.89	11.45	13.84	11.51	18
19	14.77	11.96	14.71	12.02	14.66	12.09	14.61	12.15	19
20	15.54	12.59	15.49	12.65	15.43	12.72	15.38	12.79	20
21	16.32	13.22	16.26	13.29	16.20	13.36	16.15	13.43	21
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07	22
23	17.87	14.47	17.81	14.55	17.75	14.63	17.69	14.71	23
24	18.65	15.10	18.59	15.18	18.52	15.27	18.45	15.35	24
25	19.43	15.73	19.36	15.82	19.29	15.90	19.22	15.99	25
26	20.21	16.36	20.13	16.45	20.06	16.54	19.99	16.63	26
27	20.98	16.99	20.91	17.08	20.83	17.17	20.76	17.26	27
28	21.76	17.62	21.68	17.72	21.61	17.81	21.53	17.90	28
29	22.54	18.25	22.46	18.35	22.38	18.45	22.30	18.54	29
30	23.31	18.88	23.23	18.98	23.15	19.08	23.07	19.18	30
31	24.09	19.51	24.01	19.61	23.92	19.72	23.83	19.82	31
32	24.87	20.14	24.78	20.25	24.69	20.35	24.60	20.46	32
33	25.65	20.77	25.55	20.88	25.46	20.99	25.37	21.10	33
34	26.42	21.40	26.33	21.51	26.24	21.63	26.14	21.74	34
35	27.20	22.03	27.10	22.14	27.01	22.26	26.91	22.38	35
36	27.98	22.66	27.88	22.78	27.78	22.90	27.68	23.02	36
37	28.75	23.28	28.65	23.41	28.55	23.53	28.45	23.66	37
38	29.53	23.91	29.43	24.04	29.32	24.17	29.22	24.30	38
39	30.31	24.54	30.20	24.68	30.09	24.81	29.98	24.94	39
40	31.09	25.17	30.98	25.31	30.86	25.44	30.75	25.58	40
41	31.86	25.80	31.75	25.94	31.64	26.08	31.52	26.22	41
42	32.64	26.43	32.52	26.57	32.41	26.72	32.29	26.86	42
43	33.42	27.06	33.30	27.21	33.18	27.35	33.06	27.50	43
44	34.19	27.69	34.07	27.84	33.95	27.99	33.83	28.14	44
45	34.97	28.32	34.85	28.47	34.72	28.62	34.60	28.77	45
46	35.75	28.95	35.62	29.10	35.49	29.26	35.37	29.41	46
47	36.53	29.58	36.40	29.74	36.27	29.90	36.14	30.05	47
48	37.30	30.21	37.17	30.37	37.04	30.53	36.90	30.69	48
49	38.08	30.84	37.95	31.00	37.81	31.17	37.67	31.33	49
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	51 Deg.		50¼ Deg.		50½ Deg.		50¾ Deg.		

TRAVERSE TABLE.

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Distance.	39 Deg.		39½ Deg.		39¾ Deg.		39¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	39.63	32.10	39.49	32.27	39.35	32.44	39.21	32.61	51
52	40.41	32.72	40.27	32.90	40.12	33.08	39.98	33.25	52
53	41.19	33.35	41.04	33.53	40.90	33.71	40.75	33.89	53
54	41.97	33.98	41.82	34.17	41.67	34.35	41.52	34.53	54
55	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17	55
56	43.52	35.24	43.37	35.43	43.21	35.62	43.06	35.81	56
57	44.30	35.87	44.14	36.06	43.98	36.26	43.82	36.45	57
58	45.07	36.50	44.91	36.70	44.75	36.89	44.59	37.09	58
59	45.85	37.13	45.69	37.33	45.53	37.53	45.36	37.73	59
60	46.63	37.76	46.46	37.96	46.30	38.16	46.13	38.37	60
61	47.41	38.39	47.24	38.60	47.07	38.80	46.90	39.01	61
62	48.18	39.02	48.01	39.23	47.84	39.44	47.67	39.65	62
63	48.96	39.65	48.79	39.86	48.61	40.07	48.44	40.28	63
64	49.74	40.28	49.56	40.49	49.38	40.71	49.21	40.92	64
65	50.51	40.91	50.34	41.13	50.16	41.35	49.97	41.56	65
66	51.29	41.54	51.11	41.76	50.93	41.98	50.74	42.20	66
67	52.07	42.16	51.88	42.39	51.70	42.62	51.51	42.84	67
68	52.85	42.79	52.66	43.02	52.47	43.25	52.28	43.48	68
69	53.52	43.42	53.43	43.66	53.24	43.89	53.05	44.12	69
70	54.40	44.05	54.21	44.29	54.01	44.53	53.82	44.76	70
71	55.18	44.68	54.98	44.92	54.79	45.16	54.59	45.40	71
72	55.95	45.31	55.76	45.55	55.56	45.80	55.36	46.04	72
73	56.73	45.94	56.53	46.19	56.33	46.43	56.13	46.68	73
74	57.51	46.57	57.31	46.82	57.10	47.07	56.89	47.32	74
75	58.29	47.20	58.08	47.45	57.87	47.71	57.66	47.96	75
76	59.06	47.83	58.85	48.09	58.64	48.34	58.43	48.60	76
77	59.84	48.46	59.63	48.72	59.42	48.98	59.20	49.24	77
78	60.62	49.09	60.40	49.35	60.19	49.61	59.97	49.88	78
79	61.39	49.72	61.18	49.98	60.96	50.25	60.74	50.52	79
80	62.17	50.35	61.95	50.62	61.73	50.89	61.51	51.16	80
81	62.95	50.97	62.73	51.25	62.50	51.52	62.28	51.79	81
82	63.73	51.60	63.51	51.88	63.27	52.16	63.04	52.43	82
83	64.50	52.23	64.27	52.51	64.04	52.79	63.81	53.07	83
84	65.28	52.86	65.05	53.15	64.82	53.43	64.58	53.71	84
85	66.06	53.49	65.82	53.78	65.59	54.07	65.35	54.35	85
86	66.83	54.12	66.60	54.41	66.36	54.70	66.12	54.99	86
87	67.61	54.75	67.37	55.05	67.13	55.34	66.89	55.63	87
88	68.39	55.38	68.15	55.68	67.90	55.97	67.66	56.27	88
89	69.17	56.01	68.92	56.32	68.67	56.61	68.43	56.91	89
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20	57.55	90
91	70.72	57.27	70.47	57.58	70.22	57.88	69.96	58.19	91
92	71.50	57.90	71.24	58.21	70.99	58.52	70.73	58.83	92
93	72.27	58.53	72.02	58.84	71.76	59.16	71.50	59.47	93
94	73.05	59.16	72.79	59.47	72.53	59.79	72.27	60.11	94
95	73.83	59.79	73.57	60.11	73.30	60.43	73.04	60.75	95
96	74.61	60.41	74.34	60.74	74.08	61.06	73.81	61.39	96
97	75.38	61.04	75.12	61.37	74.85	61.70	74.58	62.03	97
98	76.16	61.67	75.89	62.01	75.62	62.34	75.35	62.66	98
99	76.94	62.30	76.66	62.64	76.39	62.97	76.12	63.30	99
100	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	51 Deg.		50½ Deg.		50¾ Deg.		50¾ Deg.		

TRAVERSE TABLE.

Distance.	40 Deg.		40½ Deg.		40¾ Deg.		40¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.77	0.64	0.76	0.65	0.76	0.65	0.76	0.65	1
2	1.53	1.29	1.53	1.29	1.52	1.30	1.52	1.31	2
3	2.30	1.93	2.29	1.94	2.28	1.95	2.27	1.96	3
4	3.06	2.57	3.05	2.58	3.04	2.60	3.03	2.61	4
5	3.83	3.21	3.82	3.23	3.80	3.25	3.79	3.26	5
6	4.60	3.86	4.58	3.88	4.56	3.90	4.55	3.92	6
7	5.36	4.50	5.34	4.52	5.32	4.55	5.30	4.57	7
8	6.13	5.14	6.11	5.17	6.08	5.20	6.06	5.22	8
9	6.89	5.79	6.87	5.82	6.84	5.84	6.82	5.87	9
10	7.66	6.43	7.63	6.46	7.60	6.49	7.58	6.53	10
11	8.43	7.07	8.40	7.11	8.36	7.14	8.33	7.18	11
12	9.19	7.71	9.16	7.75	9.12	7.79	9.09	7.83	12
13	9.96	8.36	9.92	8.40	9.89	8.44	9.85	8.49	13
14	10.72	9.00	10.69	9.05	10.65	9.09	10.61	9.14	14
15	11.49	9.64	11.45	9.69	11.41	9.74	11.36	9.79	15
16	12.26	10.28	12.21	10.34	12.17	10.39	12.12	10.44	16
17	13.02	10.93	12.97	10.98	12.93	11.04	12.88	11.10	17
18	13.79	11.57	13.74	11.63	13.69	11.69	13.64	11.75	18
19	14.55	12.21	14.50	12.28	14.45	12.34	14.39	12.40	19
20	15.32	12.86	15.26	12.92	15.21	12.99	15.15	13.06	20
21	16.09	13.50	16.03	13.57	15.97	13.64	15.91	13.71	21
22	16.85	14.14	16.79	14.21	16.73	14.29	16.67	14.36	22
23	17.62	14.78	17.55	14.86	17.49	14.94	17.42	15.01	23
24	18.39	15.43	18.32	15.51	18.25	15.59	18.18	15.67	24
25	19.15	16.07	19.08	16.15	19.01	16.24	18.94	16.32	25
26	19.92	16.71	19.84	16.80	19.77	16.89	19.70	16.97	26
27	20.68	17.36	20.61	17.45	20.53	17.54	20.45	17.62	27
28	21.45	18.00	21.37	18.09	21.29	18.18	21.21	18.28	28
29	22.22	18.64	22.13	18.74	22.05	18.83	21.97	18.93	29
30	22.98	19.28	22.90	19.38	22.81	19.48	22.73	19.58	30
31	23.75	19.93	23.66	20.03	23.57	20.13	23.48	20.24	31
32	24.51	20.57	24.42	20.68	24.33	20.78	24.24	20.89	32
33	25.28	21.21	25.19	21.32	25.09	21.43	25.00	21.54	33
34	26.05	21.85	25.95	21.97	25.85	22.08	25.76	22.19	34
35	26.81	22.50	26.71	22.61	26.61	22.73	26.51	22.85	35
36	27.58	23.14	27.48	23.26	27.37	23.38	27.27	23.50	36
37	28.34	23.78	28.24	23.91	28.13	24.03	28.03	24.15	37
38	29.11	24.43	29.00	24.55	28.90	24.68	28.79	24.80	38
39	29.88	25.07	29.77	25.20	29.66	25.33	29.54	25.46	39
40	30.64	25.71	30.53	25.84	30.42	25.98	30.30	26.11	40
41	31.41	26.35	31.29	26.49	31.18	26.63	31.06	26.76	41
42	32.17	27.00	32.06	27.14	31.94	27.28	31.82	27.42	42
43	32.94	27.64	32.82	27.78	32.70	27.93	32.58	28.07	43
44	33.71	28.28	33.58	28.43	33.46	28.58	33.33	28.72	44
45	34.47	28.93	34.35	29.08	34.22	29.23	34.09	29.37	45
46	35.24	29.57	35.11	29.72	34.98	29.87	34.85	30.03	46
47	36.00	30.21	35.87	30.37	35.74	30.52	35.61	30.68	47
48	36.77	30.85	36.64	31.01	36.50	31.17	36.36	31.33	48
49	37.54	31.50	37.40	31.66	37.26	31.82	37.12	31.99	49
50	38.30	32.14	38.16	32.31	38.02	32.47	37.88	32.64	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	50 Deg.		49½ Deg.		49¾ Deg.		49¼ Deg.		

TRAVERSE TABLE.

Distance.	40 Deg.		40½ Deg.		40¾ Deg.		40¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	39.07	32.78	38.92	32.95	38.78	33.12	38.64	33.29	51
52	39.83	33.42	39.69	33.60	39.54	33.77	39.39	33.94	52
53	40.60	34.07	40.45	34.24	40.30	34.42	40.15	34.60	53
54	41.37	34.71	41.21	34.89	41.06	35.07	40.91	35.25	54
55	42.13	35.35	41.98	35.54	41.82	35.72	41.67	35.90	55
56	42.90	36.00	42.74	36.18	42.58	36.37	42.42	36.55	56
57	43.66	36.64	43.50	36.83	43.34	37.02	43.18	37.21	57
58	44.43	37.28	44.27	37.48	44.10	37.67	43.94	37.86	58
59	45.20	37.92	45.03	38.12	44.86	38.32	44.70	38.51	59
60	45.96	38.57	45.79	38.77	45.62	38.97	45.45	39.17	60
61	46.73	39.21	46.56	39.41	46.38	39.62	46.21	39.82	61
62	47.49	39.85	47.32	40.06	47.15	40.27	46.97	40.47	62
63	48.26	40.50	48.08	40.71	47.91	40.92	47.73	41.12	63
64	49.03	41.14	48.85	41.35	48.67	41.56	48.48	41.78	64
65	49.79	41.78	49.61	42.00	49.43	42.21	49.24	42.43	65
66	50.56	42.42	50.37	42.64	50.19	42.86	50.00	43.08	66
67	51.32	43.07	51.14	43.29	50.95	43.51	50.76	43.73	67
68	52.09	43.71	51.90	43.94	51.71	44.16	51.51	44.39	68
69	52.86	44.35	52.66	44.58	52.47	44.81	52.27	45.04	69
70	53.62	45.00	53.43	45.23	53.23	45.46	53.03	45.69	70
71	54.39	45.64	54.19	45.87	53.99	46.11	53.79	46.35	71
72	55.16	46.28	54.95	46.52	54.75	46.76	54.54	47.00	72
73	55.92	46.92	55.72	47.17	55.51	47.41	55.30	47.65	73
74	56.69	47.57	56.48	47.81	56.27	48.06	56.06	48.30	74
75	57.45	48.21	57.24	48.46	57.03	48.71	56.82	48.96	75
76	58.22	48.85	58.01	49.11	57.79	49.36	57.57	49.61	76
77	58.99	49.49	58.77	49.75	58.55	50.01	58.33	50.26	77
78	59.75	50.14	59.53	50.40	59.31	50.66	59.09	50.92	78
79	60.52	50.78	60.30	51.04	60.07	51.31	59.85	51.57	79
80	61.28	51.42	61.06	51.69	60.83	51.96	60.61	52.22	80
81	62.05	52.07	61.82	52.34	61.59	52.61	61.36	52.87	81
82	62.82	52.71	62.59	52.98	62.35	53.25	62.12	53.53	82
83	63.58	53.35	63.35	53.63	63.11	53.90	62.88	54.18	83
84	64.35	53.99	64.11	54.27	63.87	54.55	63.64	54.83	84
85	65.11	54.64	64.87	54.92	64.63	55.20	64.39	55.48	85
86	65.88	55.28	65.64	55.57	65.39	55.85	65.15	56.14	86
87	66.65	55.92	66.40	56.21	66.16	56.50	65.91	56.79	87
88	67.41	56.57	67.16	56.86	66.92	57.15	66.67	57.44	88
89	68.18	57.21	67.93	57.50	67.68	57.80	67.42	58.10	89
90	68.94	57.85	68.69	58.15	68.44	58.45	68.18	58.75	90
91	69.71	58.49	69.45	58.80	69.20	59.10	68.94	59.40	91
92	70.48	59.14	70.22	59.44	69.96	59.75	69.70	60.05	92
93	71.24	59.78	70.98	60.09	70.72	60.40	70.45	60.71	93
94	72.01	60.42	71.74	60.74	71.48	61.05	71.21	61.36	94
95	72.77	61.06	72.51	61.38	72.24	61.70	71.97	62.01	95
96	73.54	61.71	73.27	62.03	73.00	62.35	72.73	62.66	96
97	74.31	62.35	74.03	62.67	73.76	63.00	73.48	63.32	97
98	75.07	62.99	74.80	63.32	74.52	63.65	74.24	63.97	98
99	75.84	63.64	75.56	63.97	75.28	64.30	75.00	64.62	99
100	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	100
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	50 Deg.		49½ Deg.		49¼ Deg.		49¼ Deg.		



TRAVERSE TABLE.

Distance.	41 Deg.		41¼ Deg.		41½ Deg.		41¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.75	0.66	0.75	0.66	0.75	0.66	0.75	0.67	1
2	1.51	1.31	1.50	1.32	1.50	1.33	1.49	1.33	2
3	2.26	1.97	2.26	1.98	2.25	1.99	2.24	2.00	3
4	3.02	2.62	3.01	2.64	3.00	2.65	2.98	2.66	4
5	3.77	3.28	3.76	3.30	3.74	3.31	3.73	3.33	5
6	4.53	3.94	4.51	3.96	4.49	3.98	4.48	4.00	6
7	5.28	4.59	5.26	4.62	5.24	4.64	5.22	4.66	7
8	6.04	5.25	6.01	5.27	5.99	5.30	5.97	5.33	8
9	6.79	5.90	6.77	5.93	6.74	5.96	6.71	5.99	9
10	7.55	6.56	7.52	6.59	7.49	6.63	7.46	6.66	10
11	8.30	7.22	8.27	7.25	8.24	7.29	8.21	7.32	11
12	9.06	7.87	9.02	7.91	8.99	7.95	8.95	7.99	12
13	9.81	8.53	9.77	8.57	9.74	8.61	9.70	8.66	13
14	10.57	9.18	10.53	9.23	10.49	9.28	10.44	9.32	14
15	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99	15
16	12.08	10.50	12.03	10.55	11.98	10.60	11.94	10.65	16
17	12.83	11.15	12.78	11.21	12.73	11.26	12.68	11.32	17
18	13.58	11.81	13.53	11.87	13.48	11.93	13.43	11.99	18
19	14.34	12.47	14.28	12.53	14.23	12.59	14.18	12.65	19
20	15.09	13.12	15.04	13.19	14.98	13.25	14.92	13.32	20
21	15.85	13.78	15.79	13.85	15.73	13.91	15.67	13.98	21
22	16.60	14.43	16.54	14.51	16.48	14.58	16.41	14.65	22
23	17.36	15.09	17.29	15.16	17.23	15.24	17.16	15.32	23
24	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98	24
25	18.87	16.40	18.80	16.48	18.72	16.57	18.65	16.65	25
26	19.62	17.06	19.55	17.14	19.47	17.23	19.40	17.31	26
27	20.38	17.71	20.30	17.80	20.22	17.89	20.14	17.98	27
28	21.13	18.37	21.05	18.46	20.97	18.55	20.89	18.64	28
29	21.89	19.03	21.80	19.12	21.72	19.22	21.64	19.31	29
30	22.64	19.68	22.56	19.78	22.47	19.88	22.38	19.98	30
31	23.40	20.34	23.31	20.44	23.22	20.54	23.13	20.64	31
32	24.15	20.99	24.06	21.10	23.97	21.20	23.87	21.31	32
33	24.91	21.65	24.81	21.76	24.72	21.87	24.62	21.97	33
34	25.66	22.31	25.56	22.42	25.46	22.53	25.37	22.64	34
35	26.41	22.96	26.31	23.08	26.21	23.19	26.11	23.31	35
36	27.17	23.62	27.07	23.74	26.96	23.85	26.86	23.97	36
37	27.92	24.27	27.82	24.40	27.71	24.52	27.60	24.64	37
38	28.68	24.93	28.57	25.06	28.46	25.18	28.35	25.30	38
39	29.43	25.59	29.32	25.71	29.21	25.84	29.10	25.97	39
40	30.19	26.24	30.07	26.37	29.96	26.50	29.84	26.64	40
41	30.94	26.90	30.83	27.03	30.71	27.17	30.59	27.30	41
42	31.70	27.55	31.58	27.69	31.46	27.83	31.33	27.97	42
43	32.45	28.21	32.33	28.35	32.21	28.49	32.08	28.63	43
44	33.21	28.87	33.08	29.01	32.95	29.16	32.83	29.30	44
45	33.96	29.52	33.83	29.67	33.70	29.82	33.57	29.97	45
46	34.72	30.18	34.58	30.33	34.45	30.48	34.32	30.63	46
47	35.47	30.83	35.34	30.99	35.20	31.14	35.06	31.30	47
48	36.23	31.49	36.09	31.65	35.95	31.81	35.81	31.96	48
49	36.98	32.15	36.84	32.31	36.70	32.47	36.56	32.63	49
50	37.74	32.80	37.59	32.97	37.45	33.13	37.30	33.29	50

Distance.	49 Deg.		48¾ Deg.		48½ Deg.		48¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

TRAVERSE TABLE.

Distance.	41 Deg.		41½ Deg.		41¾ Deg.		41¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	38.49	33.46	38.34	33.63	38.20	33.79	38.05	33.96	51
52	39.24	34.12	39.10	34.29	38.95	34.46	38.79	34.63	52
53	40.00	34.77	39.85	34.95	39.69	35.12	39.54	35.29	53
54	40.75	35.43	40.60	35.60	40.44	35.78	40.29	35.96	54
55	41.51	36.08	41.35	36.26	41.19	36.44	41.03	36.62	55
56	42.26	36.74	42.10	36.92	41.94	37.11	41.78	37.29	56
57	43.02	37.40	42.85	37.58	42.69	37.77	42.53	37.96	57
58	43.77	38.05	43.61	38.24	43.44	38.43	43.27	38.62	58
59	44.53	38.71	44.36	38.90	44.19	39.09	44.02	39.29	59
60	45.28	39.36	45.11	39.56	44.94	39.76	44.76	39.95	60
61	46.04	40.02	45.86	40.22	45.69	40.42	45.51	40.62	61
62	46.79	40.68	46.61	40.88	46.44	41.08	46.26	41.28	62
63	47.55	41.33	47.37	41.54	47.18	41.75	47.00	41.95	63
64	48.30	41.99	48.12	42.20	47.93	42.41	47.75	42.62	64
65	49.06	42.64	48.87	42.86	48.68	43.07	48.49	43.28	65
66	49.81	43.30	49.62	43.52	49.43	43.73	49.24	43.95	66
67	50.57	43.96	50.37	44.18	50.18	44.40	49.99	44.61	67
68	51.32	44.61	51.13	44.84	50.93	45.06	50.73	45.28	68
69	52.07	45.27	51.88	45.49	51.68	45.72	51.48	45.95	69
70	52.83	45.92	52.63	46.15	52.43	46.38	52.22	46.61	70
71	53.58	46.58	53.38	46.81	53.18	47.05	52.97	47.28	71
72	54.34	47.24	54.13	47.47	53.92	47.71	53.72	47.94	72
73	55.09	47.89	54.88	48.13	54.67	48.37	54.46	48.61	73
74	55.85	48.55	55.64	48.79	55.42	49.03	55.21	49.28	74
75	56.60	49.20	56.39	49.45	56.17	49.70	55.95	49.94	75
76	57.36	49.86	57.14	50.11	56.92	50.36	56.70	50.61	76
77	58.11	50.52	57.89	50.77	57.67	51.02	57.45	51.27	77
78	58.87	51.17	58.64	51.43	58.42	51.68	58.19	51.94	78
79	59.62	51.83	59.40	52.09	59.17	52.35	58.94	52.60	79
80	60.38	52.48	60.15	52.75	59.92	53.01	59.68	53.27	80
81	61.13	53.14	60.90	53.41	60.67	53.67	60.43	53.94	81
82	61.89	53.80	61.65	54.07	61.41	54.33	61.18	54.60	82
83	62.64	54.45	62.40	54.73	62.16	55.00	61.92	55.27	83
84	63.40	55.11	63.15	55.38	62.91	55.66	62.67	55.93	84
85	64.15	55.76	63.91	56.04	63.66	56.32	63.41	56.60	85
86	64.90	56.42	64.66	56.70	64.41	56.99	64.16	57.27	86
87	65.66	57.08	65.41	57.36	65.16	57.65	64.91	57.93	87
88	66.41	57.73	66.16	58.02	65.91	58.31	65.65	58.60	88
89	67.17	58.39	66.91	58.68	66.66	58.97	66.40	59.26	89
90	67.92	59.05	67.67	59.34	67.41	59.64	67.15	59.93	90
91	68.68	59.70	68.42	60.00	68.15	60.30	67.89	60.60	91
92	69.43	60.36	69.17	60.66	68.90	60.96	68.64	61.26	92
93	70.19	61.01	69.92	61.32	69.65	61.62	69.38	61.93	93
94	70.94	61.67	70.67	61.98	70.40	62.29	70.13	62.59	94
95	71.70	62.33	71.43	62.64	71.15	62.95	70.88	63.26	95
96	72.45	62.98	72.18	63.30	71.90	63.61	71.62	63.92	96
97	73.21	63.64	72.93	63.96	72.65	64.27	72.37	64.59	97
98	73.96	64.29	73.68	64.62	73.40	64.94	73.11	65.26	98
99	74.72	64.95	74.43	65.28	74.15	65.60	73.86	65.92	99
100	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	100

Distance.	49 Deg.		48¾ Deg.		48½ Deg.		48¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	42 Deg.		42½ Deg.		42¾ Deg.		43 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.74	0.67	0.74	0.67	0.74	0.68	0.73	0.68	1
2	1.49	1.34	1.48	1.34	1.47	1.35	1.47	1.36	2
3	2.23	2.01	2.22	2.02	2.21	2.03	2.20	2.04	3
4	2.97	2.68	2.96	2.69	2.95	2.70	2.94	2.72	4
5	3.72	3.35	3.70	3.36	3.69	3.38	3.67	3.39	5
6	4.46	4.01	4.44	4.03	4.42	4.05	4.41	4.07	6
7	5.20	4.68	5.18	4.71	5.16	4.73	5.14	4.75	7
8	5.95	5.35	5.92	5.38	5.90	5.40	5.87	5.43	8
9	6.69	6.02	6.66	6.05	6.64	6.08	6.61	6.11	9
10	7.43	6.69	7.40	6.72	7.37	6.76	7.34	6.79	10
11	8.17	7.36	8.14	7.40	8.11	7.43	8.08	7.47	11
12	8.92	8.03	8.88	8.07	8.85	8.11	8.81	8.15	12
13	9.66	8.70	9.62	8.74	9.58	8.78	9.55	8.82	13
14	10.40	9.37	10.36	9.41	10.32	9.46	10.28	9.50	14
15	11.15	10.04	11.10	10.09	11.06	10.13	11.01	10.18	15
16	11.89	10.71	11.84	10.76	11.80	10.81	11.75	10.86	16
17	12.63	11.38	12.58	11.43	12.53	11.48	12.48	11.54	17
18	13.38	12.04	13.32	12.10	13.27	12.16	13.22	12.22	18
19	14.12	12.71	14.06	12.77	14.01	12.84	13.95	12.90	19
20	14.86	13.38	14.80	13.45	14.75	13.51	14.69	13.58	20
21	15.61	14.05	15.54	14.12	15.48	14.19	15.42	14.25	21
22	16.35	14.72	16.28	14.79	16.22	14.86	16.16	14.93	22
23	17.09	15.39	17.02	15.46	16.96	15.54	16.89	15.61	23
24	17.84	16.06	17.77	16.14	17.69	16.21	17.62	16.29	24
25	18.58	16.73	18.51	16.81	18.43	16.89	18.36	16.97	25
26	19.32	17.40	19.25	17.48	19.17	17.57	19.09	17.65	26
27	20.06	18.07	19.99	18.15	19.91	18.24	19.83	18.33	27
28	20.81	18.74	20.73	18.83	20.64	18.92	20.56	19.01	28
29	21.55	19.40	21.47	19.50	21.38	19.59	21.30	19.69	29
30	22.29	20.07	22.21	20.17	22.12	20.27	22.03	20.36	30
31	23.04	20.74	22.95	20.84	22.86	20.94	22.76	21.04	31
32	23.78	21.41	23.69	21.52	23.59	21.62	23.50	21.72	32
33	24.52	22.08	24.43	22.19	24.33	22.29	24.23	22.40	33
34	25.27	22.75	25.17	22.86	25.07	22.97	24.97	23.08	34
35	26.01	23.42	25.91	23.53	25.80	23.65	25.70	23.76	35
36	26.75	24.09	26.65	24.21	26.54	24.32	26.44	24.44	36
37	27.50	24.76	27.39	24.88	27.28	25.00	27.17	25.12	37
38	28.24	25.43	28.13	25.55	28.02	25.67	27.90	25.79	38
39	28.98	26.10	28.87	26.22	28.75	26.35	28.64	26.47	39
40	29.73	26.77	29.61	26.89	29.49	27.02	29.37	27.15	40
41	30.47	27.43	30.35	27.57	30.23	27.70	30.11	27.83	41
42	31.21	28.10	31.09	28.24	30.97	28.37	30.84	28.51	42
43	31.96	28.77	31.83	28.91	31.70	29.05	31.58	29.19	43
44	32.70	29.44	32.57	29.58	32.44	29.73	32.31	29.87	44
45	33.44	30.11	33.31	30.26	33.18	30.40	33.04	30.55	45
46	34.18	30.78	34.05	30.93	33.91	31.08	33.78	31.22	46
47	34.93	31.45	34.79	31.60	34.65	31.75	34.51	31.90	47
48	35.67	32.12	35.53	32.27	35.39	32.43	35.25	32.58	48
49	36.41	32.79	36.27	32.95	36.13	33.10	35.98	33.26	49
50	37.16	33.46	37.01	33.62	36.86	33.78	36.72	33.94	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	48 Deg.		47½ Deg.		47¼ Deg.		47¼ Deg.		



TRAVERSE TABLE.

Distance.	43 Deg.		43½ Deg.		43¾ Deg.		43¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.73	0.68	0.73	0.69	0.73	0.69	0.72	0.69	1
2	1.46	1.36	1.46	1.37	1.45	1.38	1.44	1.38	2
3	2.19	2.05	2.19	2.06	2.18	2.07	2.17	2.07	3
4	2.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77	4
5	3.66	3.41	3.64	3.43	3.63	3.44	3.61	3.46	5
6	4.39	4.09	4.37	4.11	4.35	4.13	4.33	4.15	6
7	5.12	4.77	5.10	4.80	5.08	4.82	5.06	4.84	7
8	5.85	5.46	5.83	5.48	5.80	5.51	5.78	5.53	8
9	6.58	6.14	6.56	6.17	6.53	6.20	6.50	6.22	9
10	7.31	6.92	7.28	6.85	7.25	6.88	7.22	6.92	10
11	8.04	7.50	8.01	7.54	7.98	7.57	7.95	7.61	11
12	8.78	8.18	8.74	8.22	8.70	8.26	8.67	8.30	12
13	9.51	8.87	9.47	8.91	9.43	8.95	9.39	8.99	13
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68	14
15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37	15
16	11.70	10.91	11.65	10.96	11.61	11.01	11.56	11.06	16
17	12.43	11.59	12.38	11.65	12.33	11.70	12.28	11.76	17
18	13.16	12.28	13.11	12.33	13.06	12.39	13.00	12.45	18
19	13.90	12.96	13.84	13.02	13.78	13.08	13.72	13.14	19
20	14.63	13.64	14.57	13.70	14.51	13.77	14.45	13.83	20
21	15.36	14.32	15.30	14.39	15.23	14.46	15.17	14.52	21
22	16.09	15.00	16.02	15.07	15.96	15.14	15.89	15.21	22
23	16.82	15.69	16.75	15.76	16.68	15.83	16.61	15.90	23
24	17.55	16.37	17.48	16.44	17.41	16.52	17.34	16.60	24
25	18.28	17.05	18.21	17.13	18.13	17.21	18.06	17.29	25
26	19.02	17.73	18.94	17.81	18.86	17.90	18.78	17.98	26
27	19.75	18.41	19.67	18.50	19.59	18.59	19.50	18.67	27
28	20.48	19.10	20.39	19.19	20.31	19.27	20.23	19.36	28
29	21.21	19.78	21.12	19.87	21.04	19.96	20.95	20.05	29
30	21.94	20.46	21.85	20.56	21.76	20.65	21.67	20.75	30
31	22.67	21.14	22.58	21.24	22.49	21.34	22.39	21.44	31
32	23.40	21.82	23.31	21.93	23.21	22.03	23.12	22.13	32
33	24.13	22.51	24.04	22.61	23.94	22.72	23.84	22.82	33
34	24.87	23.19	24.76	23.30	24.66	23.40	24.56	23.51	34
35	25.60	23.87	25.49	23.98	25.39	24.09	25.28	24.20	35
36	26.33	24.55	26.22	24.67	26.11	24.78	26.01	24.89	36
37	27.06	25.23	26.95	25.35	26.84	25.47	26.73	25.59	37
38	27.79	25.92	27.68	26.04	27.56	26.16	27.45	26.28	38
39	28.52	26.60	28.41	26.72	28.29	26.85	28.17	26.97	39
40	29.25	27.28	29.13	27.41	29.01	27.53	28.89	27.66	40
41	29.99	27.96	29.86	28.09	29.74	28.22	29.62	28.35	41
42	30.72	28.64	30.59	28.78	30.47	28.91	30.34	29.04	42
43	31.45	29.33	31.32	29.46	31.19	29.60	31.06	29.74	43
44	32.18	30.01	32.05	30.15	31.92	30.29	31.78	30.43	44
45	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12	45
46	33.64	31.37	33.51	31.52	33.37	31.66	33.23	31.81	46
47	34.37	32.05	34.23	32.20	34.09	32.35	33.95	32.50	47
48	35.10	32.74	34.96	32.89	34.82	33.04	34.67	33.19	48
49	35.84	33.42	35.69	33.57	35.54	33.73	35.40	33.88	49
50	36.57	34.10	36.42	34.26	36.27	34.42	36.12	34.58	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	47 Deg.		46½ Deg.		46½ Deg.		46½ Deg.		

Distance.	43 Deg.		43½ Deg.		43¾ Deg.		43¼ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
51	37.30	34.78	37.15	34.94	36.99	35.11	36.84	35.27	51
52	38.03	35.46	37.88	35.63	37.72	35.79	37.56	35.96	52
53	38.76	36.15	38.60	36.31	38.44	36.48	38.29	36.65	53
54	39.49	36.83	39.33	37.00	39.17	37.17	39.01	37.84	54
55	40.22	37.51	40.06	37.69	39.90	37.86	39.73	38.03	55
56	40.96	38.19	40.79	38.37	40.62	38.55	40.45	38.72	56
57	41.69	38.87	41.52	39.06	41.35	39.24	41.17	39.42	57
58	42.42	39.56	42.25	39.74	42.07	39.92	41.90	40.11	58
59	43.15	40.24	42.97	40.43	42.80	40.61	42.62	40.80	59
60	43.88	40.92	43.70	41.11	43.52	41.30	43.34	41.49	60
61	44.61	41.60	44.43	41.80	44.25	41.99	44.06	42.18	61
62	45.34	42.28	45.16	42.48	44.97	42.68	44.79	42.87	62
63	46.08	42.97	45.89	43.17	45.70	43.37	45.51	43.57	63
64	46.81	43.65	46.62	43.85	46.42	44.05	46.23	44.26	64
65	47.54	44.33	47.34	44.54	47.15	44.74	46.95	44.95	65
66	48.27	45.01	48.07	45.22	47.87	45.43	47.68	45.64	66
67	49.00	45.69	48.80	45.91	48.60	46.12	48.40	46.33	67
68	49.73	46.38	49.53	46.59	49.33	46.81	49.12	47.02	68
69	50.46	47.06	50.26	47.28	50.05	47.50	49.84	47.71	69
70	51.19	47.74	50.99	47.96	50.78	48.18	50.57	48.41	70
71	51.93	48.42	51.71	48.65	51.50	48.87	51.29	49.10	71
72	52.66	49.10	52.44	49.33	52.23	49.56	52.01	49.79	72
73	53.39	49.79	53.17	50.02	52.95	50.25	52.73	50.48	73
74	54.12	50.47	53.90	50.70	53.68	50.94	53.45	51.17	74
75	54.85	51.15	54.63	51.39	54.40	51.63	54.18	51.86	75
76	55.58	51.83	55.36	52.07	55.13	52.31	54.90	52.55	76
77	56.31	52.51	56.08	52.76	55.85	53.00	55.62	53.25	77
78	57.05	53.20	56.81	53.44	56.58	53.69	56.34	53.94	78
79	57.78	53.88	57.54	54.13	57.30	54.38	57.07	54.63	79
80	58.51	54.56	58.27	54.81	58.03	55.07	57.79	55.32	80
81	59.24	55.24	59.00	55.50	58.76	55.76	58.51	56.01	81
82	59.97	55.92	59.73	56.18	59.48	56.45	59.23	56.70	82
83	60.70	56.61	60.45	56.87	60.21	57.13	59.96	57.40	83
84	61.43	57.29	61.18	57.56	60.93	57.82	60.68	58.09	84
85	62.17	57.97	61.91	58.24	61.66	58.51	61.40	58.78	85
86	62.90	58.65	62.64	58.93	62.38	59.20	62.12	59.47	86
87	63.63	59.33	63.37	59.61	63.11	59.89	62.85	60.16	87
88	64.36	60.02	64.10	60.30	63.83	60.58	63.57	60.85	88
89	65.09	60.70	64.82	60.98	64.56	61.26	64.29	61.54	89
90	65.82	61.38	65.55	61.67	65.28	61.95	65.01	62.24	90
91	66.55	62.06	66.28	62.35	66.01	62.64	65.74	62.93	91
92	67.28	62.74	67.01	63.04	66.73	63.33	66.46	63.62	92
93	68.02	63.43	67.74	63.72	67.46	64.02	67.18	64.31	93
94	68.75	64.11	68.47	64.41	68.19	64.71	67.90	65.00	94
95	69.48	64.79	69.20	65.09	68.91	65.39	68.62	65.69	95
96	70.21	65.47	69.92	65.78	69.64	66.08	69.35	66.39	96
97	70.94	66.15	70.65	66.46	70.36	66.77	70.07	67.08	97
98	71.67	66.84	71.37	67.15	71.09	67.46	70.79	67.77	98
99	72.40	67.52	72.11	67.83	71.81	68.15	71.51	68.46	99
100	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	100
Distance.	47 Deg.		46½ Deg.		46¼ Deg.		46¼ Deg.		Distance.
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	

Distance.	44 Deg.		44½ Deg.		44½ Deg.		44½ Deg.		45 Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0.72	0.69	0.72	0.70	0.71	0.70	0.71	0.71	0.71	0.71	1
2	1.44	1.39	1.43	1.40	1.43	1.40	1.42	1.41	1.41	1.41	2
3	2.16	2.08	2.15	2.09	2.14	2.10	2.13	2.11	2.12	2.12	3
4	2.88	2.78	2.87	2.79	2.85	2.80	2.84	2.82	2.83	2.83	4
5	3.60	3.47	3.58	3.49	3.57	3.50	3.55	3.52	3.54	3.54	5
6	4.32	4.17	4.30	4.19	4.28	4.21	4.26	4.22	4.24	4.24	6
7	5.04	4.86	5.01	4.88	4.99	4.91	4.97	4.93	4.95	4.95	7
8	5.75	5.56	5.73	5.58	5.71	5.61	5.68	5.63	5.66	5.66	8
9	6.47	6.25	6.45	6.28	6.42	6.31	6.39	6.34	6.36	6.36	9
10	7.19	6.95	7.16	6.98	7.13	7.01	7.10	7.01	7.07	7.07	10
11	7.91	7.64	7.88	7.68	7.85	7.71	7.81	7.74	7.78	7.78	11
12	8.63	8.34	8.60	8.37	8.56	8.41	8.52	8.45	8.49	8.49	12
13	9.35	9.03	9.31	9.07	9.27	9.11	9.23	9.15	9.19	9.19	13
14	10.07	9.73	10.03	9.77	9.99	9.81	9.94	9.86	9.90	9.90	14
15	10.79	10.42	10.74	10.47	10.70	10.51	10.65	10.56	10.61	10.61	15
16	11.51	11.11	11.46	11.16	11.41	11.21	11.36	11.26	11.31	11.31	16
17	12.23	11.81	12.18	11.86	12.13	11.92	12.07	11.97	12.02	12.02	17
18	12.95	12.50	12.89	12.56	12.84	12.62	12.78	12.67	12.73	12.73	18
19	13.67	13.20	13.61	13.26	13.55	13.32	13.49	13.38	13.43	13.43	19
20	14.39	13.89	14.33	13.96	14.26	14.02	14.20	14.08	14.14	14.14	20
21	15.11	14.59	15.04	14.65	14.98	14.72	14.91	14.78	14.85	14.85	21
22	15.83	15.28	15.76	15.35	15.69	15.42	15.62	15.49	15.56	15.56	22
23	16.54	15.98	16.47	16.05	16.40	16.12	16.33	16.19	16.26	16.26	23
24	17.26	16.67	17.19	16.75	17.12	16.82	17.04	16.90	16.97	16.97	24
25	17.98	17.37	17.91	17.44	17.83	17.52	17.75	17.60	17.68	17.68	25
26	18.70	18.06	18.62	18.14	18.54	18.22	18.46	18.30	18.38	18.38	26
27	19.42	18.76	19.34	18.84	19.26	18.92	19.17	19.01	19.09	19.09	27
28	20.14	19.45	20.06	19.54	19.97	19.63	19.89	19.71	19.80	19.80	28
29	20.86	20.15	20.77	20.24	20.68	20.33	20.60	20.42	20.51	20.51	29
30	21.58	20.84	21.49	20.93	21.40	21.03	21.31	21.12	21.21	21.21	30
31	22.30	21.53	22.21	21.63	22.11	21.73	22.02	21.82	21.92	21.92	31
32	23.02	22.23	22.92	22.33	22.82	22.43	22.73	22.53	22.63	22.63	32
33	23.74	22.92	23.64	23.03	23.54	23.13	23.44	23.23	23.33	23.33	33
34	24.46	23.62	24.35	23.72	24.25	23.83	24.15	23.94	24.04	24.04	34
35	25.18	24.31	25.07	24.42	24.96	24.53	24.86	24.64	24.75	24.75	35
36	25.90	25.01	25.79	25.12	25.68	25.23	25.57	25.34	25.46	25.46	36
37	26.62	25.70	26.50	25.82	26.39	25.93	26.28	26.05	26.16	26.16	37
38	27.33	26.40	27.22	26.52	27.10	26.63	26.99	26.75	26.87	26.87	38
39	28.05	27.09	27.94	27.21	27.82	27.34	27.70	27.46	27.58	27.58	39
40	28.77	27.79	28.65	27.91	28.53	28.04	28.41	28.16	28.28	28.28	40
41	29.49	28.48	29.37	28.61	29.24	28.74	29.12	28.86	28.99	28.99	41
42	30.21	29.18	30.08	29.31	29.96	29.44	29.83	29.57	29.70	29.70	42
43	30.93	29.87	30.80	30.00	30.67	30.14	30.54	30.27	30.41	30.41	43
44	31.65	30.56	31.52	30.70	31.38	30.84	31.25	30.98	31.11	31.11	44
45	32.37	31.26	32.23	31.40	32.10	31.54	31.96	31.68	31.82	31.82	45
46	33.09	31.95	32.95	32.10	32.81	32.24	32.67	32.38	32.53	32.53	46
47	33.81	32.65	33.67	32.80	33.52	32.94	33.38	33.09	33.23	33.23	47
48	34.53	33.34	34.38	33.49	34.24	33.64	34.09	33.79	33.94	33.94	48
49	35.25	34.04	35.10	34.19	34.95	34.34	34.80	34.50	34.65	34.65	49
50	35.97	34.73	35.82	34.89	35.66	35.05	35.51	35.20	35.36	35.36	50
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Distance.
	46 Deg.		45½ Deg.		45½ Deg.		45½ Deg.		45 Deg.		





## A TABLE OF RHUMBS.

SHOWING

THE DEGREES, MINUTES, AND SECONDS, THAT EVERY POINT AND QUARTER-POINT OF THE COMPASS MAKES WITH THE MERIDIAN.

NORTH.		Pts.	qr.	°	'	"	Pts.	qr.	SOUTH.	
		0	1	2	48	45	0	1		
		1	2	5	37	30	0	2		
		0	3	8	26	15	0	3		
N by E.	N. by W.	1	0	11	15	0	1	0	S. by E.	S. by W.
		1	1	14	3	45	1	1		
		1	2	16	52	30	1	2		
		1	3	19	41	15	1	3		
N.N.E.	N.N.W.	2	0	22	30	0	2	0	S.S.E.	S.S.W.
		2	1	25	18	45	2	1		
		2	2	28	7	30	2	2		
		2	3	30	56	15	2	3		
N.E. by N.	N.W. by N.	3	0	33	45	0	3	0	S.E. by S.	S.W. by S.
		3	1	36	33	45	3	1		
		3	2	39	22	30	3	2		
		3	3	42	11	15	3	3		
N.E.	N.W.	4	0	45	0	0	4	0	S.E.	S.W.
		4	1	47	48	45	4	1		
		4	2	50	37	30	4	2		
		4	3	53	26	15	4	3		
N.E. by E.	N.W. by W.	5	0	56	15	0	5	0	S.E. by E.	S.W. by W.
		5	1	59	3	45	5	1		
		5	2	61	52	30	5	2		
		5	3	64	41	15	5	3		
E.N.E.	W.N.W.	6	0	67	30	0	6	0	E.S.E.	W.S.W.
		6	1	70	18	45	6	1		
		6	2	73	7	30	6	2		
		6	3	75	56	15	6	3		
E. by N.	W. by N.	7	0	78	45	0	7	0	E. by S.	W. by S.
		7	1	81	33	45	7	1		
		7	2	84	22	30	7	2		
		7	3	87	11	15	7	3		
East.	West.	8	0	90	0	0	8	0	East.	West.

WORKMAN'S TABLE, FOR CORRECTING THE MIDDLE LATITUDE. 93

Mid. Lat.	30	40	50	60	70	80	90	100	110
15	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 19	0 23
16	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 18	0 22
17	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 21
18	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 20
19	0 02	0 03	0 04	0 06	0 07	0 10	0 13	0 16	0 19
20	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
21	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
22	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 17
23	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 17
24	0 02	0 03	0 04	0 06	0 07	0 09	0 11	0 14	0 16
25	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
26	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
27	0 02	0 03	0 04	0 05	0 07	0 08	0 11	0 14	0 16
28	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
29	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
30	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
31	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
32	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
33	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
34	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
35	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
36	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
37	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
38	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
39	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
40	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
41	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
42	0 02	0 03	0 04	0 05	0 06	0 08	0 10	0 13	0 15
43	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
44	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
45	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
46	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
47	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
48	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 16
49	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
50	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
51	0 02	0 03	0 04	0 05	0 07	0 09	0 11	0 14	0 17
52	0 02	0 03	0 04	0 05	0 07	0 09	0 12	0 15	0 18
53	0 02	0 03	0 04	0 06	0 07	0 09	0 12	0 15	0 18
54	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 19
55	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 19
56	0 02	0 03	0 04	0 06	0 08	0 10	0 13	0 16	0 20
57	0 02	0 03	0 04	0 06	0 08	0 11	0 14	0 17	0 20
58	0 02	0 03	0 04	0 06	0 09	0 11	0 14	0 17	0 21
59	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 18	0 22
60	0 02	0 03	0 04	0 06	0 09	0 12	0 15	0 19	0 23
61	0 02	0 03	0 05	0 07	0 09	0 12	0 15	0 19	0 23
62	0 02	0 03	0 05	0 07	0 09	0 12	0 16	0 20	0 24
63	0 02	0 04	0 05	0 07	0 09	0 13	0 16	0 20	0 24
64	0 02	0 04	0 06	0 08	0 09	0 13	0 17	0 21	0 25
65	0 02	0 04	0 06	0 08	0 10	0 13	0 17	0 21	0 25
66	0 02	0 04	0 06	0 08	0 10	0 14	0 18	0 22	0 26
67	0 02	0 04	0 06	0 08	0 11	0 15	0 18	0 23	0 27
68	0 02	0 04	0 06	0 08	0 11	0 15	0 19	0 24	0 28
69	0 02	0 05	0 06	0 09	0 12	0 16	0 20	0 25	0 30
70	0 03	0 05	0 06	0 09	0 13	0 17	0 21	0 26	0 31
71	0 04	0 06	0 07	0 09	0 13	0 18	0 22	0 27	0 33
72	0 04	0 06	0 08	0 10	0 14	0 19	0 23	0 29	0 35

94 WORKMAN'S TABLE, FOR CORRECTING THE MIDDLE LATITUDE.

Mid. Lat.	12°	13°	14°	15°	16°	17°	18°	19°	20°
0	0	0	0	0	0	0	0	0	0
15	0 27	0 31	0 35	0 40	0 45	0 51	0 58	1 06	1 14
16	0 26	0 30	0 34	0 38	0 43	0 49	0 56	1 03	1 11
17	0 25	0 28	0 32	0 37	0 42	0 48	0 54	1 01	1 08
18	0 24	0 27	0 31	0 36	0 41	0 46	0 52	0 58	1 06
19	0 23	0 26	0 30	0 34	0 40	0 45	0 50	0 56	1 03
20	0 22	0 25	0 29	0 33	0 38	0 43	0 48	0 54	1 00
21	0 21	0 25	0 29	0 33	0 37	0 42	0 47	0 53	0 58
22	0 20	0 24	0 28	0 32	0 36	0 41	0 46	0 51	0 56
23	0 20	0 24	0 28	0 32	0 36	0 40	0 45	0 50	0 55
24	0 19	0 23	0 27	0 31	0 35	0 39	0 44	0 48	0 53
25	0 19	0 23	0 27	0 31	0 35	0 39	0 43	0 47	0 52
26	0 19	0 22	0 26	0 30	0 34	0 38	0 42	0 47	0 52
27	0 19	0 22	0 26	0 30	0 33	0 38	0 42	0 46	0 51
28	0 18	0 21	0 25	0 29	0 33	0 37	0 41	0 46	0 51
29	0 18	0 21	0 25	0 29	0 32	0 36	0 41	0 45	0 50
30	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
31	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
32	0 18	0 21	0 25	0 28	0 31	0 36	0 41	0 45	0 50
33	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
34	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
35	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
36	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
37	0 18	0 21	0 24	0 27	0 31	0 35	0 40	0 44	0 49
38	0 18	0 21	0 24	0 27	0 31	0 36	0 40	0 45	0 50
39	0 18	0 21	0 25	0 28	0 32	0 36	0 41	0 45	0 50
40	0 18	0 22	0 25	0 28	0 32	0 36	0 41	0 45	0 50
41	0 18	0 22	0 25	0 28	0 32	0 37	0 41	0 45	0 50
42	0 18	0 22	0 26	0 29	0 33	0 37	0 42	0 46	0 51
43	0 19	0 23	0 26	0 30	0 34	0 38	0 42	0 46	0 51
44	0 19	0 23	0 27	0 30	0 34	0 38	0 43	0 47	0 52
45	0 19	0 23	0 27	0 31	0 35	0 39	0 43	0 47	0 52
46	0 19	0 23	0 27	0 31	0 35	0 39	0 44	0 48	0 53
47	0 20	0 23	0 27	0 31	0 35	0 40	0 44	0 49	0 54
48	0 20	0 23	0 27	0 31	0 35	0 40	0 45	0 50	0 55
49	0 21	0 24	0 28	0 32	0 36	0 41	0 45	0 51	0 57
50	0 21	0 24	0 28	0 32	0 36	0 41	0 46	0 52	0 58
51	0 21	0 24	0 28	0 32	0 37	0 42	0 47	0 53	0 59
52	0 22	0 25	0 29	0 33	0 37	0 42	0 48	0 54	1 00
53	0 22	0 25	0 29	0 33	0 38	0 43	0 49	0 55	1 01
54	0 23	0 26	0 30	0 34	0 39	0 44	0 50	0 56	1 02
55	0 23	0 26	0 30	0 35	0 40	0 45	0 51	0 57	1 03
56	0 24	0 27	0 31	0 36	0 41	0 46	0 52	0 58	1 04
57	0 24	0 28	0 32	0 37	0 42	0 48	0 54	1 00	1 06
58	0 25	0 29	0 33	0 38	0 44	0 50	0 55	1 02	1 08
59	0 26	0 30	0 34	0 39	0 45	0 51	0 57	1 04	1 10
60	0 27	0 31	0 35	0 40	0 46	0 52	0 59	1 06	1 13
61	0 27	0 31	0 36	0 41	0 47	0 54	1 01	1 08	1 15
62	0 28	0 32	0 37	0 42	0 49	0 56	1 03	1 10	1 18
63	0 29	0 33	0 39	0 44	0 51	0 58	1 05	1 12	1 21
64	0 29	0 34	0 40	0 46	0 53	1 00	1 07	1 14	1 24
65	0 30	0 35	0 41	0 48	0 55	1 02	1 09	1 17	1 27
66	0 31	0 37	0 43	0 50	0 58	1 05	1 12	1 21	1 31
67	0 33	0 38	0 45	0 53	1 00	1 07	1 16	1 25	1 35
68	0 34	0 40	0 48	0 55	1 02	1 10	1 19	1 30	1 39
69	0 36	0 42	0 50	0 58	1 05	1 13	1 23	1 34	1 44
70	0 38	0 44	0 52	1 00	1 08	1 17	1 28	1 39	1 50
71	0 40	0 46	0 55	1 03	1 12	1 22	1 32	1 44	1 56
72	0 42	0 49	0 58	1 06	1 16	1 27	1 38	1 50	2 04

TABLE OF MERIDIONAL PARTS.

M.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°
0	0	60	120	180	240	300	361	421	482	542	603	664	725	787
1	1	61	121	181	241	301	362	422	483	543	604	665	726	788
2	2	62	122	182	242	302	363	423	484	544	605	666	727	789
3	3	63	123	183	243	303	364	424	485	545	606	667	728	790
4	4	64	124	184	244	304	365	425	486	546	607	668	729	791
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792
6	6	66	126	186	246	306	367	427	488	548	609	670	731	793
7	7	67	127	187	247	307	368	428	489	549	610	671	732	794
8	8	68	128	188	248	308	369	429	490	550	611	672	733	795
9	9	69	129	189	249	309	370	430	491	551	612	673	735	796
10	10	70	130	190	250	310	371	431	492	552	613	664	736	797
11	11	71	131	191	251	311	372	432	493	553	614	675	737	798
12	12	72	132	192	252	312	373	433	494	554	615	676	738	799
13	13	73	133	193	253	313	374	434	495	555	616	677	739	800
14	14	74	134	194	254	314	375	435	496	556	617	678	740	801
15	15	75	135	195	255	315	376	436	497	557	618	679	741	802
16	16	76	136	196	256	316	377	437	498	558	619	680	742	803
17	17	77	137	197	257	317	378	438	499	559	620	681	743	804
18	18	78	138	198	258	318	379	439	500	560	621	682	744	805
19	19	79	139	199	259	319	380	440	501	561	622	683	745	806
20	20	80	140	200	260	320	381	441	502	562	623	684	746	807
21	21	81	141	201	261	321	382	442	503	563	624	685	747	808
22	22	82	142	202	262	322	383	443	504	564	625	687	748	809
23	23	83	143	203	263	323	384	444	505	565	626	688	749	810
24	24	84	144	204	264	324	385	445	506	567	627	689	750	811
25	25	85	145	205	265	325	386	446	507	568	628	690	751	812
26	26	86	146	206	266	326	387	447	508	569	629	691	752	813
27	27	87	147	207	267	327	388	448	509	570	631	692	753	815
28	28	88	148	208	268	328	389	449	510	571	632	693	754	816
29	29	89	149	209	269	330	390	450	511	572	633	694	755	817
30	30	90	150	210	270	331	391	451	512	573	634	695	756	818
31	31	91	151	211	271	332	392	452	513	574	635	696	757	819
32	32	92	152	212	272	333	393	453	514	575	636	697	758	820
33	33	93	153	213	273	334	394	454	515	576	637	698	759	821
34	34	94	154	214	274	335	395	455	516	577	638	699	760	822
35	35	95	155	215	275	336	396	456	517	578	639	700	761	823
36	36	96	156	216	276	337	397	457	518	579	640	701	762	824
37	37	97	157	217	277	338	398	458	519	580	641	702	763	825
38	38	98	158	218	278	339	399	459	520	581	642	703	764	826
39	39	99	159	219	279	340	400	460	521	582	643	704	765	827
40	40	100	160	220	280	341	401	461	522	583	644	705	766	828
41	41	101	161	221	281	342	402	462	523	584	645	706	767	829
42	42	102	162	222	282	343	403	463	524	585	646	707	768	830
43	43	103	163	223	283	344	404	464	525	586	647	708	769	831
44	44	104	164	224	284	345	405	465	526	587	648	709	770	832
45	45	105	165	225	285	346	406	466	527	588	649	710	771	833
46	46	106	166	226	286	347	407	467	528	589	650	711	772	834
47	47	107	167	227	287	348	408	468	529	590	651	712	773	835
48	48	108	168	228	288	349	409	469	530	591	652	713	774	836
49	49	109	169	229	289	350	410	470	531	592	653	714	775	837
50	50	110	170	230	290	351	411	471	532	593	654	715	777	838
51	51	111	171	231	291	352	412	472	533	594	655	716	778	839
52	52	112	172	232	292	353	413	473	534	595	656	717	779	840
53	53	113	173	233	293	354	414	474	535	596	657	718	780	841
54	54	114	174	234	294	355	415	476	536	597	658	719	781	842
55	55	115	175	235	295	356	416	477	537	598	659	720	782	843
56	56	116	176	236	296	357	417	478	538	599	660	721	783	844
57	57	117	177	237	297	358	418	479	539	600	661	722	784	845
58	58	118	178	238	298	359	419	480	540	601	662	723	785	846
59	59	119	179	239	299	360	420	481	541	602	663	724	786	847

TABLE OF MERIDIONAL PARTS.

M.	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°
0	818	910	973	1035	1098	1161	1225	1289	1354	1419	1484	1550	1616	1684
1	850	911	974	36	99	63	26	90	55	20	85	51	18	85
2	851	913	975	37	1100	64	27	91	56	21	86	52	19	86
3	852	914	976	38	01	65	28	92	57	22	87	53	20	87
4	853	915	977	39	02	66	29	93	58	23	88	54	21	88
5	854	916	978	41	03	67	30	95	59	24	90	56	22	89
6	855	917	979	42	05	68	32	96	60	25	91	57	23	90
7	856	918	980	43	06	69	33	97	61	26	92	58	24	91
8	857	919	981	44	07	70	34	98	62	27	93	59	25	93
9	858	920	982	45	08	71	35	99	63	28	94	60	26	94
10	859	921	983	1046	110	1172	1236	1300	1364	1430	1495	1561	1628	1695
11	860	922	984	47	10	73	37	01	66	31	96	62	29	96
12	861	923	985	48	11	74	38	02	67	32	97	63	30	97
13	862	924	986	49	12	75	39	03	68	33	98	64	31	98
14	863	925	987	50	13	76	40	04	69	34	99	65	32	99
15	864	926	988	51	14	77	41	05	70	35	1500	67	33	1700
16	865	927	989	52	15	78	42	06	71	36	02	68	34	01
17	866	928	990	53	16	79	43	07	72	37	03	69	35	03
18	867	929	991	54	17	81	44	08	73	38	04	70	37	04
19	868	930	993	55	18	82	45	10	74	39	05	71	38	05
20	869	931	994	1056	1119	1183	1246	1311	1375	1440	1506	1572	1639	1706
21	870	932	995	57	20	84	48	12	76	41	07	73	40	07
22	871	933	996	58	21	85	49	13	77	43	08	74	41	08
23	872	934	997	59	22	86	50	14	79	44	09	75	42	09
24	873	935	998	60	23	87	51	15	80	45	10	77	43	11
25	874	936	999	61	25	88	52	16	81	46	11	78	44	12
26	875	937	1000	63	26	89	53	17	82	47	13	79	45	13
27	876	938	1001	64	27	90	54	18	83	48	14	80	47	14
28	877	939	1002	65	28	91	55	19	84	49	15	81	48	15
29	878	941	1003	66	29	92	56	20	85	50	16	82	49	16
30	879	942	1004	1067	1130	1193	1257	1321	1386	1451	1517	1583	1650	1717
31	880	943	05	68	31	94	58	22	87	52	18	84	51	18
32	882	944	06	69	32	95	59	24	88	53	19	85	52	20
33	883	945	07	70	33	96	60	25	89	55	20	86	53	21
34	884	946	08	71	34	98	61	26	90	56	21	88	54	22
35	885	947	09	72	35	99	62	27	92	57	22	89	56	23
36	886	948	10	73	36	1200	64	28	93	58	24	90	57	24
37	887	949	11	74	37	01	65	29	94	59	25	91	58	25
38	888	950	12	75	38	02	66	30	95	60	26	92	59	26
39	889	951	13	76	39	03	67	31	96	61	27	93	60	27
40	890	952	1014	1077	1140	1204	1268	1332	1397	1462	1528	1594	1661	1729
41	891	953	15	78	41	05	69	33	98	63	29	96	62	30
42	892	954	16	79	42	06	70	34	99	64	30	97	63	31
43	893	955	18	80	44	07	71	35	1400	65	31	98	64	32
44	894	956	19	81	45	08	72	36	01	67	32	99	66	33
45	895	957	20	82	46	09	73	38	02	68	33	1600	67	34
46	896	958	21	84	47	10	74	39	03	69	35	01	68	35
47	897	959	22	85	48	11	75	40	05	70	36	02	69	36
48	898	960	23	86	49	12	76	41	06	71	37	03	70	38
49	899	961	24	87	50	13	77	42	07	72	38	04	71	39
50	900	962	1025	1088	1151	1215	1278	1343	1408	1473	1539	1605	1672	1740
51	901	963	26	89	52	16	80	44	09	74	40	06	73	41
52	902	964	27	90	53	17	81	45	10	75	41	08	75	42
53	903	965	28	91	54	18	82	46	11	76	42	09	76	43
54	904	966	29	92	55	19	83	47	12	77	43	10	77	44
55	905	968	30	93	56	20	84	48	13	79	44	11	78	46
56	906	969	31	94	57	21	85	49	14	80	46	12	79	47
57	907	970	32	95	58	22	86	50	15	81	47	13	80	48
58	908	971	33	96	59	23	87	52	16	82	48	14	81	49
59	909	972	34	97	60	24	88	53	18	83	49	15	82	50

TABLE OF MERIDIONAL PARTS.

M.	28°	29°	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	40°	41°
0	1751	1819	1888	1958	2028	2100	2171	2244	2318	2393	2468	2545	2623	2702
1	52	21	90	59	30	01	73	46	19	94	70	46	24	03
2	53	22	91	60	31	02	74	47	20	95	71	48	25	04
3	55	23	92	62	32	03	75	48	22	96	72	49	27	06
4	56	24	93	63	33	04	76	49	23	98	73	50	28	07
5	57	25	94	64	34	05	78	50	24	99	75	51	29	08
6	58	26	95	65	35	07	79	52	25	2400	76	53	31	10
7	59	27	96	66	37	08	80	53	27	01	77	54	32	11
8	60	29	98	67	38	09	81	54	28	03	78	55	33	12
9	61	30	99	69	39	10	82	55	29	04	80	57	34	14
10	1762	1831	1900	1970	2040	2111	2184	2257	2330	2405	2481	2558	2636	2715
11	64	32	01	71	41	13	85	58	32	06	82	59	37	16
12	65	33	02	72	43	14	86	59	33	08	84	60	38	18
13	66	34	03	73	44	15	87	60	34	09	85	62	40	19
14	67	35	05	74	45	16	88	61	35	10	86	63	41	20
15	68	37	06	76	46	17	90	63	37	11	87	64	42	22
16	69	38	07	77	47	19	91	64	38	13	89	66	44	23
17	70	39	08	78	48	20	92	65	39	14	90	67	45	24
18	72	40	09	79	50	21	93	66	40	15	91	68	46	26
19	73	41	10	80	51	22	94	68	42	16	92	69	48	27
20	1774	1842	1912	1981	2052	2123	2196	2269	2343	2418	2494	2571	2649	2728
21	75	43	13	83	53	25	97	70	44	19	95	72	50	29
22	76	45	14	84	54	26	98	71	45	20	96	73	51	31
23	77	46	15	85	56	27	99	72	46	22	98	75	53	32
24	78	47	16	86	57	28	2200	74	48	23	99	76	54	33
25	80	48	17	87	58	29	02	75	49	24	2500	77	55	35
26	81	49	18	88	59	31	03	76	50	25	01	78	57	36
27	82	50	20	90	60	32	04	77	51	27	03	80	58	37
28	83	52	21	91	61	33	05	79	53	28	04	81	59	39
29	84	53	22	92	63	34	07	80	54	29	05	82	61	40
30	1785	1854	1923	1993	2064	2135	2208	2281	2355	2430	2506	2584	2662	2742
31	86	55	24	94	65	37	09	82	56	32	08	85	63	43
32	87	56	25	95	66	38	10	83	58	33	09	86	65	44
33	89	57	27	97	67	39	11	85	59	34	10	88	66	46
34	90	58	28	98	69	40	13	86	60	35	12	89	67	47
35	91	60	29	99	70	41	14	87	61	37	13	90	69	48
36	92	61	30	2000	71	43	15	88	63	38	14	91	70	50
37	93	62	31	01	72	44	16	90	64	39	15	93	71	51
38	94	63	32	02	73	45	17	91	65	40	17	94	73	52
39	95	64	34	04	75	46	19	92	66	42	18	95	74	54
40	1797	1865	1935	2005	2076	2147	2220	2293	2368	2443	2519	2597	2675	2755
41	98	66	36	06	77	49	21	95	69	44	21	98	76	56
42	99	68	37	07	78	50	22	96	70	45	22	99	78	58
43	1800	69	38	08	79	51	24	97	71	47	23	2600	79	59
44	01	70	39	10	80	52	25	98	73	48	24	02	80	60
45	02	71	41	11	82	53	26	99	74	49	26	03	82	62
46	03	72	42	12	83	55	27	2301	75	51	27	04	83	63
47	05	73	43	13	84	56	28	02	76	52	28	06	84	64
48	06	75	44	14	85	57	30	03	78	53	30	07	86	66
49	07	76	45	15	86	58	31	04	79	54	31	08	87	67
50	1808	1877	1946	2017	2088	2159	2232	2306	2380	2456	2532	2610	2688	2768
51	09	78	48	18	89	61	33	07	81	57	33	11	90	70
52	10	79	49	19	90	62	35	08	83	58	35	12	91	71
53	11	80	50	20	91	63	36	09	84	59	36	14	92	72
54	13	81	51	21	92	64	37	11	85	61	37	15	94	74
55	14	83	52	22	94	65	38	12	86	62	38	16	95	75
56	15	84	53	24	95	67	39	13	88	63	40	17	96	76
57	16	85	55	25	96	68	41	14	89	64	41	19	98	78
58	17	86	56	26	97	69	42	16	90	66	42	20	99	79
59	18	87	57	27	98	70	43	17	91	67	44	21	2700	80

TABLE OF MERIDIONAL PARTS.

M.	42°	43°	44°	45°	46°	47°	48°	49°	50°	51°	52°	53°	54°	55°
0	2782	2863	2946	3030	3116	3203	3292	3382	3474	3569	3665	3764	3865	3968
1	83	64	47	31	17	04	93	84	76	70	67	65	67	70
2	84	66	49	33	18	06	95	85	78	72	68	67	68	71
3	86	67	50	34	20	07	96	87	79	74	70	69	70	73
4	87	69	51	36	21	09	98	88	81	75	72	70	71	75
5	88	70	53	37	23	10	99	90	82	77	73	72	73	77
6	90	71	54	38	24	12	3301	91	84	78	75	74	75	78
7	91	73	56	40	26	13	02	93	85	80	77	75	77	80
8	92	74	57	41	27	14	03	94	87	82	78	77	78	82
9	94	75	58	43	29	16	05	96	88	83	80	79	80	84
10	2795	2877	2960	3044	3130	3217	3306	3397	3490	3585	3681	3780	3882	3985
11	97	78	61	45	31	19	08	99	92	86	83	82	83	87
12	98	80	63	47	33	20	09	3400	93	88	85	84	85	89
13	99	81	64	48	34	22	11	02	95	90	86	85	87	91
14	2801	82	65	50	36	23	12	03	96	91	88	87	89	92
15	02	84	67	51	37	25	14	05	98	93	90	89	90	94
16	03	85	68	53	39	26	16	07	99	94	91	90	92	96
17	05	86	70	54	40	28	17	08	3501	96	93	92	94	98
18	06	88	71	55	42	29	19	10	03	98	95	94	95	99
19	07	89	72	57	43	31	20	11	04	99	96	95	97	4001
20	2809	2891	2974	3058	3144	3232	3322	3413	3506	3601	3698	3797	3899	4003
21	10	92	75	60	46	34	24	14	07	02	99	99	91	05
22	11	93	76	61	47	35	25	16	09	04	3701	3800	02	06
23	13	95	78	63	49	37	26	17	10	06	03	02	04	08
24	14	96	79	64	50	38	28	19	12	07	04	01	06	10
25	15	97	81	65	52	40	29	20	14	09	06	03	07	12
26	17	99	82	67	53	41	31	22	15	10	07	07	09	14
27	18	2900	83	68	55	42	32	23	17	12	09	09	11	15
28	20	02	85	70	56	44	34	25	18	14	11	11	13	17
29	21	03	86	71	57	45	35	27	20	15	13	12	14	19
30	2822	2904	2988	3073	3159	3247	3337	3428	3521	3617	3714	3814	3916	4021
31	24	06	89	74	60	48	38	30	23	18	16	16	18	22
32	25	07	91	75	62	50	40	31	25	20	17	17	19	24
33	26	08	92	77	63	51	41	33	26	22	19	19	21	26
34	28	10	93	78	65	53	43	34	28	23	21	21	22	28
35	29	11	95	80	66	54	44	36	29	25	22	22	25	29
36	30	13	96	81	68	56	46	37	31	26	24	24	26	31
37	32	14	98	83	69	57	47	39	32	28	26	26	28	33
38	33	15	99	84	71	59	49	40	34	30	27	27	30	35
39	34	17	3000	85	72	60	50	42	36	31	29	29	32	37
40	2836	2918	3002	3087	3173	3262	3352	3443	3537	3633	3731	3831	3933	4038
41	37	19	03	88	75	63	53	45	39	34	32	32	35	40
42	39	21	05	90	76	65	55	47	40	36	34	34	37	42
43	40	22	06	91	78	66	56	48	42	38	36	36	38	44
44	41	24	07	93	79	68	58	50	43	39	37	38	40	45
45	43	25	09	94	81	69	59	51	45	41	39	39	42	47
46	44	26	10	95	82	71	61	53	47	43	41	41	44	49
47	45	28	12	97	84	72	62	54	48	44	42	43	45	51
48	47	29	13	98	85	74	64	56	50	46	44	44	47	52
49	48	31	14	3100	87	75	65	57	51	47	46	46	49	54
50	2849	2932	3016	3101	3188	3277	3367	3459	3553	3649	3747	3848	3951	4056
51	51	33	17	03	90	78	68	60	55	51	49	49	52	58
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56	58	40	24	10	97	86	76	68	62	59	57	58	61	67
57	59	42	26	11	98	87	78	70	64	60	59	60	63	69
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M.	56°	57°	58°	59°	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°
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4	81	90	02	17	35	57	84	14	49	88	33	84	42	06
5	83	92	04	19	37	60	86	16	51	91	36	87	44	09
6	85	94	06	21	39	62	88	18	53	93	38	89	47	11
7	86	95	08	23	41	64	90	20	55	95	41	92	50	14
8	88	97	09	25	43	66	92	23	58	98	43	95	52	17
9	90	99	11	27	45	68	94	25	60	5200	46	97	55	20
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12	95	05	17	33	51	74	4801	31	67	07	53	05	63	28
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14	99	08	21	36	55	78	05	36	71	12	58	10	68	34
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16	03	12	25	40	59	82	09	40	76	17	63	15	74	39
17	04	14	27	42	62	84	11	43	78	19	66	18	76	42
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19	08	18	30	46	66	89	16	47	83	24	71	23	82	48
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23	15	25	38	54	74	97	24	56	92	34	80	33	93	59
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25	19	29	42	58	78	4701	29	60	97	38	85	39	98	65
26	21	31	44	60	80	03	31	63	99	41	88	41	5701	68
27	22	32	46	62	82	05	33	65	5102	43	90	44	04	71
28	24	34	47	64	84	07	35	67	04	46	93	46	06	74
29	26	36	49	66	86	10	37	69	06	48	95	49	09	76
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32	32	42	55	72	92	16	44	76	13	55	03	57	17	85
33	33	44	57	74	94	18	46	78	15	58	06	59	20	88
34	35	46	59	76	96	20	48	81	18	60	08	62	23	91
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42	50	60	74	92	12	37	65	99	36	80	28	83	45	14
43	52	62	76	94	14	39	68	5001	39	82	31	86	47	17
44	53	64	78	95	16	41	70	03	41	84	33	88	50	19
45	55	66	80	97	18	43	72	05	43	87	36	91	53	22
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49	62	74	88	05	27	52	81	14	53	97	46	5602	64	34
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53	70	81	96	13	35	60	90	23	62	06	56	12	75	46
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55	73	85	99	17	39	64	94	28	67	11	61	17	81	51
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TABLE OF MERIDIONAL PARTS.

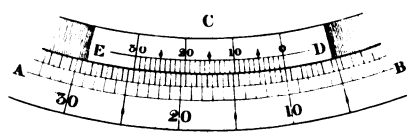
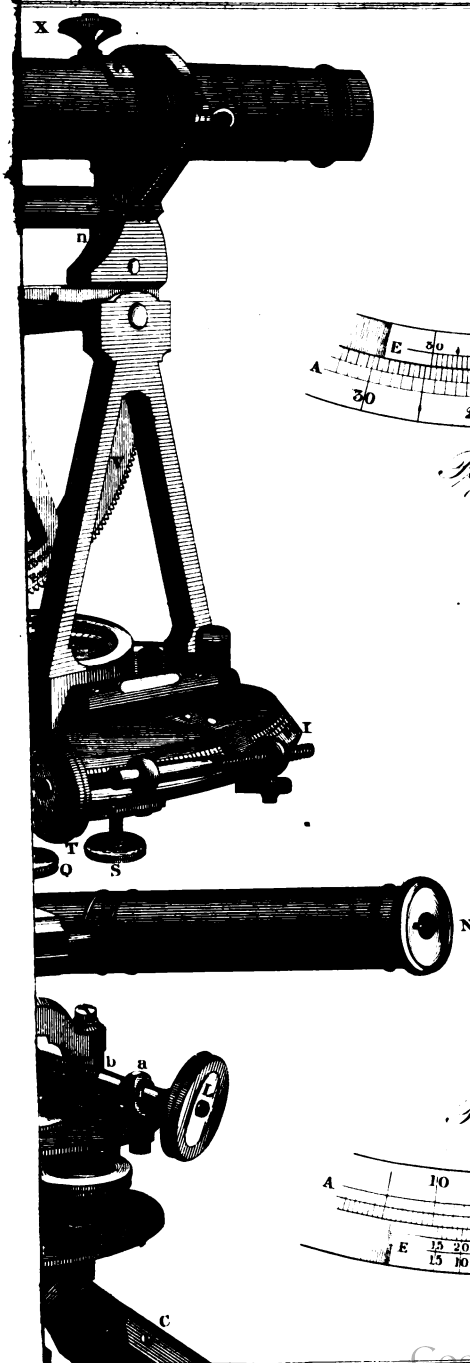
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2	84	66	49	33	18	06	95	85	78	72	68	67	68	71
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7	91	73	56	40	26	13	02	93	85	80	77	75	77	80
8	92	74	57	41	27	14	03	94	87	82	78	77	78	82
9	94	75	58	43	29	16	05	96	88	83	80	79	80	84
10	2795	2877	2960	3044	3130	3217	3306	3397	3490	3585	3681	3780	3882	3985
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13	99	81	64	48	34	22	11	02	95	90	86	85	87	91
14	2801	82	65	50	35	23	12	03	96	91	88	87	89	92
15	02	84	67	51	37	25	14	05	98	93	90	89	90	94
16	03	85	68	53	39	26	16	07	99	94	91	90	92	96
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19	07	89	72	57	43	31	20	11	04	99	96	95	97	4001
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24	14	96	79	64	50	38	28	19	12	07	04	04	06	10
25	15	97	81	65	52	40	29	20	14	09	06	05	07	12
26	17	99	82	67	53	41	31	22	15	10	07	07	09	14
27	18	2900	83	68	55	42	32	23	17	12	09	09	11	15
28	20	02	85	70	56	44	34	25	18	14	11	11	13	17
29	21	03	86	71	57	45	35	27	20	15	13	12	14	19
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34	28	10	93	78	65	53	43	34	28	23	21	21	22	28
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45	43	25	09	94	81	69	59	51	45	41	39	39	42	47
46	44	26	10	95	82	71	61	53	47	43	41	41	44	49
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48	47	29	13	98	85	74	64	56	50	46	44	44	47	52
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50	2849	2932	3016	3101	3188	3277	3367	3459	3553	3649	3747	3848	3951	4056
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56	58	40	24	10	97	86	76	68	62	59	57	58	61	67
57	59	42	26	11	98	87	78	70	64	60	59	60	63	69
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TABLE OF MERIDIONAL PARTS.

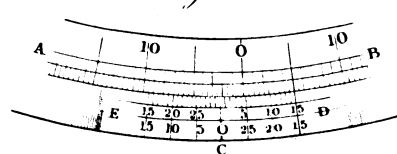
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2	77	86	98	13	31	53	79	09	44	84	28	79	36	5800
3	79	88	4300	15	33	55	81	12	46	86	31	82	39	03
4	81	90	02	17	35	57	84	14	49	88	33	84	42	06
5	83	92	04	19	37	60	86	16	51	91	36	87	44	09
6	85	94	06	21	39	62	88	18	53	93	38	89	47	11
7	86	95	08	23	41	64	90	20	55	95	41	92	50	14
8	88	97	09	25	43	66	92	23	58	98	43	95	52	17
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12	95	05	17	33	51	74	4801	31	67	07	53	05	63	28
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15	4101	10	23	38	57	80	07	38	74	14	61	13	71	37
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17	04	14	27	42	62	84	11	43	78	19	66	18	76	42
18	06	16	28	44	64	87	14	45	81	22	68	20	79	45
19	08	18	30	46	66	89	16	47	83	24	71	23	82	48
20	4110	4220	4332	4448	4568	4691	4818	4949	5085	5226	5373	5526	5685	5851
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25	19	29	42	58	78	4701	29	60	97	38	85	39	98	65
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38	42	53	67	84	04	28	57	90	27	70	18	73	34	5902
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56	75	87	4401	19	41	66	96	30	69	14	64	20	83	54
57	77	89	03	21	43	69	98	33	72	16	66	23	86	57
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TABLE OF MERIDIONAL PARTS.

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3	75	55	45	45	57	82	22	81	59	61	93	58	67	31
4	78	58	48	48	60	86	27	85	64	67	98	65	74	39
5	81	61	51	52	64	90	31	90	69	72	8404	71	82	47
6	84	64	54	55	68	94	35	94	74	77	10	78	89	55
7	86	67	58	58	71	97	39	98	78	83	16	84	96	64
8	89	70	61	62	75	7001	43	7503	83	88	22	91	9203	72
9	92	73	64	65	79	05	47	07	88	93	27	97	11	81
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12	6001	83	74	76	90	17	60	21	7803	09	45	17	33	9706
13	04	86	77	79	93	21	64	25	08	15	51	23	40	14
14	07	89	80	83	97	25	68	30	13	20	57	30	48	23
15	10	92	84	86	6801	29	73	35	17	25	63	36	55	31
16	13	95	87	90	04	33	77	39	22	31	69	43	62	40
17	16	98	90	93	08	37	81	44	27	36	74	49	70	48
18	19	6201	94	96	12	41	85	48	32	41	80	56	77	57
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39	82	68	63	70	90	24	75	45	37	56	07	98	38	42
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44	97	83	80	88	09	45	97	68	63	84	38	32	77	87
45	6100	87	83	92	13	49	7401	73	68	90	44	39	85	9996
46	04	90	87	95	17	53	06	78	73	95	51	46	93	10005
47	06	93	90	99	20	57	10	83	78	8301	57	53	9501	10015
48	09	96	94	6702	24	61	14	87	83	07	63	60	09	10024
49	12	99	97	06	28	65	19	92	89	12	69	67	17	10033
50	6115	6303	6500	6710	6932	7169	7423	7697	7994	8318	8676	9074	9525	10043
51	18	06	04	13	36	73	27	7702	99	24	82	81	33	10052
52	21	09	07	17	40	77	32	06	8004	29	88	88	41	10061
53	24	12	11	20	43	81	36	11	09	35	93	96	49	10071
54	27	15	14	24	47	85	41	16	14	41	8701	9103	57	10080
55	30	19	17	28	51	89	45	21	20	47	07	10	65	10089
56	33	22	21	31	55	94	49	25	25	52	14	17	73	10099
57	36	25	24	35	59	98	54	30	30	58	20	24	81	10108
58	40	28	29	38	63	7202	58	35	35	64	26	31	89	10118
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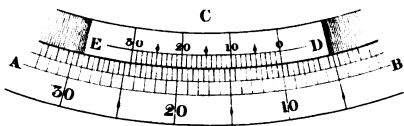
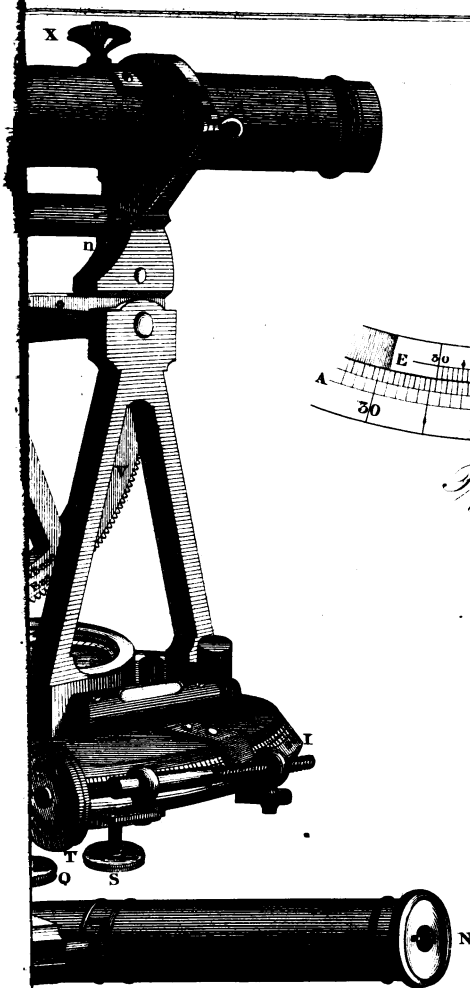


*Fig. 2.*

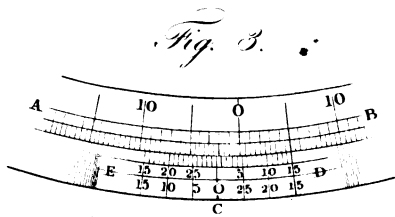
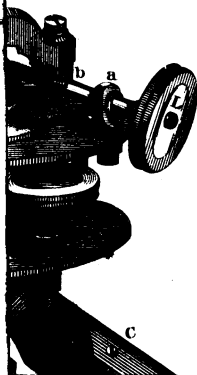


*Fig. 3.*

M.	70°	71°	72°	73°	74°	75°	76°	77°	78°	79°	80°	81°	82°	83°
0	5966	6146	6335	6534	6746	6970	7210	7467	7745	8046	8375	8739	9145	9606
1	69	49	38	38	49	74	14	72	49	51	81	45	53	14
2	72	52	41	41	53	78	18	76	54	56	87	52	60	22
3	75	55	45	45	57	82	22	81	59	61	93	58	67	31
4	78	58	48	48	60	86	27	85	64	67	98	65	74	39
5	81	61	51	52	64	90	31	90	69	72	8404	71	82	47
6	84	64	54	55	68	94	35	94	74	77	10	78	89	55
7	86	67	58	58	71	97	39	98	78	83	16	84	96	64
8	89	70	61	62	75	7001	43	7503	83	88	22	91	9203	72
9	92	73	64	65	79	05	47	07	88	93	27	97	11	81
10	5995	6177	6367	6569	6782	7009	7252	7512	7793	8099	8433	8804	9218	9689
11	98	80	71	72	86	13	56	16	98	8104	39	10	25	97
12	6001	83	74	76	90	17	60	21	7803	09	45	17	33	9706
13	04	86	77	79	93	21	64	25	08	15	51	23	40	14
14	07	89	80	83	97	25	68	30	13	20	57	30	48	23
15	10	92	84	86	6801	29	73	35	17	25	63	36	55	31
16	13	95	87	90	04	33	77	39	22	31	69	43	62	40
17	16	98	90	93	08	37	81	44	27	36	74	49	70	48
18	19	6201	94	96	12	41	85	48	32	41	80	56	77	57
19	22	05	97	6600	15	45	89	53	37	47	86	63	85	65
20	6025	6208	6400	6603	6819	7049	7294	7557	7842	8152	8492	8869	9292	9774
21	28	11	03	07	23	52	98	62	47	58	98	76	9300	83
22	31	14	07	10	26	56	7302	66	52	63	8504	83	07	91
23	34	17	10	14	30	60	06	71	57	68	10	89	15	9800
24	37	20	13	17	34	64	11	76	62	74	16	96	22	09
25	40	23	17	21	38	68	15	80	67	79	22	8903	30	17
26	43	26	20	24	41	72	19	85	72	85	28	09	38	26
27	46	30	23	28	45	76	23	89	77	90	34	16	45	35
28	49	33	27	31	49	80	28	94	82	96	40	23	53	44
29	52	36	30	35	53	84	32	98	87	8201	46	30	60	52
30	6055	6239	6433	6639	6856	7088	7336	7603	7892	8207	8552	8936	9368	9861
31	58	42	37	42	60	92	40	08	97	12	58	43	76	70
32	61	45	40	46	64	96	45	12	7902	18	64	50	83	79
33	64	49	43	49	68	7100	49	17	07	23	71	57	91	88
34	67	52	47	53	71	04	53	22	12	29	77	63	99	97
35	70	55	50	56	75	08	58	26	17	34	83	70	9407	9906
36	73	58	53	60	79	12	62	31	22	40	89	77	14	15
37	76	61	57	63	83	16	66	36	27	45	95	84	22	24
38	79	64	60	67	86	20	71	40	32	51	8601	91	30	33
39	82	68	63	70	90	24	75	45	37	56	07	98	38	42
40	6085	6271	6467	6674	6894	7128	7379	7650	7912	8262	8614	9005	9445	9951
41	88	74	70	77	98	32	84	54	48	67	20	12	53	60
42	91	77	73	81	6901	36	88	59	53	73	26	18	61	69
43	94	80	77	85	05	40	92	64	58	79	32	25	69	78
44	97	83	80	88	09	45	97	68	63	84	38	32	77	87
45	6100	87	83	92	13	49	7401	73	68	90	44	39	85	9996
46	04	90	87	95	17	53	06	78	73	95	51	46	93	10005
47	06	93	90	99	20	57	10	83	78	8301	57	53	9501	10015
48	09	96	94	6702	24	61	14	87	83	07	63	60	09	10024
49	12	99	97	06	28	65	19	92	89	12	69	67	17	10033
50	6115	6303	6500	6710	6932	7169	7423	7697	7994	8318	8676	9074	9525	10043
51	18	06	04	13	36	73	27	7702	99	24	82	81	33	10052
52	21	09	07	17	40	77	32	06	8004	29	88	88	41	10061
53	24	12	11	20	43	81	36	11	09	35	93	96	49	10071
54	27	15	14	24	47	85	41	16	14	41	8701	9103	57	10080
55	30	19	17	28	51	89	45	21	20	47	07	10	65	10089
56	33	22	21	31	55	94	49	25	25	52	14	17	73	10099
57	36	25	24	35	59	98	54	30	30	58	20	24	81	10108
58	40	28	29	38	63	7202	58	35	35	64	26	31	89	10118
59	43	32	31	42	66	06	63	40	40	69	33	38	98	10127

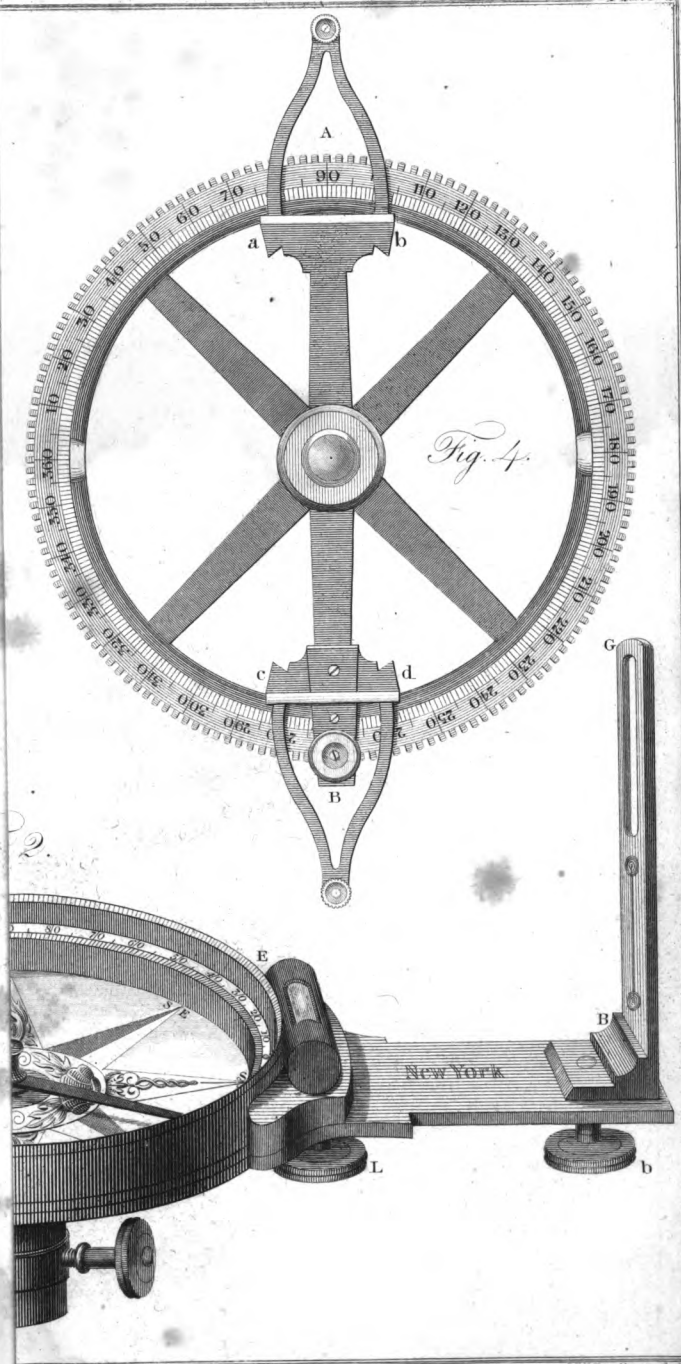


*Fig. 2.*



*Fig. 3.*





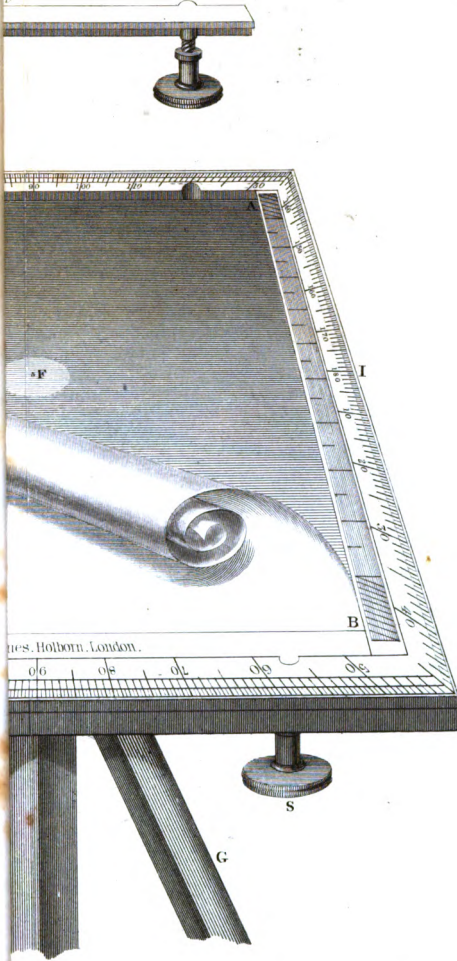
*Fig. 4.*

New York





*Fig. 3.*



nes. Holborn. London.

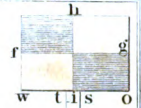
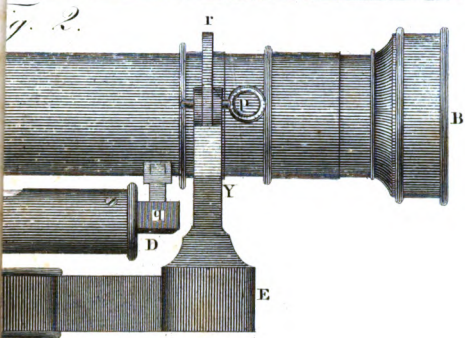
Holborn. London.

*Fig. 2.*

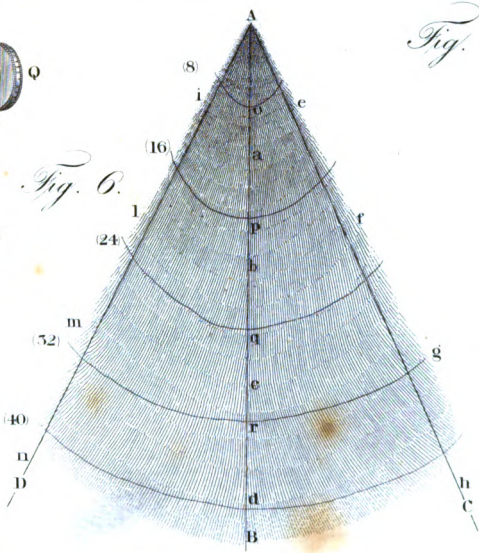


*Pruthome & AT.*

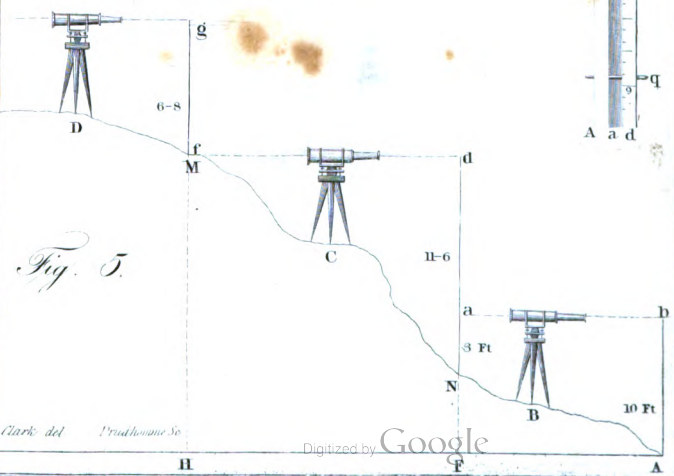




*Fig. 3.*



*Fig. 6.*



*Fig. 5.*

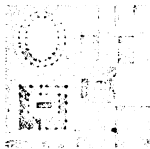
Clark del P. Mathewson Sc



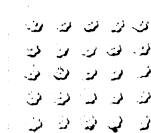
Rice Plant<sup>s</sup>



Gardens



Cotton P.



Ploughed L.



Orchards



Vine yard



DETAILS OF LEAVES

Pine



Oak



Fruit



Chestnut



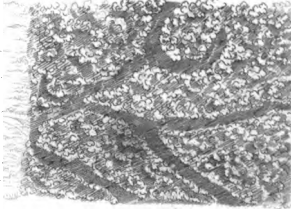
Woods



Heath



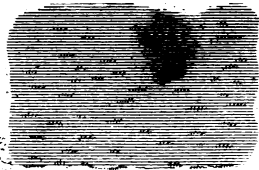
Oak Woods



Marsh



Salt Marsh



Meadows



ROADS &c.

Turnpiked road



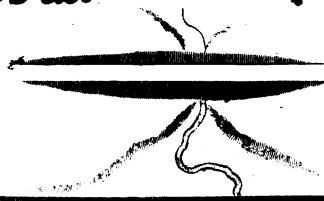
Stone Fence



Turnpike road



Foot path



Wooden Fence

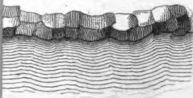


Common road





Rocky Shore

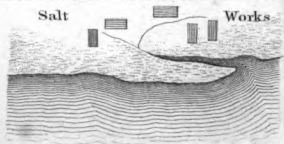


Rocks always bare

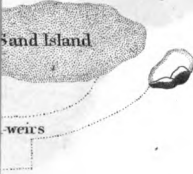


Salt

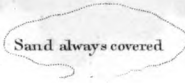
Works



Sand Island



Sand always covered

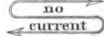
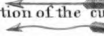


Sand sometimes bare



weirs

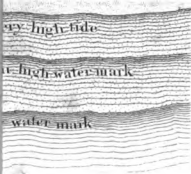
Direction of the current



High tide

High water mark

water mark



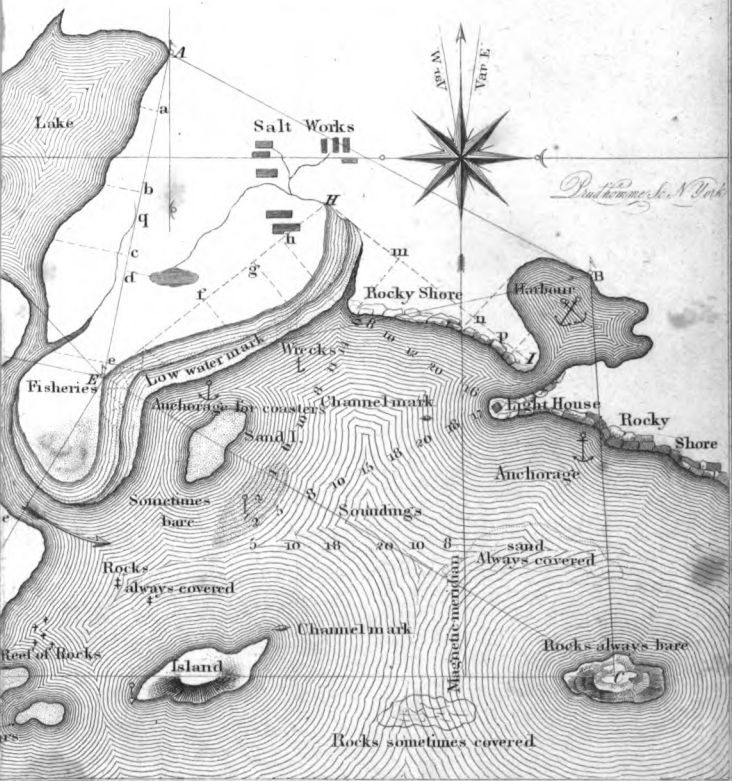
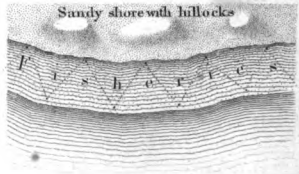
Rocks sometimes bare



Reef of Rocks



Sandy shore with hillocks







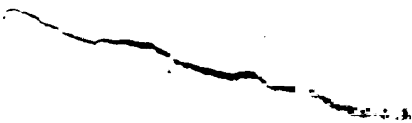












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